



Progress of CFETR Design

Ge Zhuang¹, Guoqiang Li², J. Li², Y.X. Wan^{1,2}, Y. Liu³, X.L. Wang⁴, Y.T. Song², V. Chan¹, Q.W. Yang³, B.N. Wan², X.R. Duan³, and CFETR design team

¹University of Science and Technology of China, Hefei, China

²Institute of Plasma Physics, CAS, Hefei, China

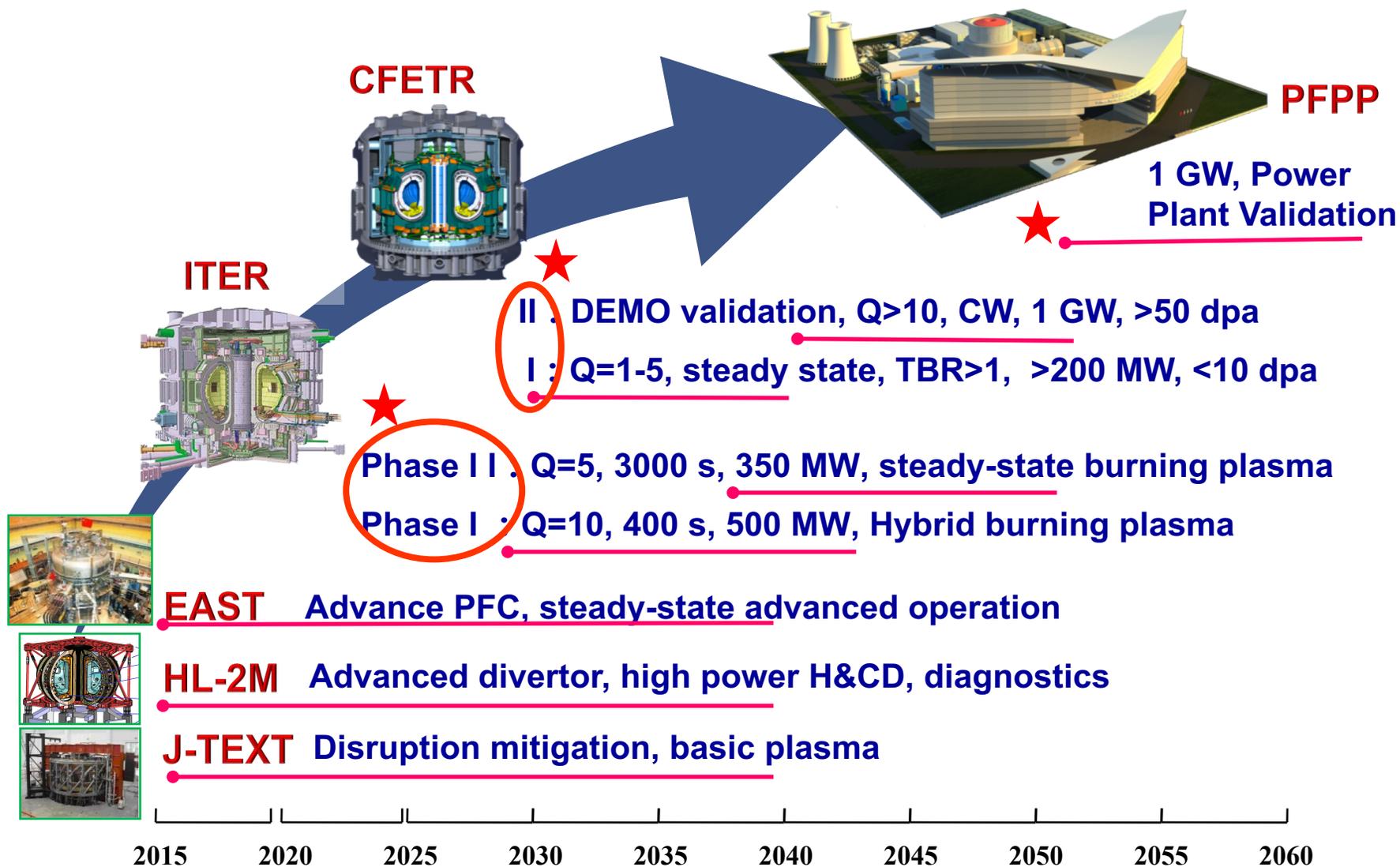
³Southwest Institute of Physics, Chengdu, China

⁴Chinese Academy of Physics Engineering, Mianyang, China

27th IAEA Fusion Energy Conference, Ahmedabad, India 22-27 October 2018



China MCF Roadmap





CFETR Mission

- Fusion power production of $P_f = 200\sim 1500$ MW
- Generates steady-state burning plasmas (duty time $\sim 50\%$)
- Tests the self-sustainable burning ($Q \geq 25\sim 30$, $H\alpha \sim 83\text{-}86\%$)
- Realizes Tritium self-breeding ($TBR \geq 1$)
- R&D for structural and functional materials which have high neutron flux resistive

Buildup the science and technology base for PFPP



Key Issues of CFETR Mission

**Obtained burning Plasma
for fusion power**

1. **P = 200-1500 MW**
2. **Q = 1-10, SSO, hours**
3. **Q = 20-30 hours-SSO**
4. **High energetic α heating**

**Steady-state operation
for fusion energy**

5. **SSO (Ext H&CD + Higher f_b)**
6. **Hybrid (OH+BS+CD)**
7. **PSI on the first wall**
8. **Heat & particle exhaust on Div.**

**Breeding tritium
for T self-sustained**

9. **T-breeding by blanket**
10. **T-plant: extract & reprocessing**
11. **Materials & components**
12. **Reliable and quick RH**
13. **Licensing & safety**



Course of CFETR Design Events

- **Concept design (2011-2017)**

- **First period (2011-2015)**

- $R = 5.7 \text{ m}, a = 1.6 \text{ m}, B_T = 4\text{--}5 \text{ T}, P_f = 200 \text{ MW}$

- **Second period (2015-2017)**

- $R = 6.6 \text{ m}, a = 1.8 \text{ m}, B_T = 5\text{--}7 \text{ T}, P_f = 1 \text{ GW}$

- **Integrated engineering design (2017-, 30 M\$)**

- **New version**

- $R = 7.2 \text{ m}, a = 2.2 \text{ m}, B_T = 6.5 \text{ T}, P_f = 200 \text{ MW} - 1 \text{ GW}$

- **Small scale R&D continues (70 M\$)**

- **Large scale R&D will start soon (500 M\$)**



Outline

- **Introduction**
 - New version of CFETR design
- **CFETR Physics Design**
 - Development of operation scenarios
 - Consideration of divertor conf. & impurity effects
 - Investigation of MHD stability
- **CFETR Engineering Design**
 - Magnet system
 - Vacuum system
 - Remote handling and maintenance system
 - Others...
- **Summary**



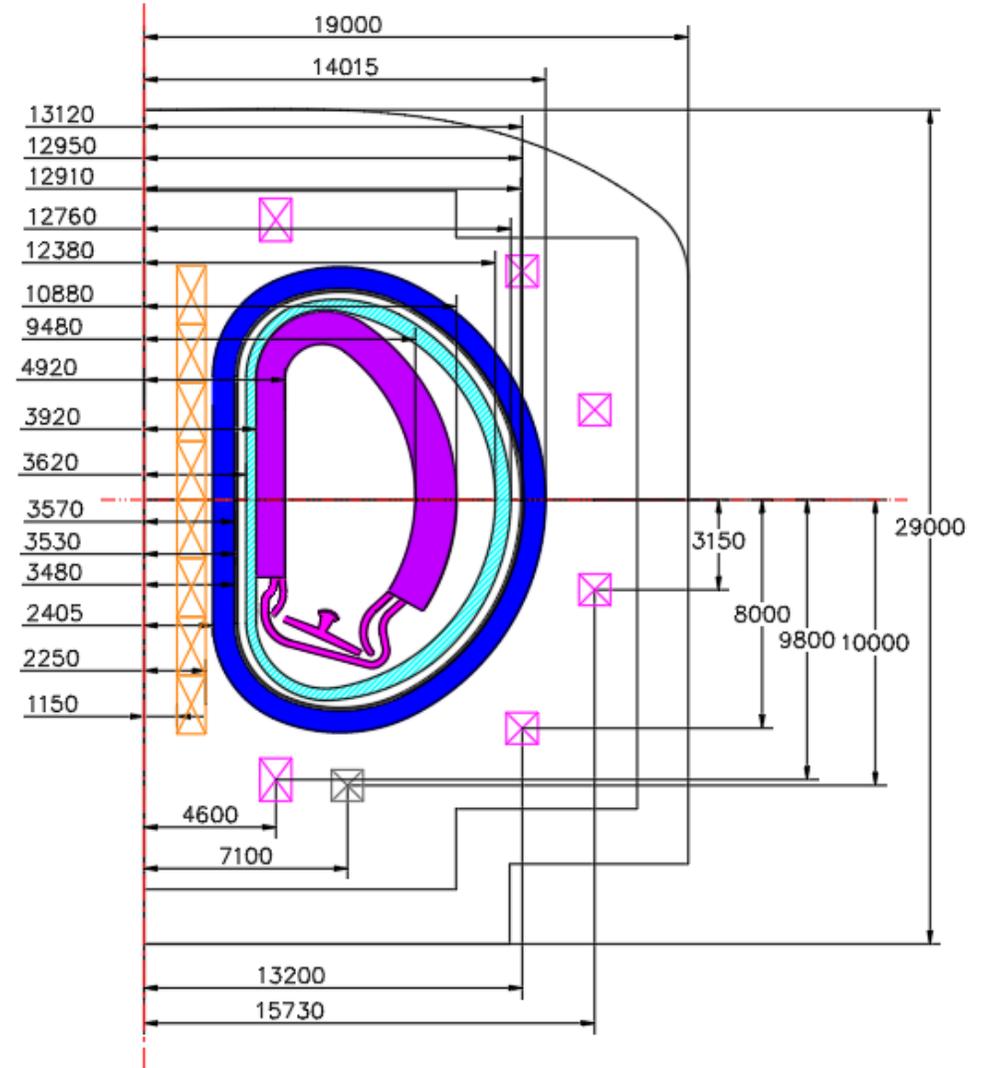
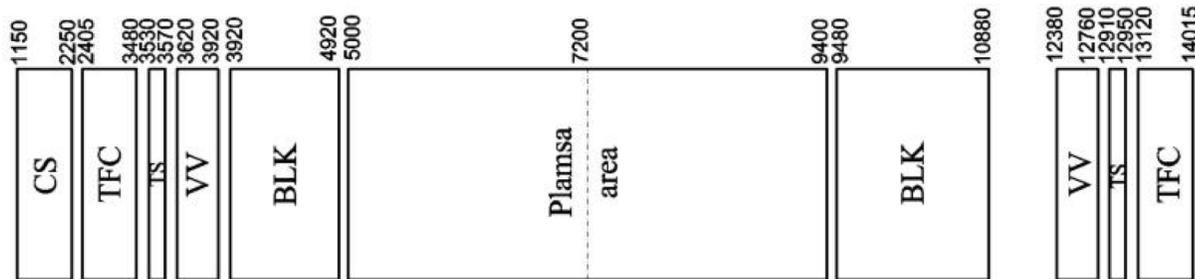
Outline

- **Introduction**
 - **New version of CFETR design**
- **CFETR Physics Design**
 - **Development of operation scenarios**
 - **Consideration of divertor conf. & impurity effects**
 - **Investigation of MHD stability**
- **CFETR Engineering Design**
 - **Magnet system**
 - **Vacuum system**
 - **Remote handling and maintenance system**
 - **Others...**
- **Summary**



New version of CFETR design

Key parameters	
Major Radius R_0	7.2 m
Minor Radius a	2.2 m
Elongation	2
Toroidal B Field B_T	6.5 T
Plasma Current I_p	14 MA
Divertor Conf.	Lower Single Null





Proposed CFETR Research Plan

- **Some new features of CFETR design**
 - Higher B_T , Lower I_p , Advanced CS (≥ 480 VS), 16 TF coils for easy RH →
More reliable plasma targets and higher confidence
- **CFETR operation plan (Staged approach)**
 - H/He: **1-2 years**
 - DD: **1-2 years**
 - DT: **< 100 MW : 1 years**
 - 200 MW, SSO, T fuel cycle, **5 years**
 - 500 MW, SSO, TBR > 1, **3 years**
 - DT: DEMO validation, 1 GW, **5 years**
 - Advance Scenario, > 1.5 GW , Q~30, **2-3 years**
 - Total: **~ 20 years**



Outline

- **Introduction**
 - New version of CFETR design
- **CFETR Physics Design**
 - Development of operation scenarios
 - Consideration of divertor conf. & impurity effects
 - Investigation of MHD stability
- **CFETR Engineering Design**
 - Magnet system
 - Vacuum system
 - Remote handling and maintenance system
 - Others...
- **Summary**



Primary Tasks of CFETR Physics Design

- **CFETR physics design mainly focuses on development and optimization of the operating scenarios with respect to physics and engineering constraints**
- **Operating scenarios will**
 - **Predict the fusion performance**
 - **Explore and determine a robust operation space possessing good confinement, MHD stability and acceptable transport level**
 - **Evaluate and limit the fraction of helium and other impurity particles while approaching the desirable fusion performance**
 - **Size up the power and particle exhaust compatibility with the chosen divertor configuration**
 - **Assess and manipulate the transit and steady heat load to the first wall and divertor to keep the machine safety**
 - ...



