

FIP/3-4Ra

Two Conceptual Designs of Helical Fusion Reactor FFHR-d1A Based on ITER Technologies and Challenging Ideas

A. Sagara, J. Miyazawa, H. Tamura, T. Tanaka, T. Goto, N. Yanagi, R. Sakamoto,
S. Masuzaki, H. Ohtani, and the FFHR Design Group (NIFS, JAPAN)

FIP/3-4Rb

Development of Remountable Joints and Heat Removable Techniques for High-temperature Superconducting Magnets

H. Hashizume¹, S. Ito¹, N. Yanagi², H. Tamura², A. Sagara² (¹Tohoku Univ., ²NIFS)

FIP/3-4Rc

Lessons Learned from the Eighteen-Year Operation of the LHD Poloidal Coils Made from CIC Conductors

K. Takahata, S. Moriuchi, K. Ooba, S. Takami, A. Iwamoto, T. Mito,
and S. Imagawa (NIFS, JAPAN)



Staged progress in designing FFHR-d1 of FERP in NIFS corroborative activities

Stage of the design

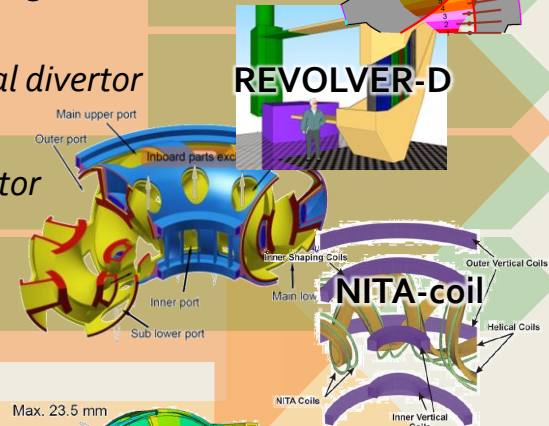
1st round 2nd round 3rd round

Construction and Maintenance

High-Temperature Superconductor
joint winding



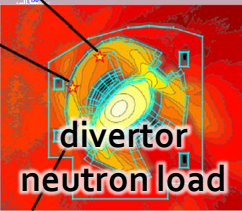
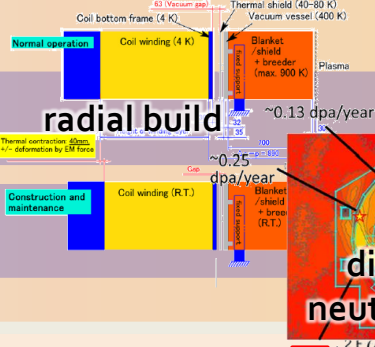
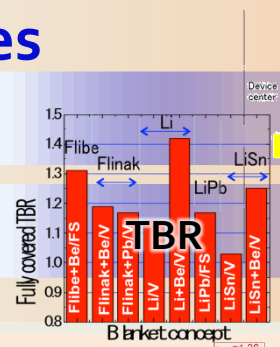
blanket segmentation
liquid metal divertor
novel divertor



All 3D Analyses

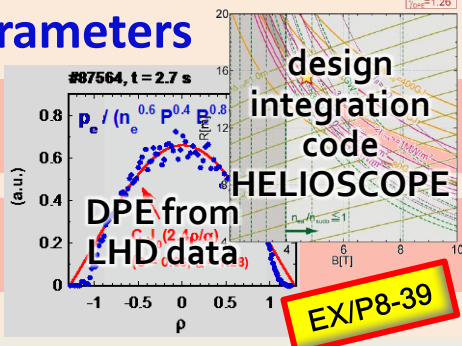
structure

neutronics



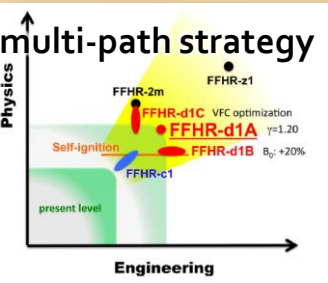
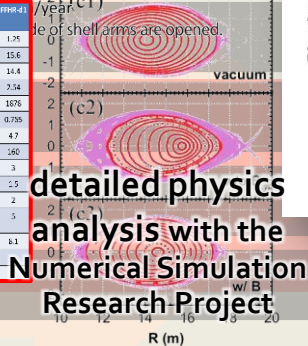
Basic Parameters

design integration
core plasma design



determination of the basic parameters

	LHD	FFHR2	FFHR2L1	FFHR2L2	FFHR-d1
Coil pitch parameter	1.75	1.15	1.15	1.3	1.05
Coil major radius	8.5	10	10	10	10
Plasma major radius	3.75	4.8	4.8	5.0	5.0
Plasma minor radius	1.5	1.5	1.5	1.5	1.5
Plasma volume	30	53	53	53	53
Blanket space	1.5	1.5	1.5	1.5	1.5
Blanket/shield + breeder (RT)	4.84	4.84	4.84	4.84	4.84
Blanket/shield + breeder (max. 900 K)	1.5	1.5	1.5	1.5	1.5
Fuelor source	1.5	1.5	1.5	1.5	1.5
Neutron wall	1.5	1.5	1.5	1.5	1.5
Factor of safety	2.80	1.52	1.52	1.54	2
Plasma beta	1.6	3.0	3.0	3.0	3.0
Plasma beta (normalized)	1.6	3.0	3.0	3.0	3.0
Divertor heat load (1.0 m)	5	7.1	7.1	8.1	8.1
Blanket heat load	4.6	5.6	5.6	7.0	7.0
CCZ	155	128	128	99	99



d1A
d1B
d1C
c1

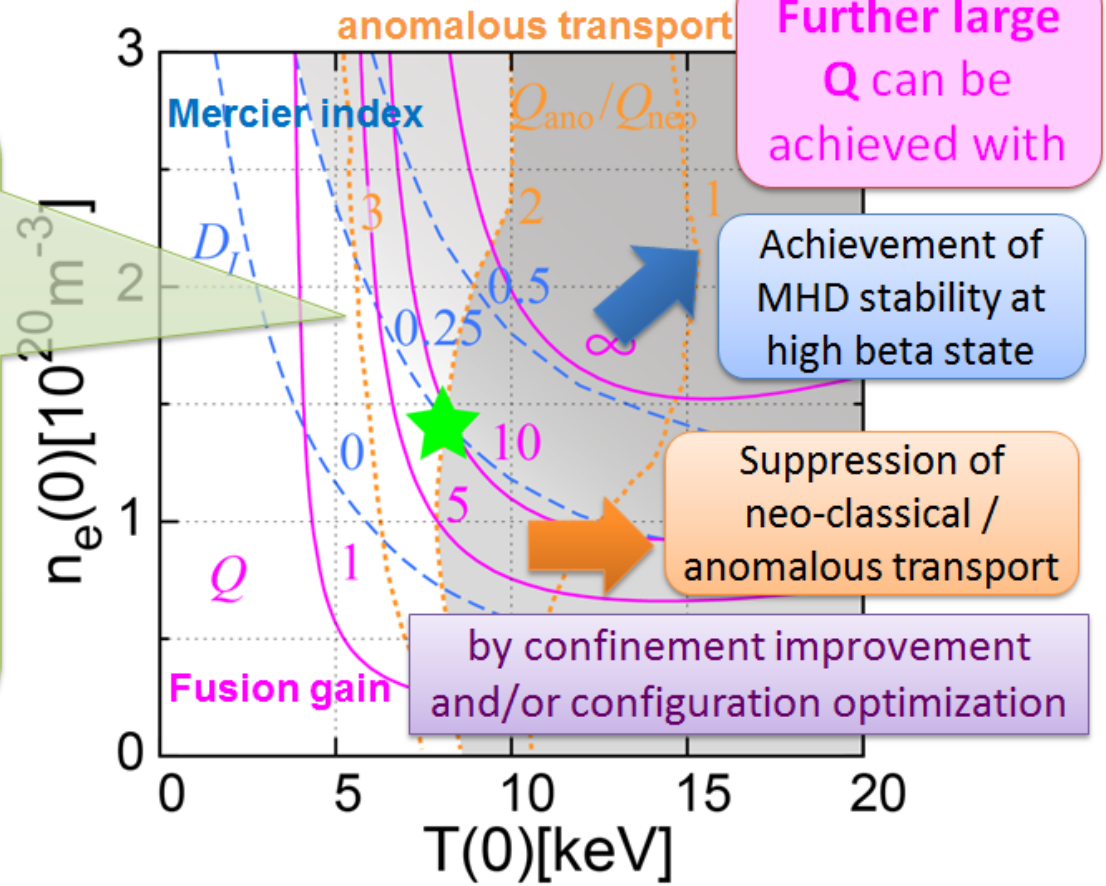
EX/P8-39

Development of a Real-time Simulation Tool towards Self-consistent Scenario of Plasma Start-up and Sustainment on Helical Fusion Reactor FFHR-d1

by Takuya GOTO *et al.*, (NIFS, Japan)

Self-consistent operation point

- Sufficiently low **neo-classical energy loss** considering anomalous transport
- **MHD equilibrium/stability** confirmed in LHD exp.
- Sufficiently low **bootstrap current**



