

Insights from Systems Code Analysis on Power Exhaust Requirements for Future Fusion Power Systems

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Presented to
**IAEA Divertor Concepts Meeting
Vienna, Austria**

November 6, 2019

General Impression is that Power Exhaust Requirements Place Significant Constraint on Minimum Size of Fusion Power Systems

- **Divertor Heat Flux:** $q_{div} \propto (1 - f_{rad}^{core})P_{heat}/2\pi R\lambda_q$
- **General Impression:**
 - P_{heat} set by need to produce requisite electricity
 - f_{rad}^{core} limited by need to stay above L-H transition power threshold
 - λ_q set by core performance requirements (choice of I_p drives B_p)
 - Primary “control” is device size R
- **In certain cases (especially at ITER-level of confinement, $H_{98y2} = 1$), this impression is accurate**
 - Places increased importance on R&D to address this issue
- **However, this is not universally this case...**

Power Exhaust Requirements are Strongly Linked to the Achievable Core Confinement

- Tendency to think power exhaust is roughly independent of confinement

.... Fusion power needed for electricity sets boundary power flow

- But it's a bit more complicated...

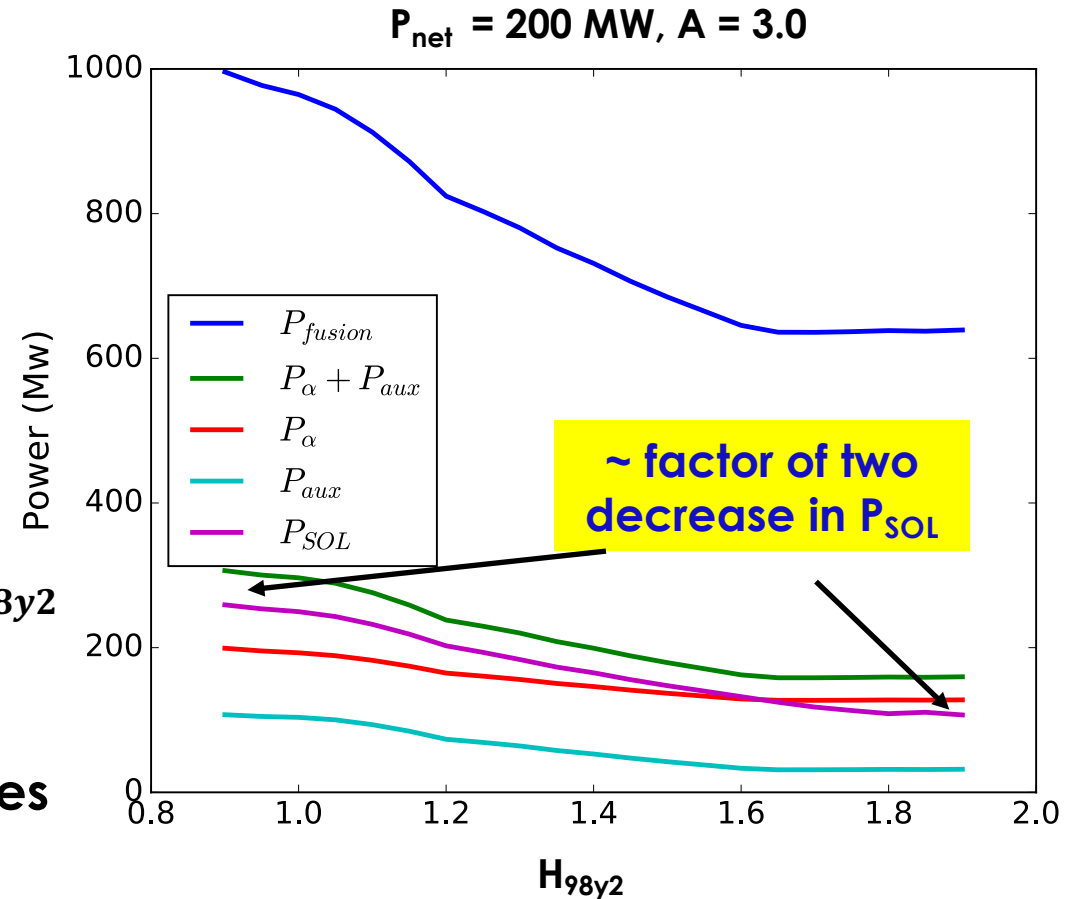
$$P_{fus} \propto p_{th}^2 \propto (P\tau_E)^2 \propto (P H P^{-\alpha_P})^2$$

$$P \propto P_{fus}^{1/2(1-\alpha_P)} / H^{1/(1-\alpha_P)}$$

→ For H_{98y2} , $\alpha_p = 0.67 \rightarrow P \propto P_{fus}^{1.5} / H_{98y2}^3$

For H_{89} , $\alpha_p = 0.5 \rightarrow P \propto P_{fus} / H_{89}^2$

- Additionally, the required P_{fus} increases as confinement quality decreases



Outline

- **Introduction/Motivation**
- **GA systems code (GASC) and Compact Fusion Pilot Plant (CFPP)**
- **Impact of Power Exhaust and Confinement on CFPP cost**
- **Insights on Important R&D for CFPP Cost Attractiveness**
- **Summary**

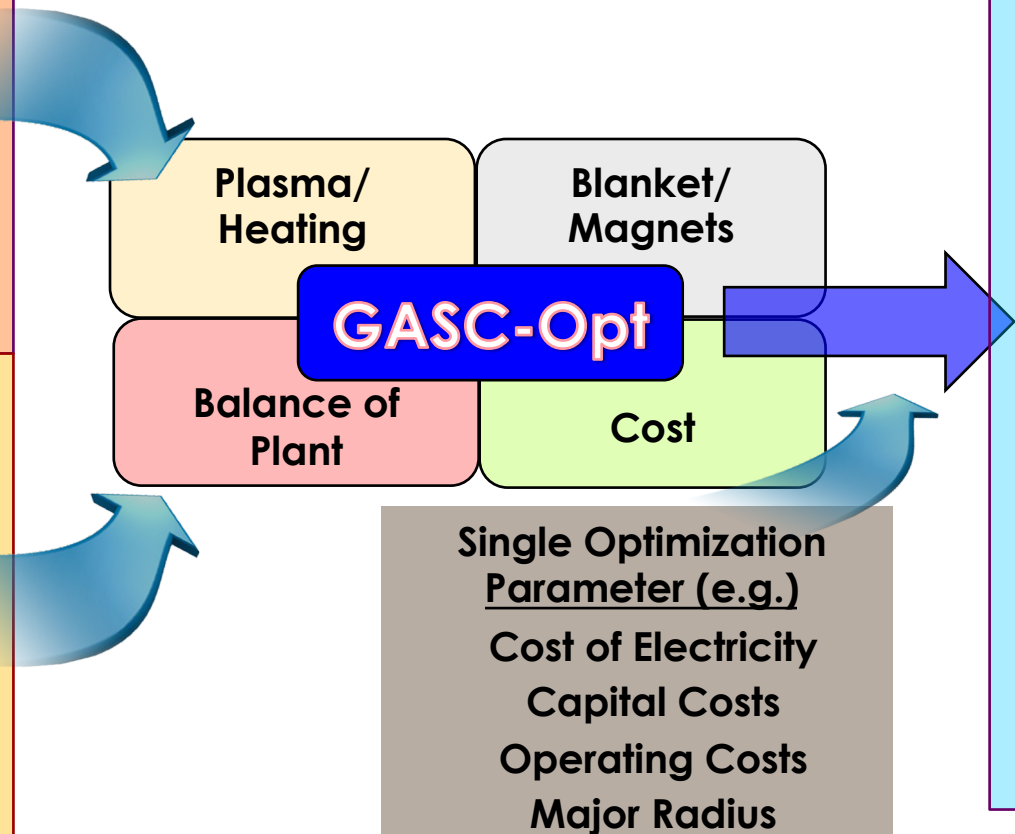
Based on a Set of Assumptions and Constraints, GASC-Opt Finds Optimal Solution to Minimize Chosen Optimization Parameter

Set of Assumptions (e.g.)