Integrated Modelling Strategy

- **0D system code used to scope out parameter space**
 - Provides 0th order engineering parameters e.g. R , a , I_p , B_T
 - Consistent set of H_{98} , β_N , f_{BS} , etc. for target Q_{fus} , P_{fus}
 - Ballpark estimates of P_{aux}
 - Does not identify actual operating scenario
- **Integrated Modeling (IM) used for scenario development**
 - Physics-based models, beyond experimental scaling laws
 - Reproducing experimentally demonstrated scenarios
 - Ensuring consistency of core, pedestal and boundary
- **IM informs key engineering design requirements**
 - H&CD, Divertor heat and particle fluxes, fueling
 - Plasma control and disruption mitigation
- **IM critical to CFETR diagnostics design and operation**
 - Provides best-guess, hard to measure profile information

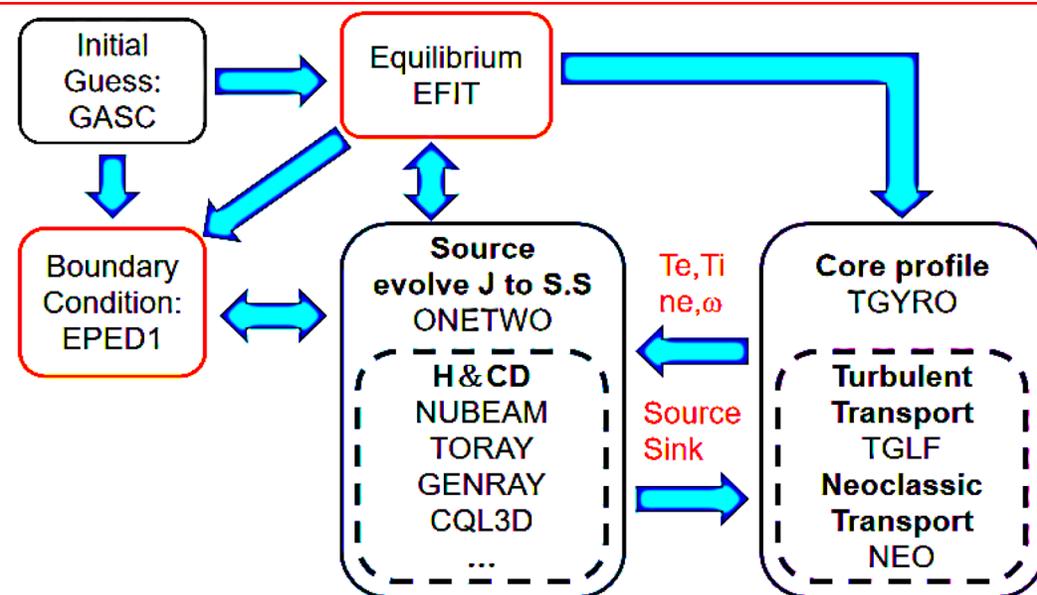


Code Suites for Multi-physics Modeling

- Core-pedestal coupling for scenario design
 - A workflow was developed under the framework **OMFIT**
- SOL and divertor **SOLPS**, **OEDGE/DIVIMP**, ...

- MHD stability **NIMROD**, **MARS-F**, **AEGIS**, **GATO** ...
- Energetic particle **NOVA-K**, **M3D**, **ORBIT** ...
- Pedestal Ana. & Opt. **ELITE**, **BOUT++** ...

- Plasma shape design **TEQ**, **EFIT**
- Discharge simulation **TSC**, **TOKSYS**



- Evolving particle densities, T_e and T_i , and momentum
 - $ne/He/impurity$ profiles evolved and D&T obey quasi-neutrality
- SOL solutions match core parameters at pivot point ~ top of pedestal
 - Heat and particle fluxes, iterate boundary densities and temperatures



Fully Non-inductive Operation Scenario Designed with System Code (0D)

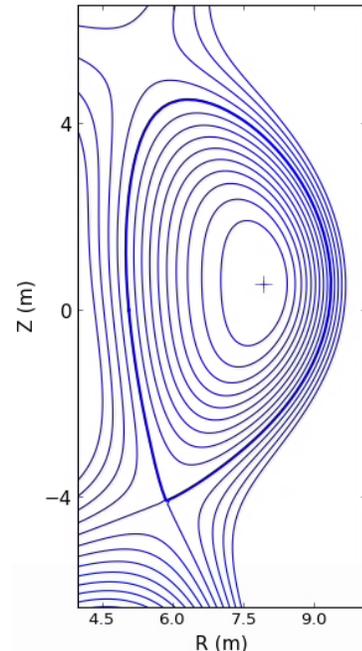
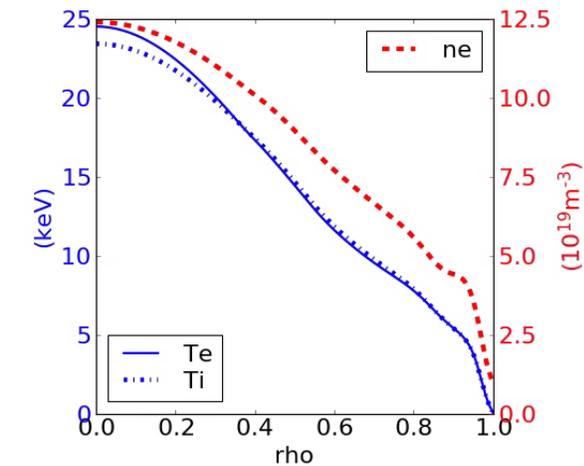
CFETR fully non-induct. R=7.2m, a=2.2m, $\kappa = 2$	Parameters	A.1 100MW	A.2 200MW	A.2 500MW	A.3 1GW	A.4 DEMO-level
fusion power	P_f	120	229	482	974	2192
power to run plant	P_{internal}	199	196	223	238	265
$P_{\text{fusion}}/P_{\text{aux}}$	Q_{plasma}	1.56	3.06	5.87	11.89	28.17
net electric power	P_{netelec}	-107	-58	30	232	738
Neutron Power at Blanket	P_n/A_{wall}	0.12	0.23	0.49	0.99	2.23
normalized beta	β_N	1.00	1.20	1.50	2.0	3.0
bootstrap fraction	f_{bs}	0.40	0.40	0.40	0.50	0.75
H factor over ELMY H_{net}	H_{ITER98Y2}	1.12	1.25	1.32	1.41	1.42
current drive power	P_{cd}	77	75	82	82	78
plasma current	I_p	8.61	10.34	12.92	13.78	13.78
field on axis	B_T	6.5	6.5	6.5	6.5	6.5
Ion/electron Temperature	$T_i(0)/T_e(0)$	18	24	32	36	32
Electron Density	$n(0)$	0.48	0.52	0.61	0.78	1.31
Ratio to Greenwald Limit	$n_{\text{bar}}/n_{\text{GR}}$	0.57	0.51	0.48	0.57	0.96
Z_{eff}	Z_{eff}	2.45	2.45	2.45	2.45	2.45
Power per unit R	P/R	8.52	9.42	11.66	15.69	30.70
q_{95_iter}	q_{95_iter}	8.87	7.39	5.91	5.54	5.54



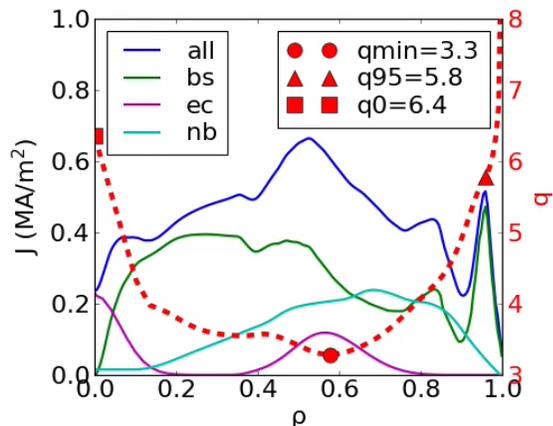
1GW Non-inductive Operation Scenario by Core-Pedestal Coupling Simulation

● Preliminary results

- No self-consistent tritium fueling
- Deviation ($\sim 30\%$ for P_{aux}) VS system code



$li \sim 0.64$
 $f_{GR,vol} \sim 0.89$



- **NBI** \rightarrow 500 keV (68 MW,CD) + 100 keV (10 MW, rotation drive)
- **EC** \rightarrow maintain large radius RS and control $q_{min} > 2$ to avoid low n deleterious MHD modes
- **Large BS current** \rightarrow RS and reduce CD power requirement
- **Moderate q_{95}**

	Simulation	Sys. Code
P_f (GW)	1.0	0.97
Q	9.1	11.9
P_{EC}/P_{NB}	31/78	82(tot)
$\beta_{N,th}(\beta_{N,tot})$	2.05(2.36)	2.0(\sim)
$H_{ITER98Y2}$	1.11	1.41
$f_{bs}(\%)$	59	50
I_p (MA)	12	14
I_{NB}/I_{EC} (MA)	4.0/0.9	\sim



Hybrid Operation Scenario Designed with System Code (0D)

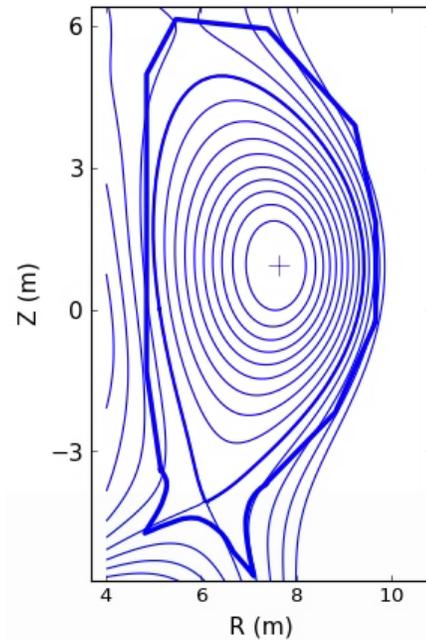
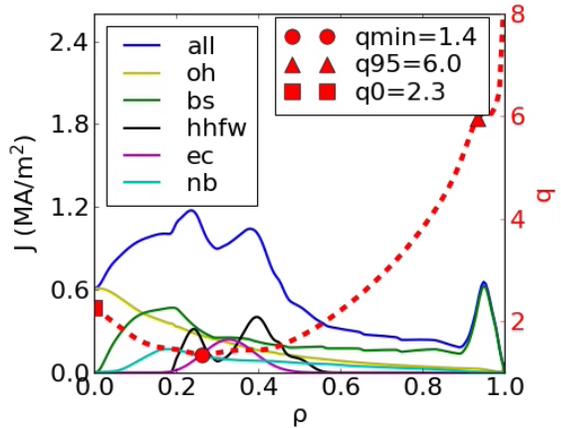
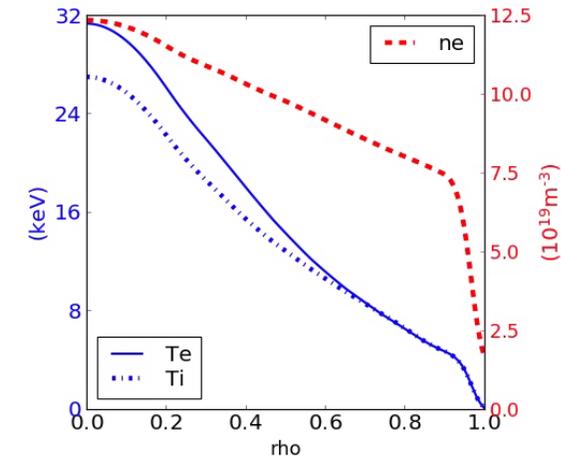
CFETR Hybrid Mode R=7.2m, a=2.2m, $\kappa = 2$	Parameters	B.1 100MW	B.2 200MW	B.2 500MW	B.3 1GW	B.4 DEMO-level
fusion power	P_f	114	250	558	1128	2192
power to run plant	P_{internal}	190	196	202	222	75
$P_{\text{fusion}}/P_{\text{aux}}$	Q_{plasma}	1.54	3.35	7.65	15.30	795.16
Neutron Power at Blanket	P_n/A_{wall}	0.12	0.25	0.57	1.15	2.23
normalized beta	β_N	1.00	1.20	1.50	2.00	3.0
bootstrap fraction	f_{bs}	0.40	0.40	0.40	0.50	0.75
H factor over ELMY H_{net}	H_{ITER98Y2}	1.01	1.09	1.18	1.19	1.54
Ohmic fraction	f_{ohm}	0.30	0.30	0.30	0.30	0.24
current drive power	P_{cd}	74	74	73	74	3
plasma current	I_p	8.61	10.34	12.92	13.78	13.78
field on axis	B_T	6.5	6.5	6.5	6.5	6.5
Ion/electron Temperature	$T_i(0)/T_e(0)$	13	17	24	24	34
Electron Density	$n(0)$	0.67	0.74	0.82	1.16	1.23
Ratio to Greenwald Limit	$n_{\text{bar}}/n_{\text{GR}}$	0.79	0.72	0.64	0.85	0.90
Zeff	Z_{eff}	2.45	2.45	2.45	2.45	2.45
Power per unit R	P/R	7.58	9.33	12.63	19.11	22.97
q95 iter	q_{95_iter}	8.87	7.39	5.91	5.54	5.54