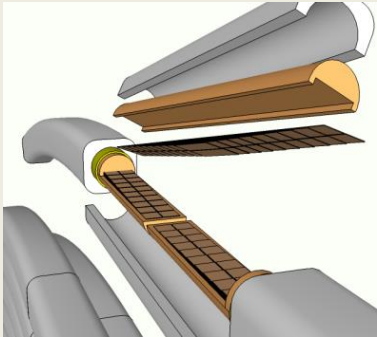
◆ Advantage of the Helical Reactor

Easy and stable plasma sustainment without plasma current

◆ Difficulty of the Helical Reactor

Need to construct a large and complicated device

➔ 2 options of Basic (based on the ITER technology) and Challenging (easier construction & maintenance) are defined



joint winding

superconducting magnet

Basic: Nb₃Sn + liquid He cooling + continuous winding

Challenging: HTS + He gas cooling + joint winding

structural materials

Basic: ferritic steel

Challenging: ferritic steel + ODS + V alloy

blanket

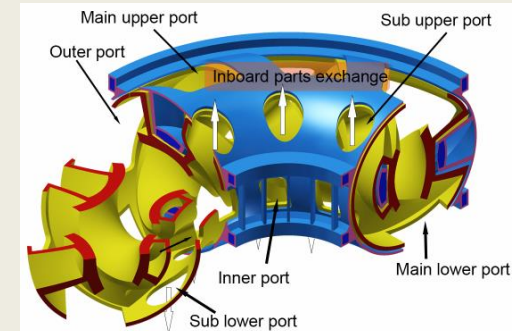
Basic: solid breeder + pressurized water + helical segmentation

Challenging: molten salt + Ti powder + horizontal / toroidal segmentation

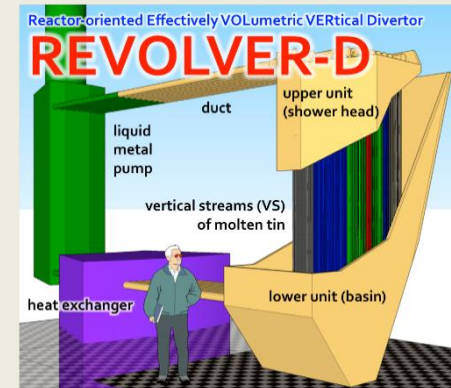
divertor

Basic: W monoblock + Cu alloy cooling pipe + pressurized water

Challenging: liquid metal (Sn) shower + novel divertor



novel divertor



liquid metal divertor
 IAEA2016_Sagara 4/22

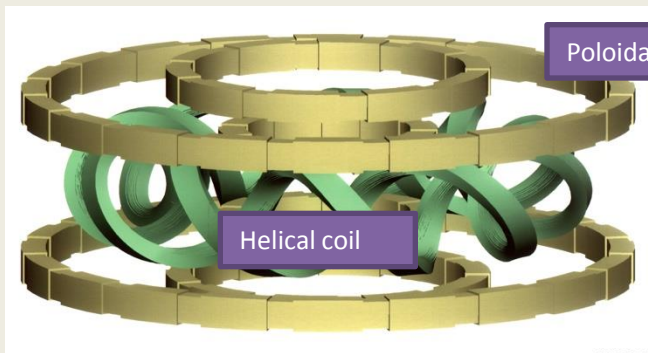
Helical Reactor
 FFHR-d1



FIP/3-4Rc

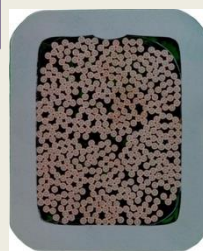
Lessons Learned from Eighteen Year Operation for the LHD Poloidal Coils Made from CIC Conductors

K. Takahata, S. Moriuchi, K. Ooba, S. Takami, A. Iwamoto, T. Mito, and S. Imagawa
National Institute for Fusion Science



Poloidal coil

Helical coil



CIC conductor

Steady Cooling 50,000 h
Excitation 10,000 h
↓
Stable operation
No superconducting-to-normal transition

The experience gained from **eighteen years of operation** has provided further useful information
– Preventive design and maintenance – Long-term changes in characteristics

Malfunction of Quench Detection System

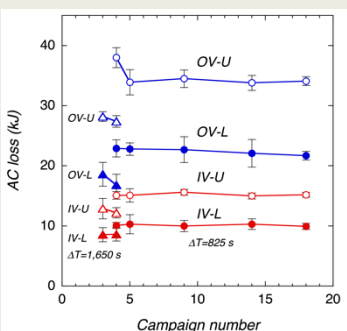
- 9 malfunction events
- Noise from NBI
- Out-of-balance voltage due to coupling currents
- No malfunction since 2010 thanks to various measures

Helium Leak from Insulation Break



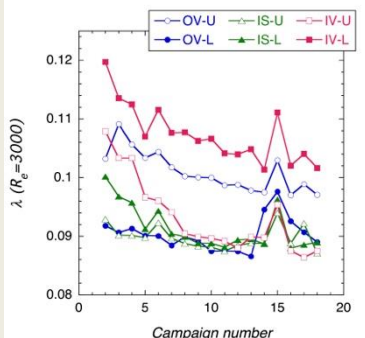
- Sudden helium leak during the 16th cool-down
- Replaced all breaks

Long-Term Changes in AC Loss



Almost unchanged

Long-Term Changes in Hydraulic Characteristics



Decreasing tendency

in good condition

1. Quench Detection System

- 9 malfunction events 2002~2009
 - Surge from plasma heating devices
 - Voltage due to coupling current

Lessons

Noises should be estimated in advance of operation

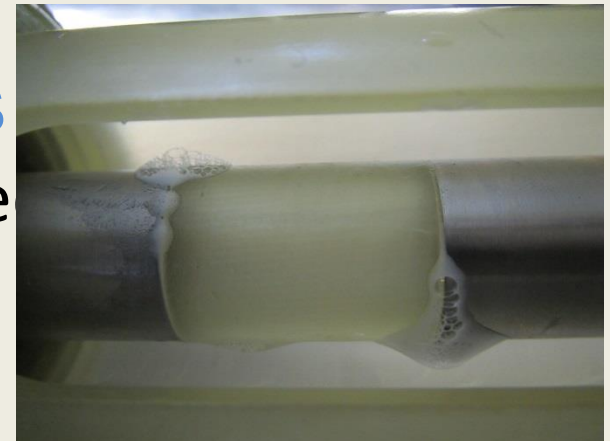


2. Cryogenic Insulating Breaks

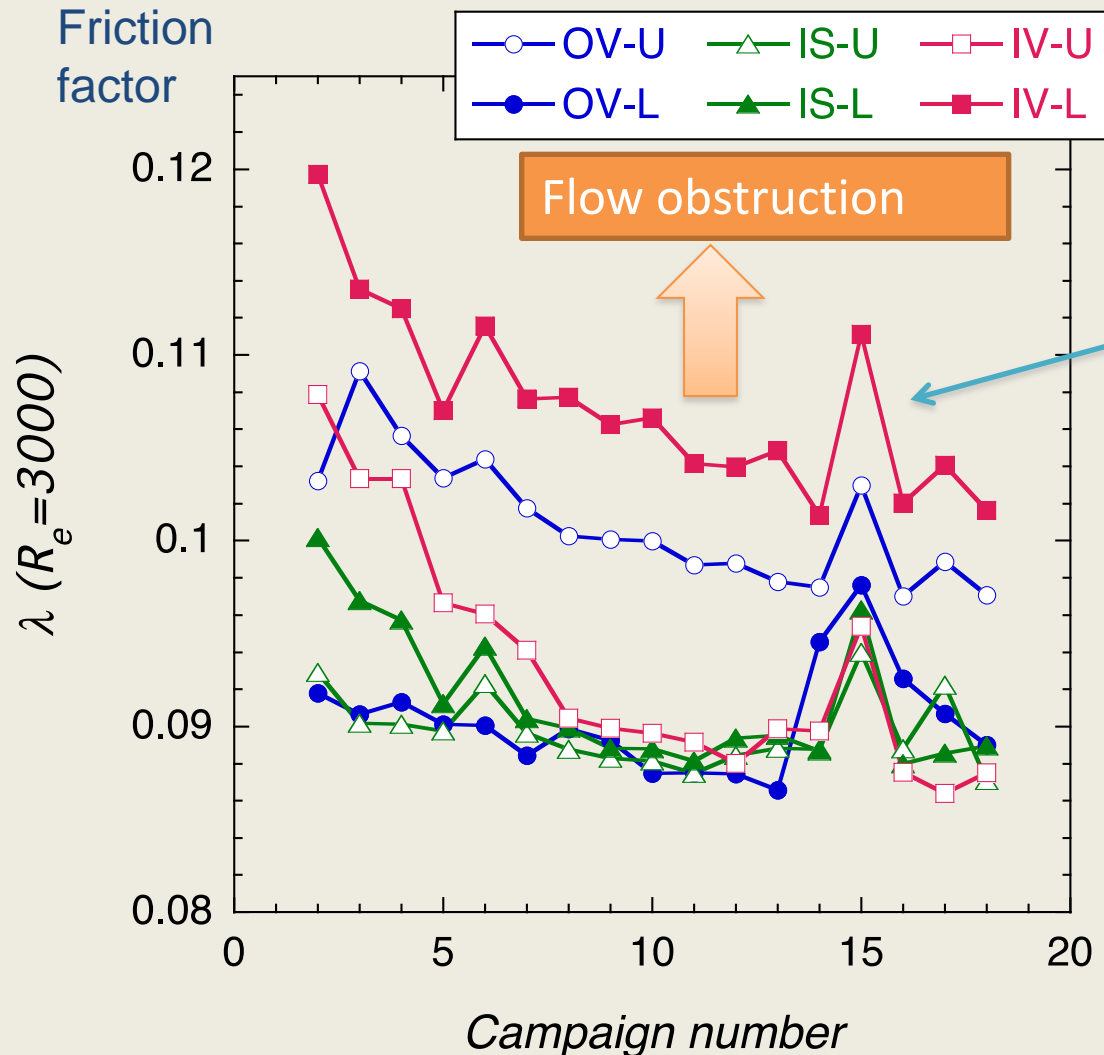
- One of the breaks suddenly leaked during the 16th cool-down in 2012

