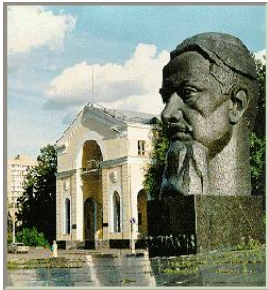




IAEA FEC 2016
26th IAEA Fusion Energy Conference

26th IAEA Fusion Energy Conference
Kyoto, Japan
17-22 October 2016

FNS/1-1



NATIONAL RESEARCH CENTER
KURCHATOV INSTITUTE



НАЦИОНАЛЬНЫЙ ИССЛЕДОВАТЕЛЬСКИЙ
ЦЕНТР «КУРЧАТОВСКИЙ ИНСТИТУТ»

STATUS OF DEMO-FNS DEVELOPMENT

B.V. Kuteev, Yu.S. Shpanskiy and DEMO-FNS Team

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STATUS OF DEMO-FNS DEVELOPMENT

DEMO-FNS Team

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Outline

- **Introduction**
- Three-dimensional modeling of neutron flux in DEMO-FNS
- First wall material damage
- Scenario for new DEMO-FNS configuration
- Passive MHD stabilization
- Upgrade of enabling systems
 - Superconducting magnet system
 - Vacuum vessel
 - Divertor cassettes
 - Blanket
 - Tritium fuel cycle
- **Conclusions**

Introduction

MISSION of DEMO-FNS:

- **Fusion-fission hybrid facility based on superconducting tokamak DEMO-FNS is developed in Russia for integrated commissioning steady-state and nuclear fusion technologies at the power level up to 40 MW for fusion and 400 MW for fission.**
- **Facility is considered in RF as the main source of technological and nuclear science information that complement the ITER research results in the fields of burning plasma physics and control.**

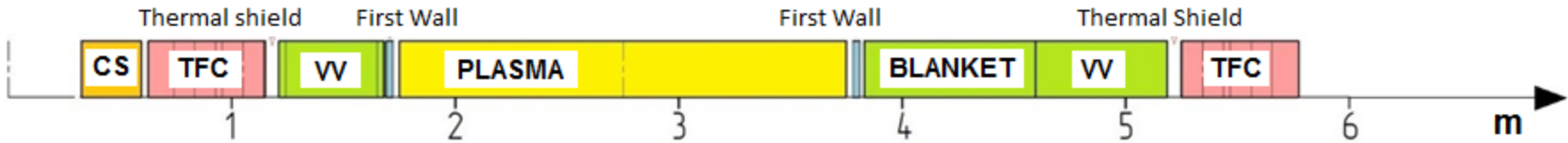
Design challenges for Q~1 tokamak in hybrid system

- **SSO**
- **Neutron environment (heating, insulation, testing, etc.)**
- **Remote handling**
- **Integration (tokamak – hybrid blanket; blanket & nuclear fuel cycle)**
- **Economics & Legislation**

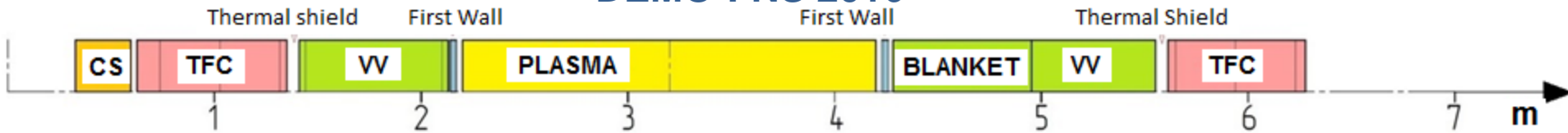
Changes of DEMO-FNS 2016 vs 2015

Development of Design
NF 55 2015 (073035)

DEMO-FNS 2015

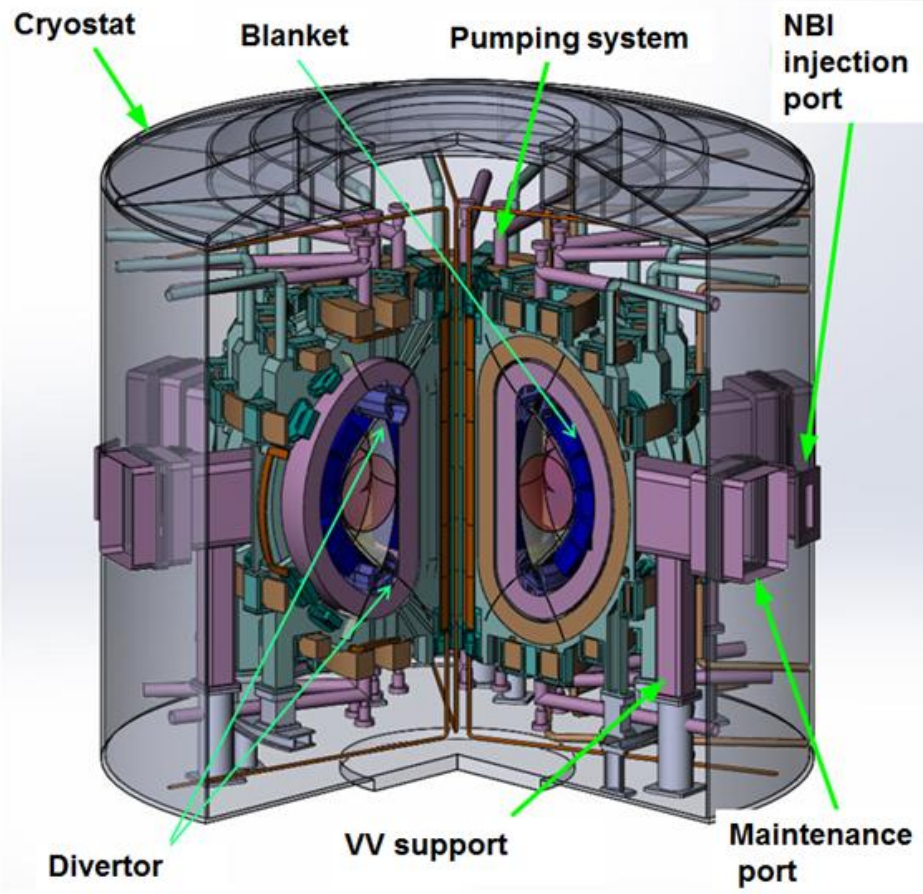


DEMO-FNS 2016



Parameters	2015	2016
Nuclear heating limit, mW/cm^3	1	0,05
Current density $\langle j_{TFi} \rangle$, MA/m^2	24	18
Toroidal coils width, m	0.525	0.725
Shielding thickness, m	0.470	0.720
Major radius R , m	2.75	3.2
Plasma elongation, k_x/k_{95}	2.1/2.0	2.0/1.9
Toroidal field max B_c , T	12	12
Magnetic Ripples d_{ripple} , %	0.15	0.28

