



The Impact of Anisotropy on ITER **Scenarios and Edge Localised Modes**



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1 (a)

⁰d/d 0.5

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Motivation

- In JET, ICRH can cause anisotropies of $p_{\perp} / p_{\parallel} = 2.5$ [W Zwingmann *et a*I.PPCF, 43(11):1441, 2001.]
- MAST has reached $p_{\parallel}/p_{\perp} \approx 1.7$ [MJ Hole et al. PPCF, 53(7):074021, 2011.]

1. Equilibrium with flow, anisotropy

 Inclusion of anisotropy and flow in equilibrium MHD equations e.g. [R. lacono, et al Phys. Fluids B 2 (8). 1990]

$$\nabla \cdot (\rho \mathbf{v}) = 0, \qquad \rho \mathbf{v} \cdot \nabla \mathbf{v} = \mathbf{J} \times \mathbf{B} - \nabla \cdot \overline{\mathbf{P}}, \qquad \nabla \cdot \mathbf{B} = 0$$

$$\mu_0 \mathbf{J} = \nabla \times \mathbf{B}, \qquad \nabla \times (\mathbf{v} \times \mathbf{B}) = 0,$$

$$\overline{\mathbf{P}} = p_{\perp} \overline{\mathbf{I}} + \Delta \mathbf{B} \mathbf{B} / \mu_0, \qquad \Delta = \frac{\mu_0 (p_{||} - p_{\perp})}{B^2}$$

2. Ballooning modes in anisotropic plasmas

- **Aim:** explore the impact of anisotropy on n=30 mode for the same q and J_{ϕ} profile
- As in Huysmans *et al* Phys. Plasmas 8 4292–305, 2001, assume a circular cross-section tokamak, $R_0/a=4$, $\beta_{pol}=1$, and $q_a=4$. $p'(\psi) = p_0(1 - \psi_n), \quad \psi_n < \psi_b$

$$p'(\psi) = p_0 \left(1 - \psi_n + p_1 \left[\frac{(\psi_n - \psi_b)^2 (3 - 2\psi_n - \psi_b)}{(1 - \psi_b)} \right]^{1/4} \right), \quad \psi_n > \psi_b$$

$$\langle J \rangle = J_0 \left(1 - 0.8\psi_n - 0.2\psi_n^2 \right), \quad \psi_b$$

Isotropic radial plasma profiles constructed by HELENA

investigate the stability of an

3. ITER Pre-fusion power operation

• Pre-fusion power operation H plasma, 5MA, B=1.8T (1/3 field) ICRH scenario: #100003, run 1 at 324s



• Fast ion distribution function from SPOT (M. Schneider).

- If toroidal flow only: $\mathbf{v} = -R\phi'_E(\psi)\mathbf{e}_{\omega} = R\Omega(\psi)\mathbf{e}_{\omega}$ $\Rightarrow F(\psi) = RB_{\phi}(1-\Delta)$
- If two temperature Bi-Maxwellian model chosen

$$p_{||}(\rho, B, \psi) = \frac{k_B}{m} \rho T_{||}(\psi), \qquad p_{\perp}(\rho, B, \psi) = \frac{k_B}{m} \rho T_{\perp}(B, \psi)$$

Can write

$$W(\rho, B, \psi) = T_{\parallel} \ln \frac{T_{\parallel} \rho}{T_{\perp} \rho_{0}}, \quad H = W - \frac{1}{2} [R \phi_{E}'(\psi)]^{2}, \quad T_{\perp}(B, \psi) = \frac{T_{\parallel} B}{|B - T_{\parallel} \Theta(\psi)|_{\parallel}},$$
$$\nabla \cdot \left[(1 - \Delta) \left(\frac{\nabla \psi}{R^{2}} \right) \right] = -\frac{\partial p_{\parallel}}{\partial \psi} - \rho H'(\psi) + \rho \frac{\partial W}{\partial \psi} - \frac{F'(\psi)F'(\psi)}{R^{2}(1 - \Delta)} + R^{2} \rho \Omega(\psi) \Omega'(\psi)$$
$$\left\{ H(\psi), T_{\parallel}(\psi), F(\psi), \Theta(\psi), \Omega(\psi) \right\}$$

- Implemented in EFIT TENSOR for equilibrium reconstruction [Fitzgerald, Appel, Hole, Nucl. Fusion **53** (2013) 113040]
- Implemented in HELENA-ATF for stability studies [Qu, Fitzgerald, Hole, PPCF **56** (2014) 075007]

Constraining HELENA+ATF





Including Anisotropy : Employ Steps (1)-4(a)

- MISHKA-A [Qu et al; Plasma Phys. Control. Fusion 57 095005] extends MISHKA to plasmas with an anisotropy and flow
- MISHKA-A assumes a conformal wall at $R_w = 1$.
- Adapt HELENA equilibrium to include an "artificial vacuum": set the p'(ψ_n)=0 for ψ_n .>0.95



continuum, and TAE mode structure.

e.g.