Lessons

Breaks should be designed conservatively



Trends in Hydraulic Characteristics



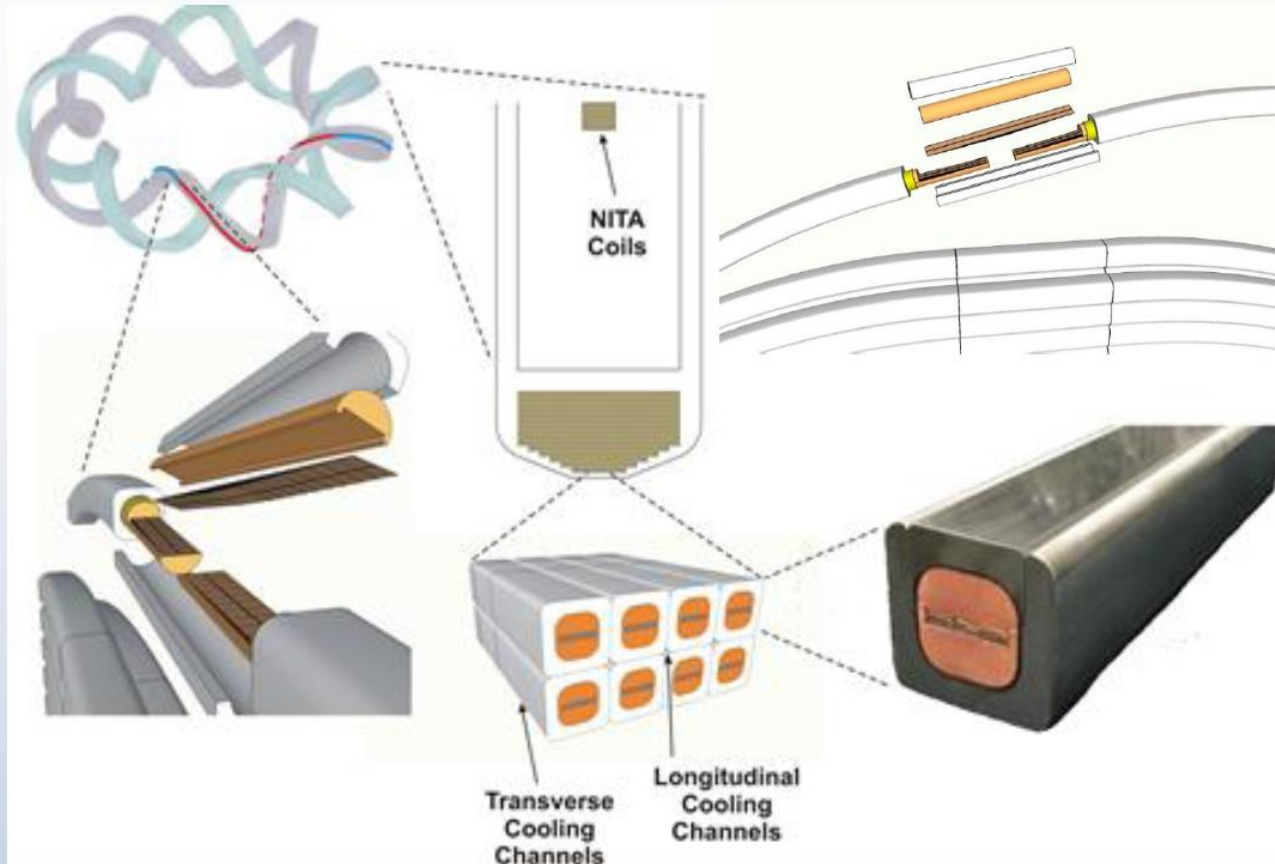
- The friction factor showed a tendency to decrease
- The sudden increase in the 15th campaign was probably caused by tiny particle of solidified gasses from new compressor oil

Lessons

- Compressor oil is a potential source of impurity gasses
- Mesh filter is effective

FIP/P7-11: N. Yanagi *et al.*, NIFS

“Helical Coil Design and Development with 100-kA HTS STARS Conductor for FFHR-d1”

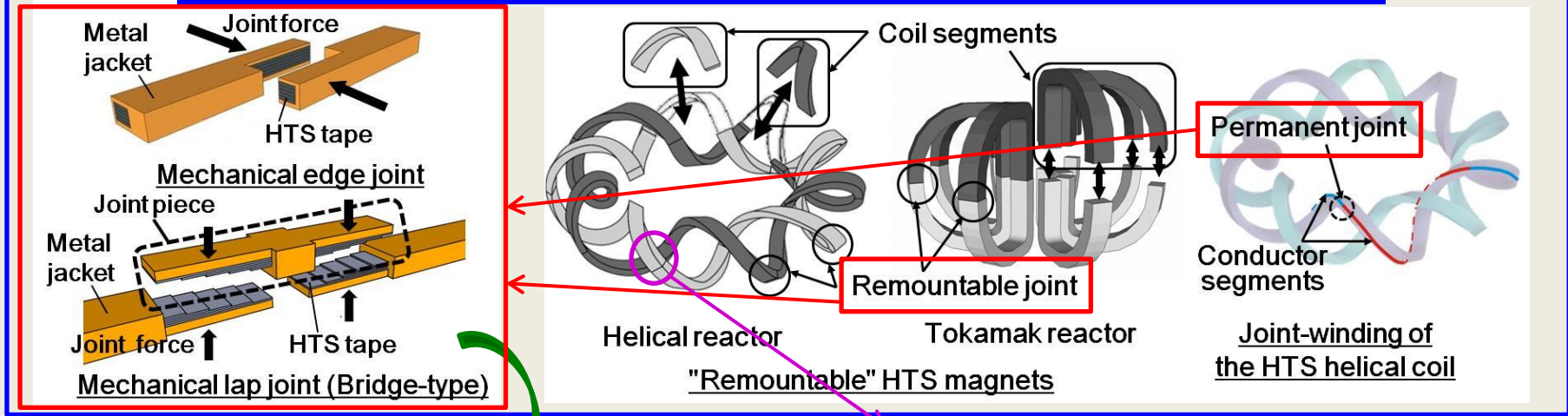


- Magnet design with High-Temperature Superconducting (HTS) option is progressing for the helical fusion reactor
- Prototype conductor sample achieved 100 kA at 5.3 T, 20 K with high stability
- Analysis on quench protection, feasibility study of helium gas cooling

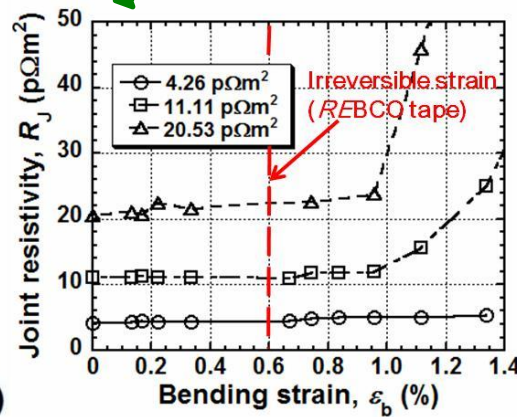
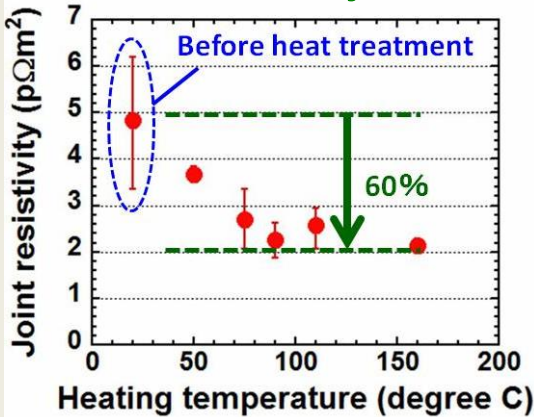
Development of Remountable Joints and Heat Removable Techniques for High-temperature Superconducting Magnets

