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Summary

- A self-consistent fluid drift-neoclassical model has been implemented in the XTOR-2F full MHD code [1,2]
 - Recovers standard neoclassical theory at equilibrium
 - Evidence of island filamentation at low dissipation
 - Bootstrap contribution mitigated by ExB flow
- Island control by ECCD is modelled [5,6]
 - Stabilization efficiency vs source width & misalignment
 - Flip instability and RF-driven island (if 3D source & no rotation)
 - Control strategies mitigating misalignment & broad source

Drift-neoclassical model and insights on NTM drive

Nonlinear MHD code XTOR-2F [1] : drift fluid 3D full MHD in a torus.
Neoclassical model [2] : ion flow and bootstrap arise from friction forces

$$\rho(\partial_t + \mathbf{V} \cdot \nabla) \mathbf{V} = -\rho \mathbf{V}_i^* \cdot \nabla \mathbf{V}_\perp + \mathbf{J} \times \mathbf{B} - \nabla p - \nabla \cdot \Pi_\parallel + \nabla \cdot \nu \nabla \mathbf{V}_i$$

$$\mathbf{E} + \mathbf{V} \times \mathbf{B} = \eta[\mathbf{J} - \mathbf{J}_{bs} - \mathbf{J}_{CD}] - d_i \frac{\nabla_\parallel p_e}{\rho}$$

$$\mathbf{J}_{bs} = \frac{\eta - \eta_{SP}}{\eta} \left[\mathbf{J}_\parallel + \frac{d_i}{\rho} \frac{3/2\pi\epsilon_e}{(\eta - \eta_{SP})} \nabla \cdot \mathbf{b} - \alpha_e \frac{d_i}{\eta - \eta_{SP}} \sum_s \Lambda_{12}^{es} \frac{u_{2\parallel,s}}{B} \right] : \text{bootstrap current}$$

$$\Pi_\parallel = \frac{3}{2}\pi_\parallel \left[\mathbf{b}\mathbf{b} - \frac{1}{3}\mathbf{I} \right] : \text{stress tensor in CGL form}$$

$$\frac{3}{2}\pi_{\parallel,s} = -\rho\alpha_s\mu_s C \left\{ \left[\mathbf{V}_s + k_s \left(\mathbf{V}_{Ts}^* + \frac{u_{\parallel,2,s}}{B^2} \mathbf{B} \right) \right] \cdot \nabla \ln B + \frac{\mathbf{b}}{B} \cdot [\nabla \times (\mathbf{V}_s \times \mathbf{B}) + k_s \nabla \times (\mathbf{V}_{Ts}^* \times \mathbf{B})] - k_s \mathbf{V}_{Ts}^* \cdot \nabla \ln p_s \right\} : \text{pressure anisotropy } (p_\parallel - p_\perp)$$

Main properties

- Equilibrium flux averaged bootstrap current consistent with neoclassical theory [3]
- Agrees with analytical estimates [4]; contribution from parallel heat flows [fig.1]
- Non linear saturation is bursty at low dissipation (χ, ν) [fig.2]
- Island shape : droplet like due to drift physics [fig.3]