Tokamak and plasma parameters



Major radius,	m	3.2
Minor radius,	m	1.0
Toroidal field,	T	5.0
Plasma current,	MA	5
NBI power,	MW	30
ECRH power,	MW	6
Electron/ion temperature,	keV	11.5/10.7
β_N		2.1
β_p		0.96
Neutron yield,	n/s	$>10^{19}$
Consumed/generated electric power,	MW	up to 200
Discharge time,	h	up to 5000
Capacity factor		0.3
Life time,	years	30

Cutaway view of DEMO- FNS tokamak

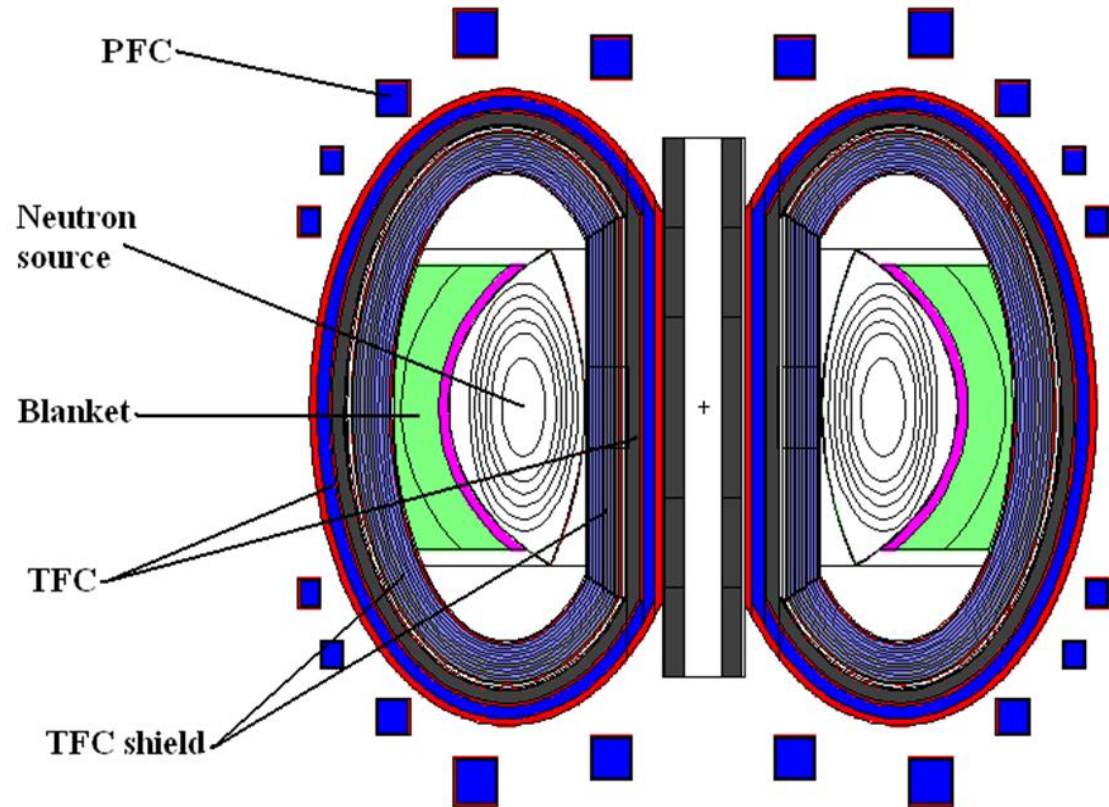
Three-dimensional modeling of neutron flux

