

Overview of the Present Progresses and Activities on the Chinese Fusion Engineering Test Reactor



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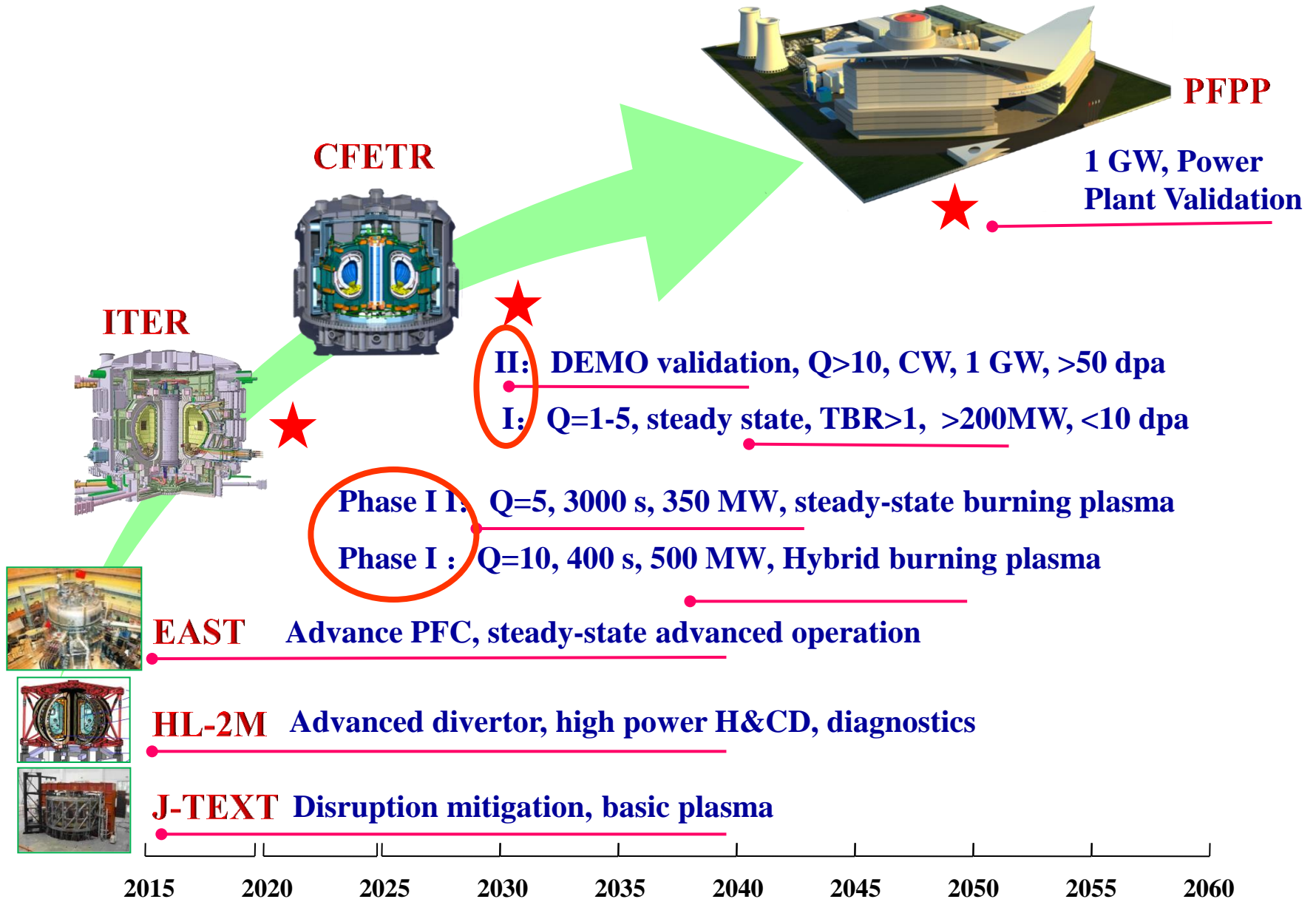
26th IAEA Fusion Energy Conference, Kyoto, Japan 17–22 October 2016



- **Introduction**
 - **CN MCF Roadmap**
 - **Mission of CFETR**
- **Progresses and activities of CFETR**
 - **Previous concept design**
 - **New design version**
 - **Phase I**
 - **Phase II**
- **Key R&D activities**
- **Summary**



CN MCF Roadmap





Mission & Objectives of CFETR

Mission: Bridge gaps between ITER and DEMO, realization of fusion energy application in China

- A good complementarities with ITER
- Rely on the existing ITER physical ($k \sim 1.8$, $q > 3$, $H \sim 1$) and technical (SC magnets, diagnostic, H&CD) bases
- **Demonstration of the burning plasma with $P_f = 200\text{MW} \sim 1000\text{MW}$**
- **Demonstration Long pulse or steady-state operation of burning with duty cycle $\geq 0.3 \sim 0.5$**
- **Demonstration of full cycle of T self-sustained with TBR over 1.0**
- Exploring options for DEMO blanket & divertor with an easy changeable core by RH
- Exploring the technical solution for licensing DEMO
- With power plant potential step-by-step approach.



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The advanced design and 3D simulation platform has been set up



Design and management servers



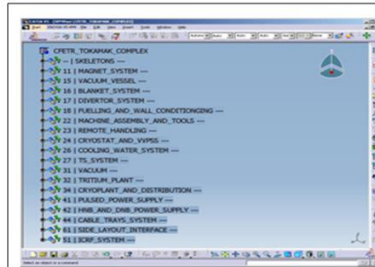
Terminals of the design cloud



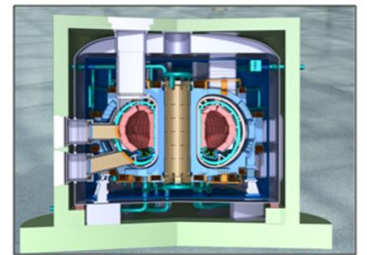
Virtual reality system



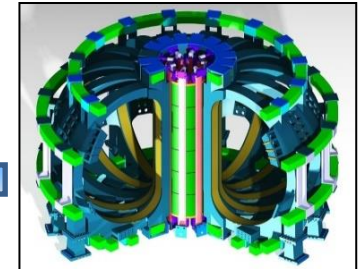
Remote handling



CFETR VPM tree



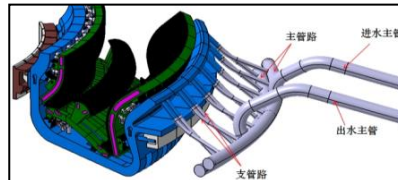
CFETR main machine



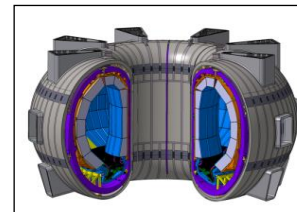
Magnet



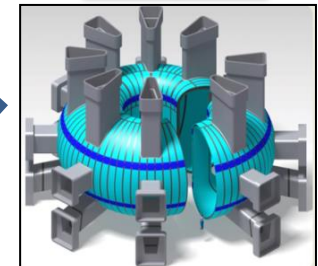
Cryostat



Divertor



Blanket



Vacuum Vessel



Advanced features of the design platform

Remote collaboration

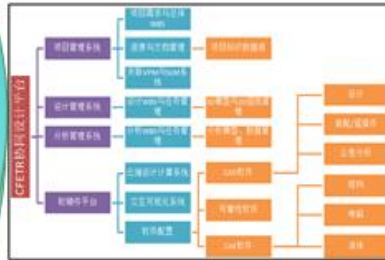


- Advanced data compression technology
- Complete data sharing
- Remote design on any terminal on the internet

Collaboration design platform



Centralized management



- Centralized data storage
- High correlation and traceability
- Safe and data tolerant

3D stereo review



- Frequent 3D stereo review
- No need of physical mockups
- Inaccessible positions in reality become examinable



First Design version of CFETR (2011.11-2015.8)

Phase I

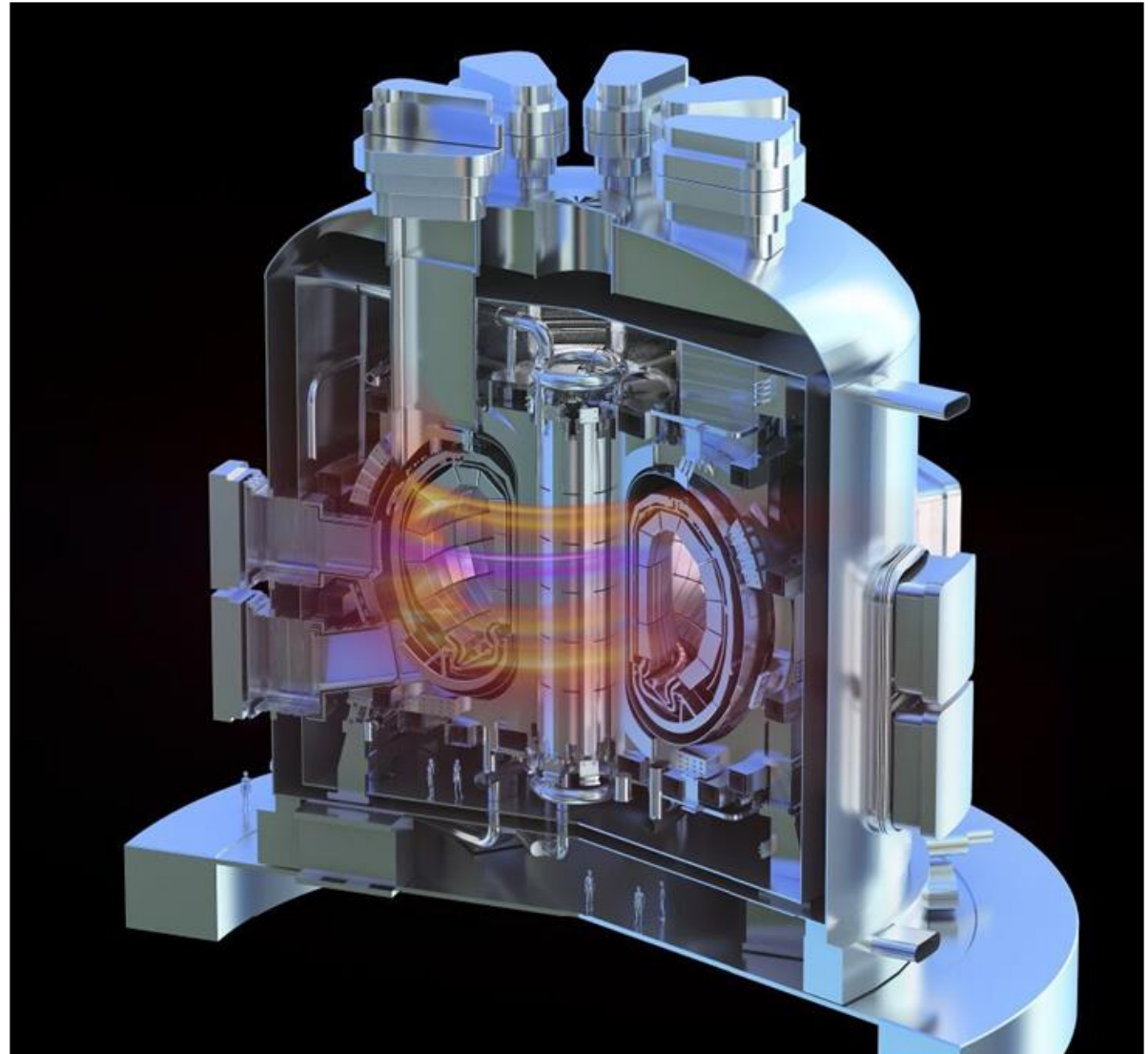
- $I_p = 7-10$ MA
- $B_{to} = 4.5-5.0$ T
- $R_0 = 5.7$ m ;
- $a = 1.6$ m;
- $k = 1.8 \sim 2.0$
- $q_{95} \geq 3$;
- $\beta_N \sim 2-3$

$P_{fusion} : 200$ MW

Phase II

**Possible upgrade
to $R \sim 5.9$ m, $a \sim 2.0$
m, $B_t = 4.8$ T,
 $I_p \sim 15$ MA**

$P_{fusion} : 1000$ MW





Key parameter investigation (180VS)