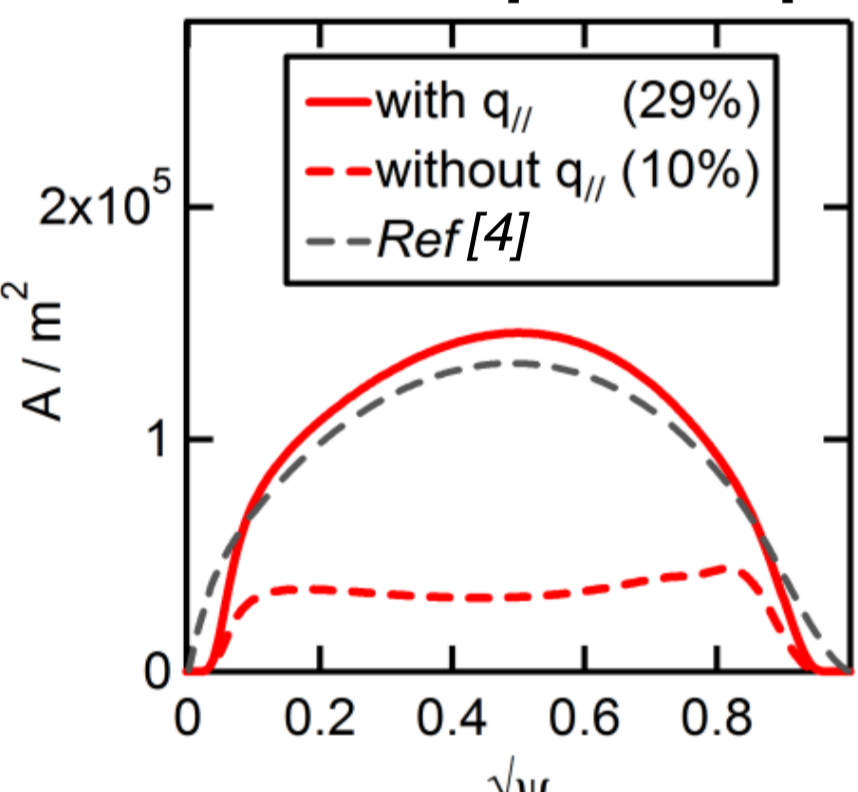


Fig.1 : Flux averaged bootstrap current

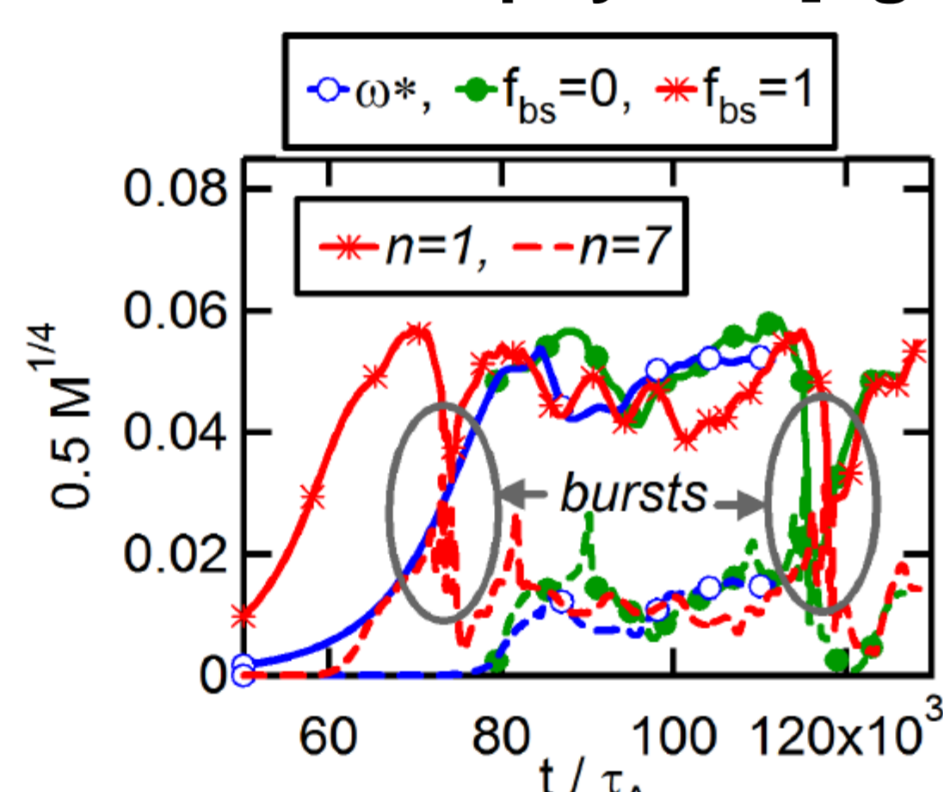


Fig.2 : Island size; bursty behaviour at low χ, ν with neoclassical model.