Materials of concern

- Superconductors
- Insulation
- Structural materials
- Plasma facing components

Zones of concern

- Central pole
- Ports for NBI

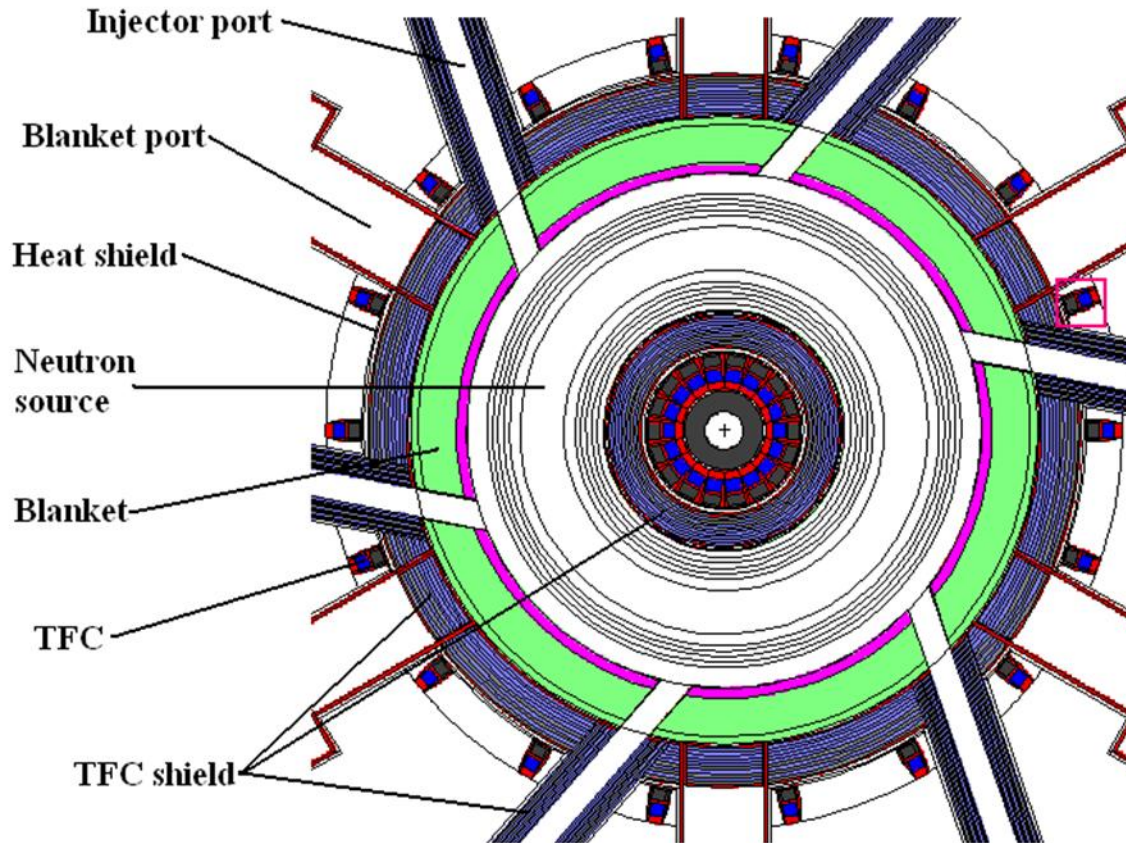


A.V. Zhirkin et al.
FEC-26 FNS/P5-11

Vertical cross-section of DEMO-FNS neutronics model

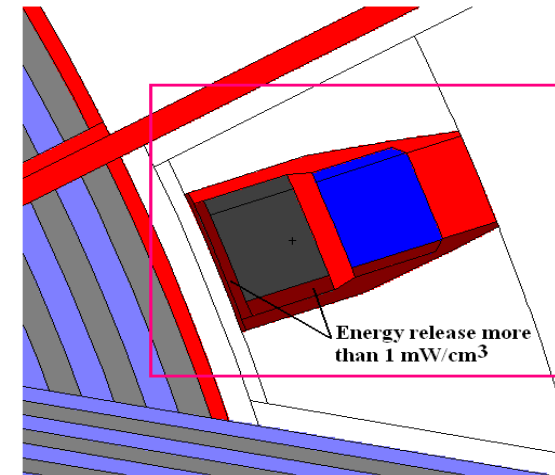
Requirements on calculation accuracy and benchmark experiment precision were addressed

Three-dimensional modeling of neutron flux



Horizontal cross-section of DEMO-FNS model

Zone with highest heat flux



•WC has high shielding effect

•SS/H₂O shielding is chosen as simplest and cheapest option

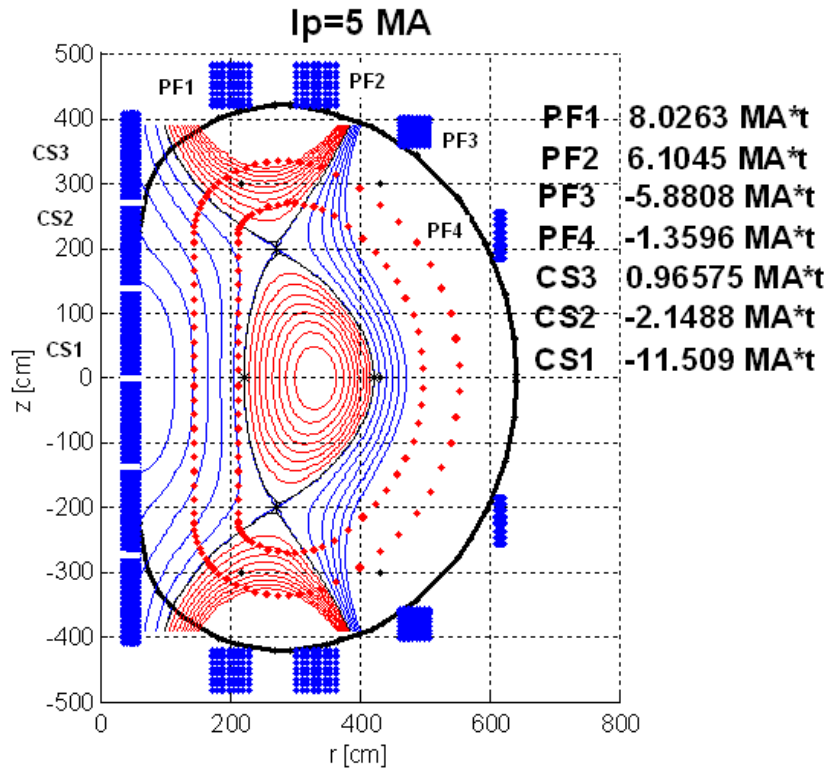
First wall material damage

- Neutronic performance and inventory analyses were carried out
- The D-T-neutron wall loading for DEMO-FNS is $\sim 0.2 \text{ MW/m}^2$

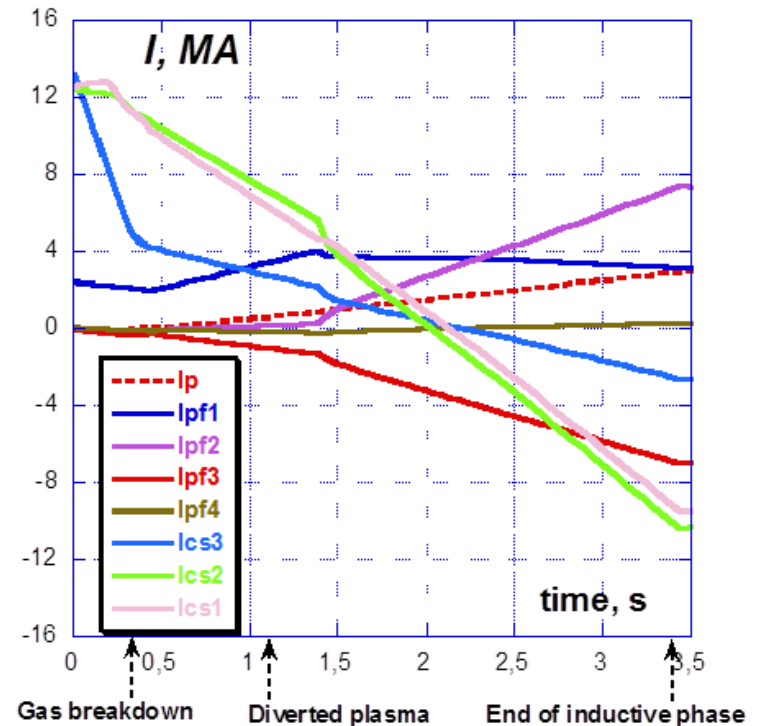
FW component	Material	dpa per fpy	He, appm per fpy	T, appm per fpy	H, appm per fpy	Heat, W/cm ³
PFC (armour)	CFC	3.2	230	0.03	0.2	4.1
	Be	2.6	670	28	29	4.9
	W	0.90	~40	0.005	~900	~100
Heat sink	CuCrZr	3.2	22	0.2	150	25
Coolant	H₂O	0	25	~0.001	-20	5.7
Structure	SS	3.1	130	0.05	140	20
	Eurofer	3.0	130	0.02	90	22
	EK-164	3.2	160	~0.01	~160	21
	V-4Cr-4Ti	3.8	12	0.01	550	~20