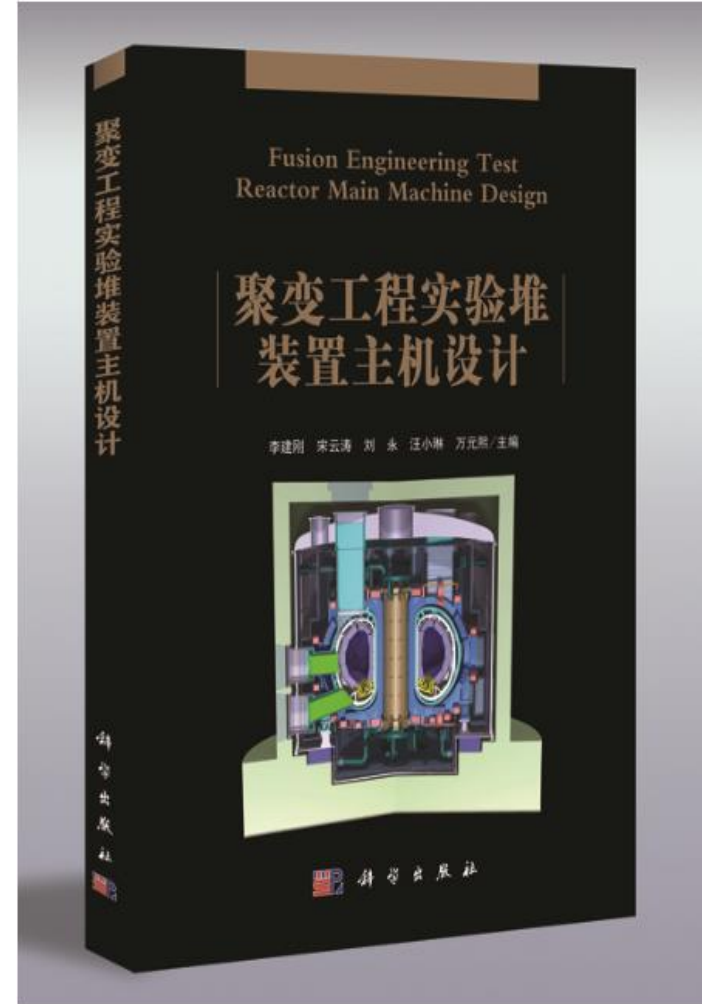
Operation mode	A	B	C	D	E	ITER-SS	Upgrade
I_p (MA)	10	10	10	8	8	9	15
P_{aux} (MW)	65	65	65	65~70	65	59	65
q_{95}	3.9	3.9	3.9	4.9	4.9	5.2	3.9
W(MJ)	171~174	193	270~278	171	255	287	540
P_{Fus} (MW)	197~230	209	468~553	187~210	409	356	1000
Q_{pl}	3.0~3.5	3.2	7.2~8.5	2.7~3.2	6.3	6.0	15
T_{i0} (keV)	17.8~18.5	29	19.8~20.8	20.6~21	21	19	25
N_{el} ($10^{20}/m^3$)	0.75	0.52	1.06	0.65	0.94		1
n_{GR}	0.6	0.42	0.85	0.65	0.95	0.82	0.85
β_N	1.59~1.62	1.58	2.51~2.59	2	2.97	3.0	2.7
β_T (%)	~2.0	2.3	3.1~3.25	2	2.97	2.8	4.2
f_{bs} (%)	31.7~32.3	35.8	50~51.5	50	73.9	48	47
τ_{98Y2} (s)	1.82~1.74	1.55	1.57~1.47	1.37	1.29	1.94	1.88
P_N/A (MW/m ²)	0.35~0.41	0.37	0.98	0.33~0.37	0.73	0.5	1.38
I_{CD} (MA)	3.0~3.1	7.0	2.45	4.0	2.76		3.0
H_{98}	1	1.3	1.2	1.2	1.5	1.57	1.2
$T_{burning}$ (S)	1250	SS	2200	SS	S		1200

$B_t=4.5T$; $R=5.7$ m; $a=1.6$ m; $k=1.8 \sim 2.0$

$B_t=4.8T$;
 $R=5.9$ m; $a=2.0$ m;



The first design version has been summarized





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Key issues for CFETR mission

**Obtained
Burning Plasma
for fusion power**

1. **Larger device (B_t , R_o , a , K)**
2. **Standard H mode**
3. **Advanced operation scenario**

**Steady-state operation
for fusion energy**

4. **Increasing flux to sustain longer I_p**
5. **CW Ext H&CD (NB,EC,LH,IC)**
6. **Higher f_b**
7. **Higher energetic α heating**
8. **Divertor physics and tech.**

**Breeding Tritium
for T self-sustained**

9. **T-breeding by blanket**
10. **T-plant: extract & reprocessing**
11. **Materials**
12. **RH**
13. **licensing**

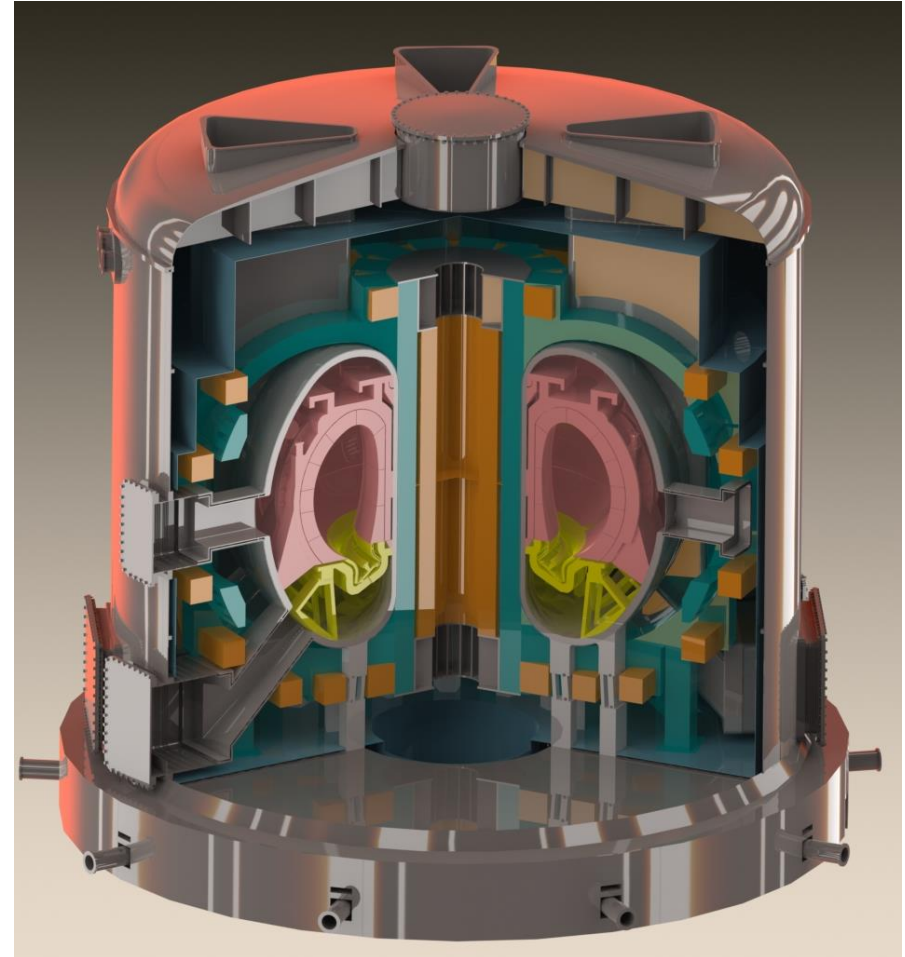


New design version (2015.8-2016.8)

Easy transfer from Phase I to Phase II

The key points changed:

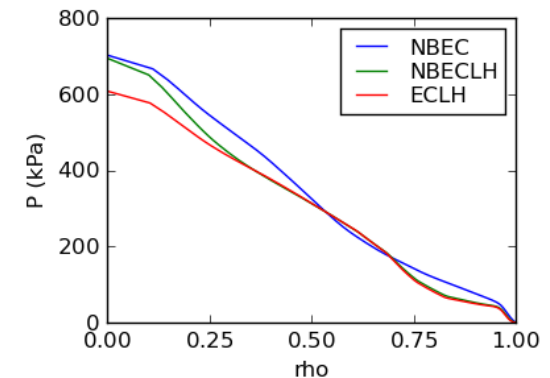
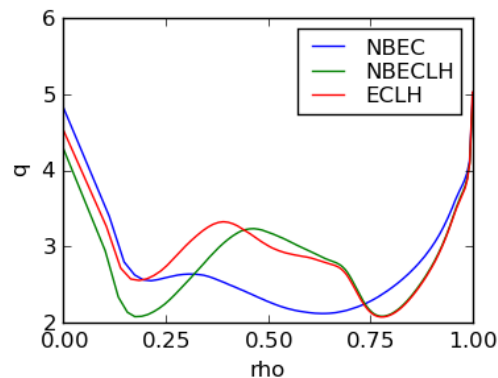
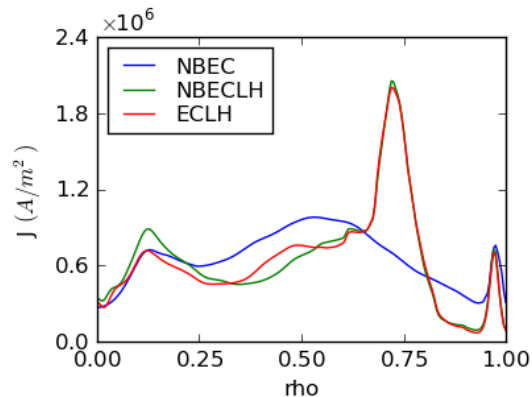
- **Larger size:**
R= 6.7m, a=1.95m
- **Higher B_T :** 5.0-7.0 T
- **Advanced CS magnet:** ≥ 480 VS
- **Lower I_p :** 6-12MA
- **12 TF coils** for easy RH, H&CD
- **More reliable Plasma targets**
- **Higher confidence for STE goals**





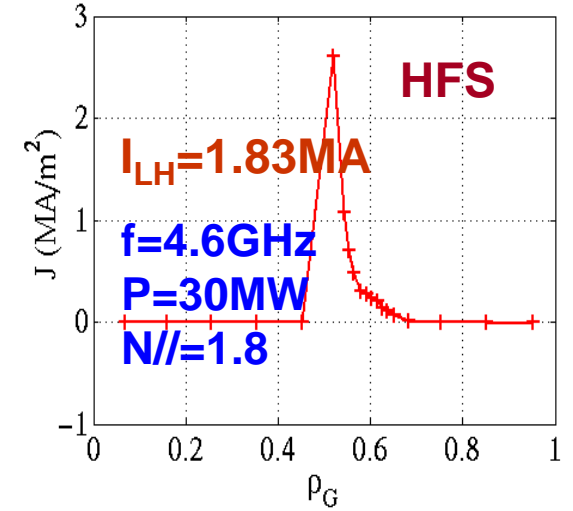
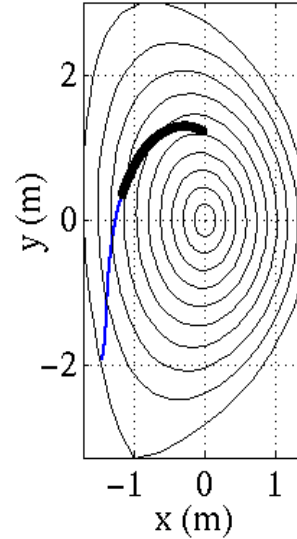
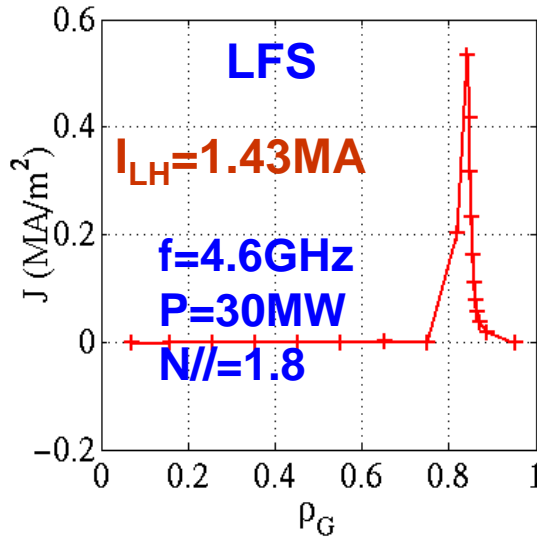
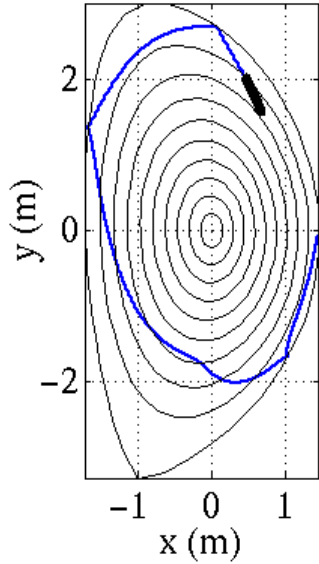
CFETR Physics design