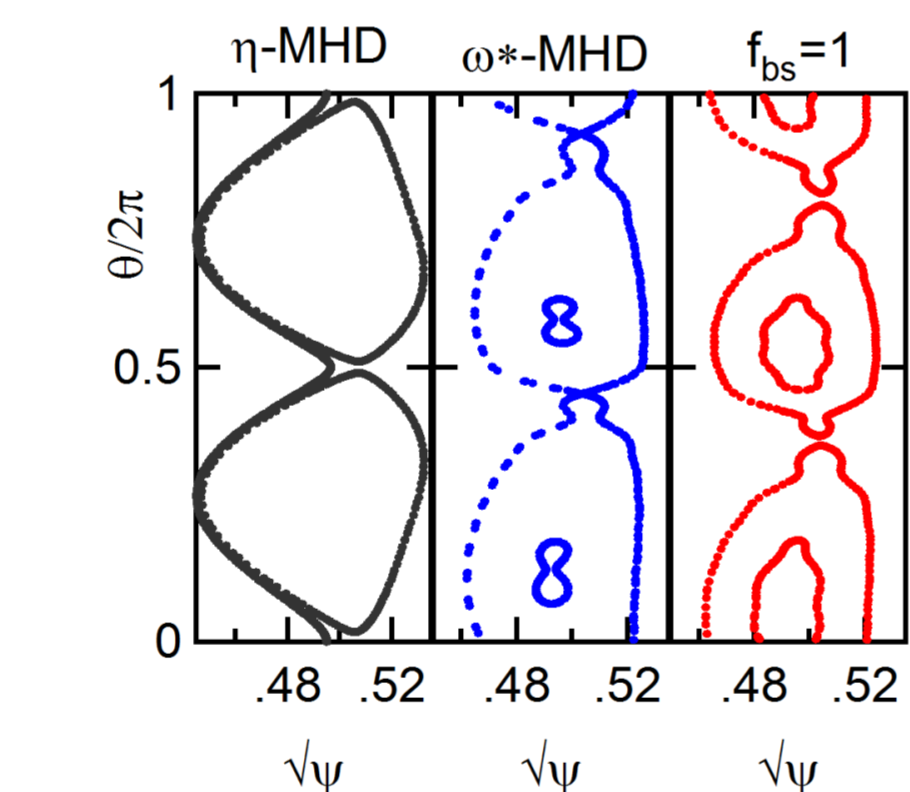


Fig.3 : Island shape with resistive, drift and neoclassical MHD models.

Comparison with Rutherford approach

- Effect of bootstrap current on saturation mitigated by ExB flow perturbation
- Measured by correlation $R_{bs}(p)$ between bootstrap and pressure perturbations
- Correlation $R_{bs}(p)$ increases with neoclassical friction μ_i and with island size [fig.4]
- In Rutherford representation, $f_{bs} [=1 \text{ for reference case}]$ replaced by $R_{bs}(p)/f_{bs}$
- Still weaker effect compared with Rutherford prediction, even for an ad-hoc implementation of the bootstrap $\mathbf{J}_{bs} \sim \nabla p$ where $R_{bs}(p)=1$

Application to Neoclassical Tearing Mode triggering on Asdex-Upgrade equilibrium

- Correlation $R_{bs}(p)$ varied by changing χ_{\parallel} (~pressure flattening inside the island)
- (3,2) NTM could be triggered for a seed $W_{seed} \sim 4\%$