Magnet Type (REBCO)
 Tritium Breeding Ratio (1.0)
 TF Bucking (Free TF)
 Thermal Efficiency (0.4)
 Blanket Power Mult. (1.2)
 Pulse Length (8 hr)

Set of Constraints (e.g.)

$P_{net} = 200 \text{ MWe}$
 $q_{div} < 10 \text{ MW/m}^2$
 $f_{GW} < 1$
 $f_{rad,core} < 0.75$
 $f_{BS} < 0.9$
 TF Stress $< 667 \text{ MPa}$
 $J_{TF,sc,limit} / J_{TF,sc} > 2$
 $\beta_N / \beta_{N,limit} < 0.75$



Outputs (e.g.)

Major Radius
 Aspect Ratio
 Plasma Current
 Toroidal Field
 Fusion Power
 CD Power
 $\beta_T, \beta_p, \beta_N,$
 $f_{BS}, f_{non-ind}, f_{ind}$
 f_{GW}, q_{div}
 $\Delta_{TF}, \Delta_{CS}, \Delta_{BI}$
 Tritium Inventory
 $\$\$_{TF}, \$\$_{BI}, \$\$_{BOP}$
 COE

Power Exhaust Models in GA System Code (GASC)

- Core: Standard power balance assuming coronal equilibrium emissivity
- Divertor → Two-point model with impurities

$$q_{div} = P_{SOL}(1 - f_{rad,div})/A_{wetted}$$

$$q_{rad,div} = n_{e,mid}T_{e,mid} \left(2\kappa_0 f_{z,core} \eta_{z,div} \int_{T_{e,div}}^{T_{e,mid}} L_Z(T_e) T_e^{0.5} Z_{eff}^{-0.3} dT_e \right)$$

$$A_{wetted} = 2\pi N_{div} R \lambda_q F_{exp} \sin(\theta_{div})$$

$$F_{exp} = F_{\theta,exp} F_{\phi,exp}$$

$$f_{rad,div} = q_{rad,div}/q_{\parallel}$$

$$\theta_{div} = \sin^{-1}[(1 + 1/\alpha_{div}^2) \sin \beta_{div}]$$

$$\alpha_{div} = F_{exp} \sin(\tan^{-1}(B_{p,mid}/B_{T,mid}))$$

- **Typical assumptions:**

- Number of Divertors: $N_{div} = 2$
- Heat Flux Width: $\lambda_{int} = \lambda_{q,Eich} + 1.64 S_{Scarabosio}$
- Flux Expansion: $F_{\theta,exp} = 5$; $F_{\phi,exp} = 0.75$
- Divertor Impurity Enrichment: $\eta_{z,div} = n_{z,div}/n_{z,core} = 3$

T. Eich et al. Nucl. Fusion 53 (2013) 093031
A. Scarabosio et al., J. Nucl. Mater. 463 (2015) 49

Costing Model in GASC

- **Costing model adapted from Sheffield et al. 1986, updated by Sheffield et al 2016 (includes all core components and balance of plant)**
- **We Include cost of tritium required to run facility for 2 years in the capital cost**
 - Initial Inventory + (Consumption – Breeding - loss/decay) at \$30M/kg
- **GASC configured to minimize the capital cost given a set of assumptions**

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Technical Requirements for a Compact Fusion Pilot Plant (CFPP)

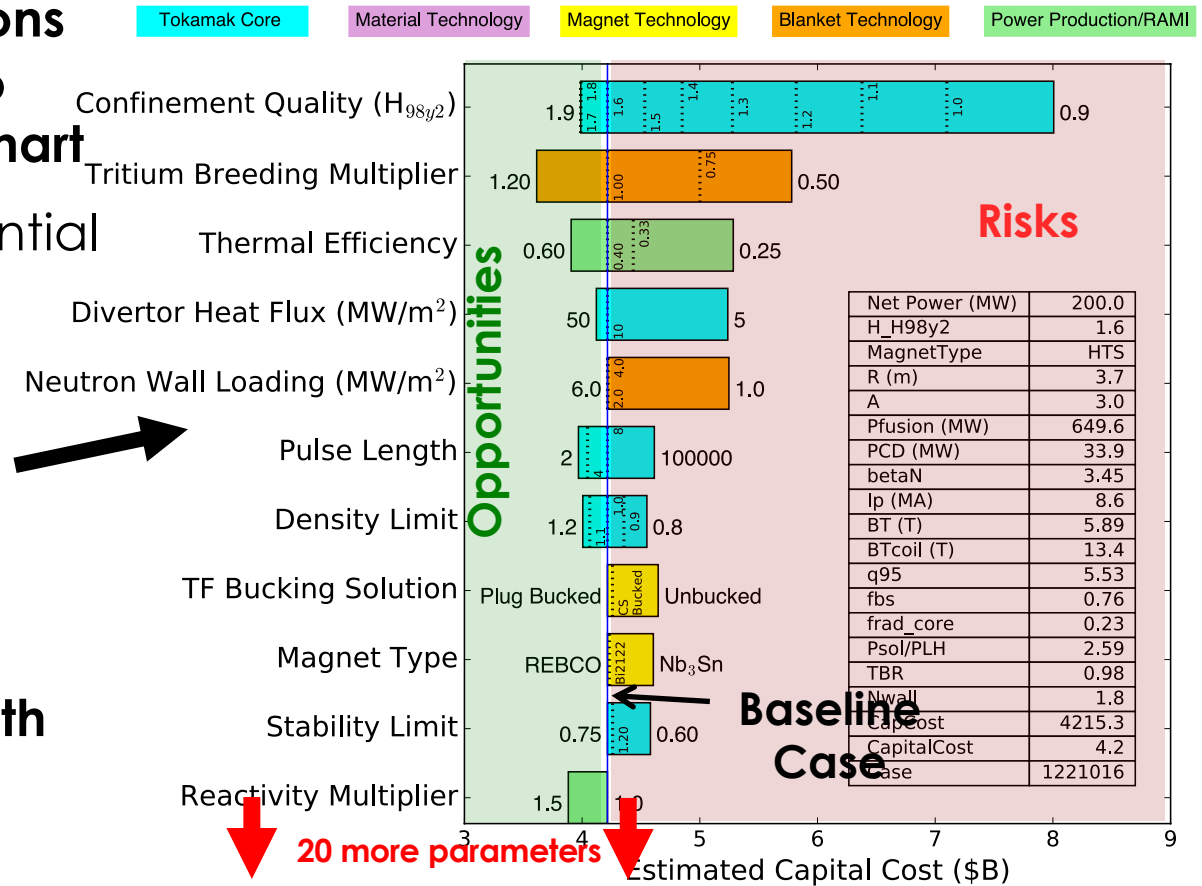
- **At present, no agreed upon technical requirements for a CFPP**
- **My assumptions for those requirements:**
 - 1) **Produce 200 MW-e** (provide sufficient headroom that if device doesn't perform as projected, can still produce net electricity)
 - 2) **Produce (or purchase) its own tritium** (not required to produce tritium for follow-up facilities)
 - 3) **Produce power continuously for a 2-year calendar lifetime** (balance between demonstrating feasibility of fusion electricity and introducing significant set of materials issues) – can be pulsed
 - 4) **Capital costs to construct should be minimized**; operating costs is secondary consideration; COE not important at all
- **Note that these assumptions significantly reduce or even eliminate potential impact of material lifetime and RAMI requirements**