σ

్లా -0.2

Cross-section across midplane







Anisotropy Scans Methodology

Addition of physics produces free parameters that are either not fully constrained (or self-consistent), or it is the inferred quantities (e.g. q profile) that are effectively constrained.

 \Rightarrow choose appropriate constraints to resolve impact of pressure anisotropy cf q profile.

1 Constrain to Grad-Shafranov solution

- **2.** Select target $\Theta(\psi)$
- **3** Constrain thermal energy W_{th} such that $p = (2p_{\perp} + p_{\parallel})/3$. Modify β to match W_{th} by iterating HELENA+ATF until $\Delta W_{th}/W_{th} < \varepsilon_{WV}$

 (∂p_i)

 $1 \left(\partial \left(RB_{\phi,i} \right)^2 \right)$

 \boldsymbol{R}

(2)

(3)

- **4.** Modify current profile to match q. Either
- (a) <u>Single pass</u>: Assume $B_{\phi} >> B_{\theta}$ and low $\beta = 2\mu_0 p/B^2$

In the isotropic case:
$$J_{\phi,i} = R \left(\frac{1}{\partial \psi}\right)_B + \frac{1}{2\mu_0 R} \left(\frac{1}{\partial \psi}\right)_B + \frac{1}{2\mu_0 R} \left(\frac{1}{\partial \psi}\right)_B$$

In the anisotropic case: $J_{\phi,a} = R \left(\frac{\partial p_{\perp,a}}{\partial \psi}\right)_B + \frac{1}{2\mu_0 R} \left(\frac{\partial \left(RB_{\phi,a}\right)^2}{\partial \psi}\right)_B$
Force $J_{\phi,i} = J_{\phi,a..}$
Integrate over ψ : $F_a^2 = F_i^2 \frac{1 - \Delta^2}{1 - \frac{2}{3}\Delta} \approx F_i^2 \left(1 - \frac{4}{3}\Delta\right)$
Rerun HELENA+ATF

(b) <u>Iteration: In general the toroidal current can be written</u>

$$J_{\phi} = -\frac{F(\psi)F'(\psi)}{(1-\Delta)R\mu_0} - \left[T_{\parallel}'(\psi) + H'(\psi) - \left(\frac{\partial W}{\partial \psi}\right)_{\rho,B}\right].$$

Next, we assume: $J_{\phi,a} + \frac{F_a(\psi)F_a'(\psi)}{(1-\Delta_a)R\mu_0} \approx J_{\phi,i} + \frac{F_i(\psi)F_i'(\psi)}{R\mu_0},$
Compute

$$\int_{1}^{\psi_n} \langle J_{\phi,a}(1 - \Delta_a) R \mu_0 - J_{\phi,i} R \mu_0 \rangle (\psi_a - \psi_0) d\psi_n \approx \begin{bmatrix} -F_a^2 + F_i^2 \end{bmatrix}$$
(1)
$$= -\delta F^2(\overline{\psi_n}) + \delta F^2$$

... and then update

$$F^2(\overline{\psi_n}) \to F^2(\overline{\psi_n}) - \delta F^2(\overline{\psi_n}).$$

Rerun in HELENAT+ATF and compute

 $\Delta q = \int_{\Omega} \left(q_{target} - q \right) d\psi_n$

Iterate Eqs. (1) – (3), and the replacement for F until $\Delta q < \varepsilon_q$

0.8 1 1.2 1.4 (ie.
$$|\widetilde{\Theta}_0| < 0.2$$
)

<u>Reason</u>: As T₁ increases over T_{11} , p_{1} surfaces are displaced outboard to bad curvature region *cf* an inward shift of surfaces stabilises the mode.



- > Over parameter range explored growth rate has same dependence with a
- \succ First step to (s, α) marginal stability boundaries with anisotropy.
- γ^2/ω^2 increases with increasing p_\perp/p_{\parallel} (increasing $\widetilde{\Theta}_0 = 0$ $T_0/T_{||}(1-T_{||}/T_{\perp}).$
- Suggests *increasing* p_{\parallel}/p_{\perp} in the pedestal region might lead to higher ELM-free performance
- \blacktriangleright Density / pressure axis shift \propto anisotropy
- Little difference to shear continuum and gap eigenmodes
- Significant difference to compressional continuum,

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