❑ FW radiation damage for Hybrid System with $k_{\text{eff}} 0.95$ is ~ 2 times higher than that for pure fusion system under the same 14 MeV neutron FW loading

Magnetic configuration and scenarios for new DEMO-FNS design



➤ Discharge scenarios were simulated using DINA code



The magnetic configuration was optimized for new design requirements to minimize currents in poloidal field coils

- Unique feature – X-points are far from PFC
 → much higher currents needed (like in ITER)

Evolution of currents at ramp-up stage

The current ramp-up scenario in DEMO-FNS

Time, s	0.1	3	300 (DD)	1000 (DT)
I _{pl} , MA	0.1	3	4.25	5.05
R, m	2.45	3.2	3.2	3.2
a, m	0.25	1	1	1
k	1	2	2	2
δ	0	0.5	0.5	0.5
β _{pol}	2.6	0.31	1	0.88
li	0.82	0.72	0.7	0.8
Ψ _{res} , V*s	0	-1.43	-0.23	0.77
Ψ _{tot} , V*s	8	0.1	0.12	0.12
ECRH, MW	1	3.5	6	6
NBI, MW	0	0	30	30
P _α , MW				12
<n>, 10 ¹⁹ m ⁻³	2.5	8	8	8
H-factor	1	1	1.3	1.3
Neutrons, s ⁻¹	-	-	3x10 ¹⁷ (DD)	2.3x10 ¹⁹ (DT)

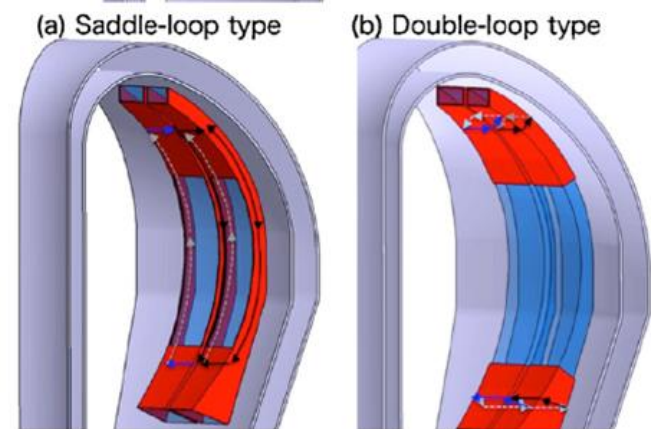
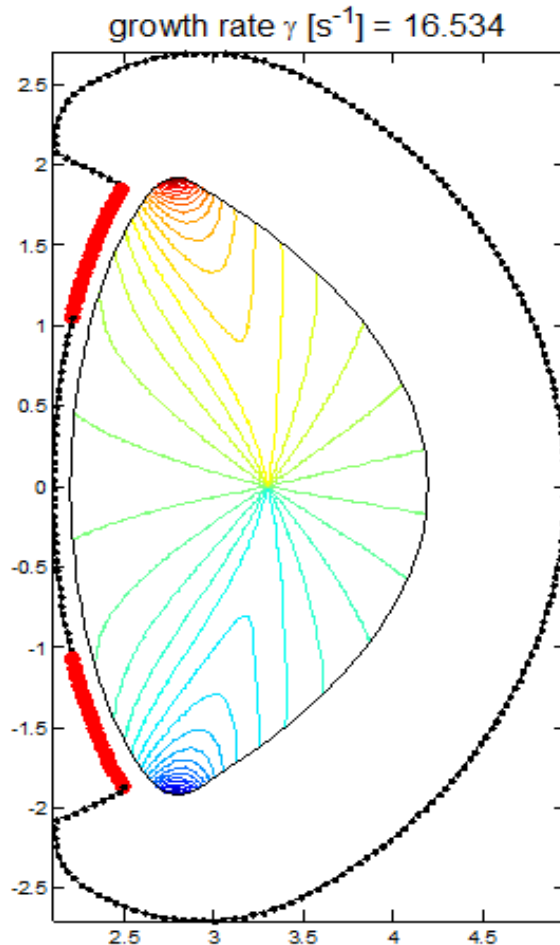
ASTRA
code

Scenario stages:

- Breakdown period with current 0.1 MA during 0.1 s.
- Inductive current ramp-up to 3 MA in 3 seconds by a solenoid.
- A further current rise due to the generation of current on the beam, and the bootstrap current.