H. Hashizume¹, S. Ito¹, N. Yanagi², H. Tamura², A. Sagara² (¹Tohoku Univ., ²NIFS)

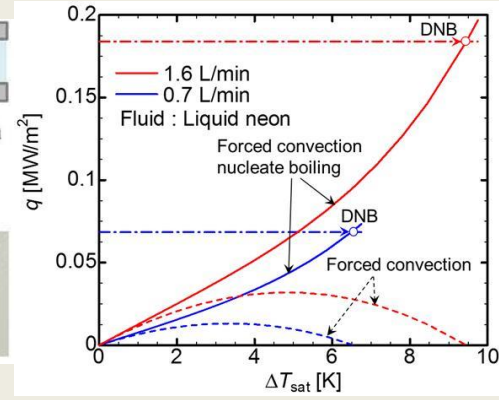
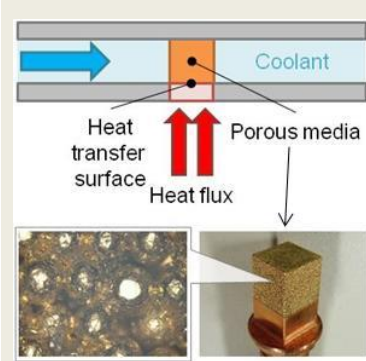
Innovative design for superconducting magnet, "Segment-fabrication"



Mechanical joints



Local heat removal with porous media



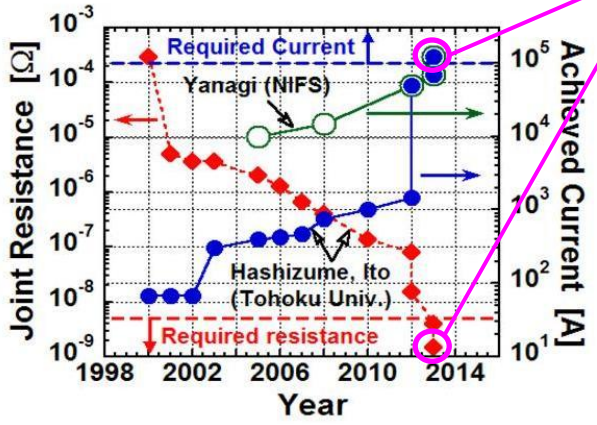
- Heat treatment → reduce joint resistance and its dispersion
- Bending strength (Joint) > Irreversible strain (REBCO tapes)
→ can fabricate curved joint by "joining-then-bending"

- New heat transfer correlation was established
→ can predict heat transfer performance
(needed for thermal stability analysis)

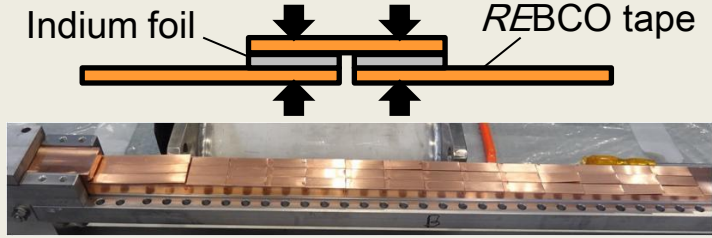
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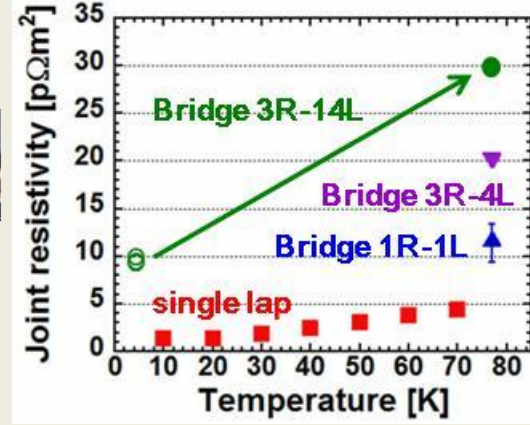
Mechanical joints



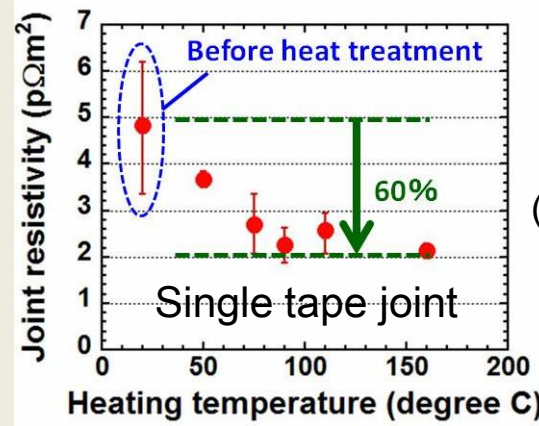
Bridge-type mechanical lap joint (100-kA-class HTS conductor)



- Joint resistivity > expected value
- The joint has a straight geometry...
→ Ideally bent and twisted



Heat treatment

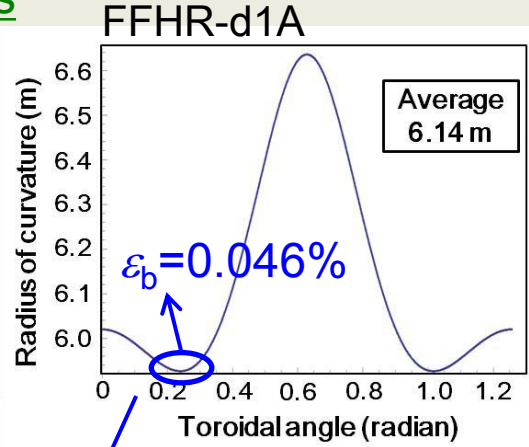
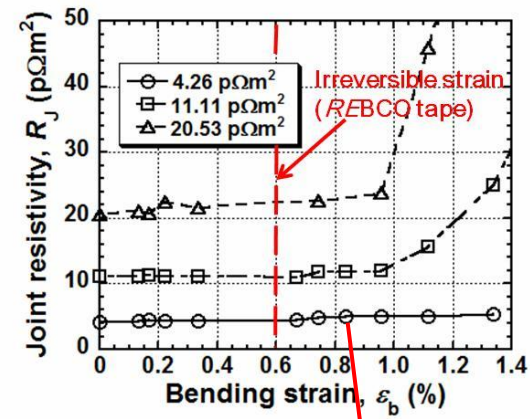


3-row, 1-layer
25 pΩm²
→ 8 pΩm²
(Heat treatment)



- Baking + Heat treatment (~100 °C)
→ promising to be applied to large-scale conductor joints

Bending characteristics



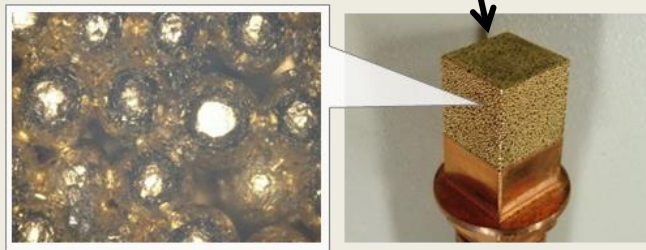
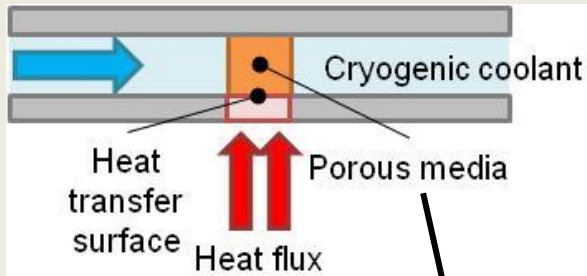
- Strength (Joint) > Irreversible strain (REBCO tapes)
- Bending strain: 0.046%
Tensile strain (EM forces): 0.145% < Irreversible strain (0.6%)

→ can fabricate curved joint by "joining then bending"

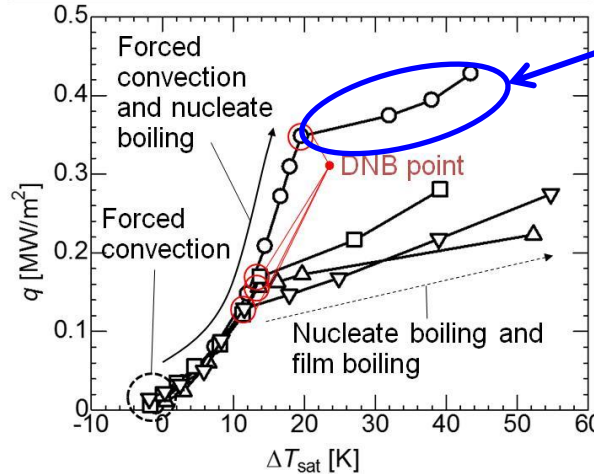
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Local heat removal with porous media