1GW Hybrid Operation Scenario by Core-Pedestal Coupling Simulation

● Preliminary result

- No self-consistent tritium fueling
- Deviation ($\sim 25\%$ for P_{aux}) VS system



$li \sim 0.93$
 $f_{GR,vol} \sim 1.0$

- **NBI** \rightarrow 1 MeV (32 MW, CD) + 600 keV (11 MW, CD & rotation drive)
- **EC** \rightarrow maintain flat q profile and control $q_{min} > 1$
- **Moderate li** \rightarrow plasma stability
- **~ 300 Volt-sec** (8-hours in flattop)

	Simulation	Sys. code
P_f (GW)	0.92	1.1
Q	10	15
$P_{EC}/P_{FW}/P_{NB}$	30/20/43	74(tot)
$\beta_{N,th}(\beta_{N,tot})$	2.09(2.3)	2.0(\sim)
$H_{ITER98Y2}$	1.16	1.19
$f_{bs}(\%)$	49	50
I_p (MA)	13	14
$I_{NB}/I_{EC}/I_{FW}/I_{OH}$	1.4/0.8/1.6/3	$\sim/\sim/\sim/4$



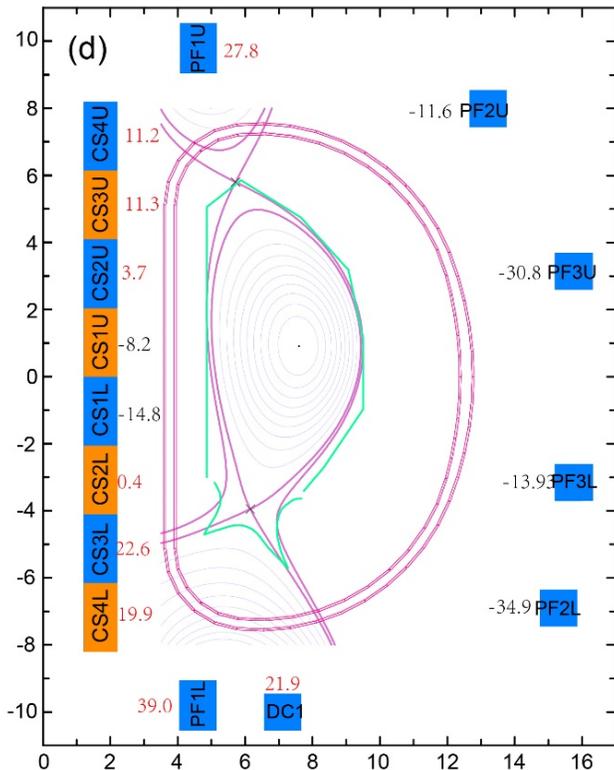
H & CD Scheme Consideration

- **EC: necessary tool for current profile control**
 - Optional freq/power: 190 GHz ~ 250 GHz, 20 ~ 40 MW
 - HFS top launched with high freq. for efficient off-axis ECCD
 - LFS above midplane for flexible location of ECCD
 - Optional application in NTM control
- **LH: efficient far off-axis current drive**
 - Optional freq/power: 4.6 GHz or beyond, ~20 MW
 - HFS launched above midplane (adapting for toroidal field along counter-clockwise direction) for CD at $r/a \geq 0.7$
- **HHFW: efficient off-axis or near-axis current drive**
 - Optional freq/power: 0.8 ~ 2 GHz, ~20 MW
 - Optional launched positions: HFS, LFS
 - High CD efficiency at $r/a < 0.6$
- **NB: broad current drive and possible significant rotation drive**
 - Option for CD: 600 keV ~ 1 MeV NNBI, 16 ~ 32 MW, (1 ~ 2 beam)
 - Option for rotation drive: 100 keV PNBI, 10 MW, (1 beam)



Considerations of Plasma Shape and Divertor

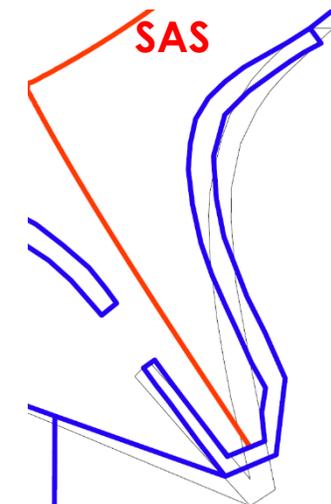
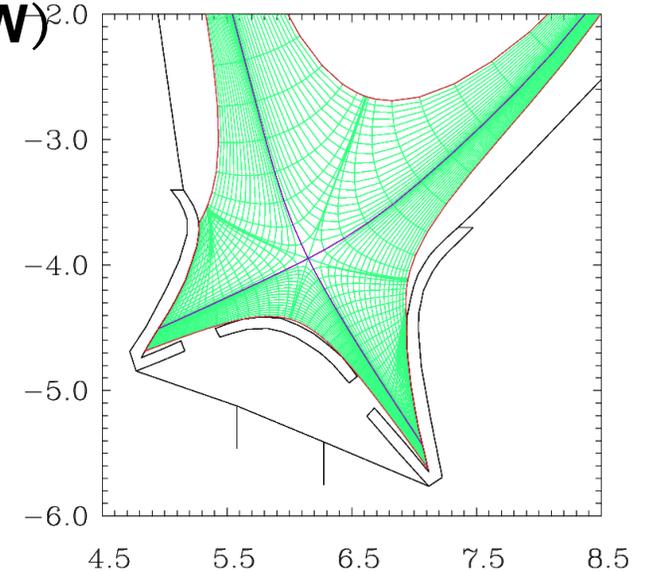
- ITER-like plasma configuration
 $\kappa_{sep}=2.0$, $\delta_u = 0.39$, $\delta_l = 0.45$
- A divertor coil (DC1) is added for possible advanced divertor configuration (Snowflake+)



$\kappa_{sep}=2.0$
 $\delta_u = 0.39$
 $\delta_l = 0.45$
 $dR_{sep} = 6.0 \text{ cm}$

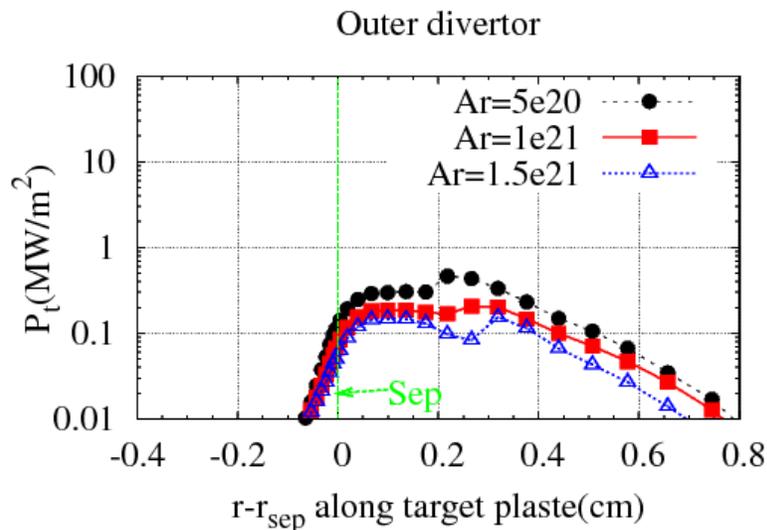
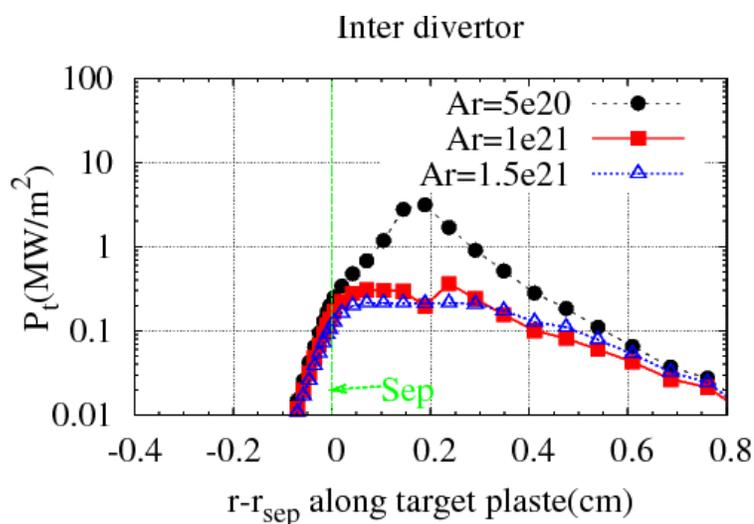
- Plasma-facing Materials (W)
- Different Divertor configurations
 - Conventional
 - Small Angle Slot (SAS)
 - Snowflake+
- Optimization target
 - $P_{peak} \leq 10 \text{ MW/m}^2$
 - $T_e \leq 5-10 \text{ eV}$
 - $n_{e-sep} \leq 5 \times 10^{19} \text{ m}^{-3}$
 - $Z_{eff-ped} \leq 3$