- **0D system code + 1.5D integrated modeling (OMFIT, EFT, ONETWO, GATO, TGYRO/TGLF, NEO, ELITE)**
- **Off-axis NBI + ECCD, LHCD are major H&CD tools together with bootstrap current for SSO**
- **Using 800 kV NBI(1.1MA/10MW) + 190GHz ECCD for phase I operation.**





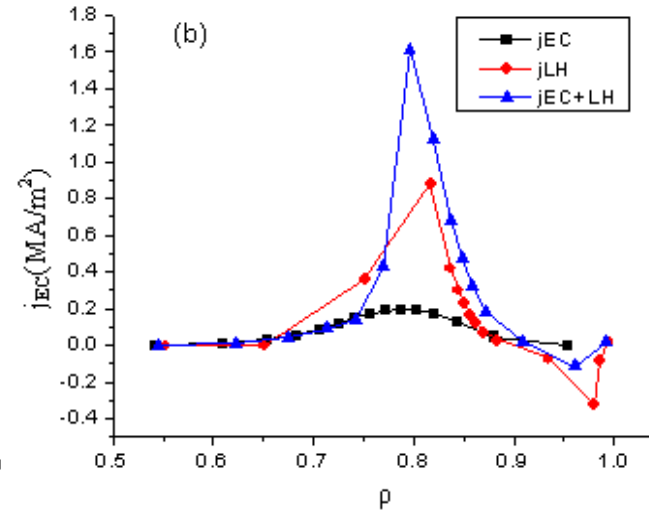
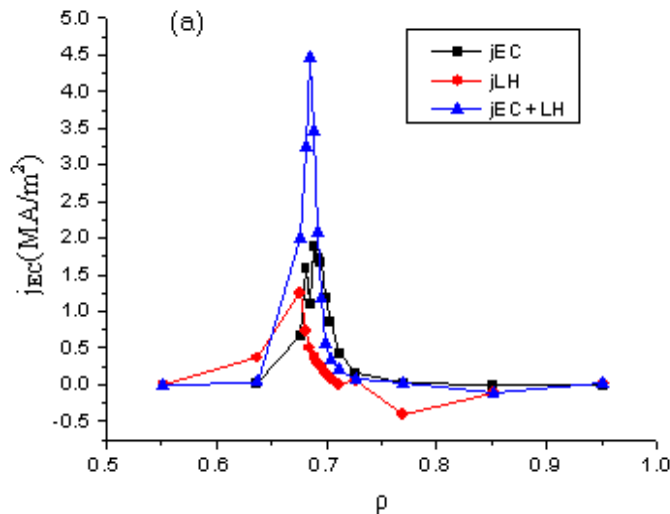
More effective current drive – HFS LHCD+Top ECCD



$I_{EC} = 0.975 \text{ MA} (\phi = 205^\circ, \theta = 110^\circ)$
 $I_{LH} = 2.7305 \text{ MA} (N// = 2.04)$
 $I_{EC+LH} = 4.0062 \text{ MA}$
 $\Delta I = I_{EC+LH} - I_{EC} - I_{LH} = 0.3007 \text{ MA}$

$I_{EC} = 0.698 \text{ MA} (\phi = 250^\circ, \theta = 130^\circ)$
 $I_{LH} = 1.45 \text{ MA} (N// = 2.04)$
 $I_{EC+LH} = 2.4923 \text{ MA}$
 $\Delta I = I_{EC+LH} - I_{EC} - I_{LH} = 0.3443 \text{ MA}$

HFS LHCD
TOP ECCD
 $\Delta I = 0.3 \text{ MA}$
 $I_{CD} = 4.0 \text{ MA}$



LFS LHCD
LFS ECCD
 $\Delta I = 0.34 \text{ MA}$
 $I_{CD} = 2.49 \text{ MA}$



Two New Fully Non-Inductive CFETR Scenarios with Larger Size Have Been Evaluated

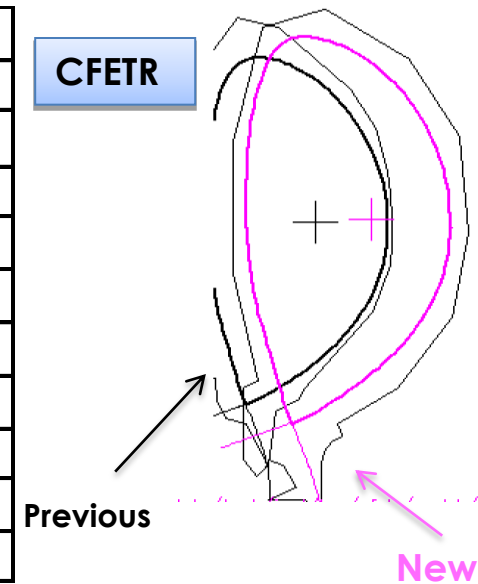
- Computed with self-consistent core-pedestal-equilibrium model under *OMFIT*

	Previous	Phase I	OD Phase I	Phase II	OD Phase II
R_0, a (m)	5.70 / 1.60	6.60 / 1.80	6.62 / 1.79	6.60 / 1.80	6.63 / 1.79
NBI Input Power (MW)	10, 58.5	13, 22.8	132	20.0, 14.3	62
NBI Voltages (keV)	100, 400	100, 500	/	100, 500	/
NBI Absorbed Power (MW)	59.3	32.2	/	33.9	/
EC Power (MW), Freq (GHz)	8, 170	20, 230	/	20, 230	/
EC Absorbed Power (MW)	8	19.8	/	20	/
Fusion Gain Q_{FUS}	2.0	3.0	1.5	14.9	16.4
Fusion Power P_{FUS} (MW)	149.5	169	200.4	811.0	1019.2
B_T (T), I_p (MA)	5.0, 10.0	6.0, 7.6	5.8, 7.5	6.0, 10.0	5.9, 10.0
NBI CD I_{NBI} (MA)	5.5	2.0	/	0.9	/
RF CD I_{RF} (MA)	0.3	0.8	/	0.6	/
Bootstrap I_{BS} (MA), Fraction f_{BS}	4.3 (43%)	4.8 (64%)	3.8 (50%)	8.4 (84%)	7.5 (75%)
Central T_{i0}, T_{e0} (keV)	23.5, 24.9	18.8, 25.3	12.7, 12.7	25.6, 33.5	21.7, 21.7
Central Density n_e ($10^{20}/m^3$)	0.80	0.80	1.2	1.4	1.6
Greenwald Density Ratio	49%	51%	82%	87%	81%
Z_{EFF}	2.1	2.0	2.0	2.0	2.4
β_N, H_{98y2}	1.90, 1.02	1.89, 1.32	1.60, 1.0	3.15, 1.34	2.81, 1.5
Neutron Wall Loading Γ_{NW} (MW/m ²)	0.22	0.19	0.21	0.92	1.03
Diverter heat loading P_{DIV}/R_0 (MW/m)	15.7	10.4	/	25.8	/



New Larger CFETR Reduces Heating and Current Drive Requirements, and Lower Divertor and Wall Power Loading

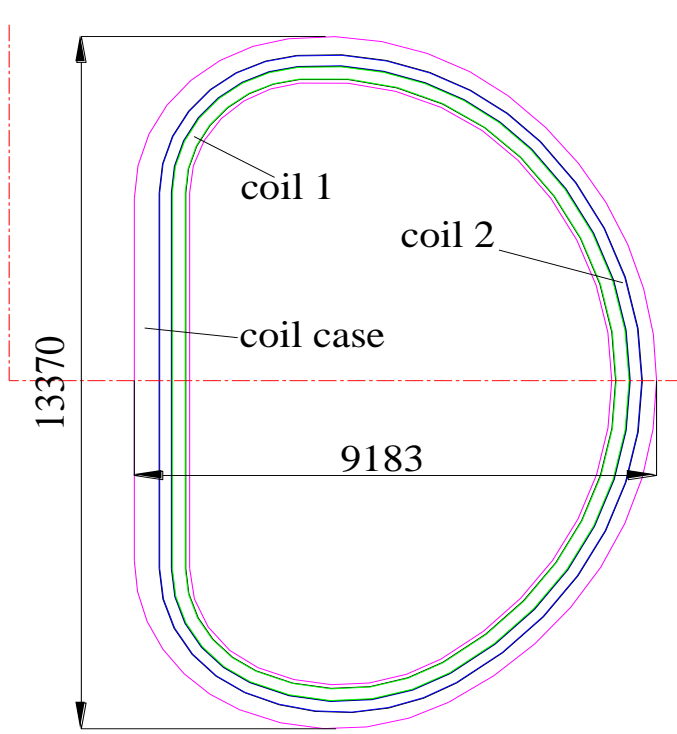
	Previous	New Phase I	New Phase II
R_0, a (m)	5.7, 1.6	6.6, 1.8	6.6, 1.8
P_{NBI}, P_{ECH} (MW)	68.5, 8.0	35.8, 20.0	33.9, 20.1
Fusion Gain Q_{FUS}	2.0	3.0	14.9
Fusion Power P_{fus} (MW)	150	169	811
B_T (T), I_p (MA)	5.0, 10.0	6.0, 7.6	6.0, 10.0
Bootstrap Fraction f_{BS}	43.3%	63.6%	84.4%
Normalized beta β_N	1.90	1.89	3.15
H_{98Y2}	1.0	1.3	1.3
Neutron Wall Loading Γ_{NW} (MW/m ²)	0.22	0.19	0.92
Divertor Loading P_{DIV}/R_0 (MW/m)	15.7	10.4	25.8



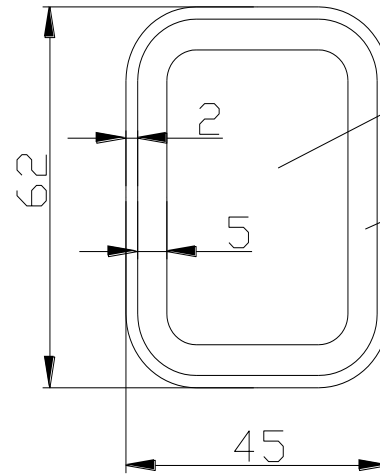
- Fully non-inductive CFETR scenarios have been developed with a self-consistent core-pedestal-equilibrium model
- New larger CFETR reduces heating and current drive requirements, lower divertor heat flux and neutron wall loading, higher bootstrap current fraction and H_{98y2} at similar β_N
- Higher $\beta_N \sim 3.2$ Phase II configuration requires a close conducting wall for $n = 1, 2$ ideal stability but for Phase I don't need the conducting wall



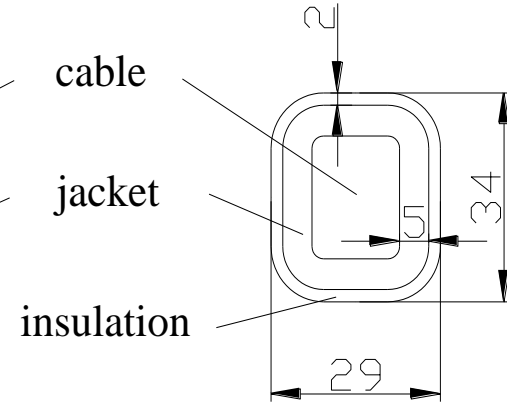
12 TF Coil design (High Performance Nb₃Sn)