- $d = 790 \mu\text{m}$ ($G = 1.4 \text{ L/min}$, $\Delta T_{\text{sub}} = 2.2 \text{ K}$)
- △ $d = 464 \mu\text{m}$ ($G = 1.5 \text{ L/min}$, $\Delta T_{\text{sub}} = 0.9 \text{ K}$)
- $d = 429 \mu\text{m}$ ($G = 1.6 \text{ L/min}$, $\Delta T_{\text{sub}} = 4.3 \text{ K}$)
- ▽ $d = 234 \mu\text{m}$ ($G = 1.3 \text{ L/min}$, $\Delta T_{\text{sub}} = 2.0 \text{ K}$)

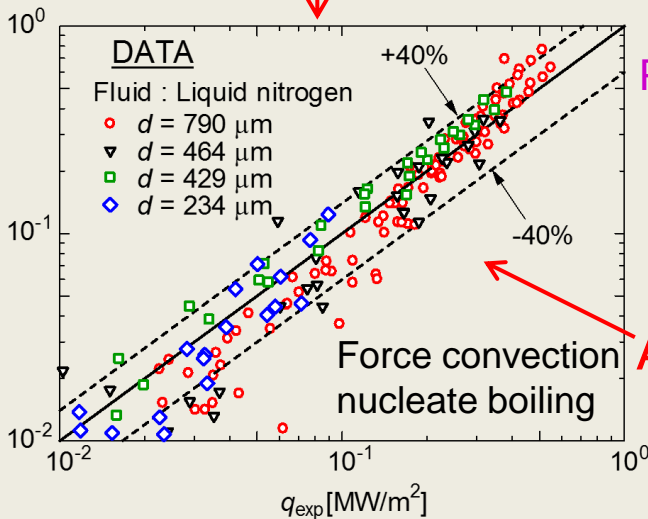


Large heat-transfer surface area

Prevention of transition to film boiling by capillary action



This study established new heat transfer correlation



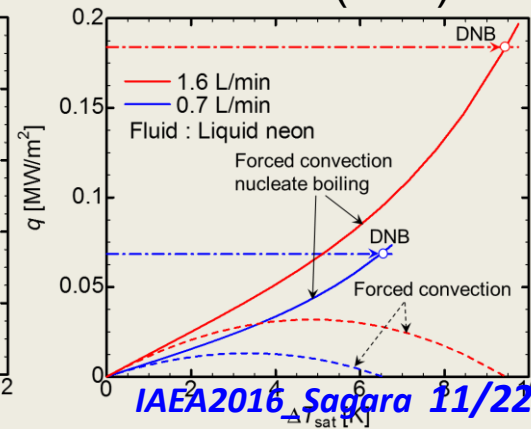
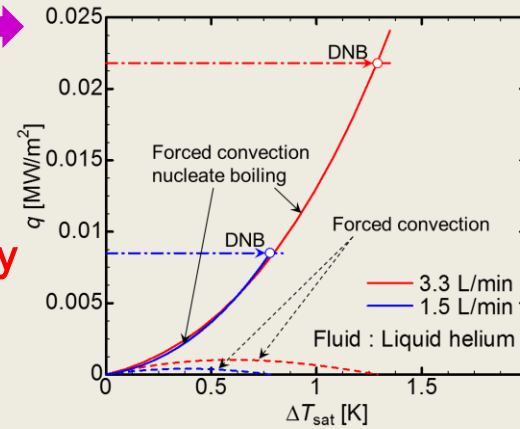
Prediction

Accuracy ±40%

DNB(LHe)

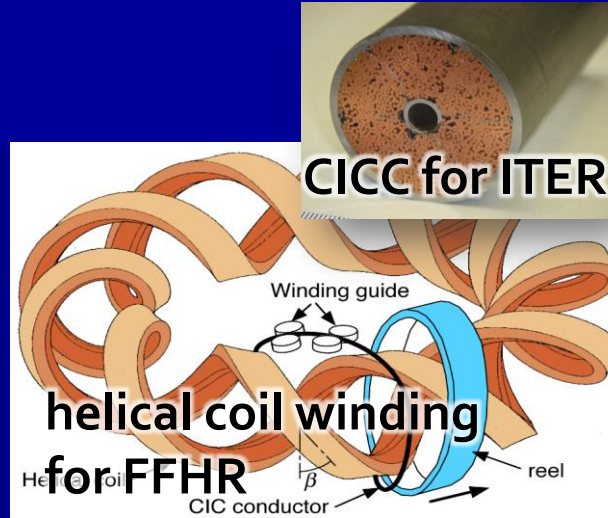
10 times

DNB(LNe)
DNB(LH2)



Superconducting Magnet

Basic

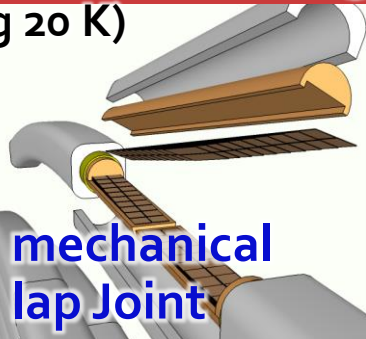


- Cable in Conduit Conductor (CICC) of Nb_3Sn as ITER (or NB_3Al)
- Continuous winding of helical coil using a winding machine as LHD
- Cooled by liquid He

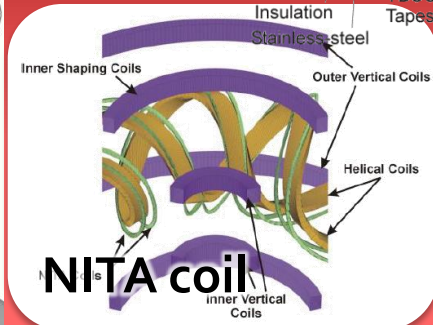
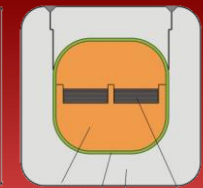
FIP/3-4Rc

Challenging

helical coil for FFHR-d1 (helium gas cooling 20 K)



100 kA-class HTS conductor



- High Temperature Superconductor (HTS) of ReBCO (YBCO, GdBCO...)
- Joint winding of helical coil based on the lap joint technique
- Indirectly cooled by He gas

FIP/P7-11

FIP/3-4Rb

Optimal welding conditions were obtained for joints between 9Cr-ODS and JLF-1 steels

Nagasaka et al., MPT/P5-21

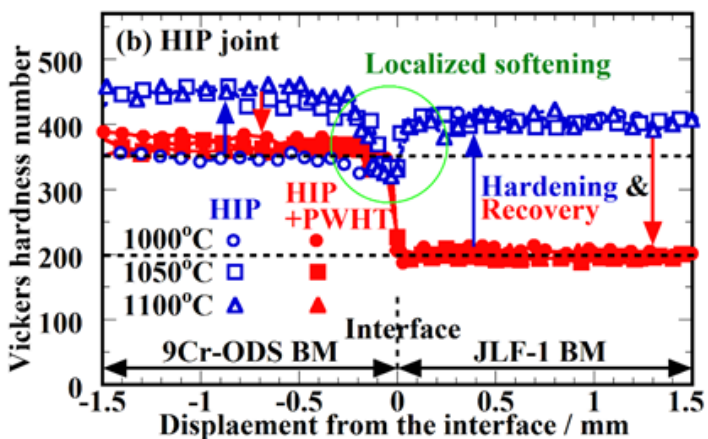
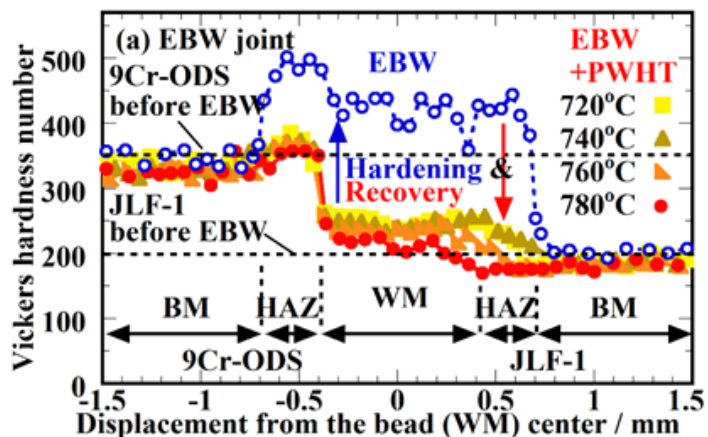


Fig. Hardness around the bonding interface in the dissimilar-metals joints

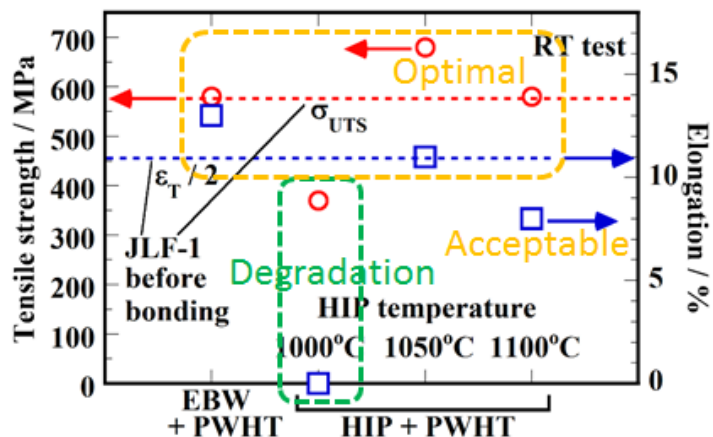


Fig. Tensile properties of dissimilar-metals joint with various welding conditions