Conventional



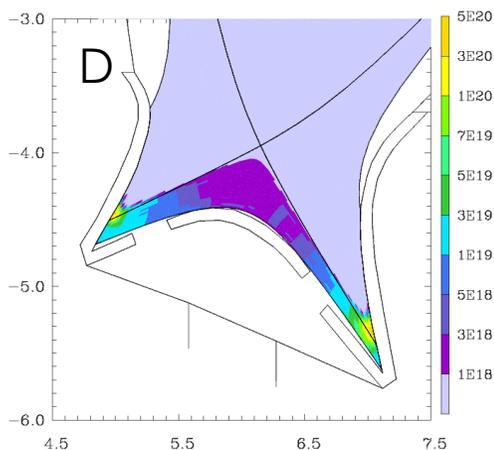


Ar Injection Can Effectively Reduce the Divertor Heat Load to below 10 MW/m²



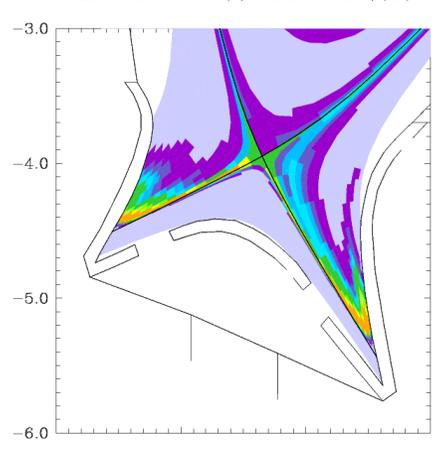
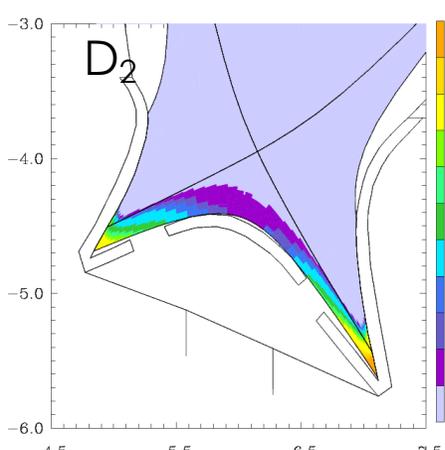
- Simulation performed with SOLPS code
- The peak heat fluxes on both inner and outer divertor are below 10 MW/m²
- Total radiation is higher than 80%, mainly by Ar impurities
- Detachment occurs at the strike points, but still too high T_e in far SOL region
- Fueling dilution and fusion performance degradation in core region should be carefully concerned for high radiation scenarios

Neutral density (m⁻³)



Ar radiation (W/m³)

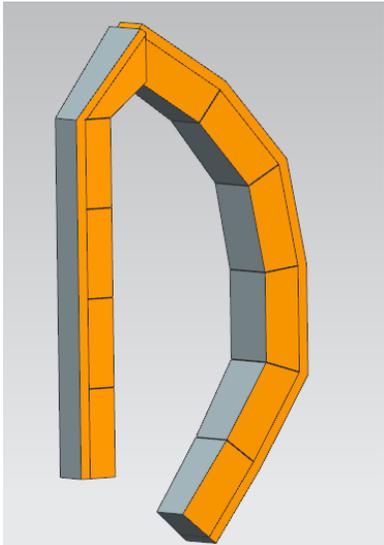
Line radiation rate (W) SUM Ar⁰ to Ar⁺¹⁸/(m³)



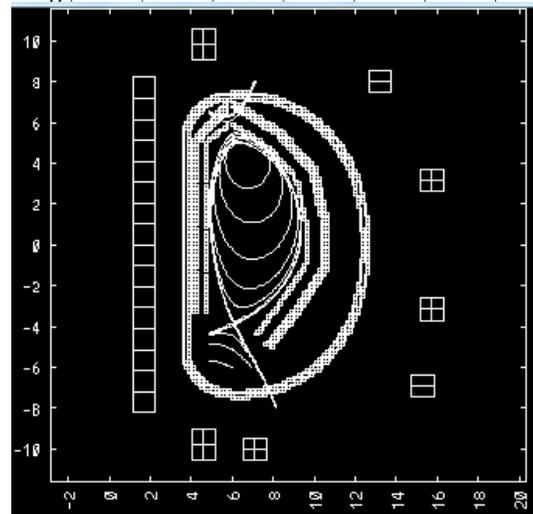
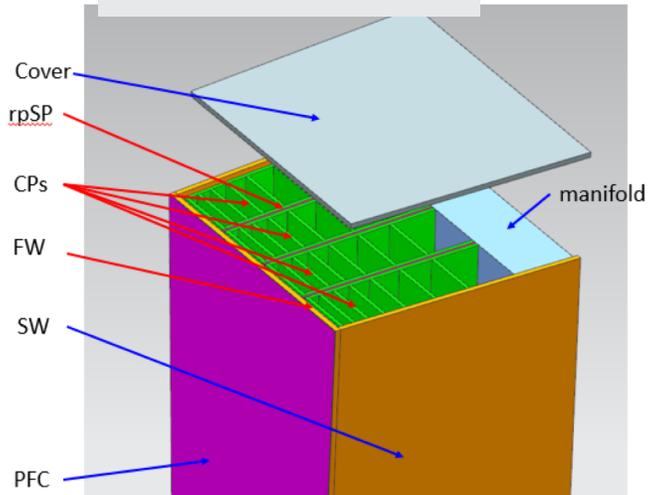
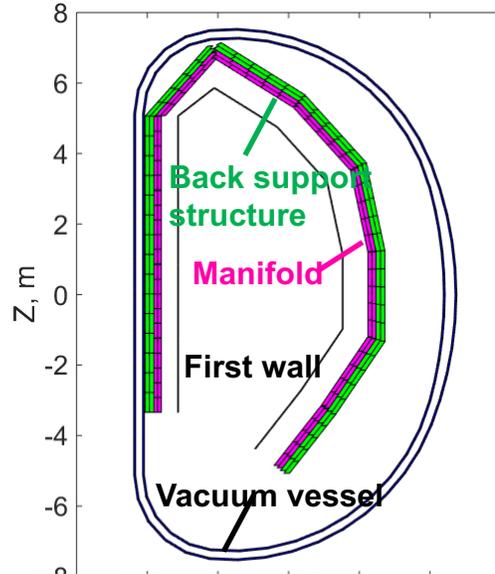


Blanket has strong stabilization effect on vertical instability

Real blanket structure



Modeled blanket structure



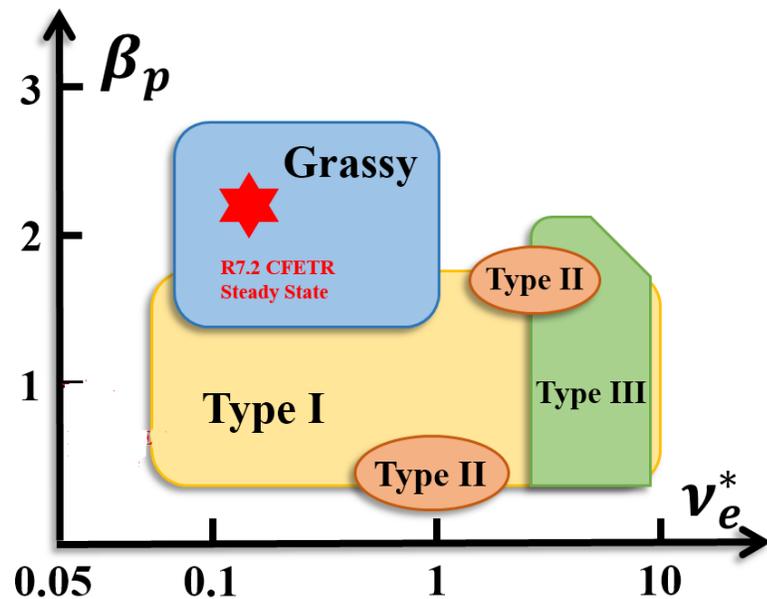
- Simulations are performed with TSC and TOKSYS codes
- Blanket modules (BM) are modeled with three-layer structures. Resistivity is evaluated and scanned
- Calculations show BM could significantly reduce the growth rate

Passive stru included	VV	VV + BM (7.6×10^{-7} ohm*m)	VV + BM (7.6×10^{-6} ohm*m)
Growth rate of VD (/s)	Out of control	2.2	18.1

- **Internal coils are still necessary to control the vertical instability. It is under assessment**



Operation in Grassy ELM regime?



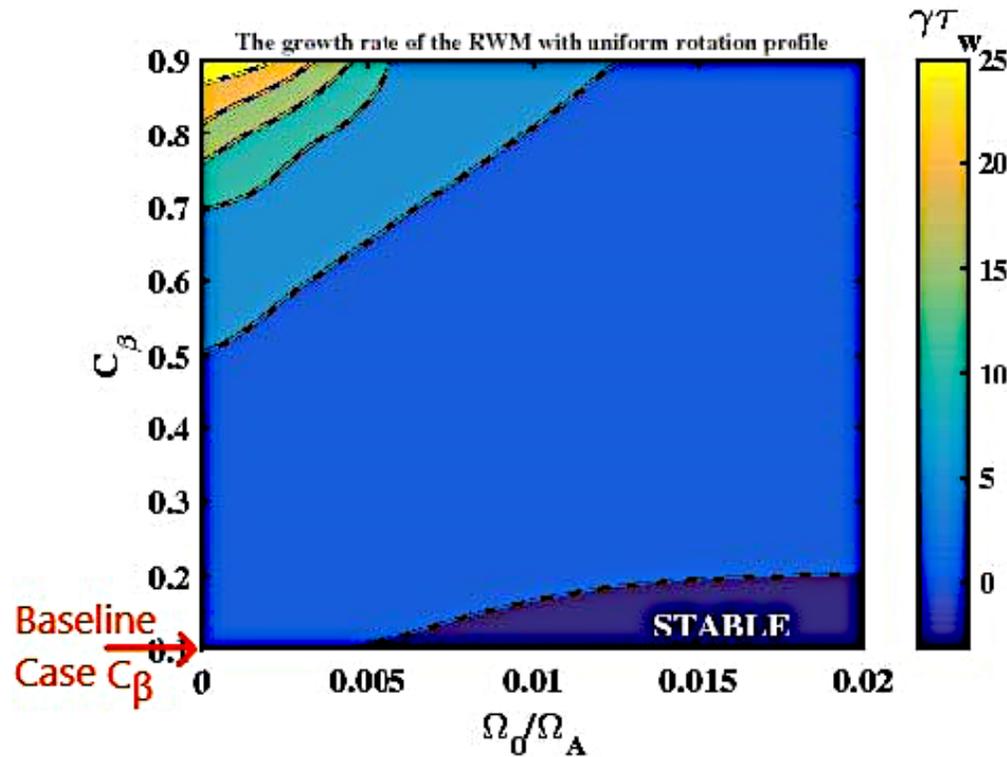
- Type-I ELM must be avoided
- Mostly likely, RMP coils will not be installed
- According to experimental data classification, β_p and v_e^* from EPED1 for the reference scenario put it in the grassy ELM regime
- BOUT++ and other codes are being used to verify the ELM prediction

Oyama N. 2008 J. Phys.: Conf. Ser.

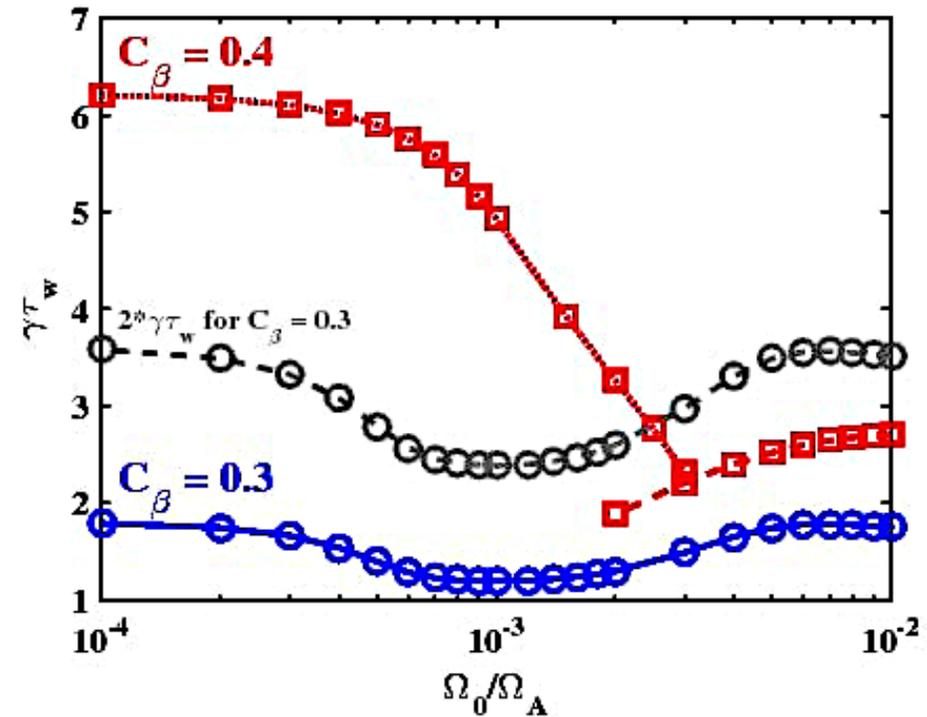


Resistive Wall Mode Should be Stable for the Steady-state Scenario

- MARS-K has been used to calculate the stability of RMWs, with uniform rotation
- The steady-state scenario is marginally unstable
- A small rotation of $\Omega_0/\Omega_A < 0.01$ could make the RMW stable