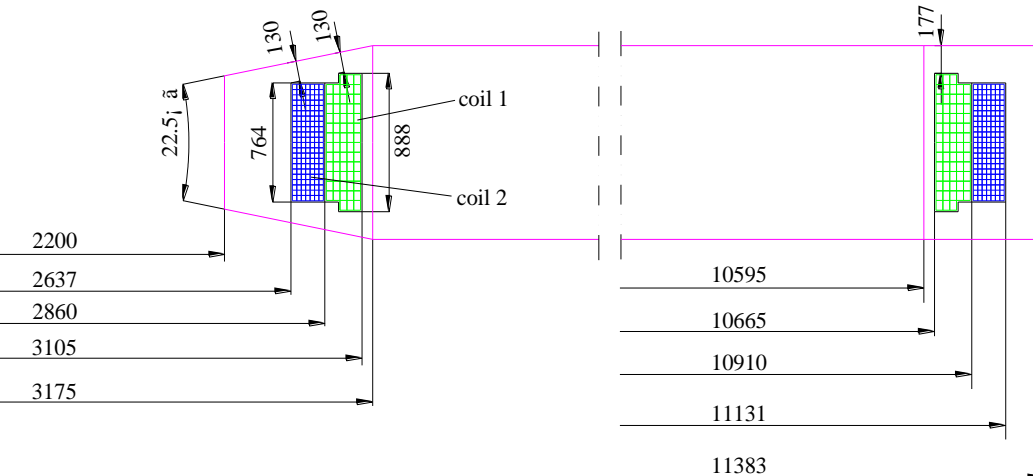
conductor for coil 1



conductor for coil 2



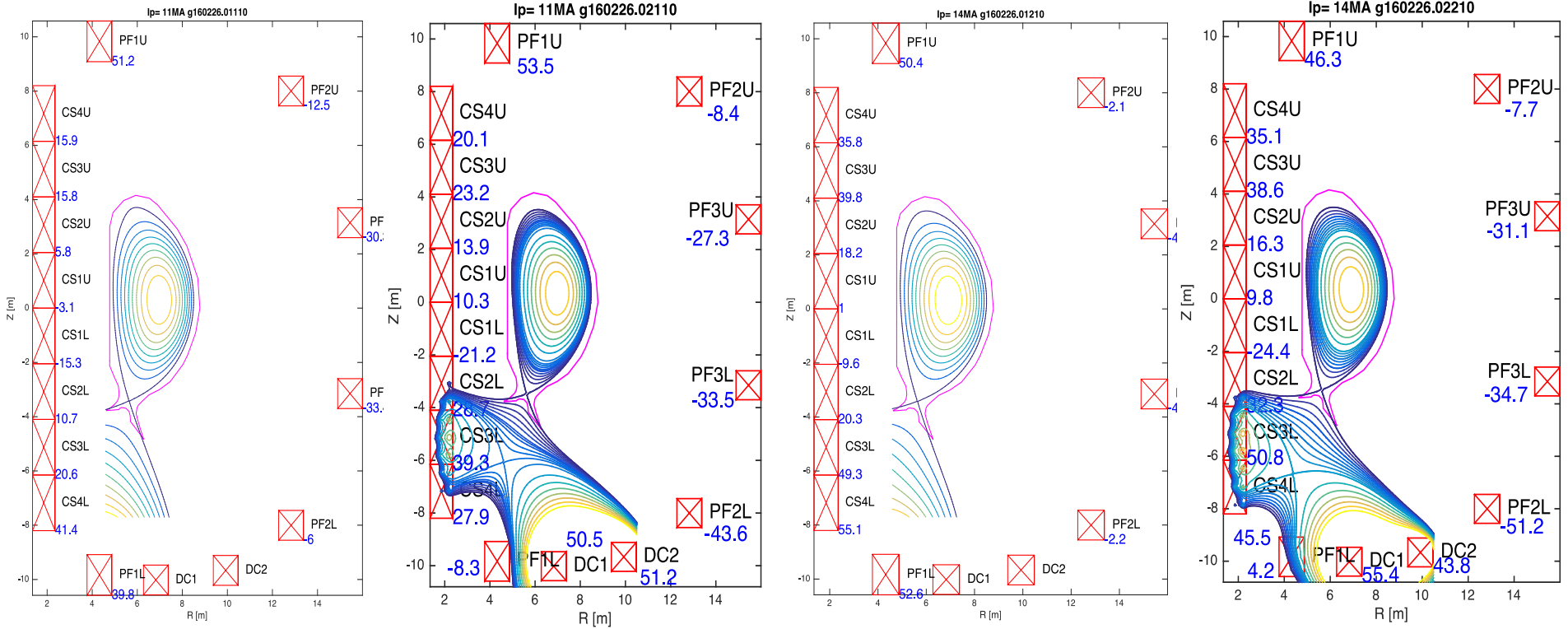
Parameters for TF magnet



Parameters	Coil 1	Coil 2
strand	high J_c (3000A/mm ²) Nb ₃ Sn Φ1.0mm strand	
No. of SC strand	1350	270
Turns	66	154
Operating current for $B_t=7.5T$	64.3kA	
B_{max} in coil	14.3T	11.4T
Max Force	643MPa	



Advanced plasma equilibrium shape



$I_p=11\text{ MA}$

$I_p=14\text{ MA}$

I_p [MA]	Type	R[m]	a[m]	β_p	ι_i	β_t	δ_u/δ_l	κ	q_{95}
11	Snowflake	6.72	1.76	1.59	1.02	0.025	0.33/0.63	1.99	3.9
14	Snowflake	6.72	1.75	1.1	0.95	0.024	0.33/0.63	1.99	3.3



Helium cooled ceramic breeder blanket design

Material section

- Li_4SiO_4 as tritium breeder
- Be as neutron multiplier.
- RAFM steel as structural material.
- Tungsten as armor material of the FW

Main features

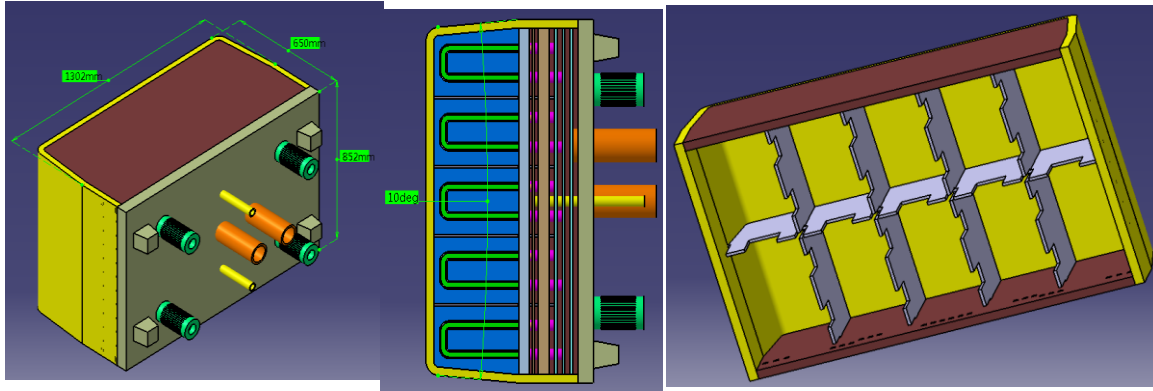
- Modularized breeding unit
- Multi-layer back plates manifold

Coolant : 8 MPa, 300 °C inlet/500 °C outlet

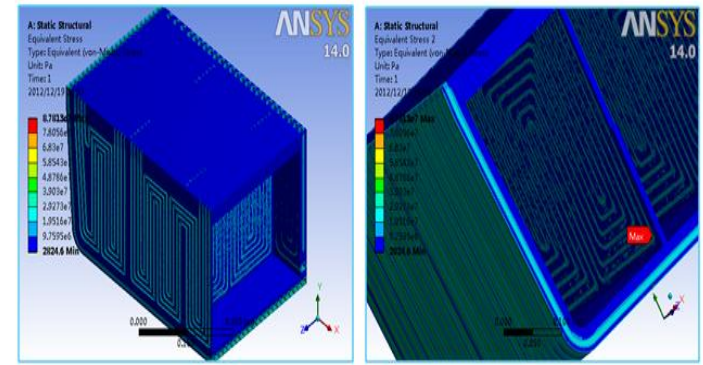
For Phase-I

5 (Tor.)×2 (Pol.) breeding unit, each has one U-shape breeder unit.

TBR: 1.213



Typical module structure

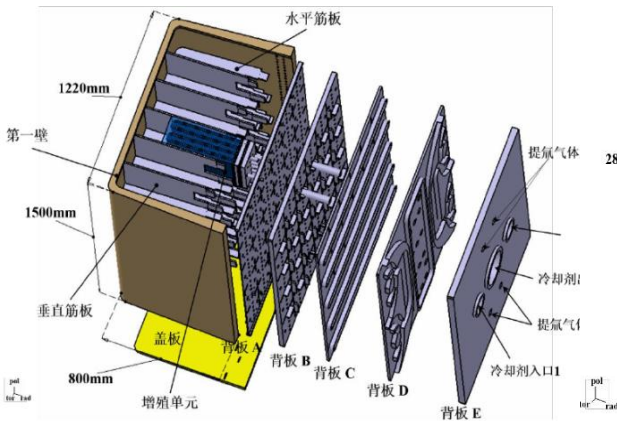


Stress analysis

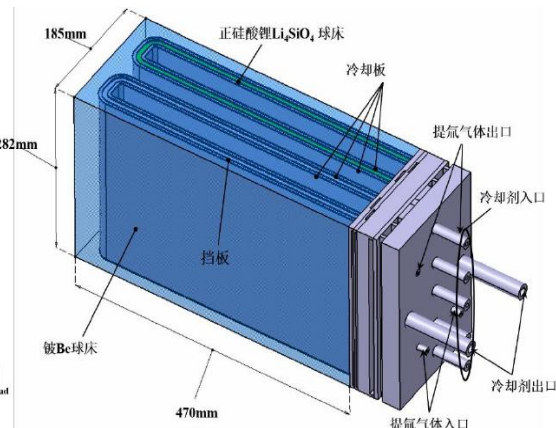
For Phase-II

6 (Tor.)×5 (Pol.) breeding unit, each has two U-shape breeder unit.

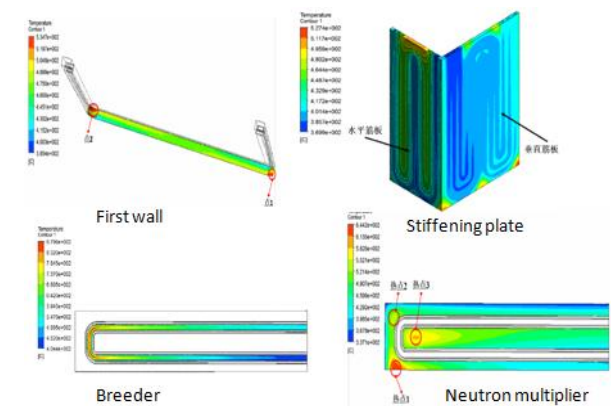
TBR: 1.15



Typical module structure



Modularized breeding unit



Temp. distribution



Water cooled ceramic breeder blanket design

Material section

Main features

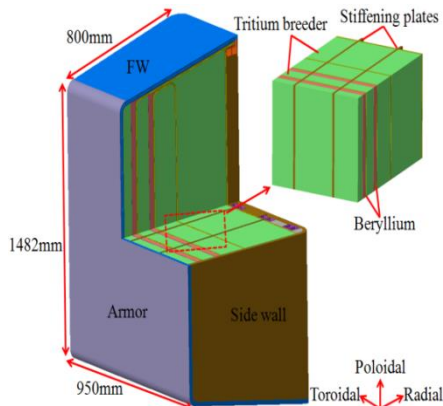
- Mixed breeder of Li_2TiO_3 and Be_{12}Ti
- A bit of Be to improve neutrons multiplying.
- RAFM steel as structural material.
- Tungsten as armor material of the FW

- **Coolant** : 15.5MPa, 285 °C inlet/325 °C outlet
- The cooling plates and the breeder zone parallel to the FW
- The compact coolant enlarges the breeder zone.
- Purge gas is directed in the toroidal direction to reduce its pressure drop.

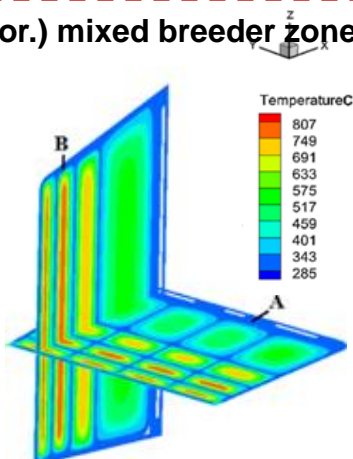
For Phase-I

4 (Rad.) \times 4 (Tor.) mixed breeder zones and 2 (Rad.) \times 4 (Tor.) thin Be layers

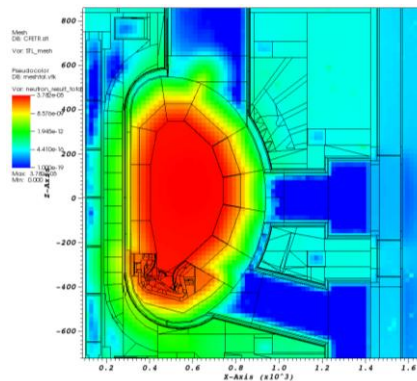
TBR: 1.21



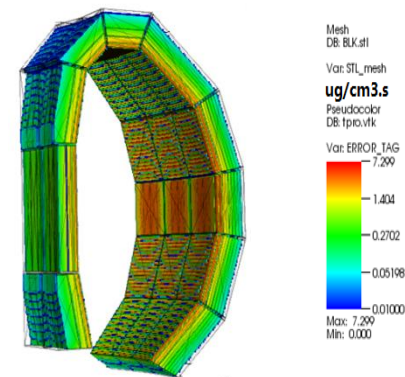
Module structure



Temp. distribution



Neutron flux distribution

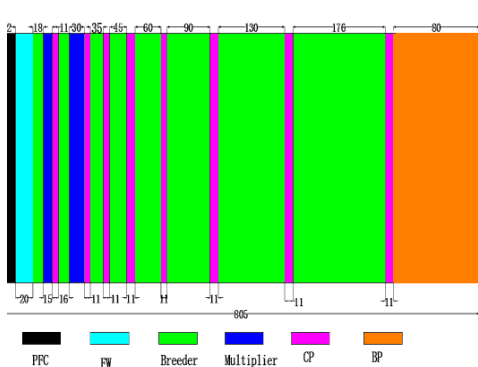


Tritium production rate (PF0.8, $^6\text{Li}80\%$ case)