Passive MHD stabilization

- needed for vertical stability and control during current rump-up and SSO



Hiroyasu Utoh et al. Fusion Engineering and Design 103 (2016) 93–97

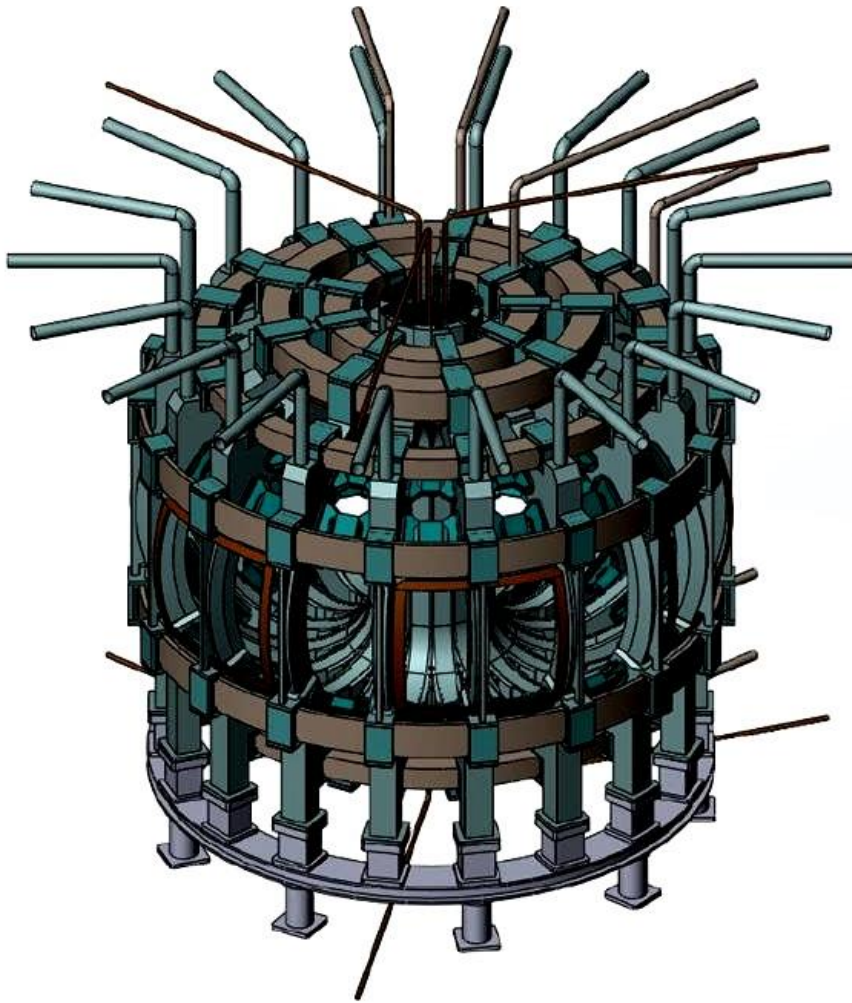
← Sadakov (1992)

KINX level lines of the normal plasma displacement for $n=0$ vertical instability with the growth rate $\gamma=17 s^{-1}$.

Plasma controllable

Wall parts marked red assumed 10 times higher conducting than chamber walls (e.g. 0.75 cm of copper vs 3 cm steel)

Electromagnetic system of DEMO-FNS



General view of EMS

Superconducting electromagnetic system (EMS) of DEMO-FNS

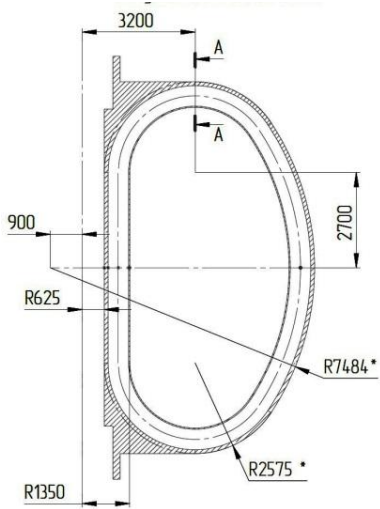
includes:

- Toroidal field coils (TFC) -18 units
- Central solenoid (CS) sectioned
- Poloidal field coils (PFC) 4 pairs
- Correction coils (CC) 3 groups, 18 units
- Vertical control coils – 2 units
- HTS current leads

materials:

**Nb₃Sn, NbTi, HTS,
SS, Cu-alloys
Polyimide insulator
He-coolant**

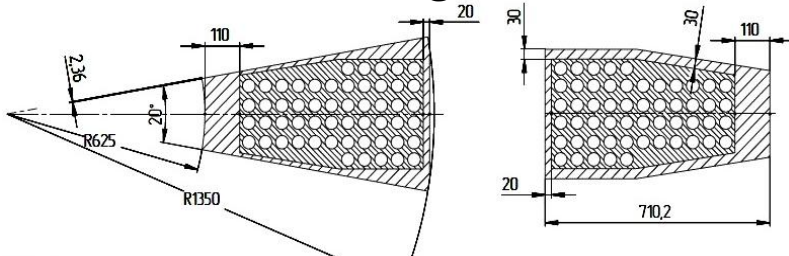
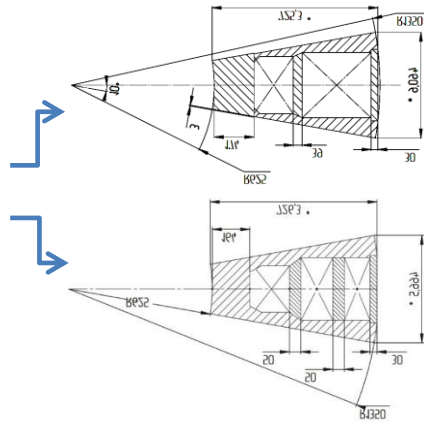
Toroidal field coils



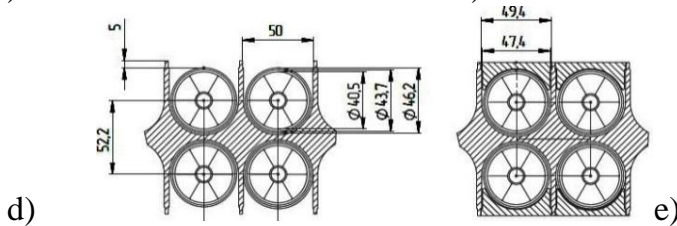
a)