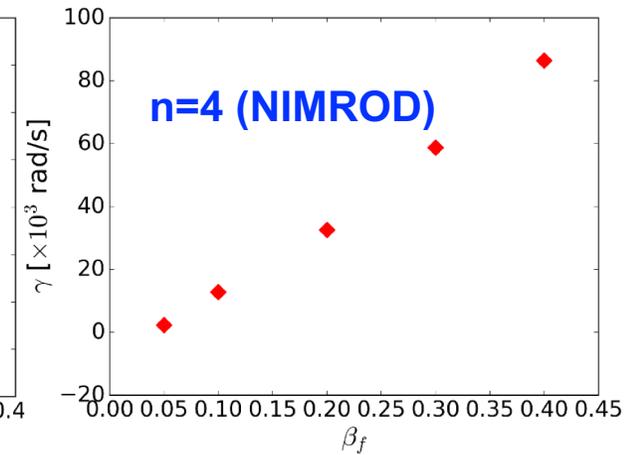
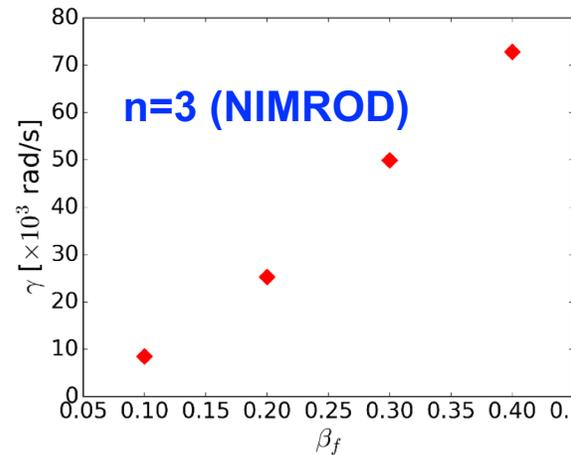
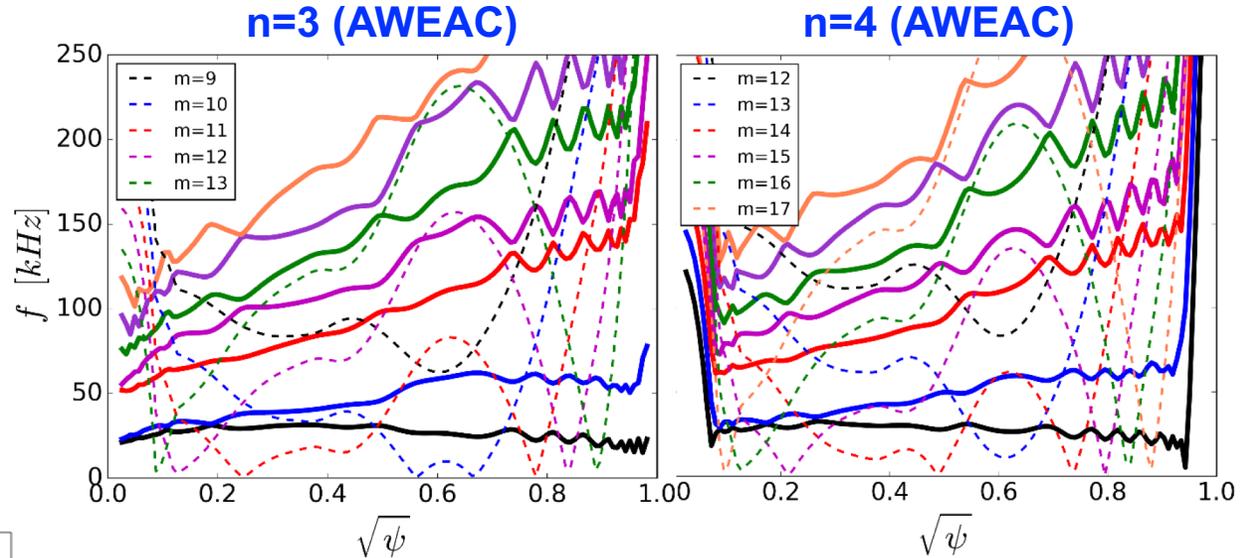
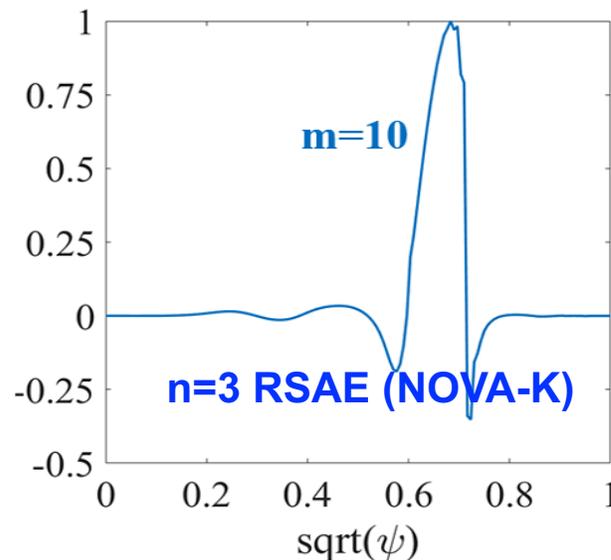
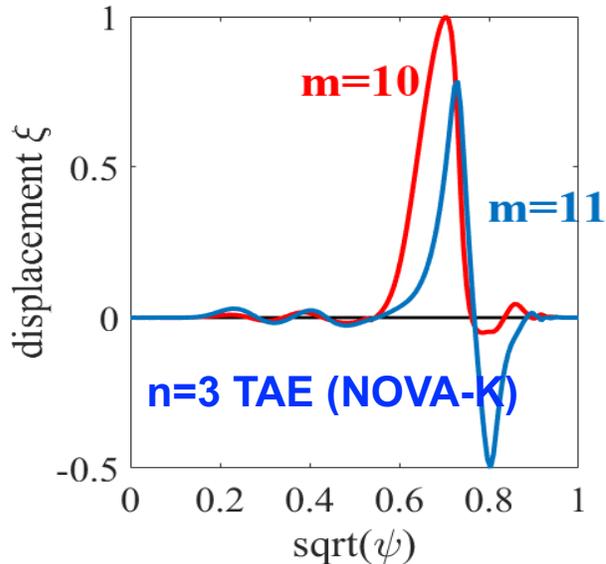
Growth rate of $n = 1$ RWM





α particle drive is weakly destabilizing for TAE and RSAE in steady state scenario

- Linear calculations show the α particle drive weakly destabilizing
- NOVA-K shows the damp effects could make TAEs and RSAEs marginally stable
- Effects of nonlinear AEs and EPs are under investigation



See Y. Hou TH/P2-7

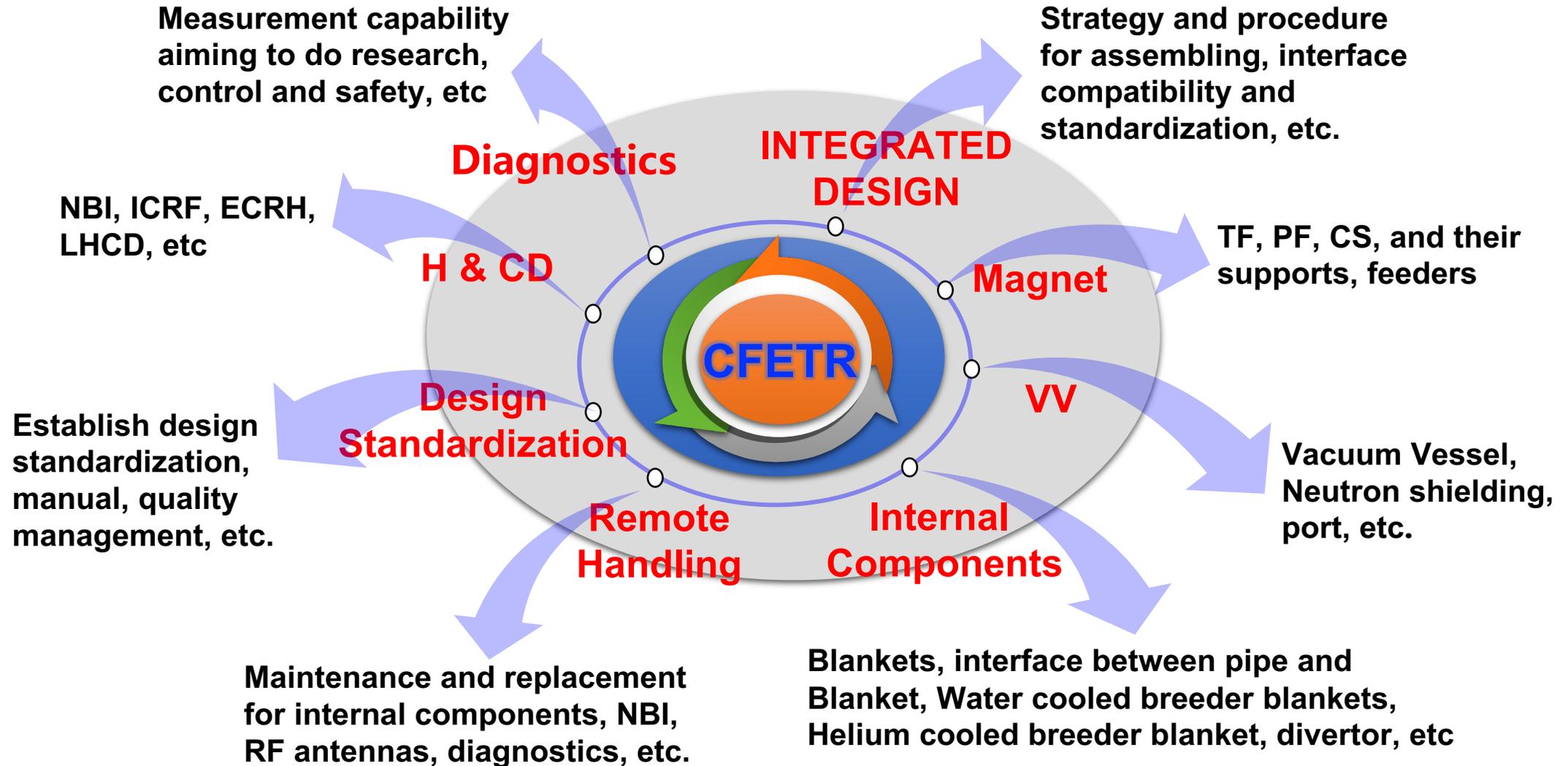


Outline

- **Introduction**
 - New version of CFETR design
- **CFETR Physics Design**
 - Development of operation scenarios
 - Consideration of divertor conf. & impurity effects
 - Investigation of MHD stability
- **CFETR Engineering Design**
 - Magnet system
 - Vacuum system
 - Remote handling and maintenance system
 - Others...
- **Summary**



CFETR Engineering Design

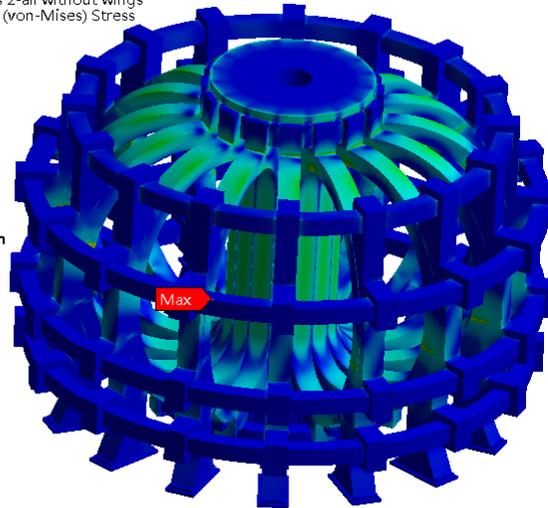


Magnet System (Toroidal Field Coils)