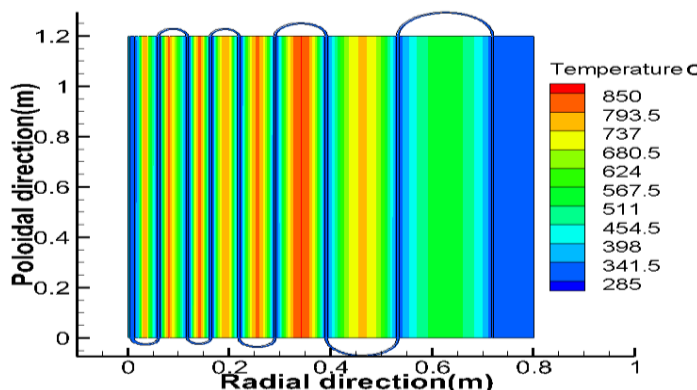
For Phase-II

8 (Rad.) \times 4 (Tor.) mixed breeder zones and 2 (Rad.) \times 4 (Tor.) thin Be layers

TBR: 1.1



Module radial building



Temp. distribution along radial direction

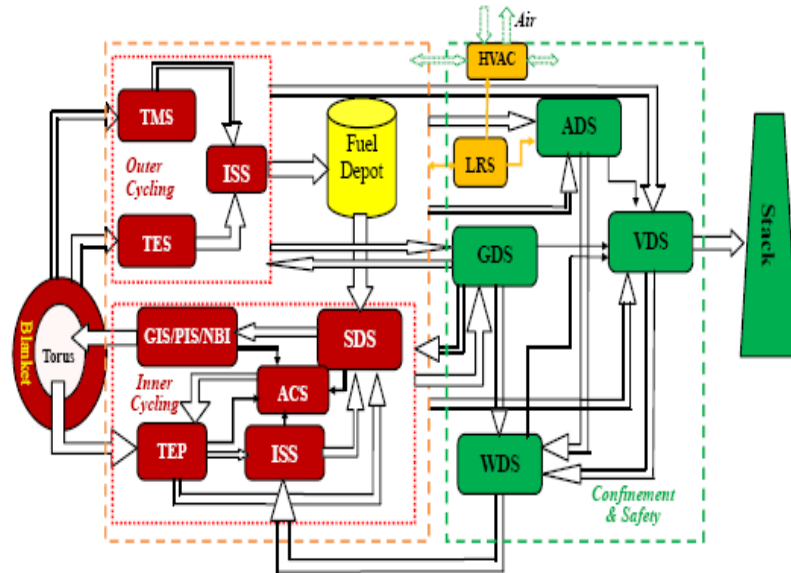
Shielding capability for TFC

Item	Limits	value
Fast neutron ($>0.1\text{MeV}$) fluence in TFC conductor (n/cm^2)	1×10^{19}	3.67×10^{16}
Fast neutron ($>0.1\text{MeV}$) fluence in TFC insulator (n/cm^2)	5×10^{17}	1.10×10^{17}
Nuclear heating rate in TFC case (W/cm^3)	2×10^{-3}	2.19×10^{-5}
Nuclear heating rate in TFC conductor (W/cm^3)	1×10^{-3}	1.88×10^{-5}

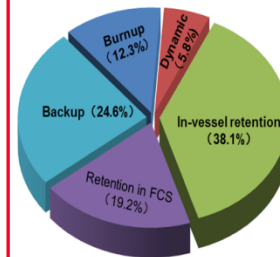


Tritium cycling systems (T-plant)

- 3 main loops for tritium recovery:
 - Inner cycling:
 - Tritium recovery, isotopic separation from plasma exhaust gases and re-fueling to torus.
 - Outer cycling:
 - Tritium extraction and measurement from in the full breeding blanket.
 - Tritium confinement and effluent detritiation.
- Main parameters for tritium process flow (4500s of time span for cycling):
 - Inner cycling: $\sim 357\text{g T/shot}$, $2\text{m}^3 (\text{D}_2, \text{T}_2)/\text{h}$ for TEP and SDS, $>4\text{m}^3/\text{h}$ for ISS.
 - Outer cycling: tritium extraction every two weeks to get more than 200g of pure tritium from the breeders.
 - Tritium confinement: 3g/a of environmental tritium release at current stage, to be minimized as 0.6 g/a for the future.
- Key technologies development for each sub-system are in progress



Simple block diagram of CFETR tritium plant



The makeup of startup tritium for CFETR.

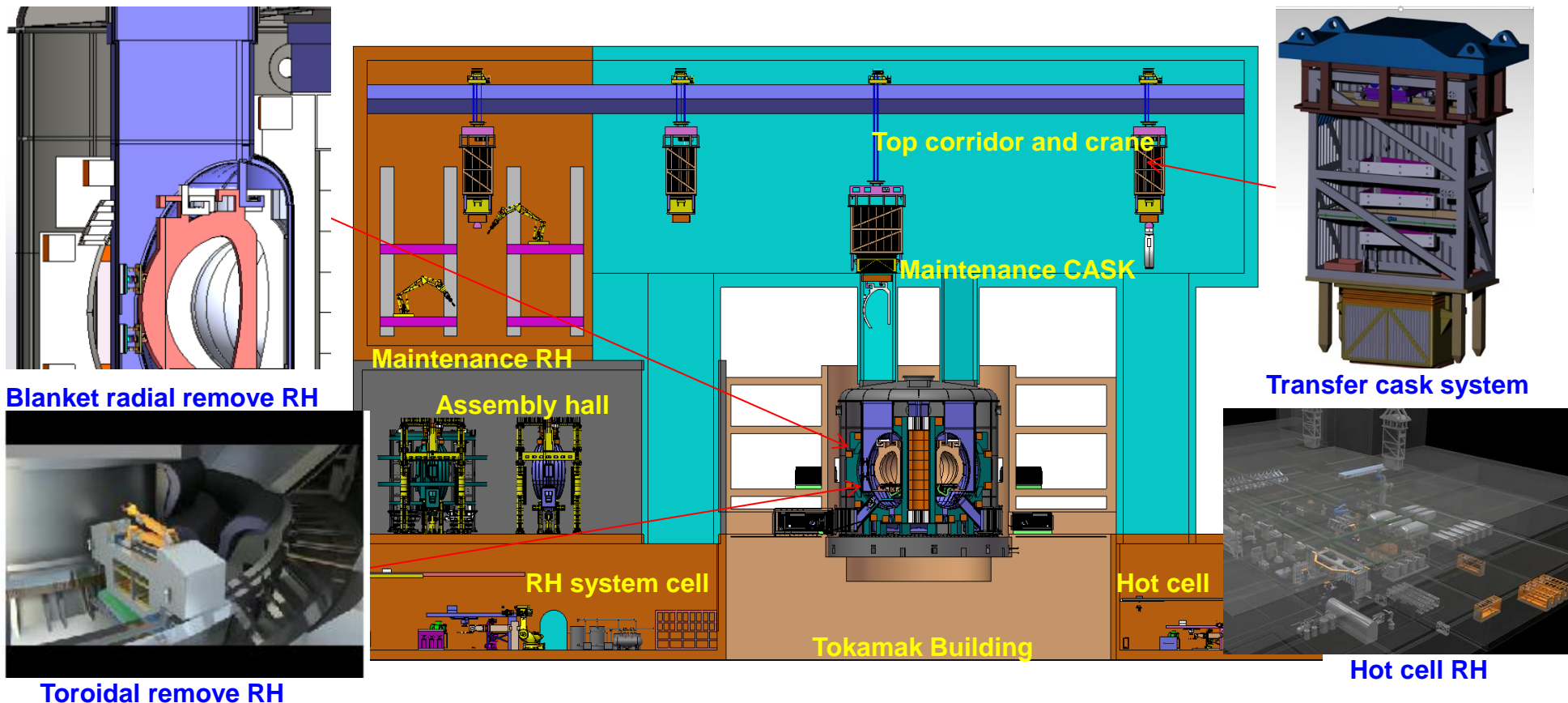
Burnup (g)	Dynamic (g)	In-vessel retention (g)	Retention in FCS (g)	Backup (g)	Total (g)
226	107	661	353	452	1799

Totally, CFETR may need around **2 kg** of tritium for startup.



RH strategy of CFETR

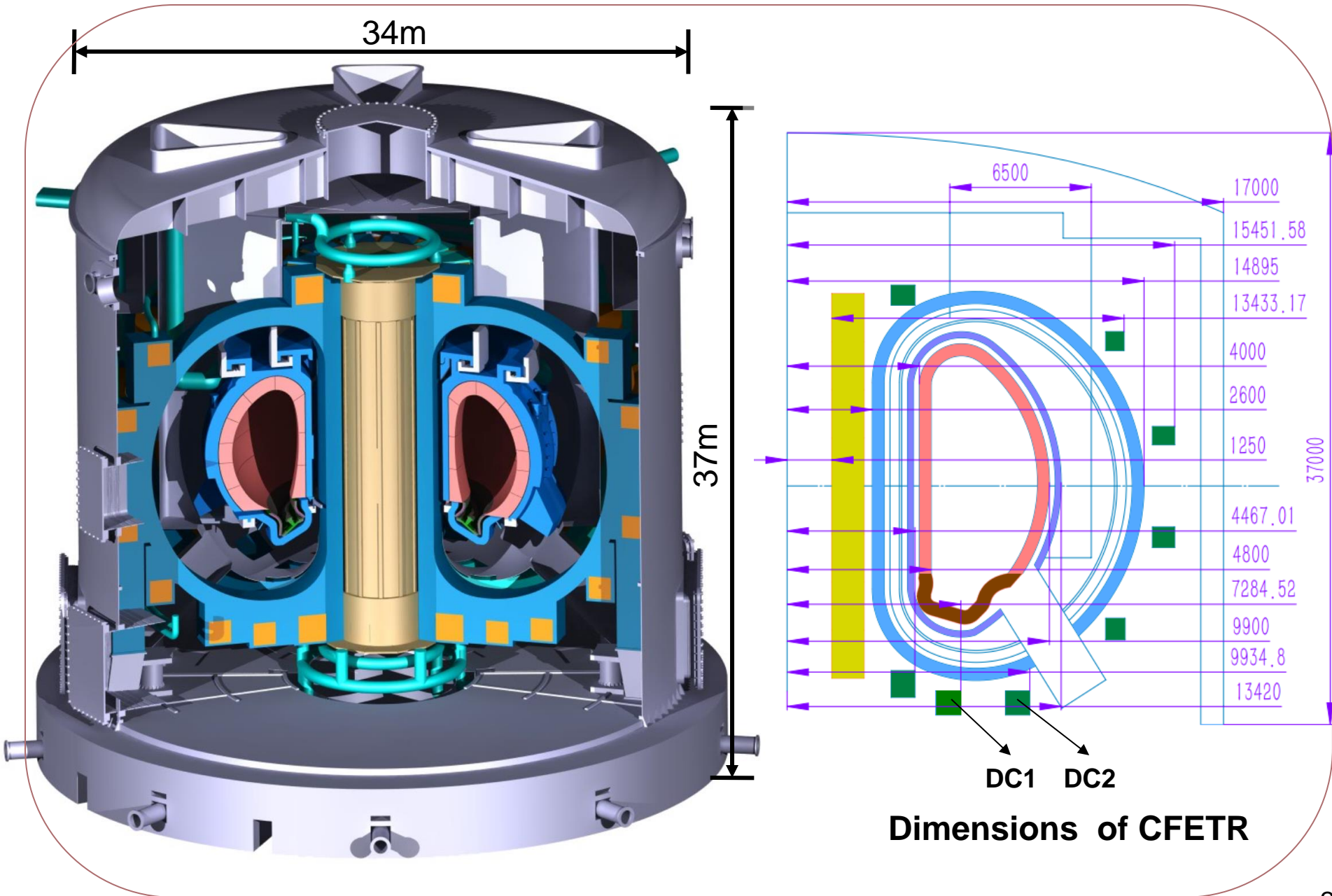
RH strategy plays the key role for the CFETR's high efficiency and reliability maintenance. The **vertical port maintenance scheme** with multi-module segment blanket and divertor was preferred for in-vessel components maintenance. It will make the RH simpler and more efficient.