Analysis of Cost Drivers for a CFPP Indicate Importance of Both Physics and Technology Towards Attractiveness

- Independently vary assumptions to determine cost sensitivity to each parameter → tornado chart

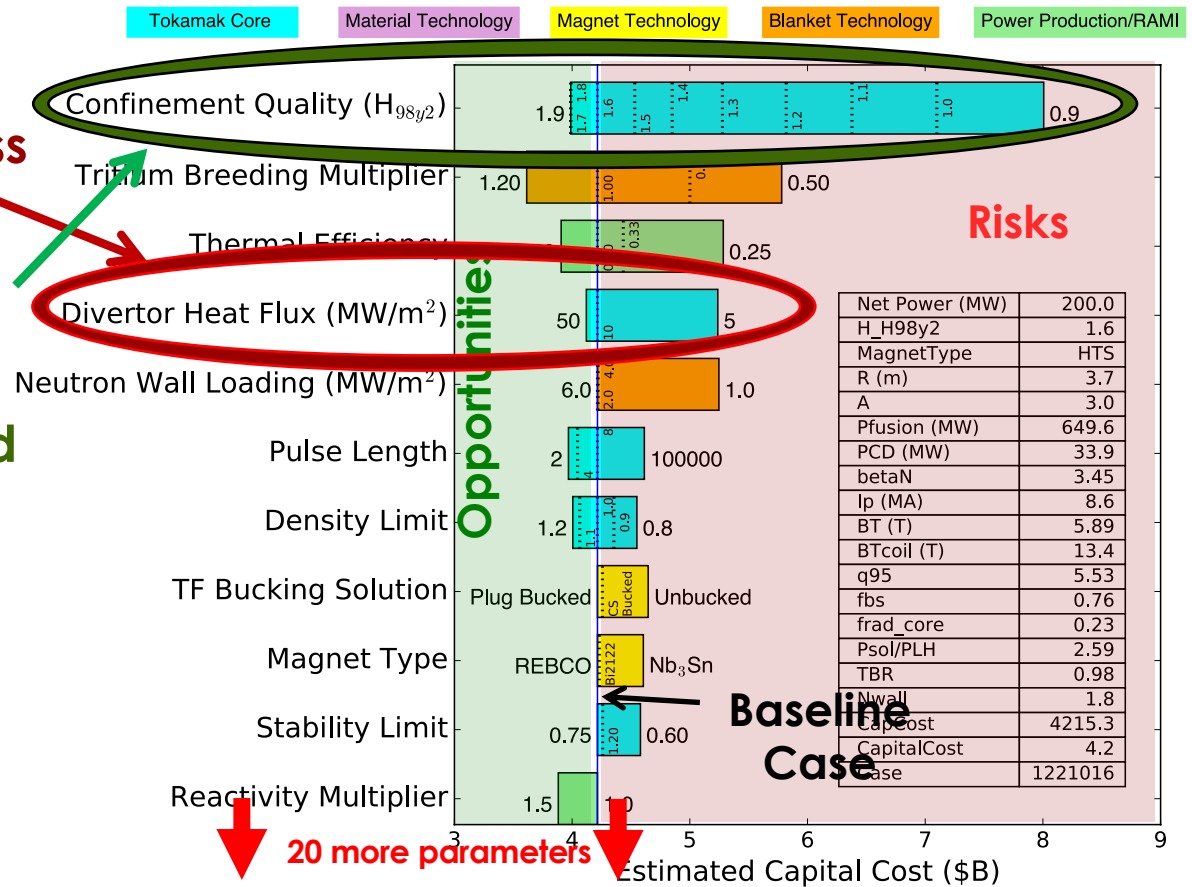
– Identifies risk/reward of potential R&D developments (or lack thereof)

- Aggressive baseline w/ $H_{98y2} = 1.6$, REBCO magnets, Plug-Bucked TF/CS
- Evident that physics and technology constraints are both critical to cost attractiveness



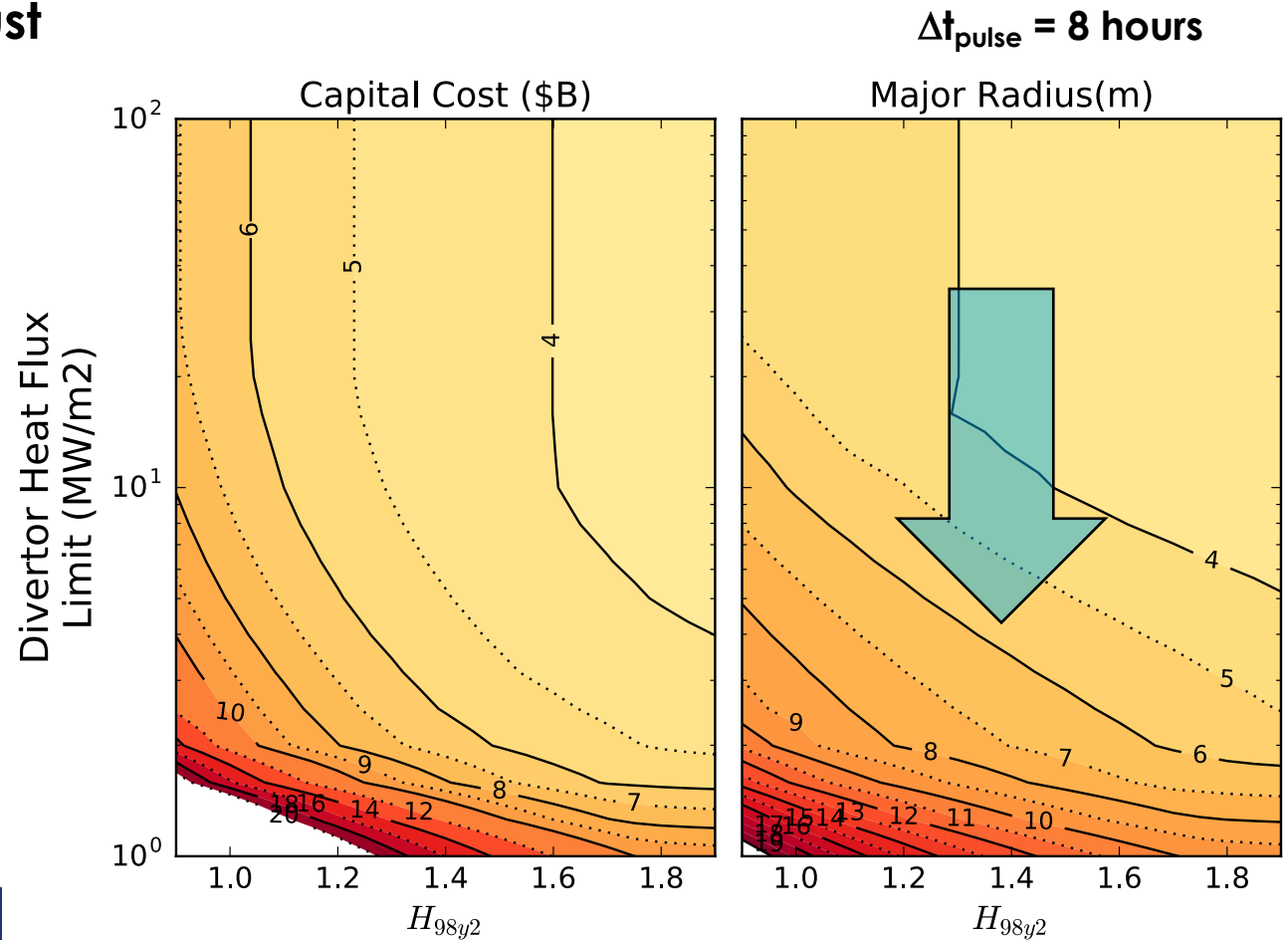
Cost Sensitivity Studies Suggest a Potential New Emphasis for Divertor Research