- Design completed
- EM & Stress analysis done

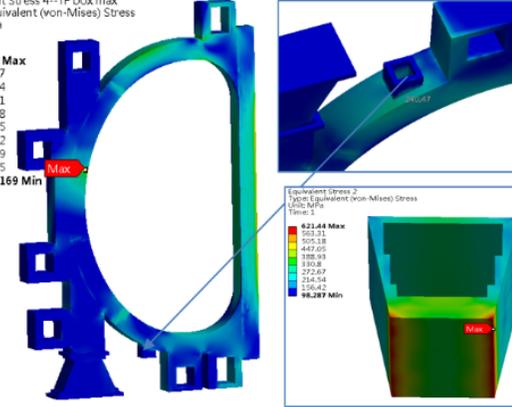
Equivalent Stress 2-all without wings
Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1

736.5 Max
654.67
572.84
491.01
409.18
327.35
245.52
163.69
81.865
0.033043 Min



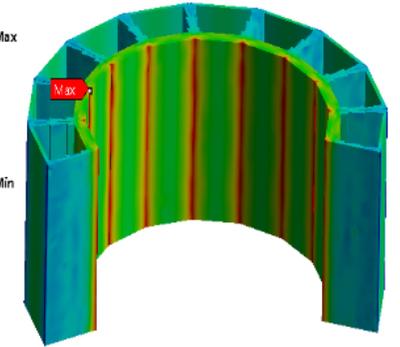
Equivalent Stress 4-TF box max
Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1

736.5 Max
654.67
572.84
491.01
409.18
327.35
245.52
163.69
81.865
0.033043 Min



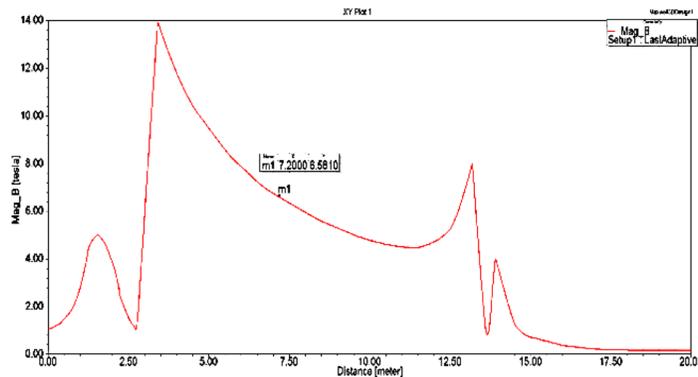
Equivalent Stress 5-TF box center
Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1

628.25 Max
568.54
509.03
449.42
389.8
330.19
270.58
210.97
151.35
91.741 Min



Max Force @TF coil ~736 Mpa; Max. Deformation ~ 16.5 mm

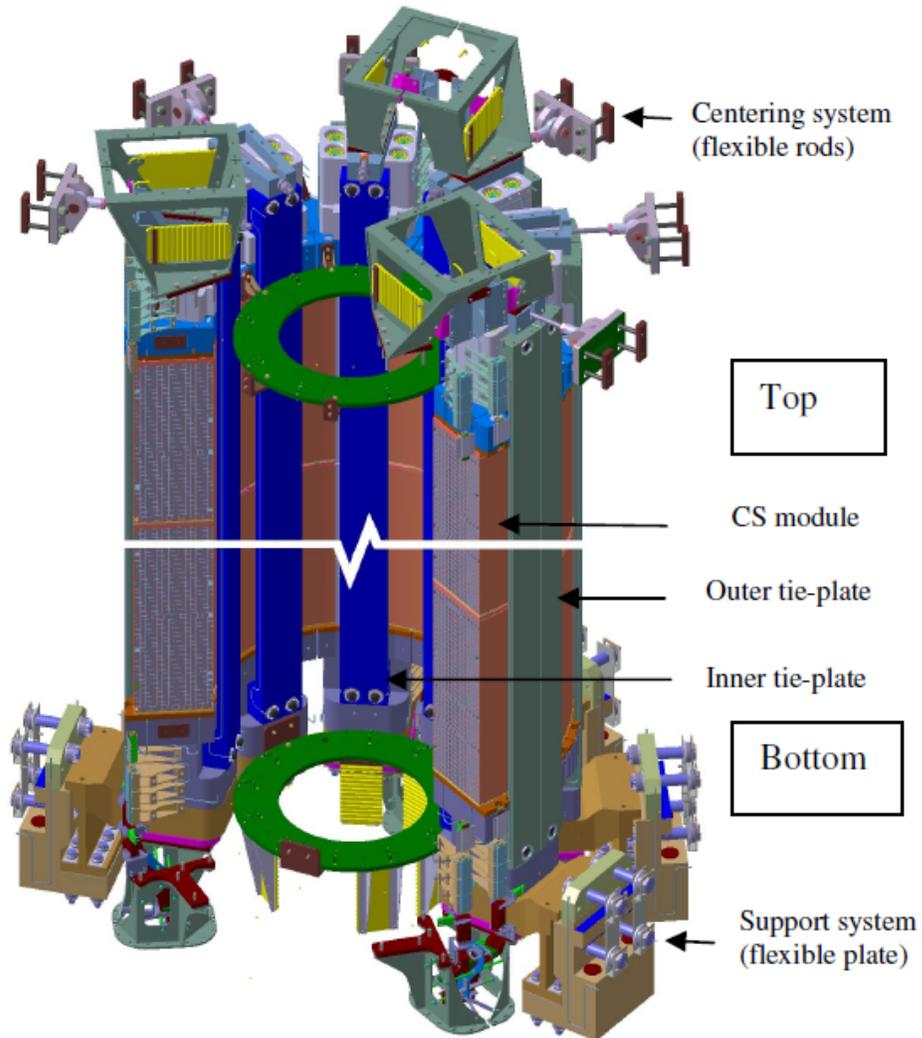
6.5 T @ R = 7.2 m; 174 Turns; 84.6 kA/Turn



	ITER TF	EU-DEMO ^[2015]	CFETR TF
No. of Coil	18	18	16
Current per Turn	68 kA	81.7 kA	84.6 kA
Total inductance	17.34 H	32.68 H	32.5 H
Total Storage Energy	40.1 GJ	109.08 GJ	116.34 GJ
Storage Energy per Coil	2.227 GJ	6.06 GJ	7.27 GJ



Magnet System (Central Solenoid)

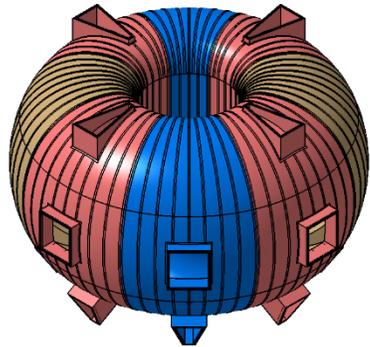


Perspective view of the CFETR CS

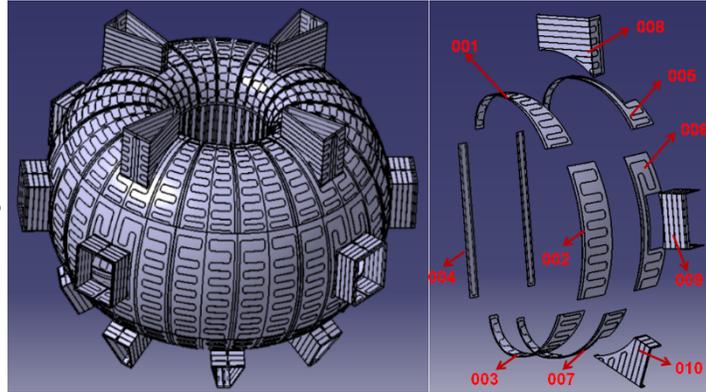
- High temperature superconductor (Bi2212) + low temperature superconductor (Nb₃Sn) → a maximum 19.9 T@ 51.25 kA/turn.
- Each module has 720 turns, powered independently
- Maximum 400 VS flux with a maximum rate of field swing of ~1.2 Ts.

Vacuum system

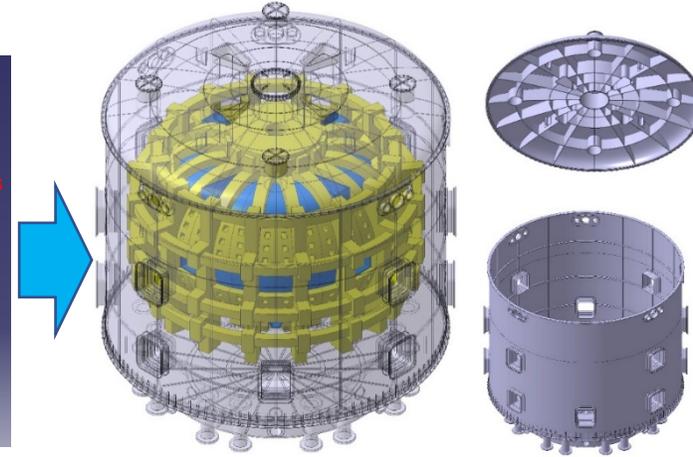
Vacuum Vessel+Thermal Shield+Dewar



H ~ 15 m , W ~ 9.1 m , Thickness ~ 50 mm , 8 Sectors, 4/6/8 ports



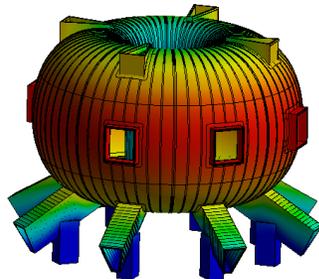
H ~ 15 m, W ~ 9.4 m, Thermal Shield ~ 40mm



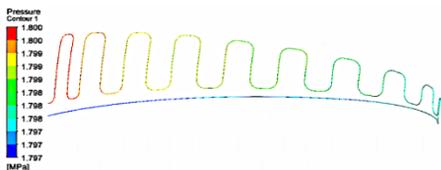
H ~ 29 m, D ~ 38 m , Background Pressure ~ 1×10^{-4} Pa

A: Modal
Total Deformation
Type: Total Deformation
Frequency: 7.1234 Hz
Unit: m

0.0010516 Max
0.00093479
0.00081794
0.00070109
0.00059424
0.00046739
0.00035054
0.0002337
0.00011685
0 Min

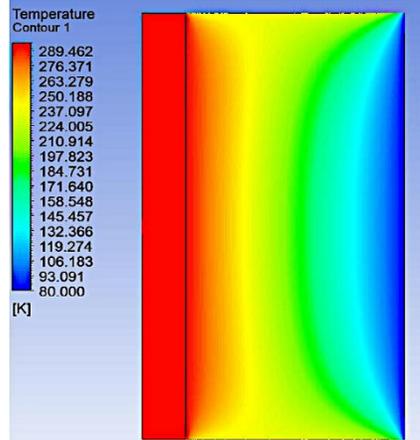


Pressure Contour 1
1.800
1.799
1.799
1.799
1.798
1.797
1.797
-1.797
[MPa]



pressure drop @ cooling pipe

Temperature Contour 1
289.462
276.371
263.279
250.188
237.097
224.005
210.914
197.823
184.731
171.640
158.548
145.457
132.366
119.274
106.183
93.091
80.000
[K]



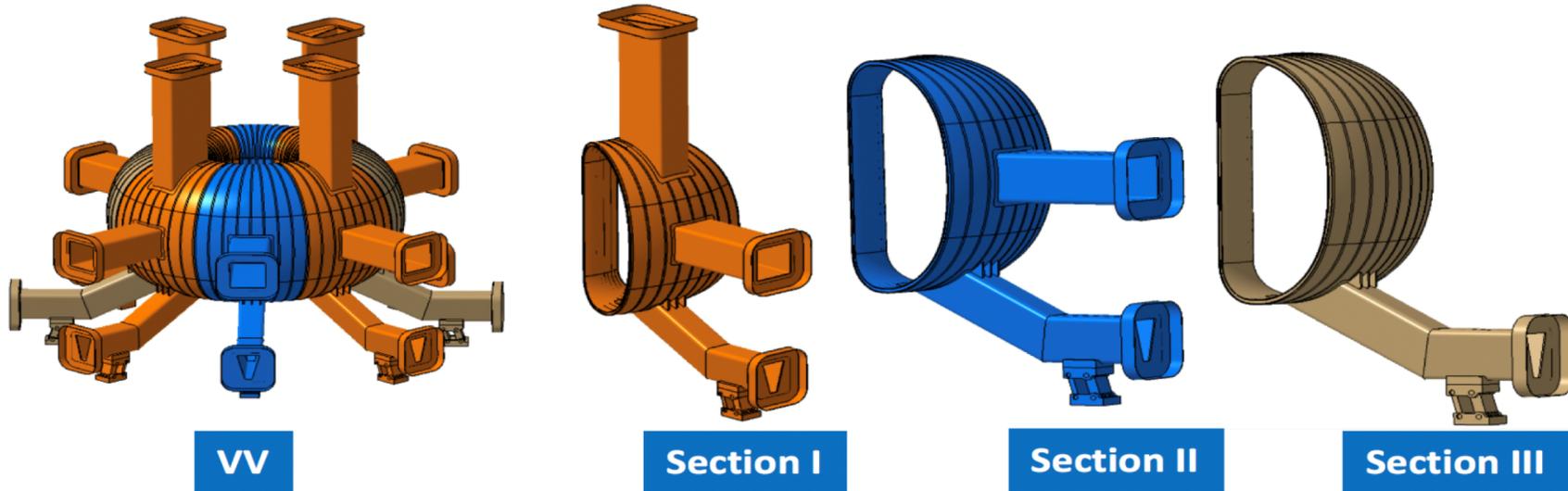
Air Dewar VV Therm. Shd

- Design completed
- Analysis on gravity load
- Analysis on freq. and mode of Vibration
- Analysis on Seismic load



Vacuum system

- Torus with D-shaped cross-section, 4 upper vertical ports, 8 lower ports and 6 equatorial ports
 - 4 upper ports → maintenance and disassembly of blanket.
 - 6 lower ports → divertor maintenance and the cryo-pumps.
 - 8 equatorial ports → NBI, diagnostic and some RH tools.
- Inner, outer shells and stiffening ribs joined by welding.
- Material of the VV is 316L(N)-IG.