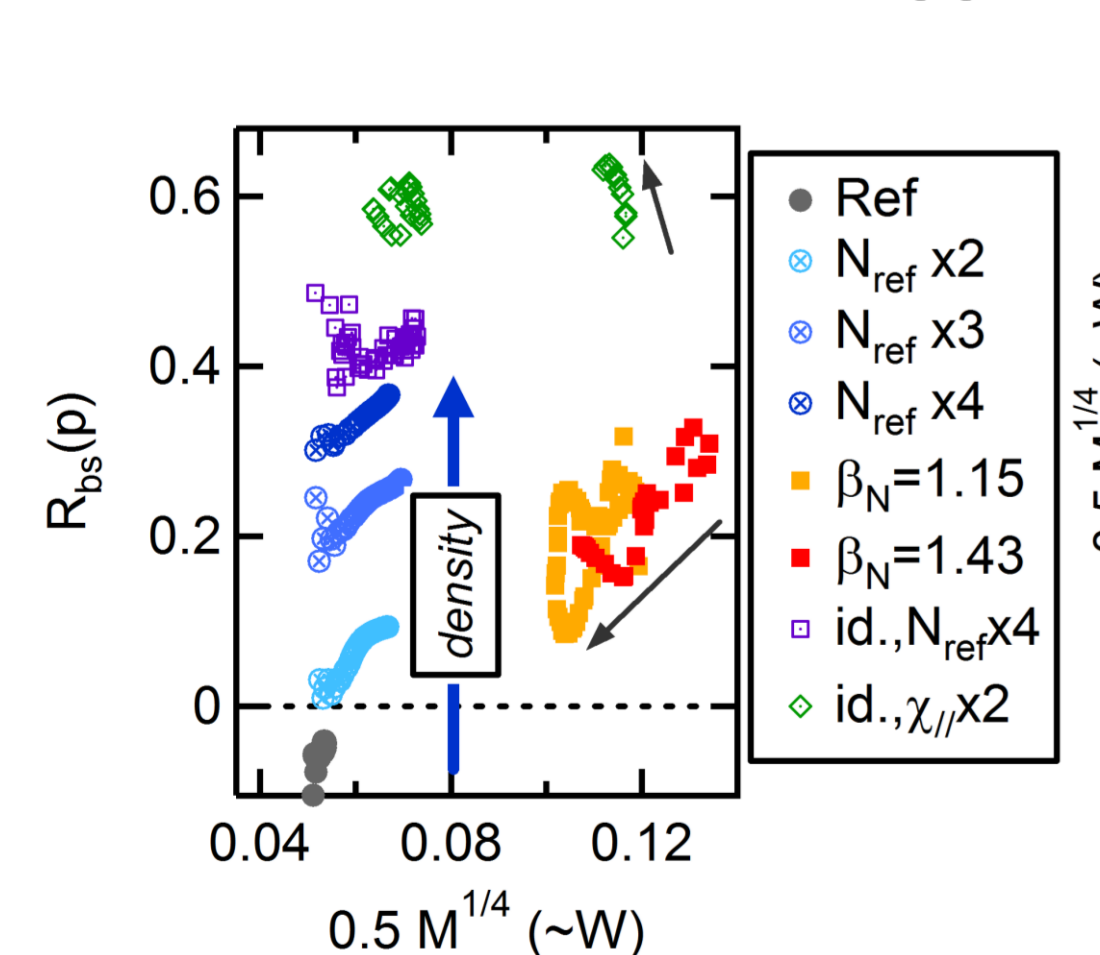


Fig.4 : Correlation between bootstrap & pressure perturbations vs island size.