- On its own, power exhaust capabilities provide modest leverage on cost attractiveness
 - $q_{div} = 5-50 \text{ MW/m}^2$
- However, cost is extremely sensitive to confinement quality, which is strongly linked to edge/divertor
- → A new direction for R&D focused on integrated performance
 - Rather than just simply divertor performance



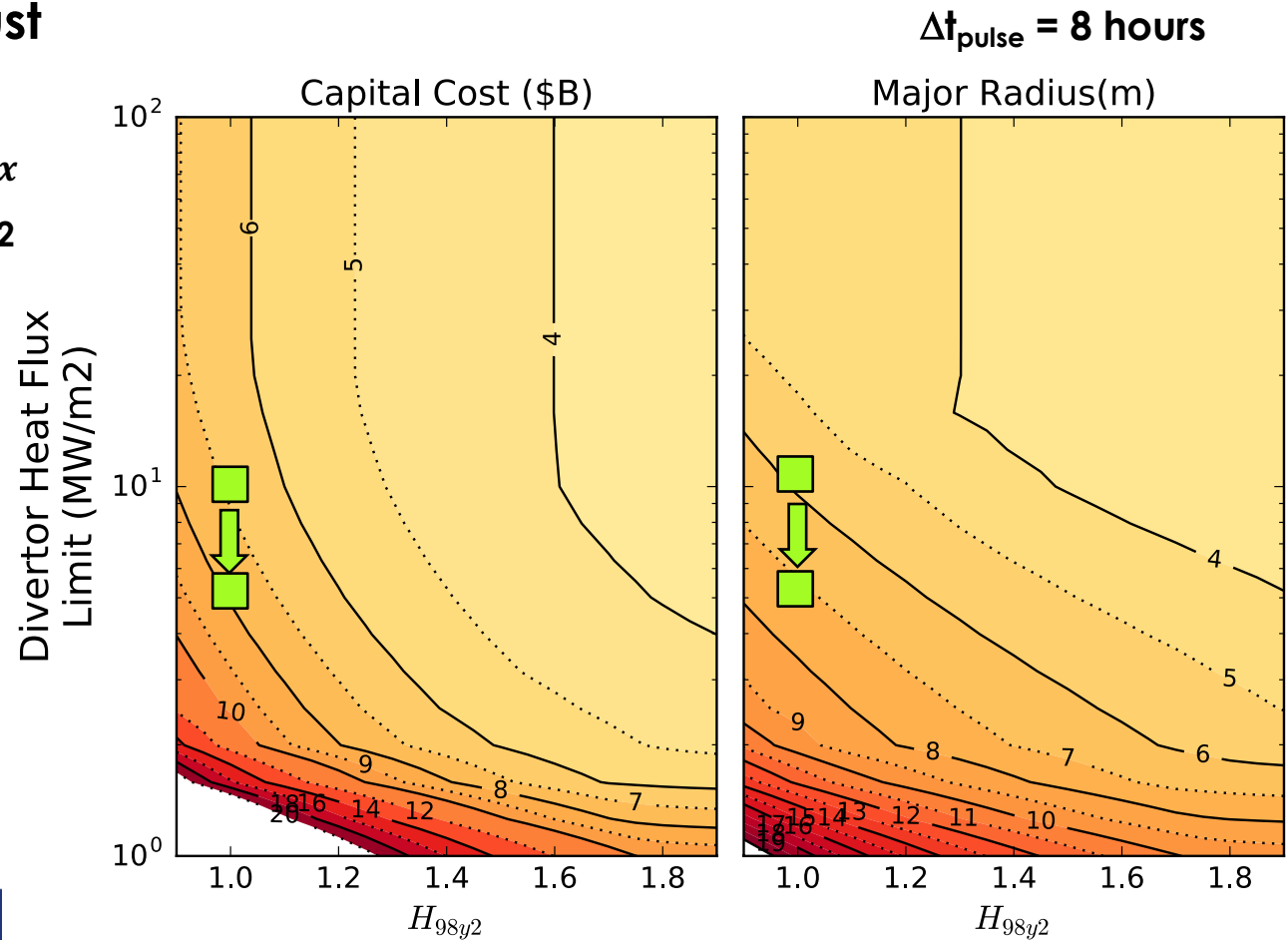
At $H_{98y2} = 1.0$, Divertor Heat Flux Capability Serves as A Primary Limitation on Device Size (and Capital Cost)