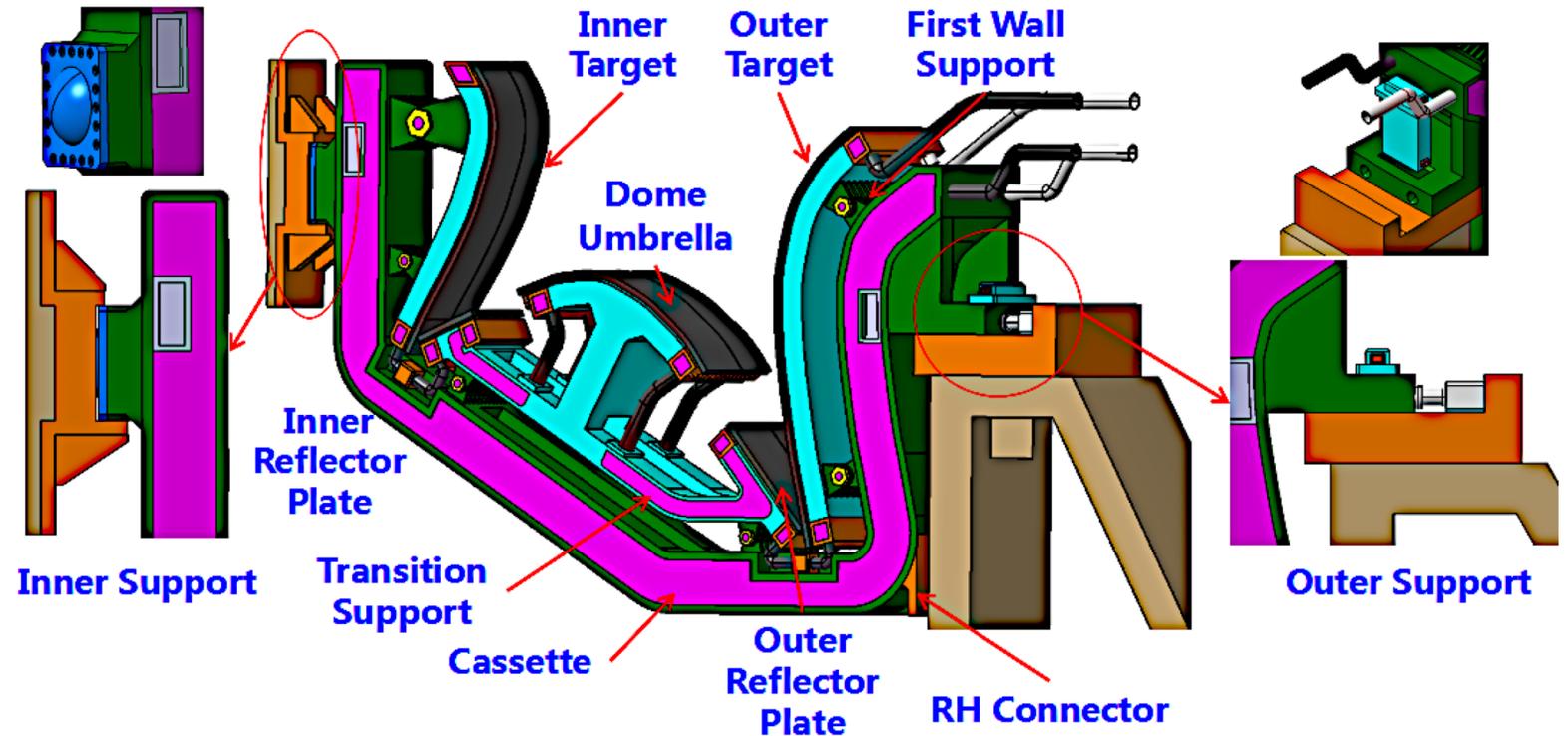


3D model Vacuum Vessel for CFETR

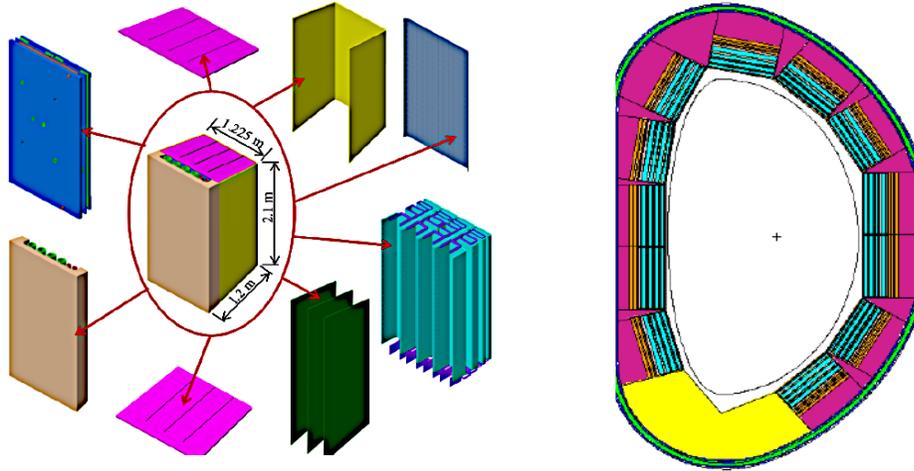
Divertor Structure

- Divertor targets divided into two halves on each module, totally 72 divertor modules, each one ~11 tons. RH from lower port
- Cooling water → outer target → inner target → baffles
- Cassette cooled separately → targets/baffles RH separately from Upper ports by Multi-Purpose Deployer

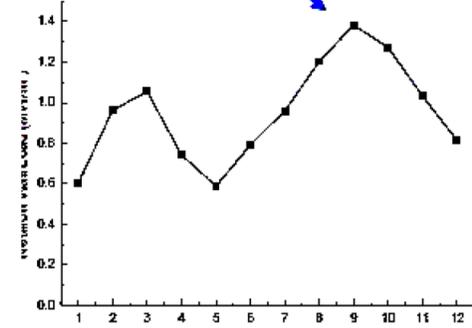
Conceptual engineering design of the CFETR divertor structure.



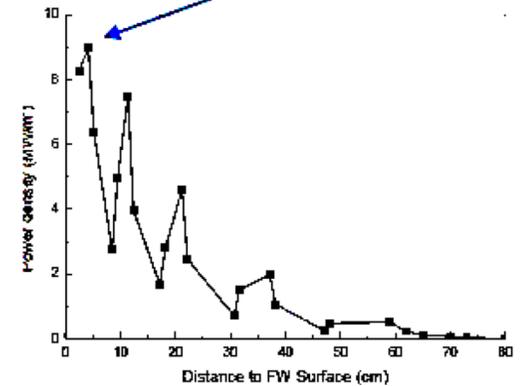
Progress on the Blanket Design



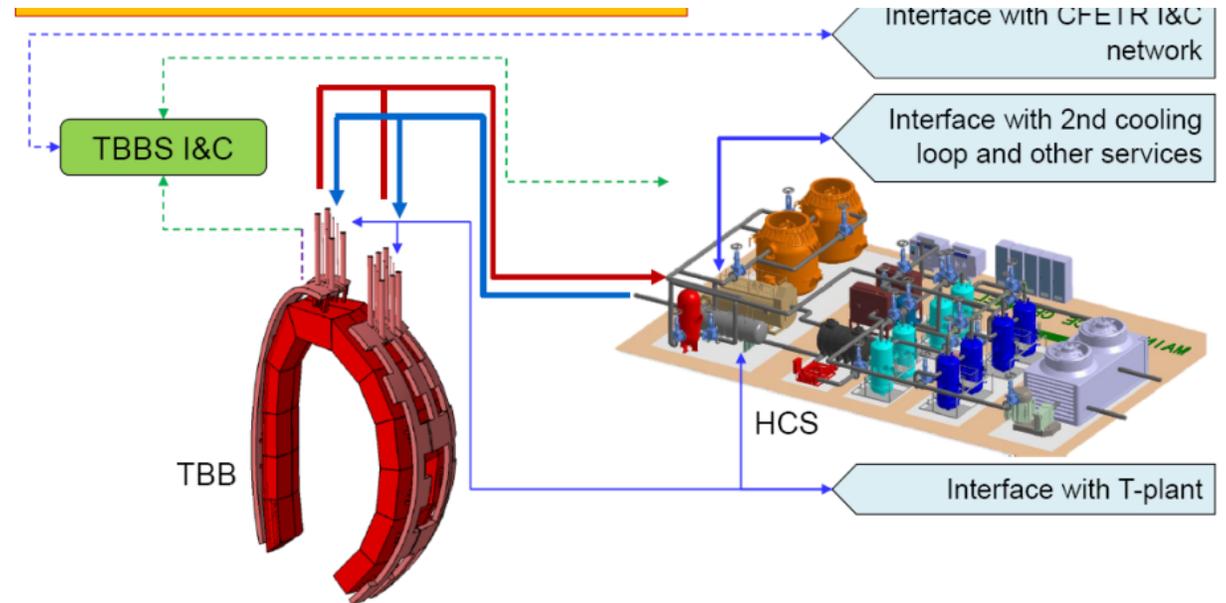
neutron wall load: 1.38 MW/m²



Peak power density: 9 MW/m³



- Helium cooled ceramic breeder blanket (HCCB) design completed
- Evaluate neutron energy deposition and wall load @ Fusion power = 1 GW, 2 GW
- Start the water cooled ceramic breeder (WCCB) design