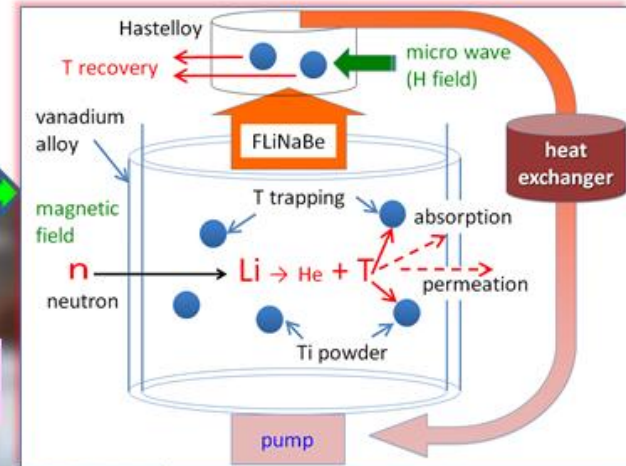
Optimal conditions:

- (1) Electron-beam welding (EBW) process
 Post-weld heat treatment (PWHT): 780°C x 1 h
 → To form tempered martensite by recovery
- (2) Hot iso-static pressing (HIP) process
 HIP temperature: 1050°C or 1100°C
 → To enhance matrix Fe diffusion
 PWHT: 1050°C x 1 h + 36°C/min cooling + 780°C x 1 h
 → To eliminate the localized softening and to form refined carbide and tempered martensite by recovery

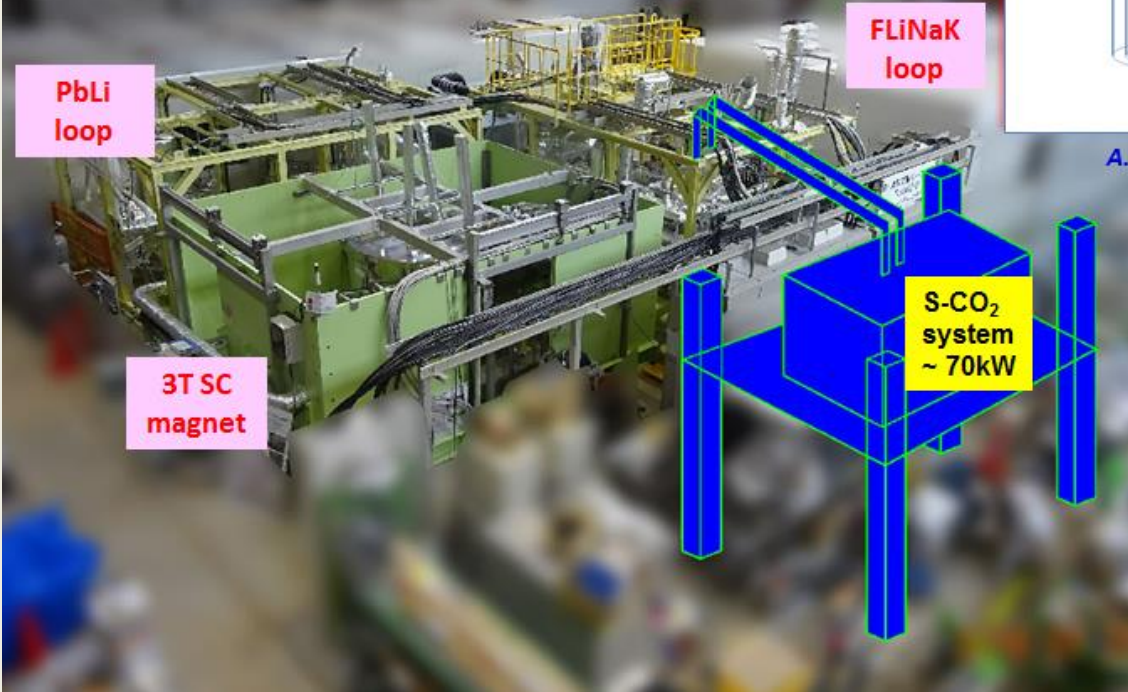
Oroshhi-2 in NIFS (2016--)

- ◆ MHD effects on LiPb
- ◆ Corrosion and mass transfer under non-equilibrium and ΔT
 - ◆ Heat transfer on FLiNaK under high B
 - ◆ Hydrogen charging and recovery
 - ◆ Metal powder mixed system
 - ◆ Operation of S-CO₂ system for Flinak

TOFE-2016 by Sagara

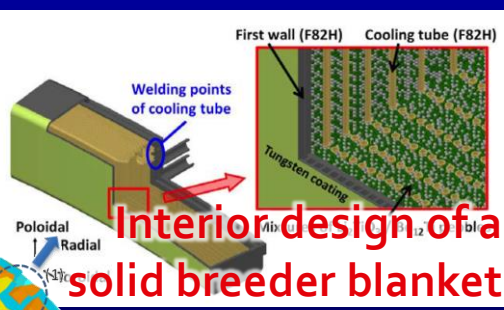
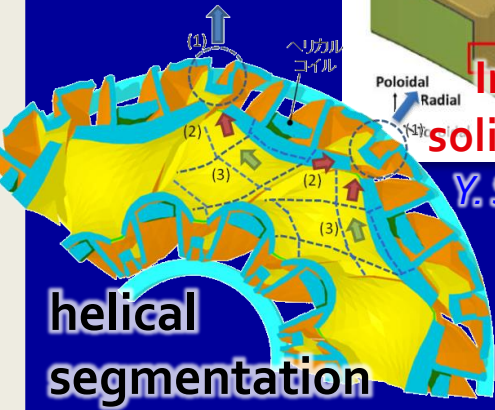


A. Sagara et al., FED 89 (2014) 2114-2120



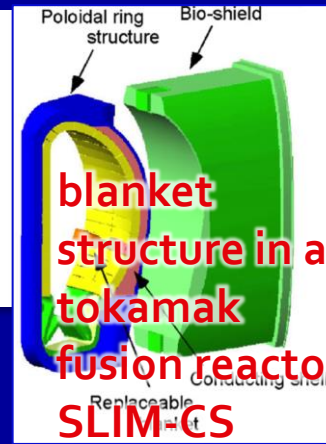
Breeding and Shielding Blankets

Basic



Interior design of a solid breeder blanket

Y. Someya, IAEA FEC 24 (2012) FTP/P7-33

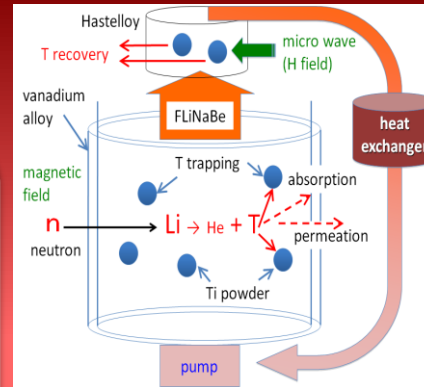
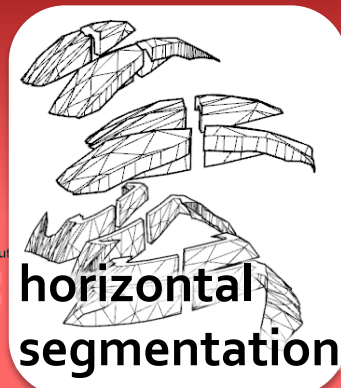
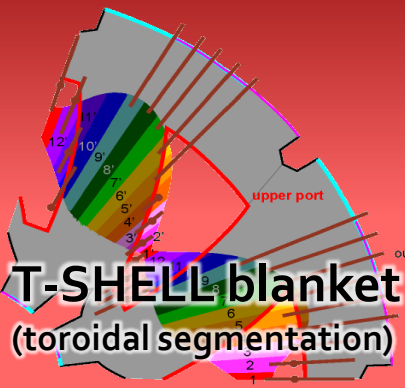


K. Tobita, FED 85 (2010) 1342

MPT/P5-21

- The 1st option of the Japanese tokamak DEMO and Japanese ITER TBM
- Cooling by highly pressurized hot water of > 200 atm and > 600 K

Challenging



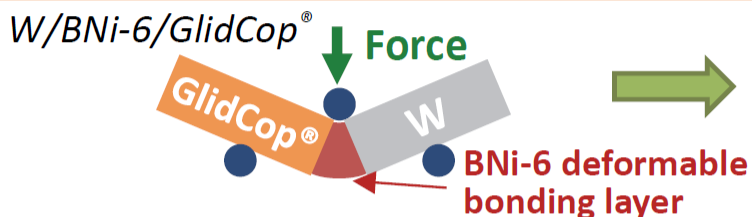
FLiNaBe mixed with Ti powder

- Use FLiNaBe ($T_m \sim 600$ K)
- Mixed with metal powders ($\sim \mu\text{m}$) (e.g., Ti) to enhance hydrogen solubility
- S-CO₂ secondary system
- Toroidal / horizontal segmentation of the blanket module