- For all H_{98y2} , device size must grow as q_{div}^{max} is decreased



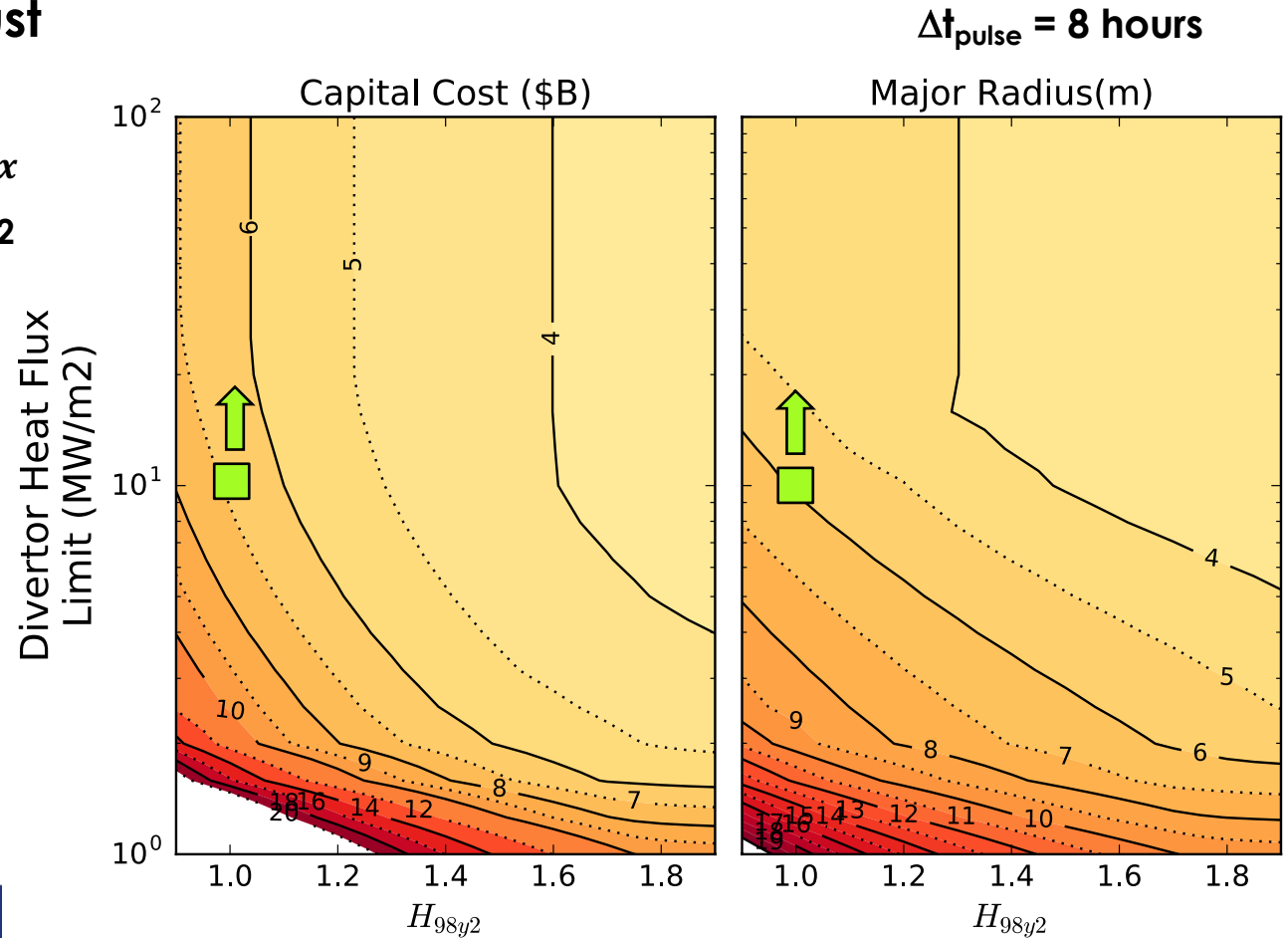
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- At $H_{98y2} = 1.0$, reducing q_{div}^{max} from 10 MW/m^2 to 5 MW/m^2 increases size (and cost) significantly
 - R_o : $5.8 \text{ m} \rightarrow 7.2 \text{ m}$
 - Capital Cost: $\uparrow 30\%$



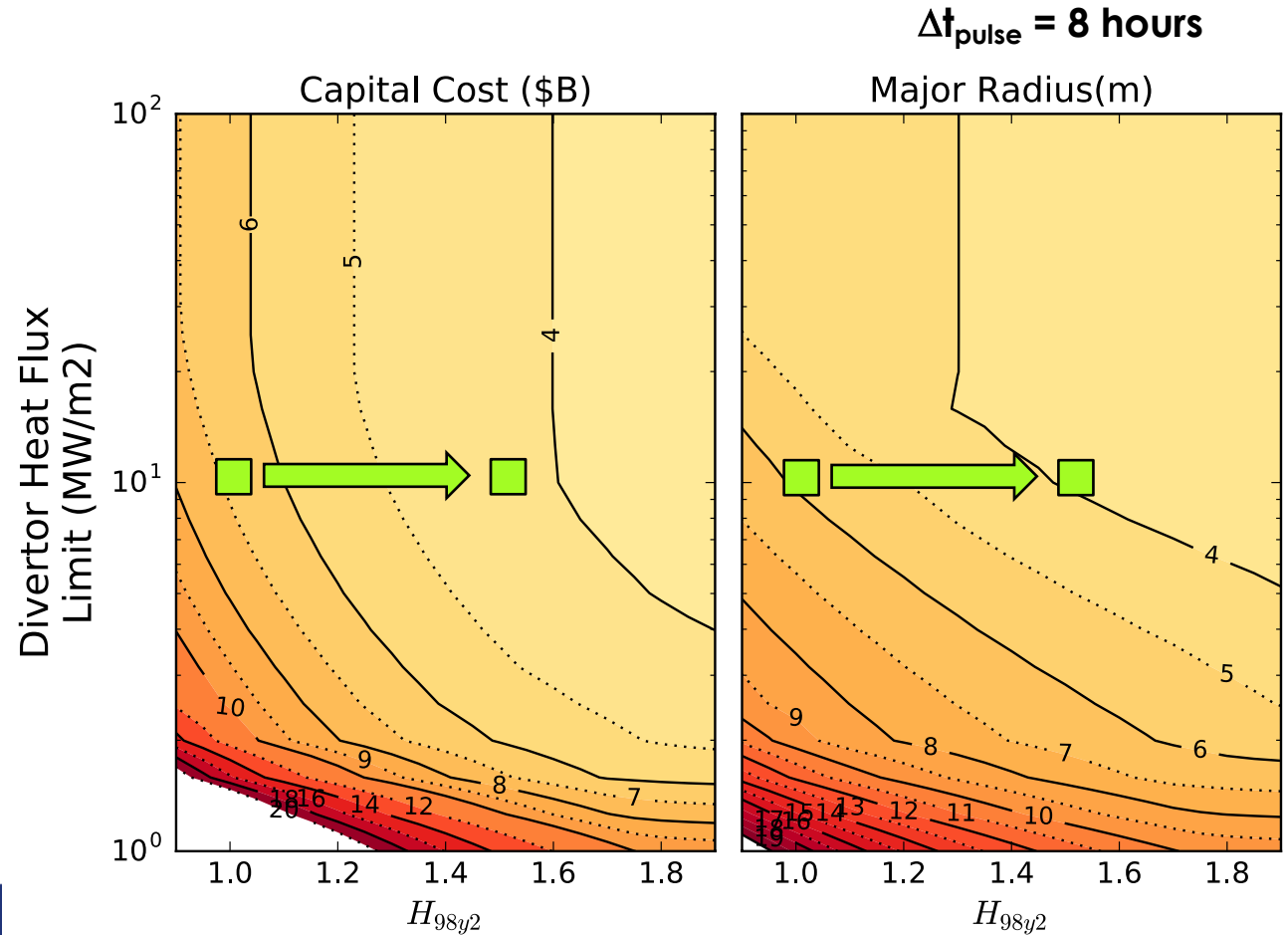
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 - R_o : $5.8 \text{ m} \rightarrow 7.2 \text{ m}$
 - Capital Cost: $\uparrow 30\%$
- Some advantage to increasing q_{div}^{max} but only up to $\sim 15 \text{ MW/m}^2$



At $q_{div}^{max} = 10 \text{ MW/m}^2$, Increasing Confinement Leads to Significant Reduction in Device Size (and Capital Cost)