The vertical port maintenance scheme for in vessel components



New Design version of CFETR

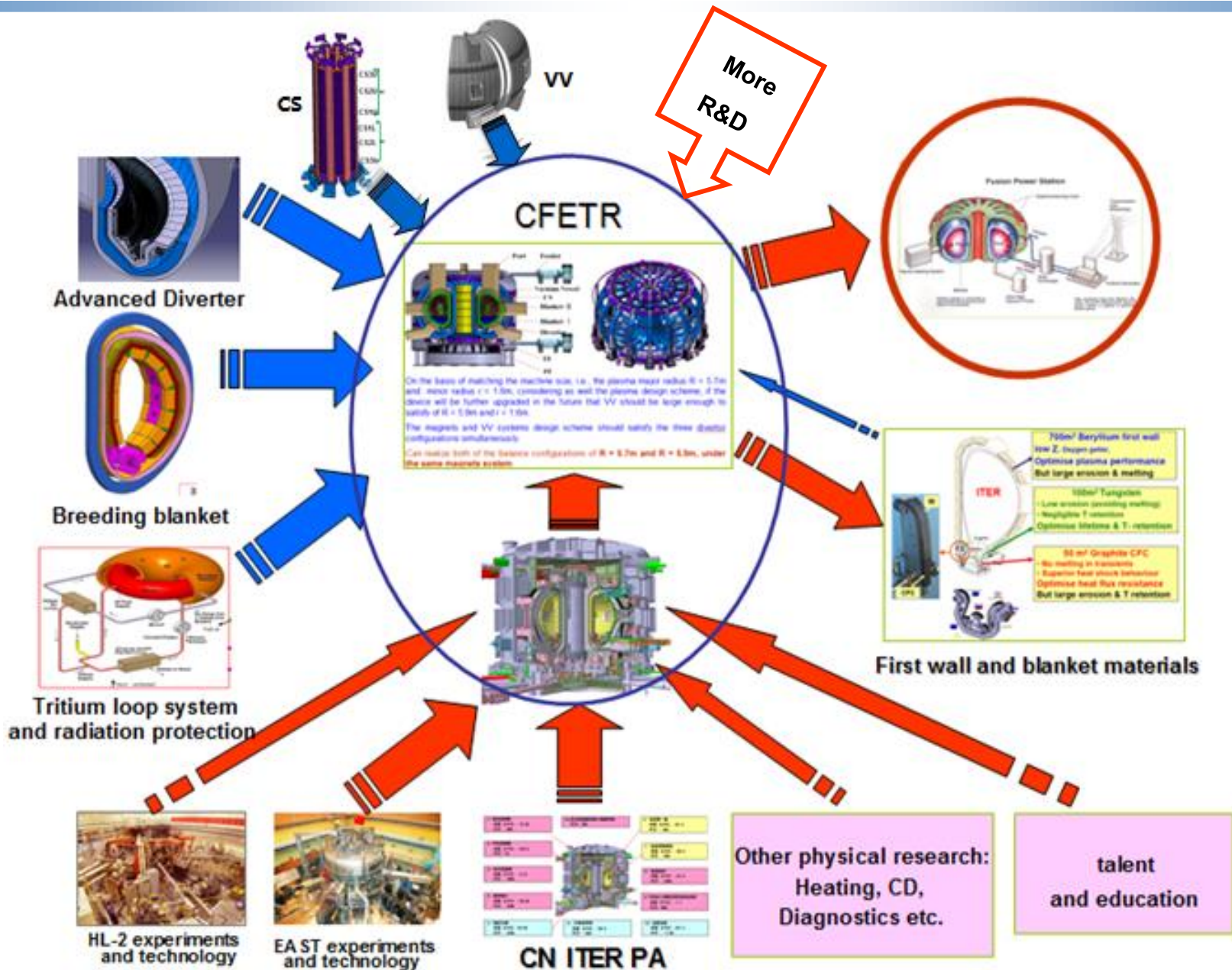




- **Introduction**
 - **CN MCF Roadmap**
 - **Mission of CFETR**
- **Progresses and activities of CFETR**
 - **Previous concept design**
 - **New design version**
 - **Phase I**
 - **Phase II**
- **Key R&D activities**
- **Summary**



R&D strategy of CFETR





Other important R&D for CFETR

- **Auxiliary Heating & CD:**
 - ✓ **Off-axis NBI (0.8MeV) + ECRH (top , 190 , 230GHz)**
 - ✓ **LHCD (HF , 4.6GHz) + ECRH (top , 230GHz)**
- **Advanced Superconducting Magnet**
 - TF (Nb₃Sn, 7.0 T); CS (Bi 2212 CICC)**
- **Advanced Divertor (X-Divertor, >20MW/m²)**
- **Blanket (He gas, water cooled)**
- **T-Plant (99.9% T recovery)**
- **Materials (First wall, structure)**
- **RH**



R&D for RF Sources

LHW:

EAST: 2.45GHz, 200kW, CW

4.6 GHz, 0.3MW, CW

CFETR: 4.6 GHz, 0.3-0.5MW, CW

7.5GHz, 0.5MW, CW



2.45GHz, 200kW



4.6 GHz, 0.3MW



140GHz, 1MW, CW

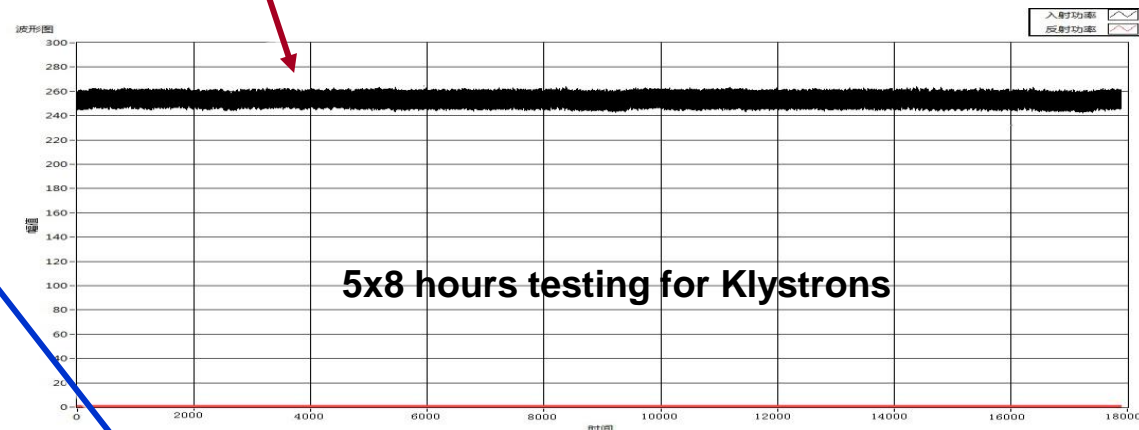
EC:

EAST: 140GHz, 1MW, CW

170GHz, 1MW, CW

CFETR: 170GHz, 1MW, CW

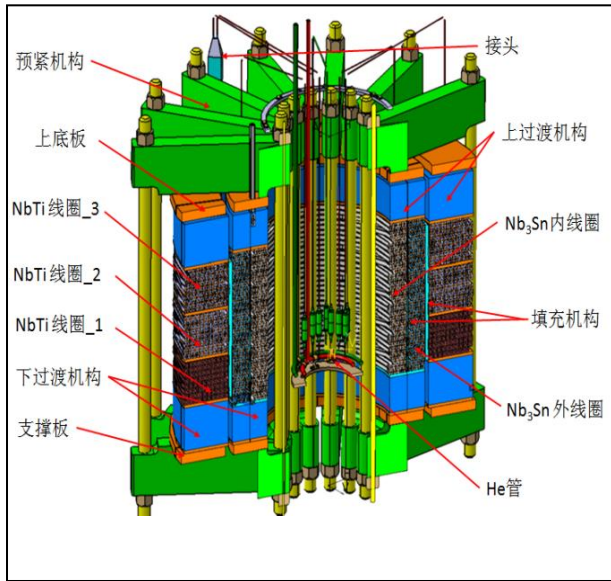
230GHz, 1MW, CW



Gyrotron: Start commissioning @ 2016.12



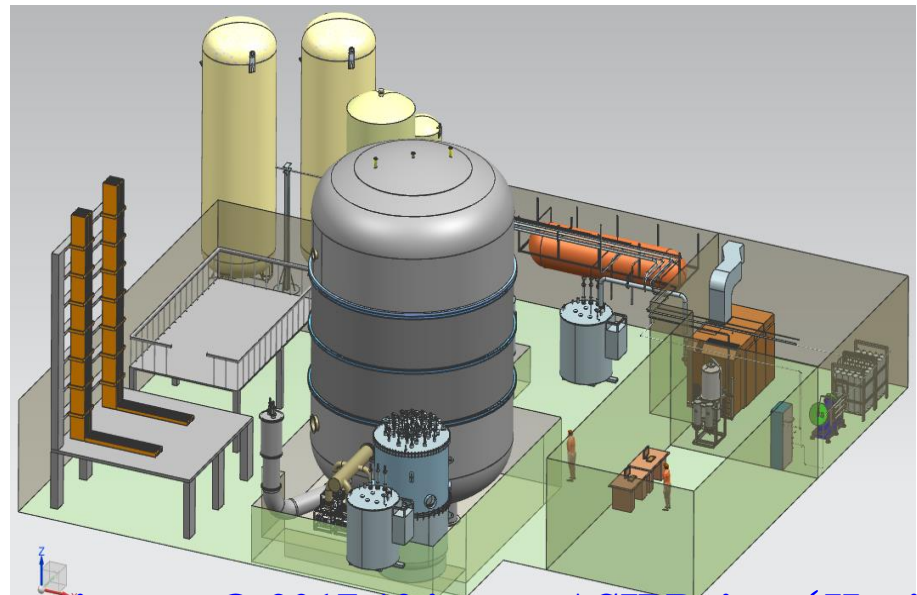
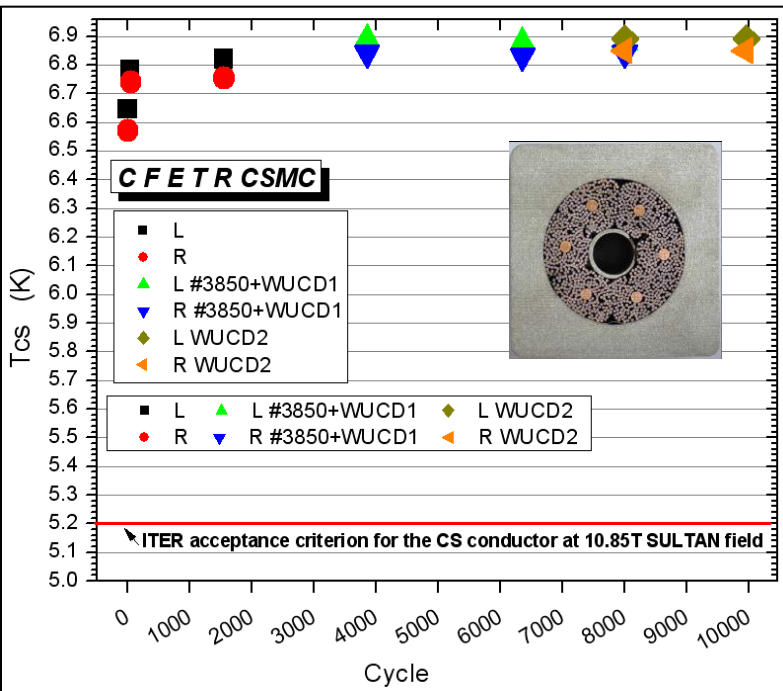
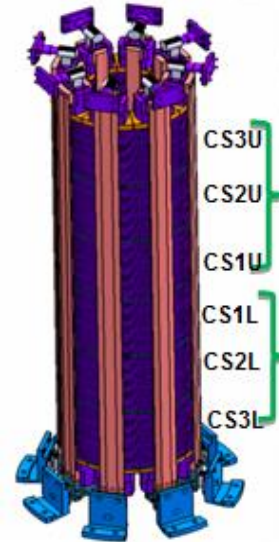
CS Model Coil –Nb₃Sn (baseline)