TOFE2016

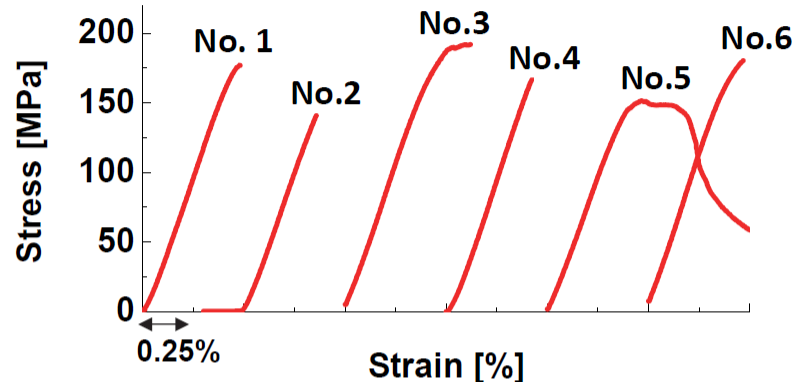
The small-scale divertor mock-up by improved brazing technique showed an excellent potential for using in the reactor divertor

Improved brazing technique between W armour and ODS-Cu (GlidCop®) heat sink was found by using BNi-6 (Ni-11%P) filler material



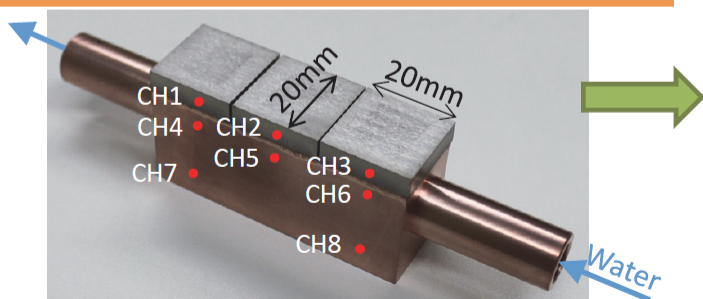
Schematic view of the three-point bending test of the W/BNi-6/GlidCop® specimen after deformation.

Tough bonding layer !!



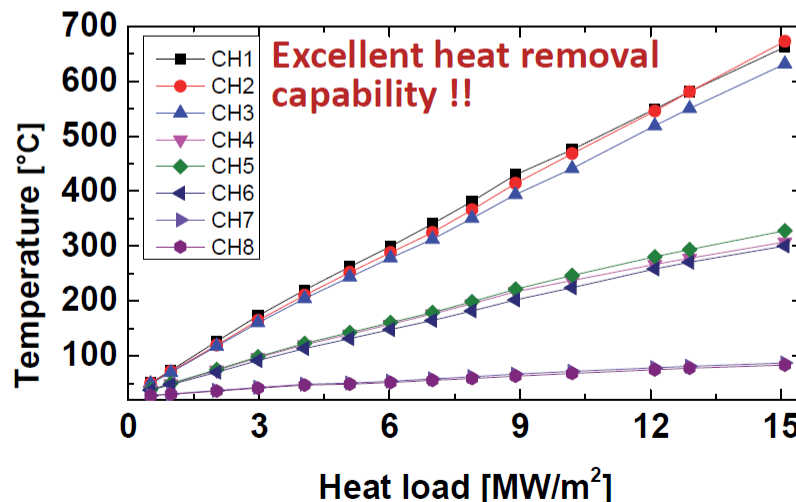
Stress-strain curves of W/BNi-6/GlidCop® specimens.

W/BNi-6/GlidCop® small-scale divertor mock-up showed an excellent heat removal capability



W/BNi-6/GlidCop® small-scale divertor mock-up.

Excellent heat removal capability !!



Temperature profile of the W/BNi-6/GlidCop® mock-up during a steady state heat loading.

M. Tokitani et al., FIP/P4-37

FIP/P7-2

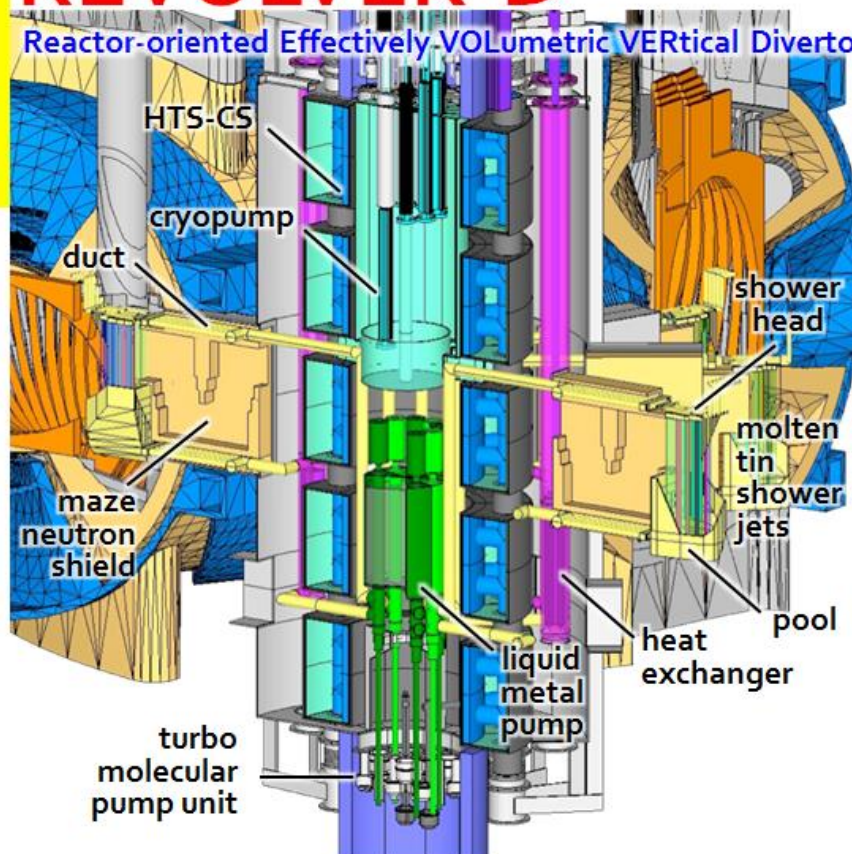
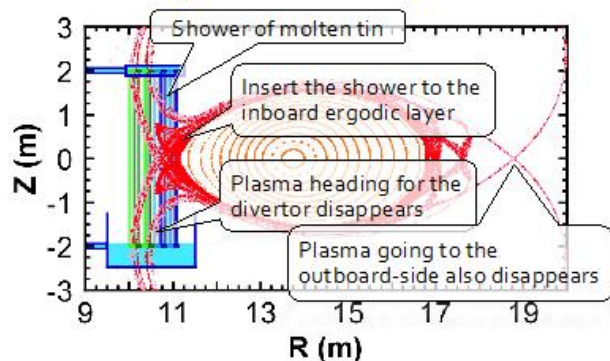
REVOLVER-D: The Ergodic Limiter/Divertor Consisting of Molten Tin Shower Jets Stabilized by Chains

J. Miyazawa, et al.
 National Institute for Fusion Science, Japan

REVOLVER-D

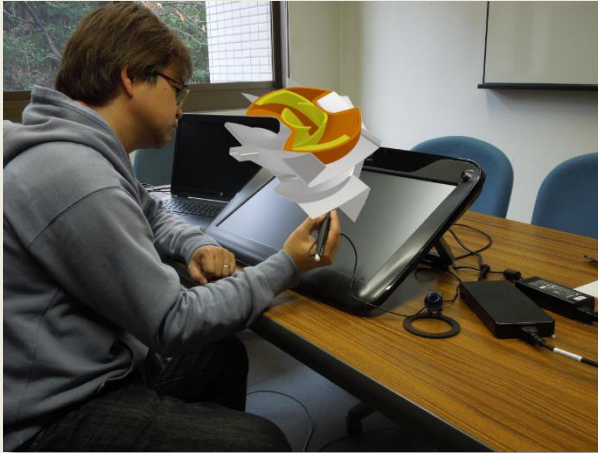
Reactor-oriented Effectively VOLumetric VERTICAL Divertor

The Ergodic Limiter/Divertor



New ergodic limiter/divertor concept with showers of molten tin sheath jets is proposed for the LHD-type helical reactor FFHR-d1