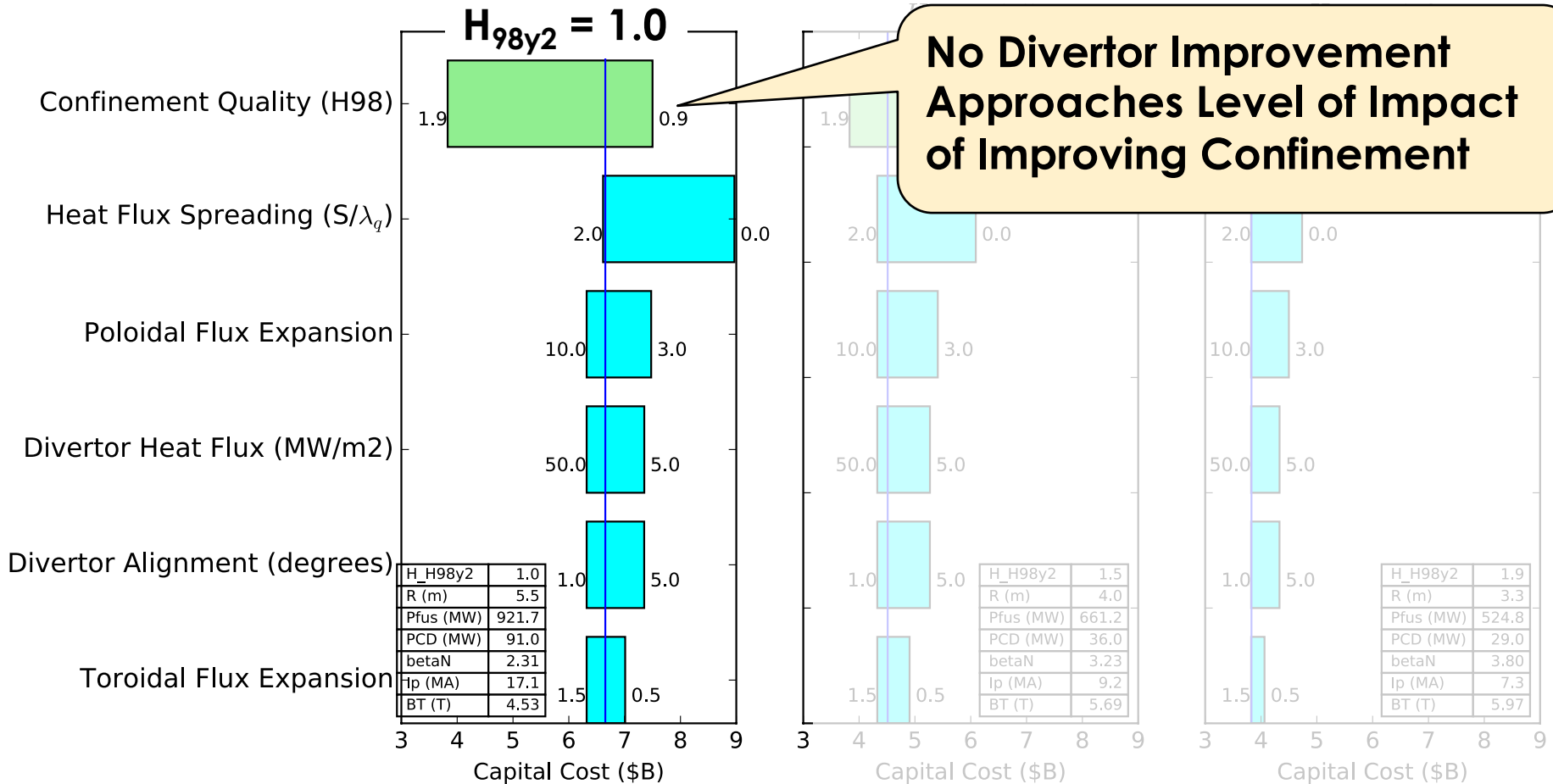
- Increasing H_{98y2} from 1.0 → 1.5 yields significant benefit
 - R_o : 5.8 m → 4.0 m
 - Capital Cost: ↓ 35%
- Similar improvements at all values of q_{div}^{max}
- Further improvements still possible at higher H_{98y2}