Coil Parameters

Design Parameters of CFETR CS Model Coil

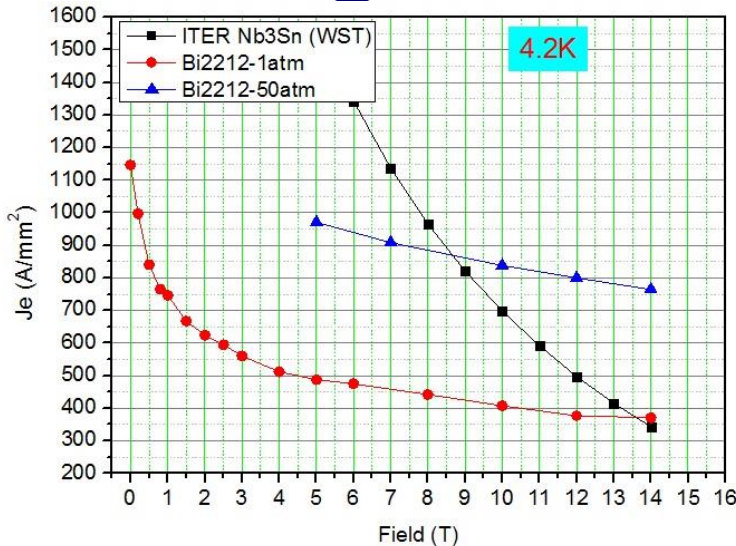
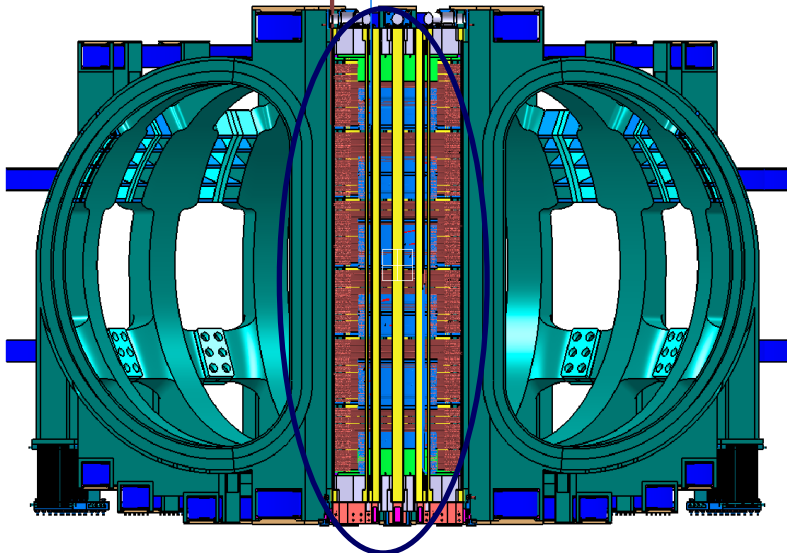
Max. field	12 T
Max. field rate	1.5 T/s
Inner radius	750 mm
Coil structure	Hybrid magnet Inner: Nb₃Sn coil
Conductor type	Nb ₃ Sn CICC



Start experiments @ 2017.12 in new ASIPP site (Huainan)

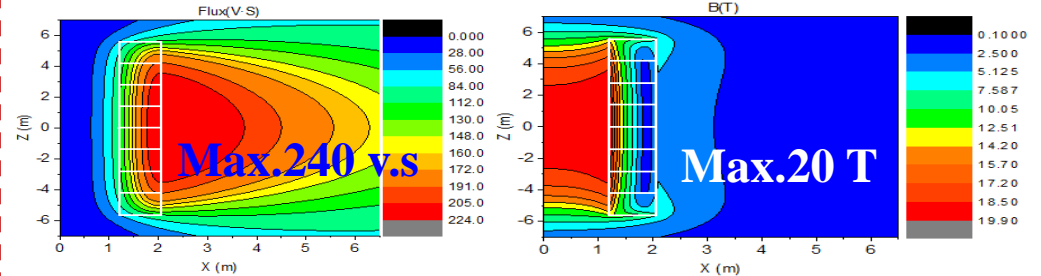


CS Model Coil (1/3 size) – 2212 CICC (Target)

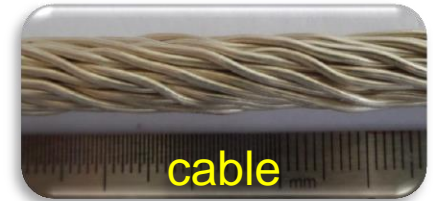
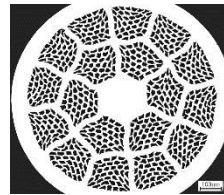


Bi2212-High temperature Superconducting Central solenoid

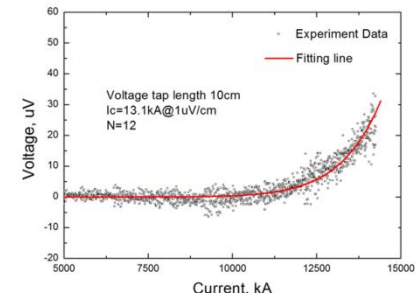
CS coils include eight Bi2212 coils. Each coil consists of 14 double pancake



Conservative: enhanced Nb₃Sn: 360VS 4-6h
Ideal: 2212CICC, 480VS, ~8h (for Ip=10MA)

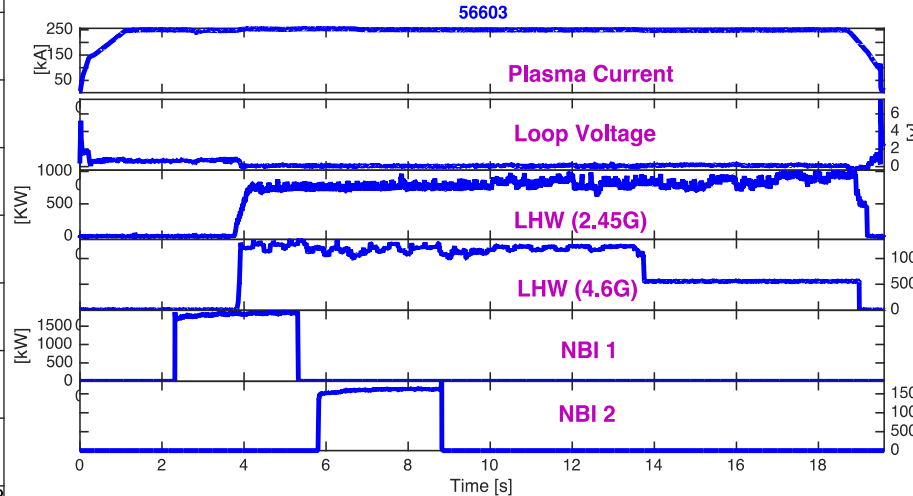
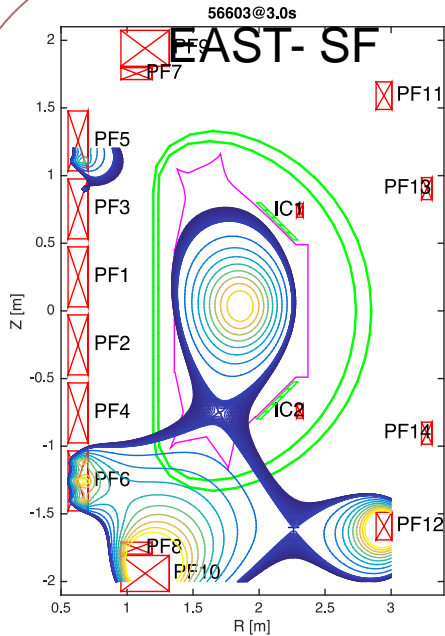


Batch production for 200-m long $\Phi 1.0$ mm wires
4.2K, 14T: $J_{ce} > 750$ A/mm², ITER~ 320A/mm².
4.2K, 20T: $J_{ce} > 660$ A/mm², ITER ~ 200A/mm².
high pressure sintering process is on the way,
 J_c -B property may be increased for 3 times.

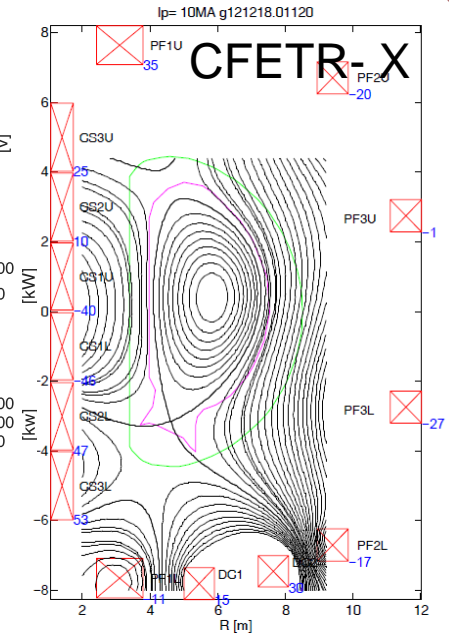




New Divertor validation



Joint Exp.with ENEA



Physics: field expansion + radiation; Reduce the heat detail simulations (5y) + experimental validation (5-8y)

Engineering : design & manufacture of key components

W mono-block: $> 20\text{MW}/\text{m}^2$

W-Cu mono-block : $> 20\text{MW}/\text{m}^2$ (5-10y)

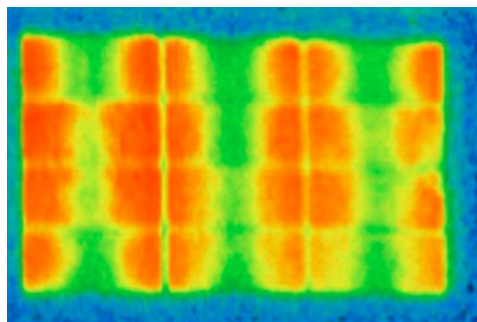
Inner+external coils optimization is underway up 15MA (**12MA**)



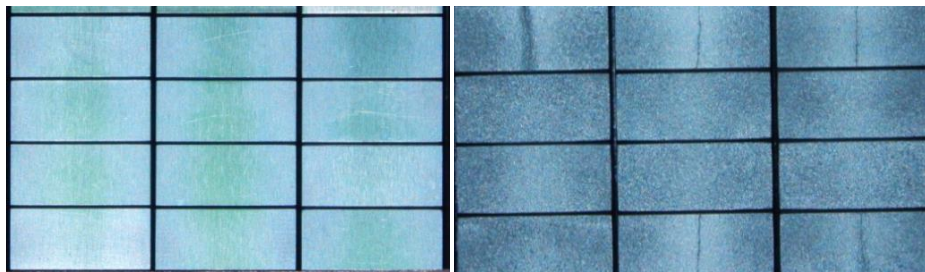
R&D for Divertor Target



Monoblock W/Cu
5000 cycles at 10MW/m²
300 cycles at 20MW/m².



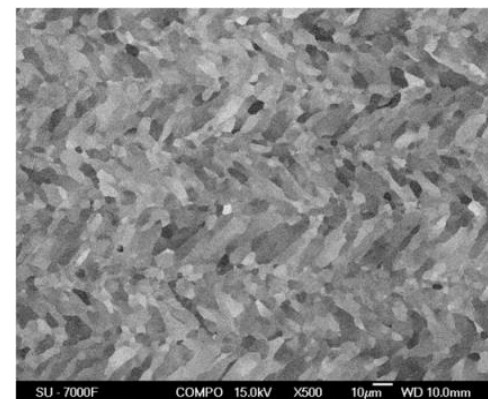
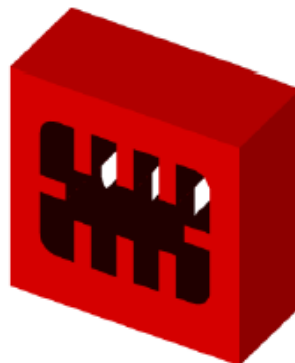
Flat tile W/Cu



5000 cycles
at 10MW/m²

1000 cycles
at 20MW/m²

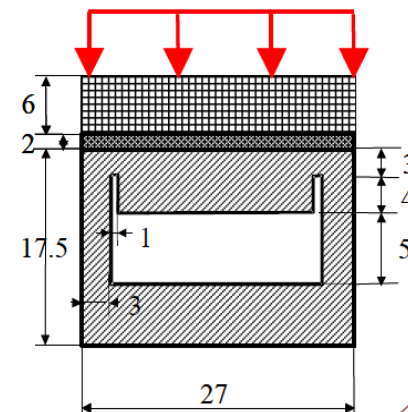
Efforts for 30MW/m²



3D printing full W block: Tw=1700C

Flat tile

W/ODS-Cu
Tw = 1650C
Tcu = 520C





CFETR T-plant technologies

1 Tritium handling technologies

- ✓ Tritium purification
- ✓ Hydrogen isotope separation
- ✓ Tritium removal/recovery in tritiated gases



Integrated hydrogen permeation



Cryogenic Distillation

2 Tritium Analysis and Monitoring

- ✓ Tritium on line detection by gas chromatograph
- ✓ Radiometric analysis



Solids contained tritium desorption and collection



3 Tritium safety techniques

- ✓ Atmospheric detritiation
- ✓ Water detritiation
- ✓ Tritium permeation barrier



D.S. for inert gas Metallic getter approach

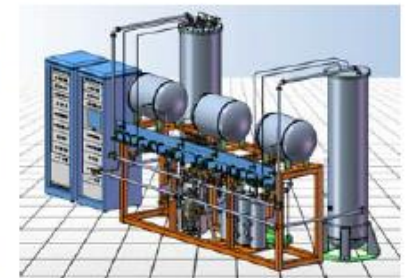
TRITIUM SYSTEM

4 ITER TBM tritium systems

- ✓ Tritium Extraction System (TES)
- ✓ Coolant purification system (CPS)
- ✓ Tritium measurement system (TMS)