Coil unit of TFC in casing

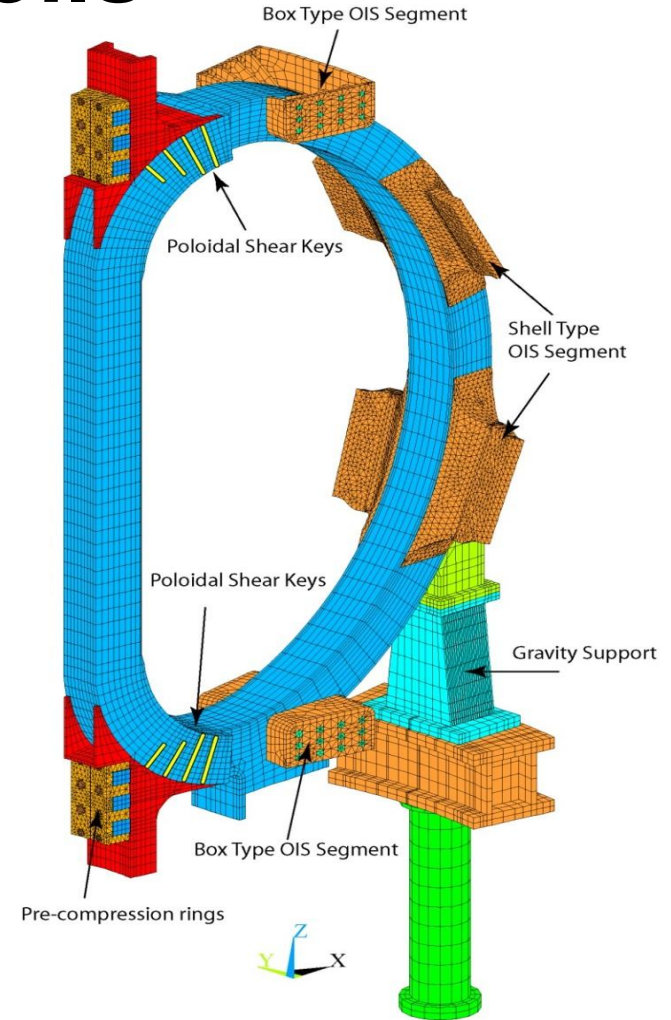
Options



cross-sections: inner and outer



conductors in radial plate



ITER like design was chosen after multi-option analysis

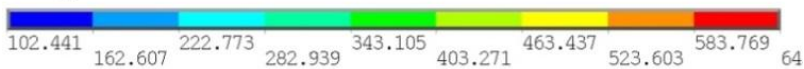
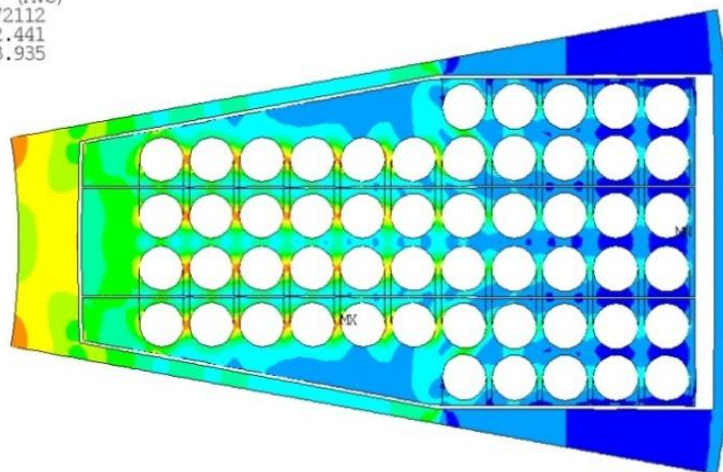
Toroidal field coils

Results of stress analyses

NODAL SOLUTION

STEP=2
SUB =1
TIME=2
SINT (AVG)
DMX =1.72112
SMN =102.441
SMX =643.935

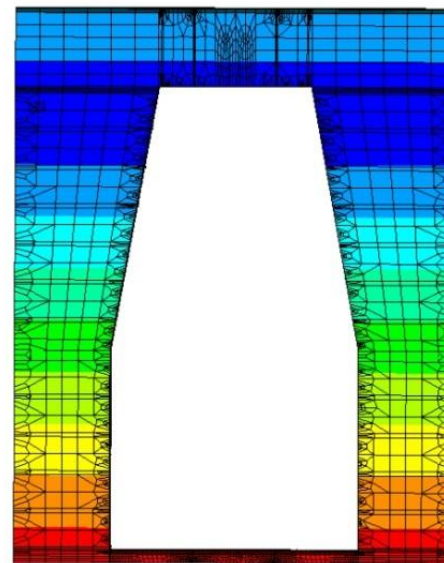
PLOT NO.



NODAL SOLUTION

STEP=1
SUB =1
TIME=1
SINT (AVG)
DMX =1.18607
SMN =.062738
SMX =327.293

PLOT NO.



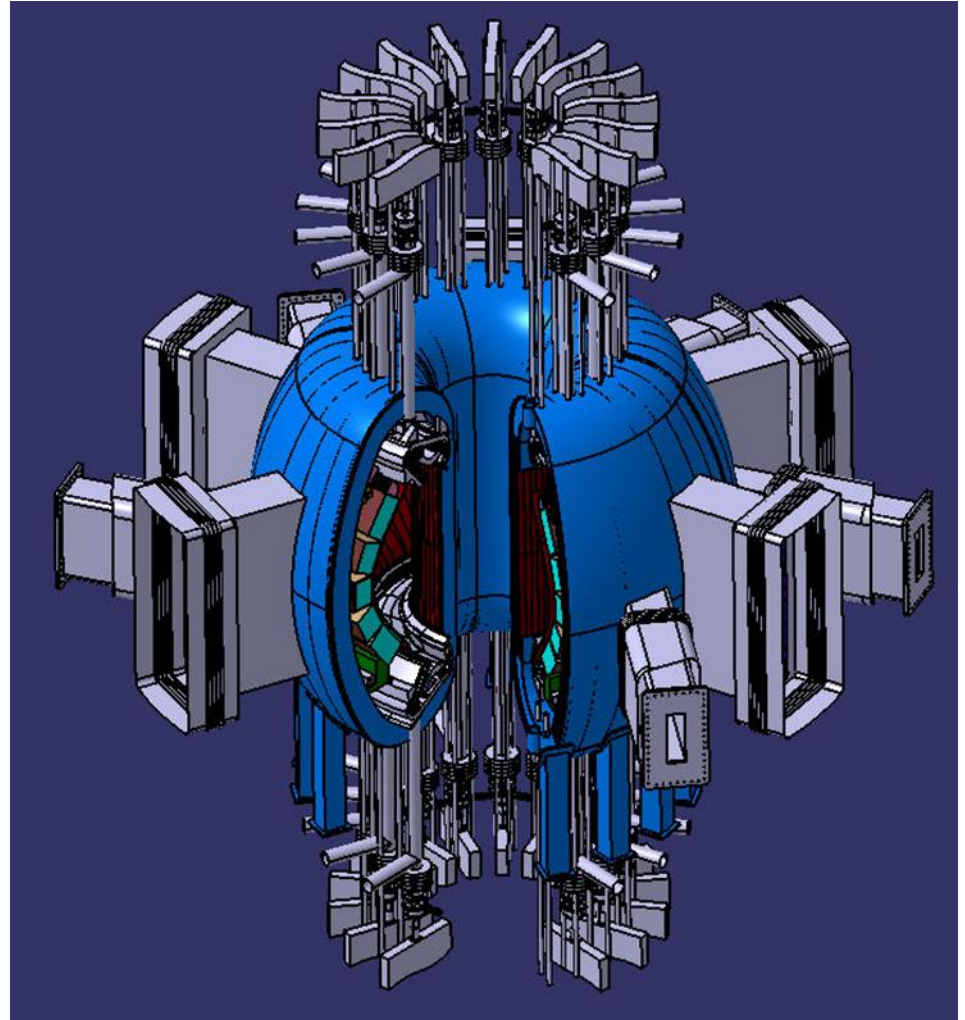
The design meets the criteria for static strength