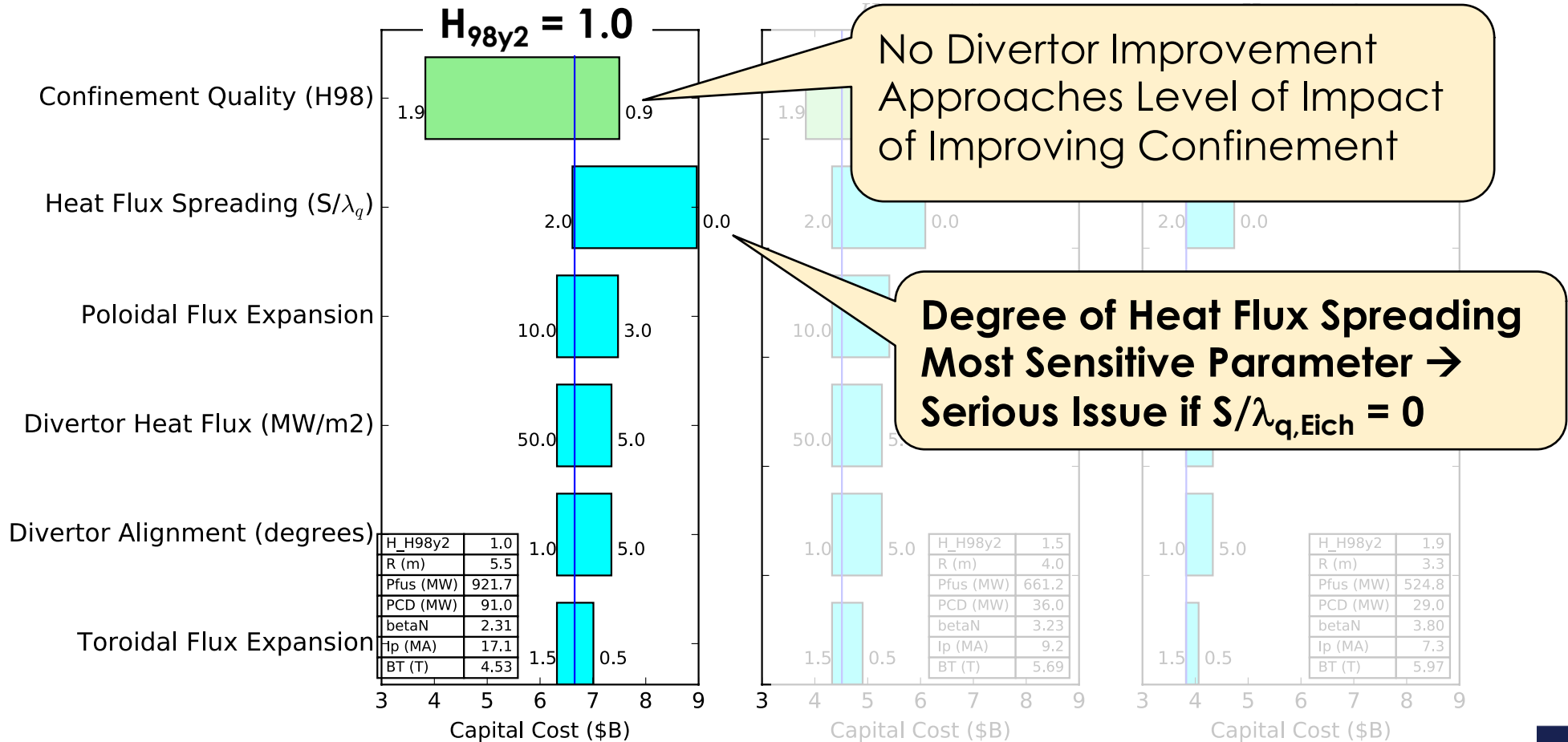
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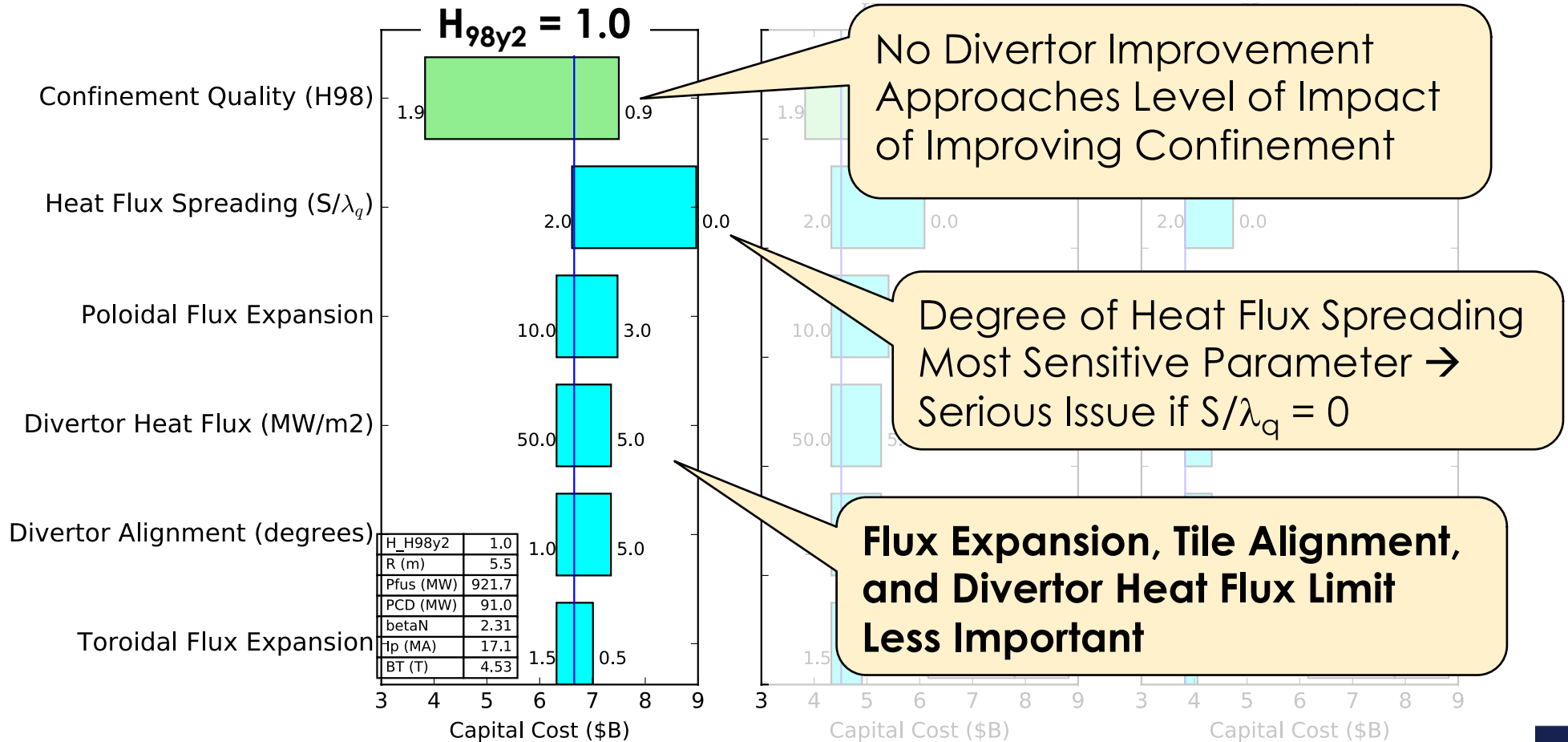
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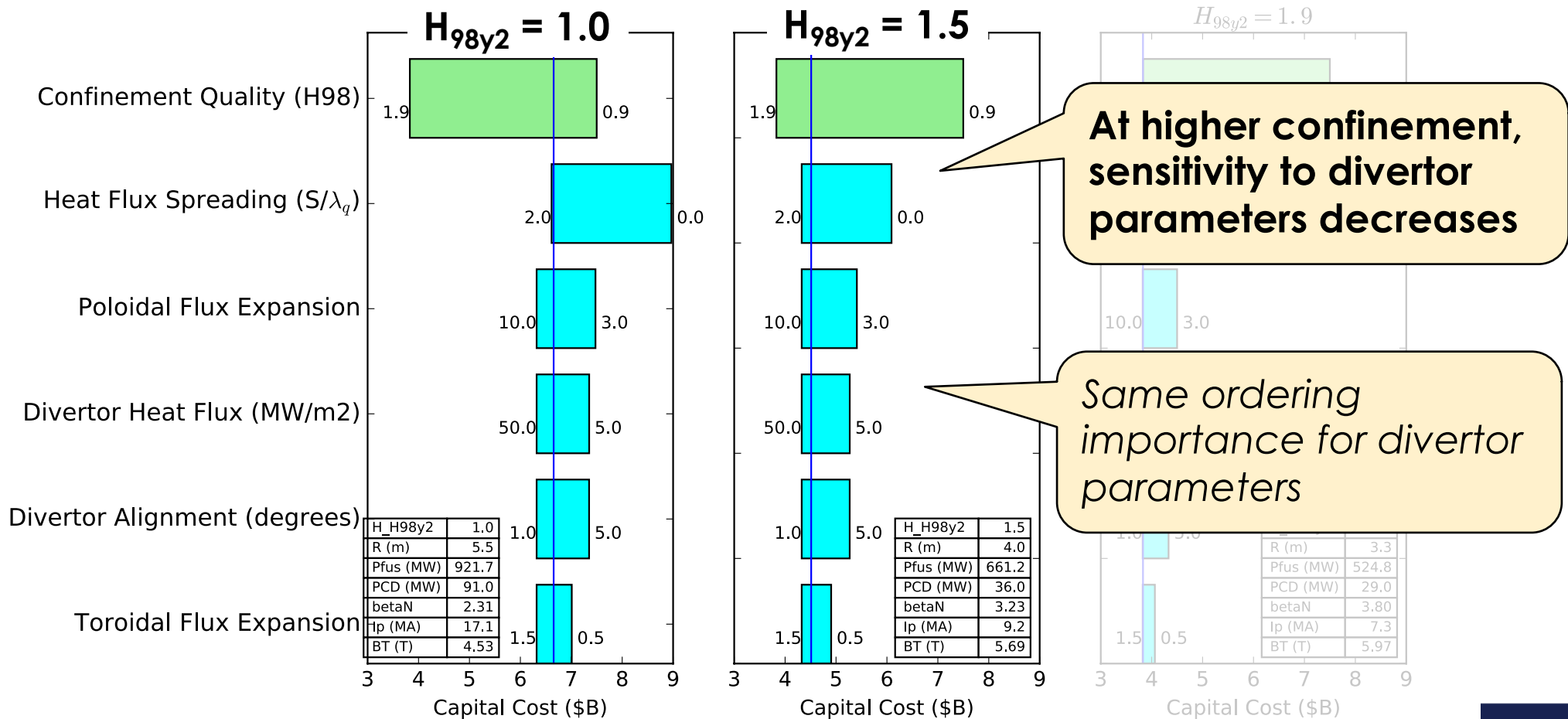
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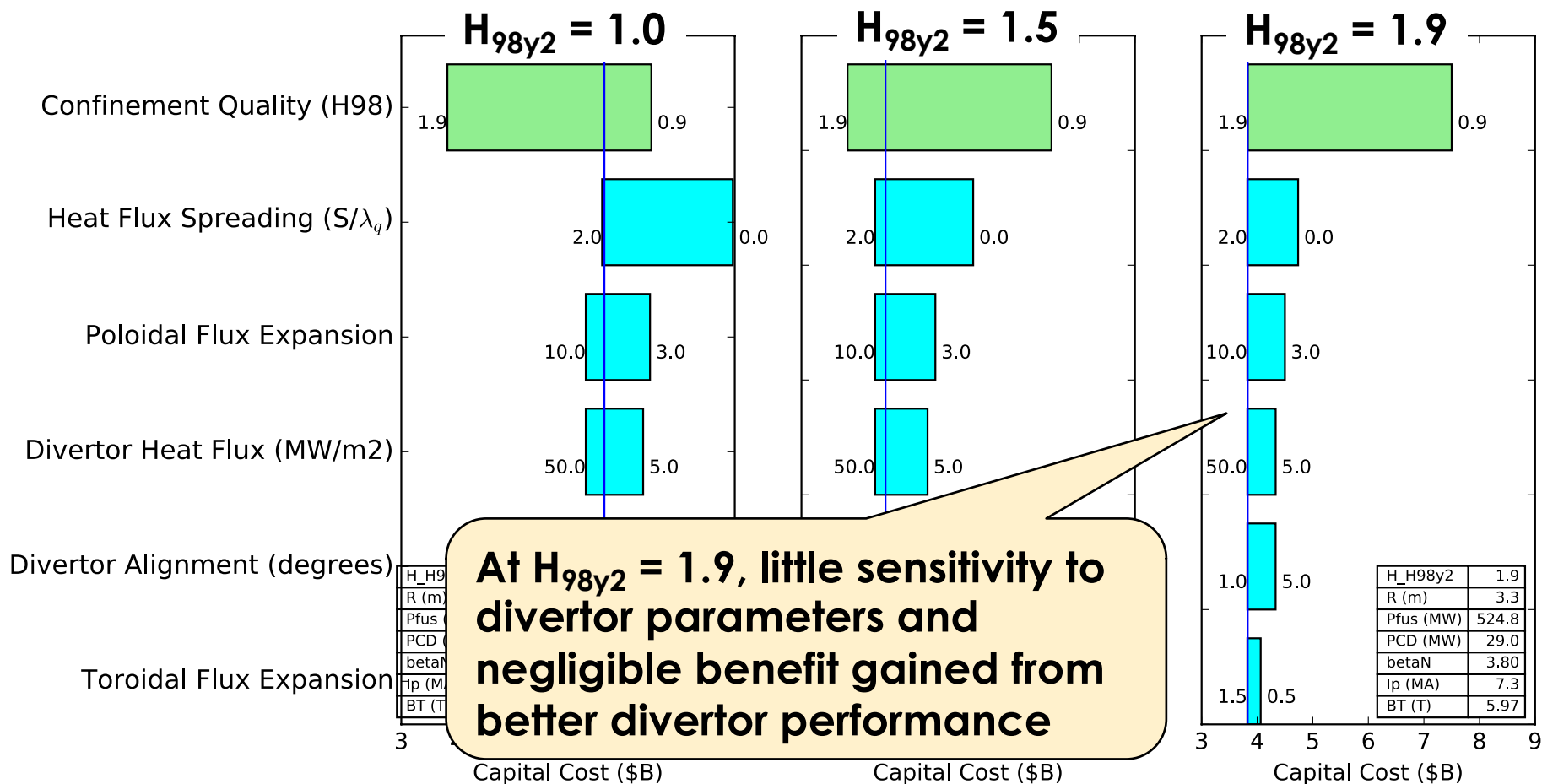
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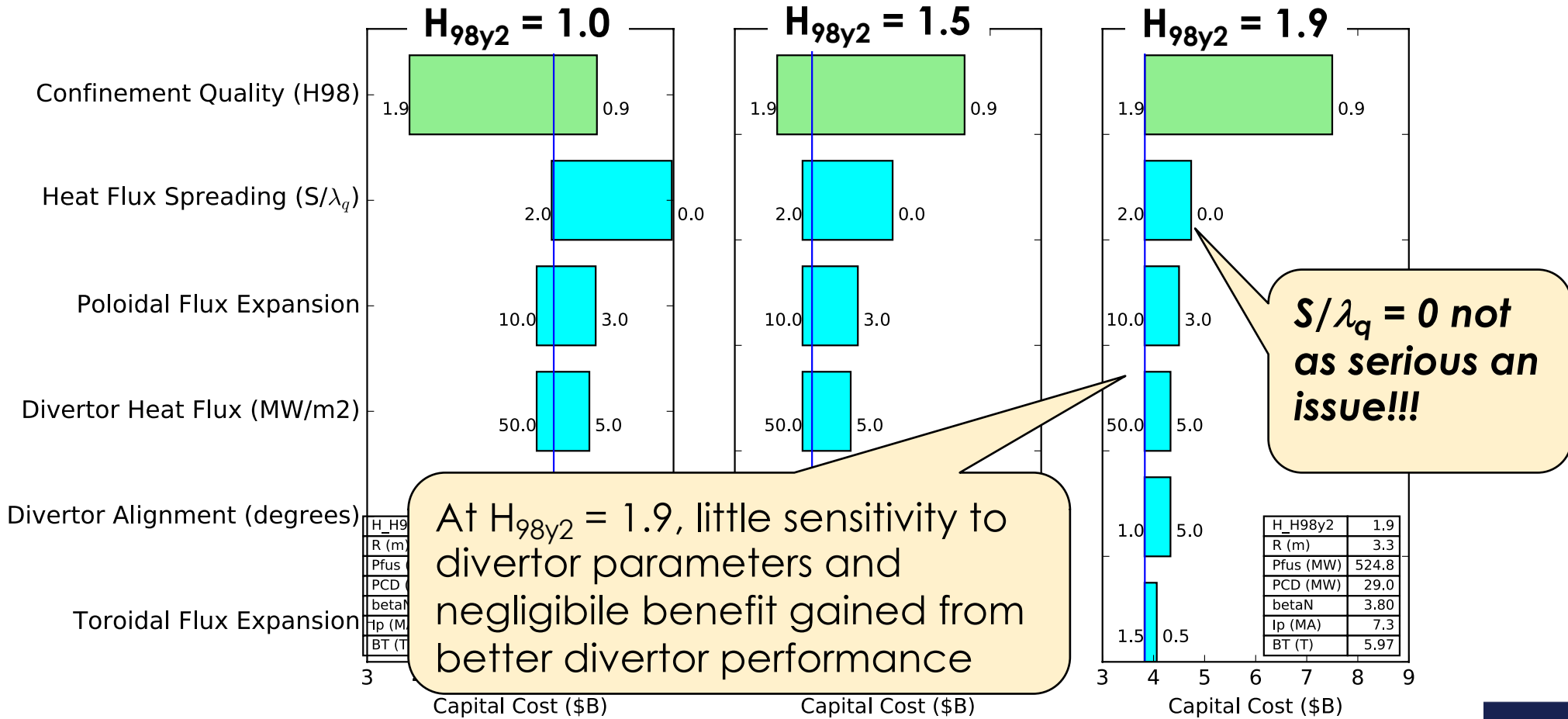
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Summary: Takeaways from this Analysis for Power Exhaust Research and Development

- **Power exhaust constraints are important at ITER-like confinement**
 - However, limited (no?) pathways to reduce device size with improved power exhaust methods
- **Achieving higher confinement offers significant benefits in reducing power exhaust requirements and device size**
 - *Aggressive R&D program in core-edge integration is needed to develop robust scenarios along this line*
- **Regardless of assumption on confinement, highest leverage R&D effort in divertor R&D should be maximizing heat flux spreading S/λ_q**
 - Flux expansion and divertor target angle offer some, but only modest, improvements