(CPS)

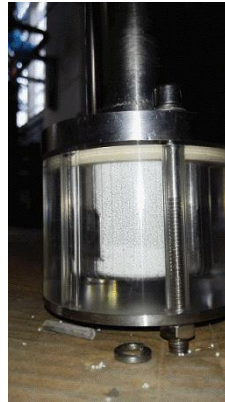
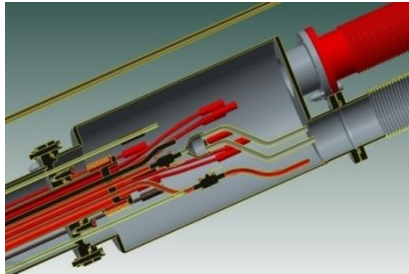


(TES)



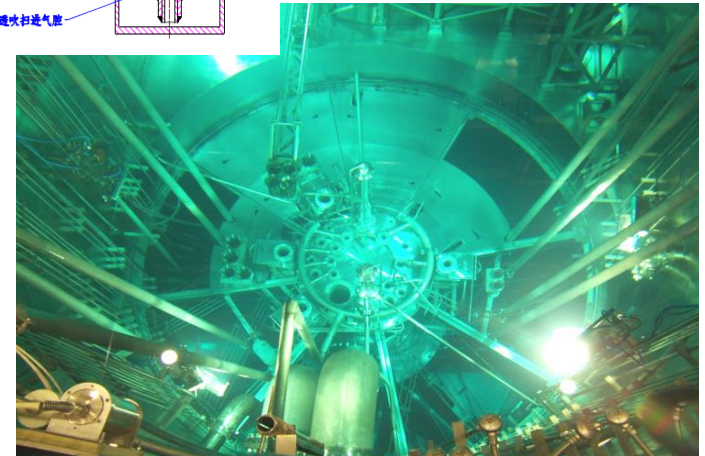
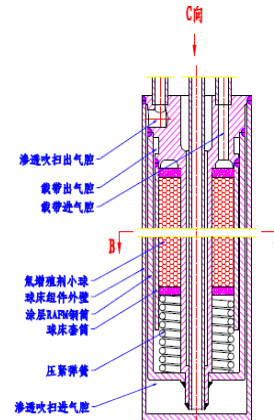
In-Pile Tritium Release and Extraction Test

Maximum load 500 g
Tritium production 1 Ci/day
Online refueling, irradiation
Irradiation temperature 300-750 °C
Neutron flux $\sim 5 \times 10^{13} \text{ n cm}^{-2} \text{ s}^{-1}$



China Mianyang Research Reactor

Maximum load 400 g
Tritium production 1 Ci/day
Online thermal conductivity test
Irradiation temperature 400 ~ 850 °C
Neutron flux $\sim 5 \times 10^{13} \text{ n cm}^{-2} \text{ s}^{-1}$



China Advanced Research Reactor



Materials Research Activities

(Simulation, manufacture, validation)

Low Activation Martensitic steel

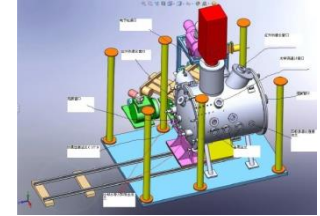
- Nominal compositions: 9Cr1.5W0.2V0.15Ta0.45Mn0.1C
- 5 ton smelting with good control of main compositions

Irradiation properties and TBM Fabrication

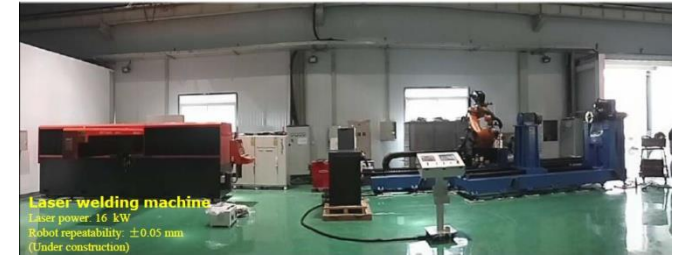
- High-dose neutron irradiation experiments
 - (Spallation source ~20dpa)
 - (High Fluence Engineering Test Reactor ~2dpa)
- Fabrication of test blanket module (TBM)
 - (1/3 scale P91 TBM, 1/3 scale CLAM first wall)



HIP(0.8x1.8m)



400kW EM facility



Laser welding machine
Laser power: 16 kW
Robot repeatability: ±0.05 mm
(Under construction)

15kW laser welding (0.05mm)

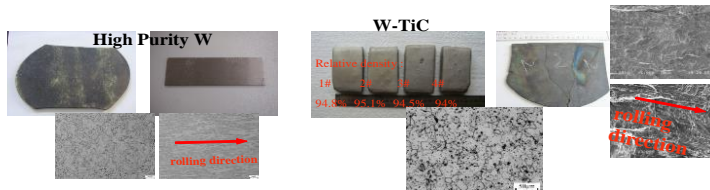
Plasma-facing materials: W

W material study scope: W alloy; W coating; W/Cu component

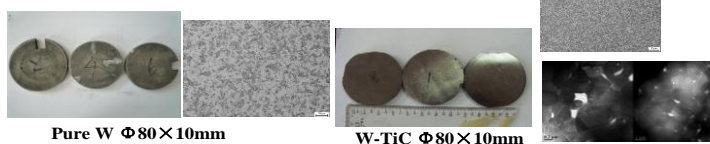


High heat-flux test facility

Conventional Powder Metallurgy Samples: High Purity W, W-TiC



SPS Samples: Pure W, W-TiC, W-La2O3

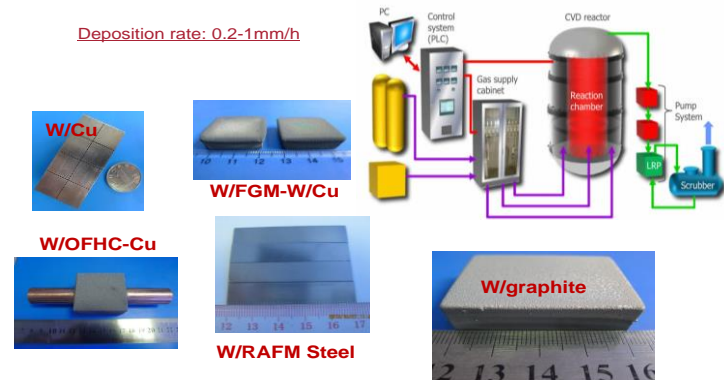


Pure W Φ80×10mm

W-TiC Φ80×10mm

(Chemical vapor deposition) CVD-W

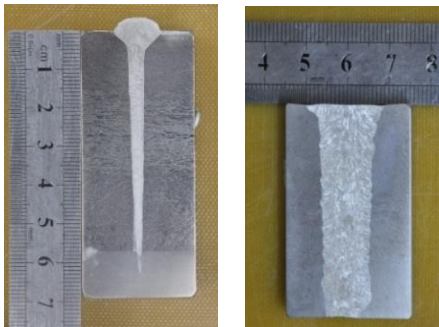
Deposition rate: 0.2-1mm/h



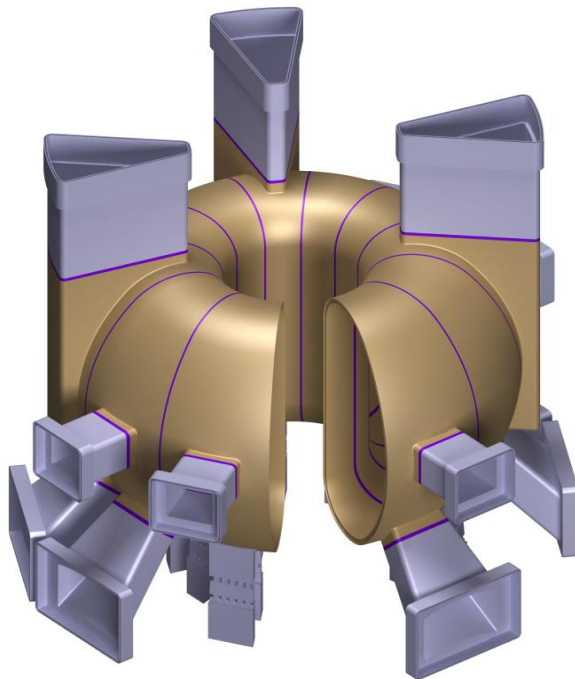


R&D on VV 1/8 mock-up

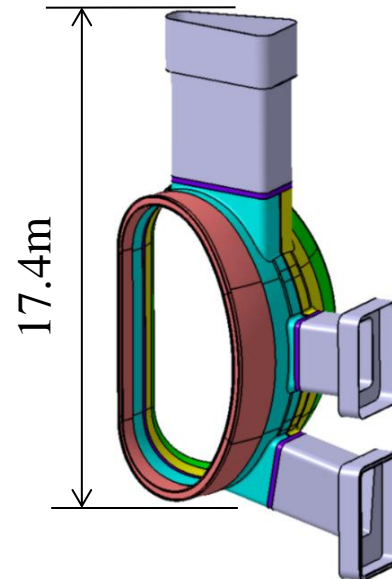
NG-TIG system



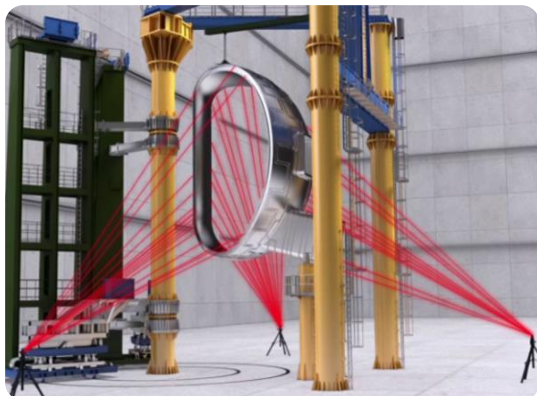
Welding samples



Overview of CFETR VV Design



Test bench for installation ,
replacement of
VV components by RH



Laser Tracker Measurement on VV Sector



R&D of Narrow Gap TIG Welding on VV



Assembly of VV Poloidal Sectors



CFETR 5 years Plan

- **Self-consistent, reliable physical design** (V.Chan)
- **Detailed engineering design** (main machine and auxiliary systems)
- **R & D for some key technologies and systems**
 - (I): Blanket related to nuclear, thermal hydraulic processes
 - (II): **magnets**、**T- factories**、**NBI**、**ECRH**、**RH**
 - (III): **Experimental verification**, diagnosis, control, divertor, cryogenic, ICRF, radiation protection, assembly and so on.



Further working Plan of CFETR

- Re-organize the design team by Drs. Li, Liu and Wang



J.Li



Y.Liu



X.L.Wang

- Promote both domestic and international collaboration more wide **on design, R&D, and construction of CFETR**



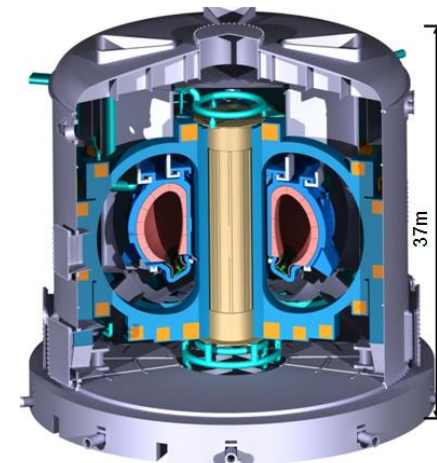
J.Li

“CIC” Director



V.Chan

Division head of fusion plasma physics





International cooperation

- **PPPL -CFETR team, H. Nielson, T.Bown, P.Titus, C.Kessel, A. Khodak.**
- **GA-CFETR team, L. Lao, R. Boivin, J. Candy, X. Chen, R. Prater, M.Christopher, A. Garofalo, O. Meneghini, M. Vanzeeland, P.B. Snyder, S.P.Smith, G.M. Staebler, E.J. Strait, and D. Zhao**
- **Useful discussion and suggestion from CFETR -IAC, CFETR Physics group IAC**
- **EU-DEMO team : (CCFE : SYScode, ENEA: Blanket, Julich: Diagnostic&Control, CCFE: RH, EPFL: H&CD, ENEA: Divertor, Julich: FM materials)**



Summary

- **Integrated Design and R&D of CFETR are in progress**
- **CFETR is moving to Phase II design of the new version with emphasis for high B_T option**
- **There are gaps to CFETR readiness, especially for phase II , need new solution and technologies.**
- **Detail engineering design and large scale R&D will continue in next 5 years.**
- **It is hoped that the proposal for CFETR construction can be approved by government within next 5 years finally**



End and Thanks!

26th IAEA Fusion Energy Conference, Kyoto, Japan 17–22 October 2016