Vacuum vessel

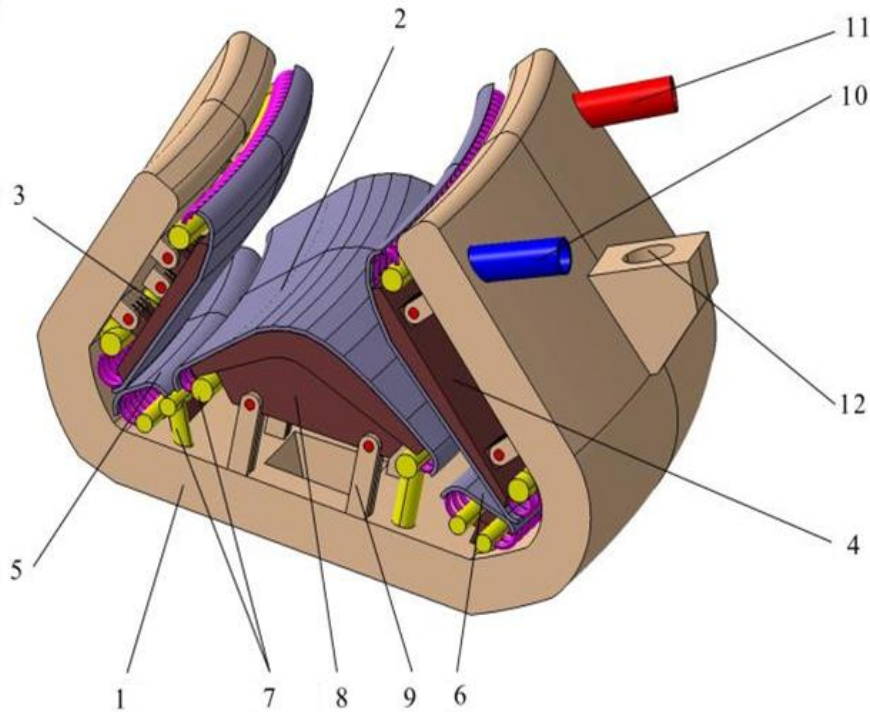
Composition of Vacuum vessel:

- 6 sectors
- Body with shielding
- Maintenance and injection ports
- Pumping ports
- VV supports
- Bearing units for in-vessel components
- Feedthroughs of the VV water cooling system and in-vessel components

- | | |
|---|----------------------|
| ➤ Material | - SS 316L |
| ➤ 2 MWa/m² – n-damage | <20 dpa |
| ➤ VV height | - 6.8 m |
| ➤ Outer diameter | - 11.1 m |
| ➤ Inner diameter | - 2.82 m |
| ➤ Inner surface of VV body | - 286 m ² |
| ➤ VV Volume | - 270 m ³ |
| ➤ Weight of the VV body | - 630 ton |
| ➤ VV temperature | - 200 °C |



Upgrade of divertor cassettes



- 1 - cassette case,
- 2 - heat removal panel,
- 3 - internal panel
- 4 - external panel
- 5 - internal reflector,
- 6 - external reflector
- 7 - collectors,
- 8 - Dome,
- 9 - supporting device with hinge
- 10 - standpipe with coolant,
- 11 - drain pipe with a coolant,
- 12 - gripper arm

Divertor is double null and consists of 36 independent cassettes
Trend – “closed configuration”

In new device configuration distance from the poloidal magnetic field coils to divertor X-point sufficiently increased (above 45 cm), which required upgrading the divertor cassette

Reduction of the outer leg length more than 2 times, from 1.3 m to 0.6 m

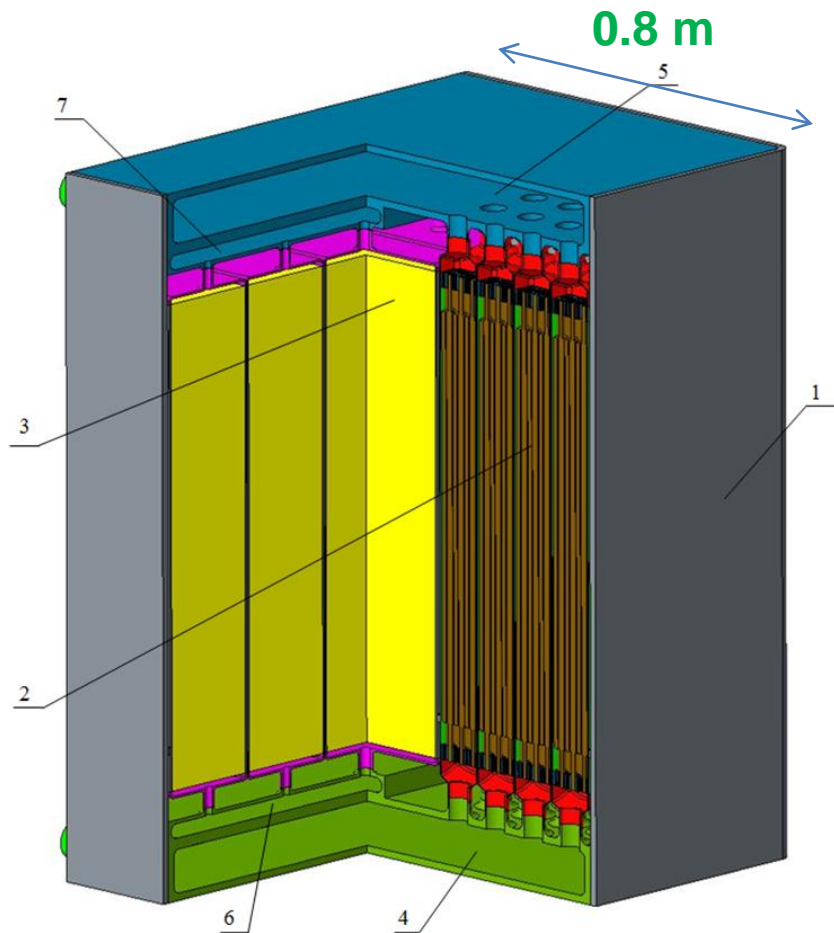
Size of the area for placing the divertor cassettes was dropped by 2 times