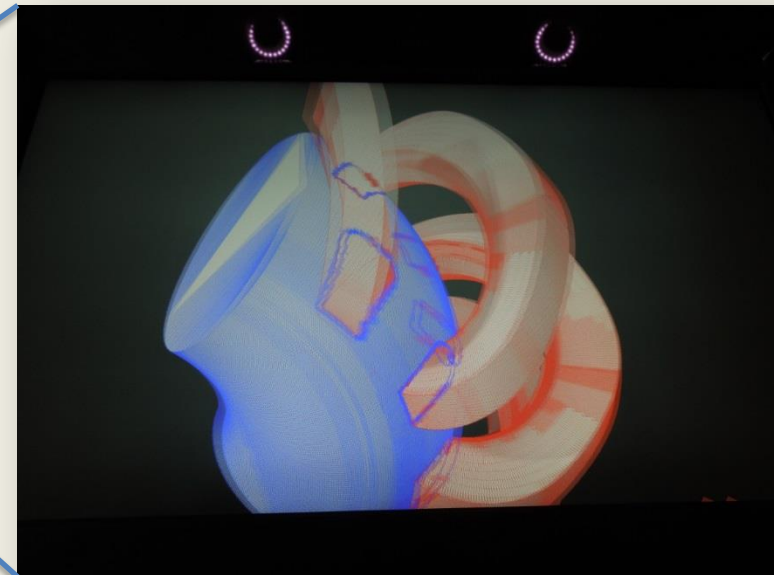
Desktop Virtual-Reality (VR) System is Ready to Support the Design Activity



A desktop-type VR system

- immersive monitor
- sensors

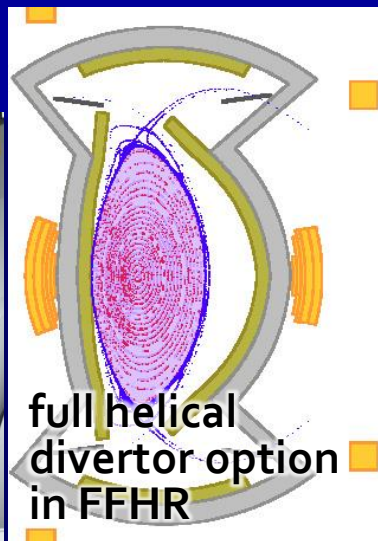
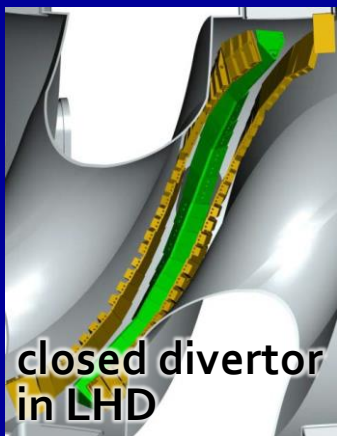
The viewer can watch, lift, and rotate the reactor components by the stylus-type 3D mouse with **collision detection**



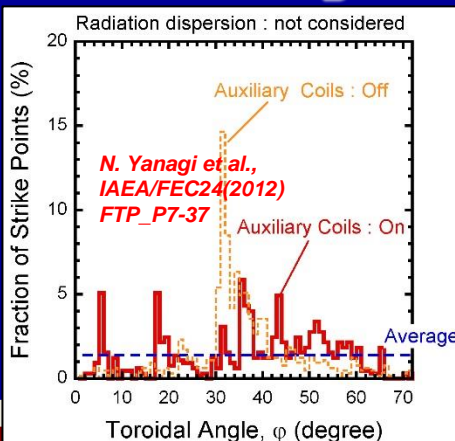
These pictures are composite photographs and only the viewer can watch the CAD data in the VR world

Divertor

Basic



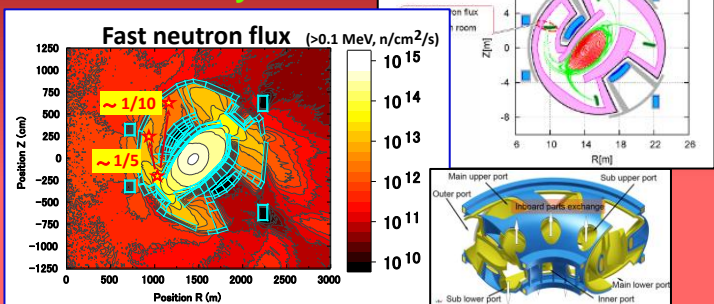
Toroidal asymmetry of heat flux is a big issue



- Developed for ITER and the 1st option of Japanese tokamak DEMO
- Use of pressurized water
- Permissible heat load below 10 MW/m²
- Issues on maintainability and radwastes

Challenging

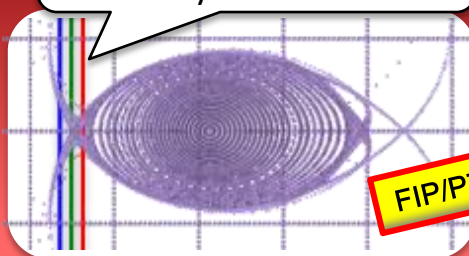
First proposal of Cu use and lifetime ~ 6 years



H. Tamura, T. Tanaka, FED98-99(2015)1629.

novel divertor

Shower of molten tin Sn stabilized by chains at only inboard side



liquid metal ergodic limiter/divertor

J. Miyazawa, submitted to FED

- Proposed recently for FFHR-d1
- Good maintainability
- Shower of molten Sn (T_m ~ 500 K) in a few m/s as an "ergodic limiter/divertor"
- Issues on temp.window for Cu and MHD for shower

FIP/P4-37

TRL		1	2	3	4	5	6	7	8	9	
Technology Readiness Levels		Basic Technology Research		<h2>Technology Development</h2> <p>Research to Prove Feasibility</p>			<h2>System/Subsystem Development</h2> <p>Technology Demonstration</p>		<h2>System Test, Launch & Operations</h2>		
Divertor	Basic	W monoblock + Cu alloy cooling pipe + pressurized water		<p>FIP/P4-37</p>		LHD / JT-60SA		ITER		<p>TRL 6 should be achieved before starting construction of DEMO</p>	
	Challenging	liquid metal (Sn) shower + novel divertor		<p>FIP/P7-2</p>		R&D in NIFS, Univs. OST		LHD			
Super-conducting magnet	Basic	Nb ₃ Sn + liquid He cooling + continuous winding		<p>FIP/3-4Rc</p>		LHD / JT-60SA		ITER			
	Challenging	HTS + He gas cooling + joint winding		<p>FIP/3-4Rb</p> <p>FIP/P7-11</p>		R&D in NIFS, Univs., OST		LHD			
Structure materials	Basic	ferritic steel		<p>Thermal stress factor / kW m⁻² vs Temperature / °C</p> <p>Curves: NIFE-SiC, NH2, P82H, SS316</p>		R&D in OST, NIFS, Univs.		ITER			<p>Basic option will be achieved in ITER</p>
	Challenging	ferritic steel + ODS + V alloy		<p>MPT/P5-21</p>		R&D in NIFS, Univs., OST		LHD			
Blanket	Basic	solid breeder + pressurized water + helical segmentation				R&D in OST, NIFS, Univs.		ITER		<p>Challenging option will be achieved in LHD</p>	
	Challenging	molten salt + Ti powder + horizontal / toroidal segmentation		<p>TOFE2016</p>		R&D in NIFS, Univs., OST		LHD			

Summary

- Conceptual design of the helical fusion reactor **FFHR-d1A** is ongoing with **2 options** based on **broad & joint R&D activities**
- The “**basic option**” is based on the **ITER technology**
- The “**challenging option**” boldly includes the **new ideas** that would possibly be beneficial for making the reactor design more attractive
 - ✧ **SC magnet:** gas He cooled **HTS** with joint winding
 - ✧ **Blanket:** self-cooling of molten salt **FLiNaBe** mixed with metal powder, with toroidally / horizontally segmented units
 - ✧ **Divertor: REVOLVER-D** (shower of molten tin inserted to the inboard ergodic layer)

Thank you for your attention

- Wed. FIP/P4-37 Tokitani
“Fabrication of Divertor Mock-up with ODS-Cu and W by Improved Brazing Technique”
- Thu. MPT/P5-21 Nagasaka
“Development of dissimilar-metals joint of oxide-dispersion-strengthened (ODS) and non-ODS reduced-activation ferritic steels”
- Fri. EX/P8-39 Goto
“Development of a Real-time Simulation Tool towards Self-consistent Scenario of Plasma Start-up and Sustainment on Helical Fusion Reactor FFHR-d1”
- Fri. FIP/P7-2 Miyazawa
“REVOLVER-D: The Ergodic Limiter/Divertor Consisting of Molten Tin Shower Jets Stabilized by Chains”
- Fri. FIP/P7-11 Yanagi
“Helical Coil Design and Development with 100-kA HTS STARS Conductor for FFHRd1”
- Sat. FIP/3-4Ra Sagara
“Two Conceptual Designs of Helical Fusion Reactor FFHR-d1A Based on ITER Technologies and Challenging Ideas”
- Sat. FIP/3-4Rb Hashizume
“Development of Remountable Joints and Heat Removable Techniques for High-temperature Superconducting Magnets”
- Sat. FIP/3-4Rc Takahata
“Lessons Learned from the Eighteen-Year Operation of the LHD Poloidal Coils Made from CIC Conductors”