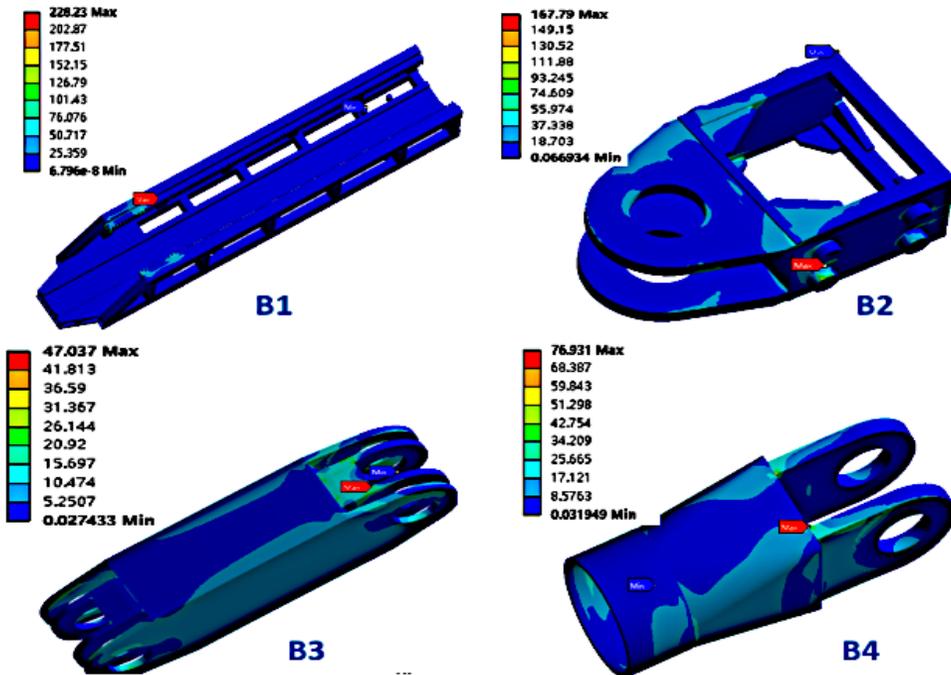


Remote Handling & Maintenance

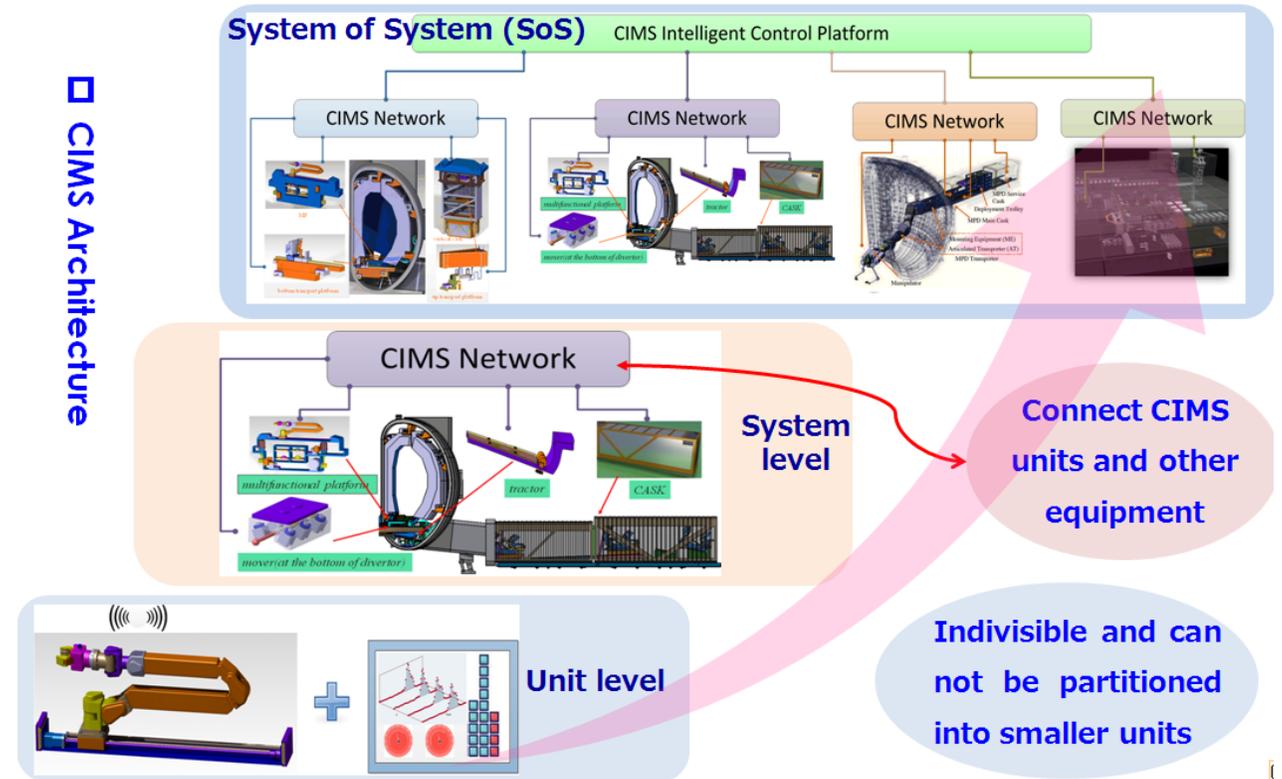
- **Blanket RHM:** Inboard & outboard blankets → from upper ports by a corridor with a crane → hot cell.
- **Divertor RHM:** circular movement → lower horizontal port → cask → hot cell.
- **MPD :** equatorial port → maintenance of small pieces, inspection, diagnosis.



Mechanical load on Manipulator joints



CIMS Architecture



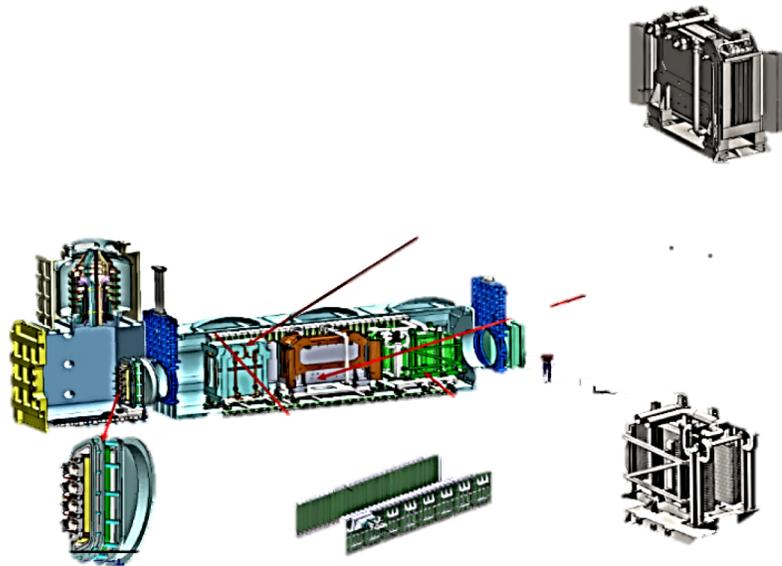
- Mechanical analysis on RHM of internal components;
- Establish overall control architecture, hardware and software control integration architecture @ Heterogeneous control architecture theory.



Design and R&D for H&CD Systems

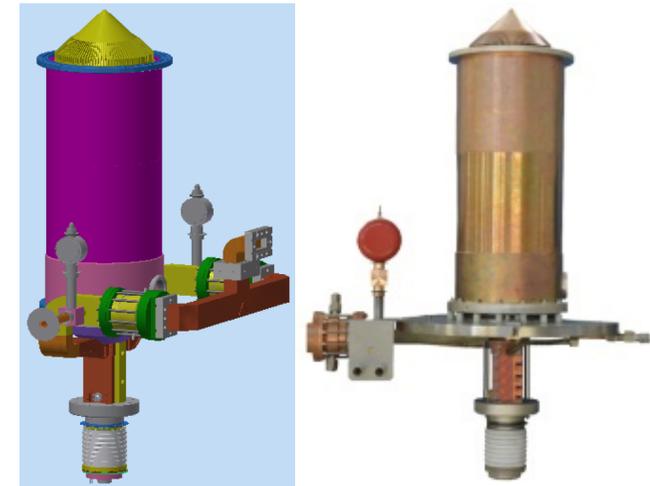
NBI

- Based on ITER NBI design, complete preliminary design of N-NBI System, R&D of key technologies of CFETR N-NBI
- Promote research of RF source, high RF power, long pulse ion source
- Achieve substantive results on isolation transformer for RF power transmission



LHW

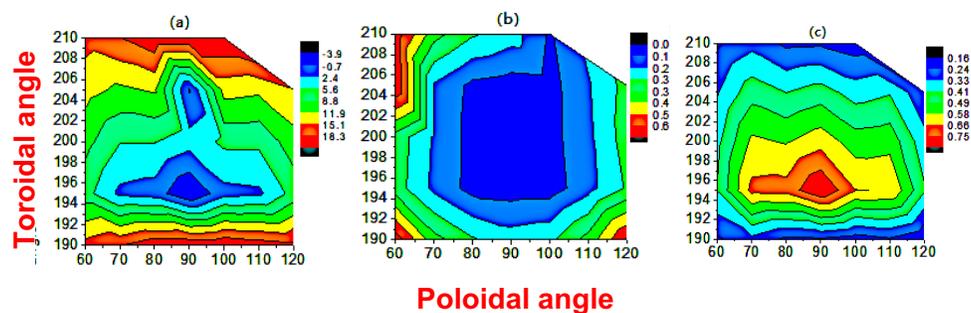
- Complete preliminary design of low power microwave power source driving circuit, control scheme of power and phase, and Investigate high-power klystron, and auxiliary power equipment
- Carry out high-field coupling and high-field antenna simulation study, R & D of key components of the transmission line



4.6GHz 500kW/CW Klystron model and structure

ECW

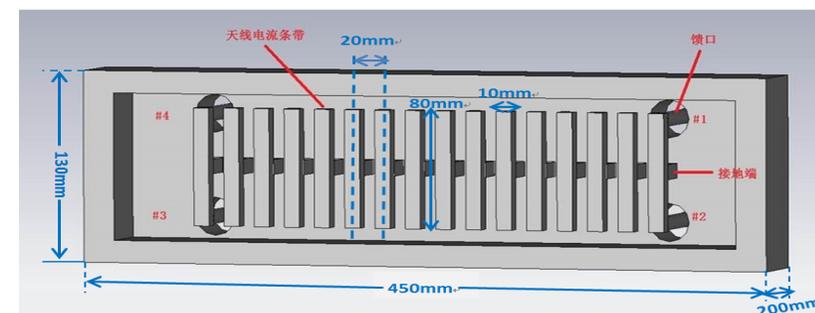
- Complete the ECRH system design, R&D of key technologies for Gyrotron
- Start the effectiveness analysis and performance evaluation of ECCD under various conditions (beam injection position, antennas incident parameter, different gyrotron freqs 170GHz, 230GHz)



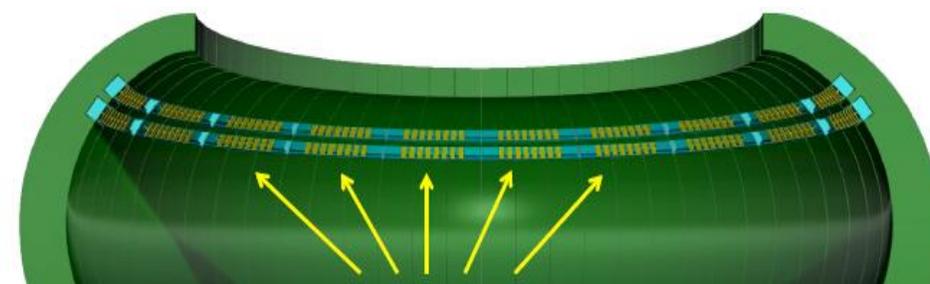
Performance of 230GHz ECCD ($Z_a = 0$ m)
 (a) ECCD (kA/MW) ; (b) Peak location of J_{CD} ; (c) 2nd Harmonic absorp. ratio (%)

Helicon Wave

- Start design and analysis antenna of travelling wave



Helicon waves traveling wave antenna module



Traveling wave antenna modules arranged in the blankets, satisfying high power requirements



Outline

- **Introduction**
 - New version of CFETR design
- **CFETR Physics Design**
 - Development of operation scenarios
 - Consideration of divertor conf. & impurity effects
 - Investigation of MHD stability
- **CFETR Engineering Design**
 - Magnet system
 - Vacuum system
 - Remote handling and maintenance system
 - Others...
- **Summary**



Summary

- **New design with $R = 7.2 \text{ m}$ / $a = 2.2 \text{ m}$ & high B_T .**
- **Detailed designs of physics and engineering are under the way.**
 - **Progress of physics design**
 - Fully non-inductive and hybrid mode scenarios with performance that meets the CFETR mission have been developed
 - Broad operation range in β_N and β_p , stable with wall at $r/a = 1.2$
 - Helium dilution f_{He} cannot exceeds 0.2 to meet P_{fus} target
 - Radiation in the core acceptable up to $Z_{\text{eff}} \sim 3$
 - Tungsten fraction at the edge can't exceed $4e-5$ to stay in H-mode
 - **Progress of engineering design**
 - Concept design of key systems completed, detailed engineering design of the systems ongoing.
- **CFETR will be fully open to our cooperators, your input in very valuable for the success of the project.**



Acknowledgements

We are grateful to General Atomics, PPPL, LLNL, Wisconsin, U. York, MPG-IPP and U. Toronto for the use of their physics code suites and data, and their helps



Thank you for your attention !