→ Ability to operate in "detached" mode requires new simulations using the two-dimensional code SOLPS (in progress)

Blanket of DEMO-FNS

Functions: transmutation of minor actinides (MA) and self-sufficient tritium breeding

Coolants: NaK, H₂O, He – choice is steel needed



- 1 - module case;
- 2 - subcritical active core;
- 3 - T-breeding zone (ceramic breeder) Li₄SiO₄;
- 4 - coolant inlet collector;
- 5 - coolant outlet collector;
- 6 - inlet He-gas collector;
- 7 - outlet He-gas collector

Initial composition of the MA mixture (total weight ~ 40 ton)

Nuclide	Mass fraction, %
Np237	44.5
Am241	48.6
Am242m	0.04
Am243	6.1
Cm243	0.02
Cm244	0.74

Tritium fuel cycle of DEMO-FNS

Burning rate ~ 2kg T per year

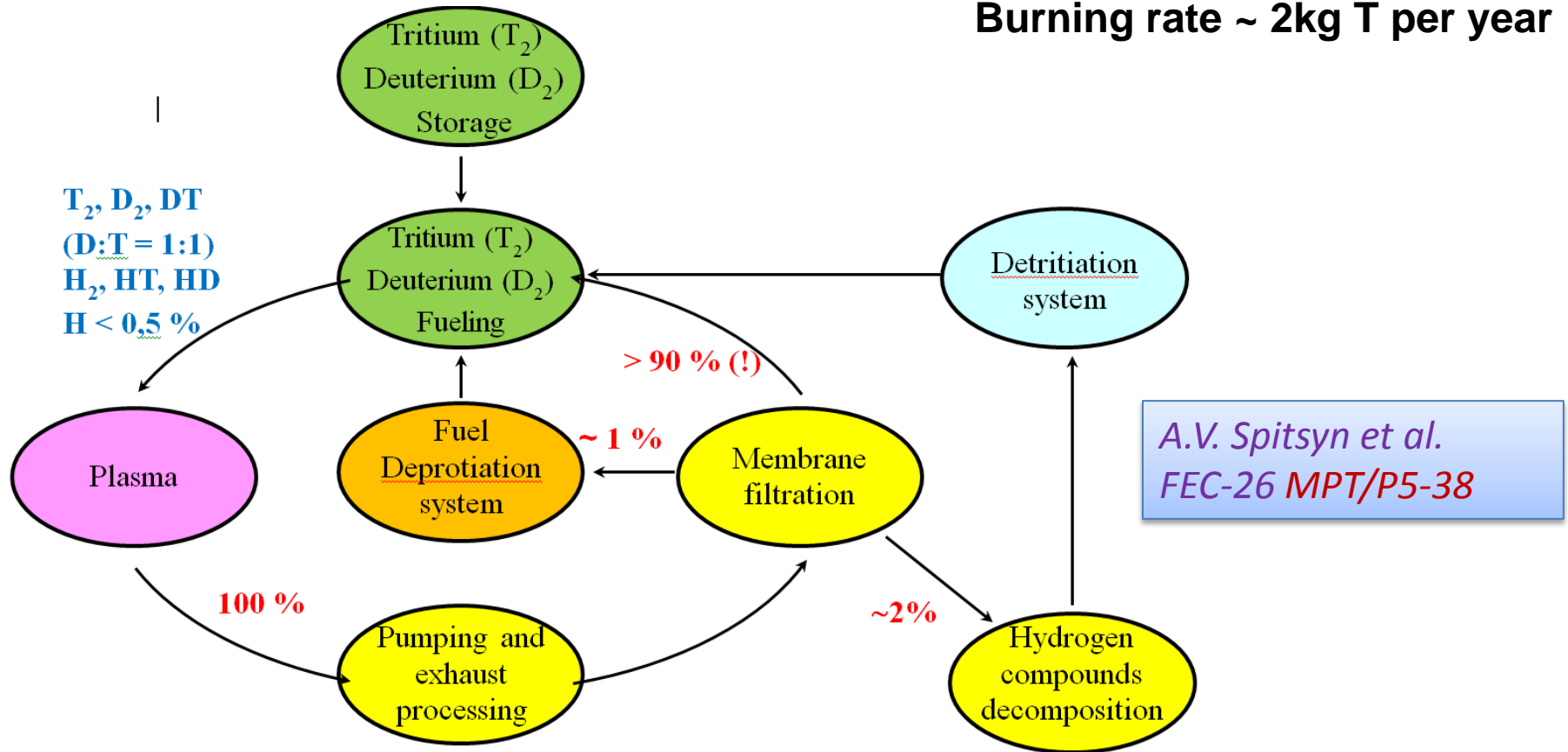


Diagram of Tritium fuel cycle

Tritium fuel cycle of DEMO-FNS

Design assumes:

- No separation of D / T mixture and use of an 50:50% of D and T
- A small fraction of the fuel (<2%) delivered to the hydrogen isotopes separation system, only for deprotection
- Separate deuterium loop (without T) used for a Neutral beam injection system

Tritium storage at the site required for operation of tokamak fueling system:

0.65 kg for D:T = 1:0

better current drive

1.0 kg for D:T = 1:1

excluding tritium in long-term storage systems and tritium retention in the structural and functional materials

Conclusions

- ❑ Safety and operation requirements initiated important changes of DEMO-FNS design in 2016
- ❑ Major radius increased from 2.75 to 3.2 m
- ❑ Enabling systems were upgraded including
 - Vacuum vessel
 - Radiation shield
 - Divertor
 - Blanket
 - Fueling cycle

- ❑ Design activity was supported by R&D in
 - Neutronics
 - Discharge scenario
 - Vertical stability
 - Optimization of the device layout
 - Subsystems including EMS, VV, divertor, blanket and T-fuel cycle

- ❑ Issues of integrating the hybrid facility in the nuclear fuel cycle of Russian nuclear power engineering are currently under consideration

THANK YOU FOR

YOUR

ATTENTION