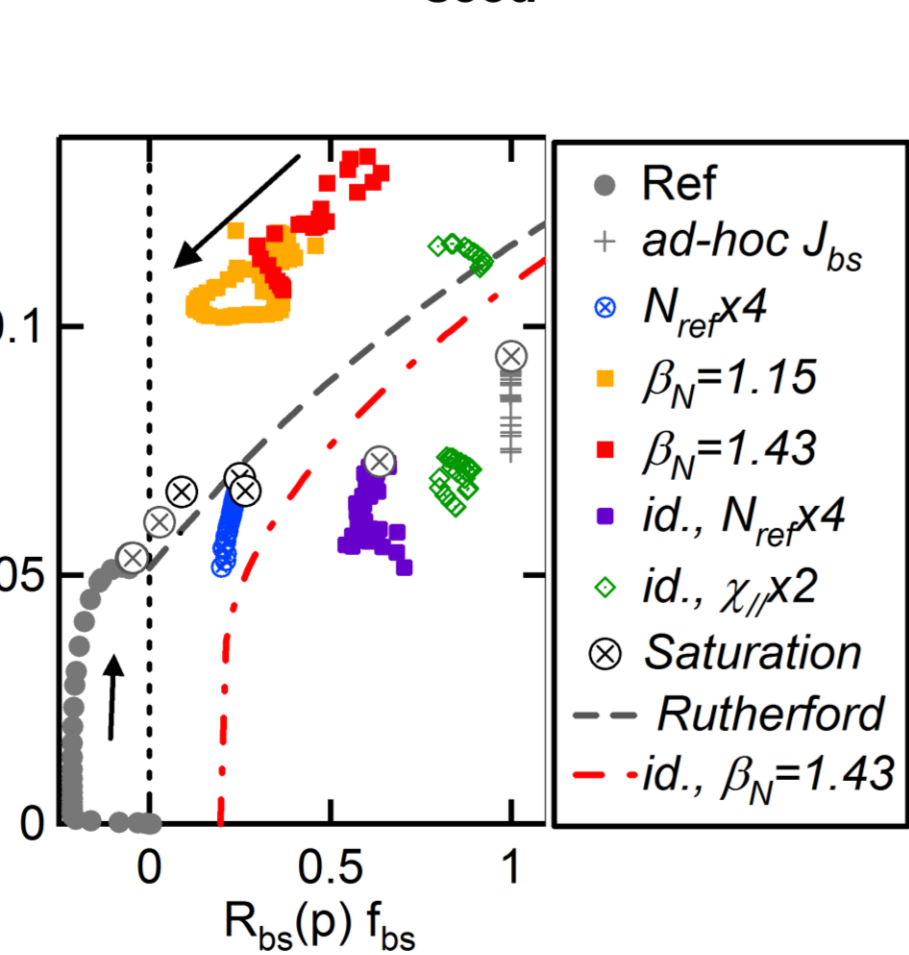


Fig.5 : Island size vs effective bootstrap current

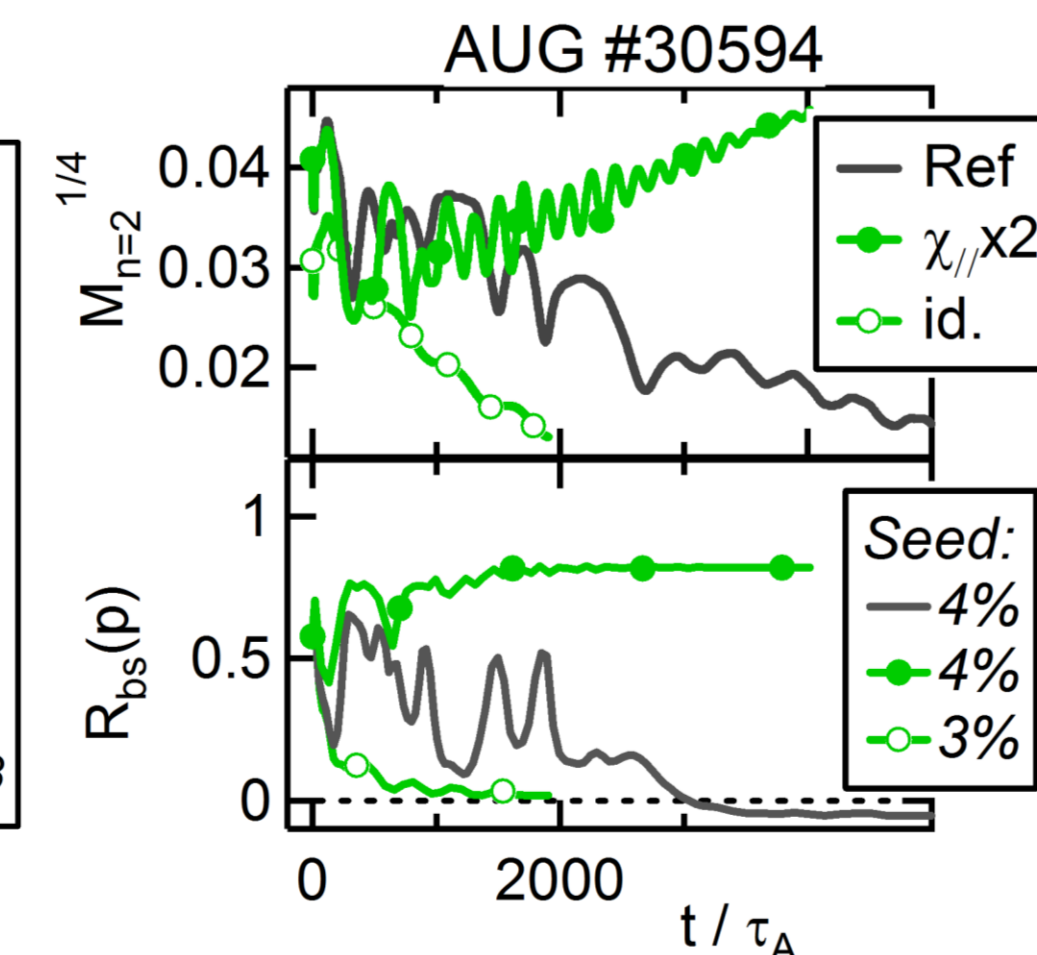


Fig.6 : (3,2) NTM triggering by changing $R_{bs}(p)$ via χ_{\parallel} .

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Island control by ECCD: validation & 3D effects

Implementation of a 3D RF current source (\mathbf{J}_s) in XTOR [5]

- Propagation along field lines through parallel diffusion: quasi-homogeneous

$$\frac{\partial \mathbf{J}_{RF}}{\partial t} = \nu_f (\mathbf{J}_s - \mathbf{J}_{RF}) + \chi_\perp^{RF} \nabla^2 \mathbf{J}_{RF} + \chi_\parallel^{RF} \nabla_\parallel^2 \mathbf{J}_{RF}$$

Validation of stabilization efficiency η_{RF} with respect to analytical theory

- Recovers predicted dependence vs source width δ_{RF} & vs misalignment [fig.7]
- But reduction of η_{RF} found in non-circular cross sections

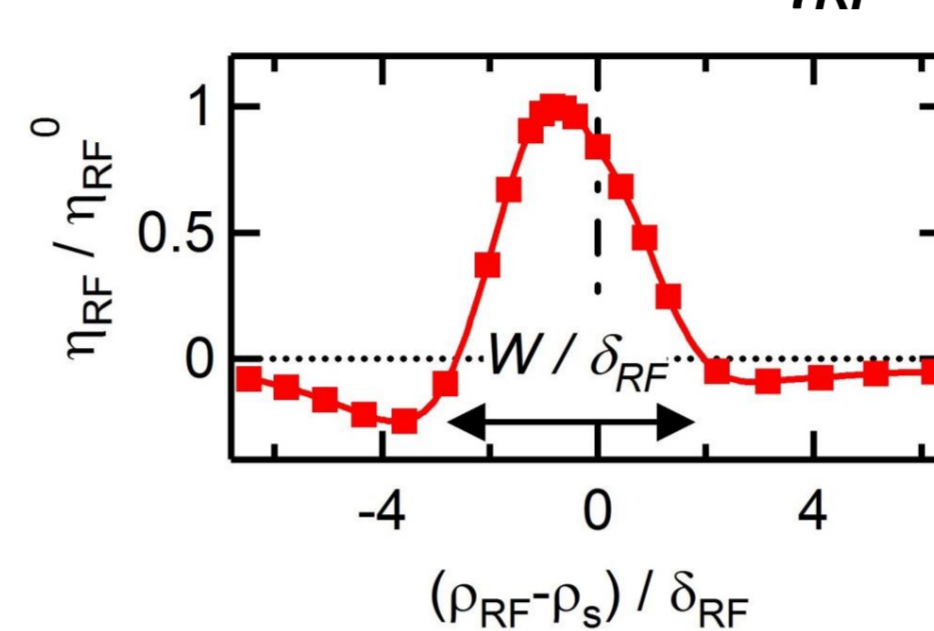


Fig.7: Stabilization efficiency vs misalignment.

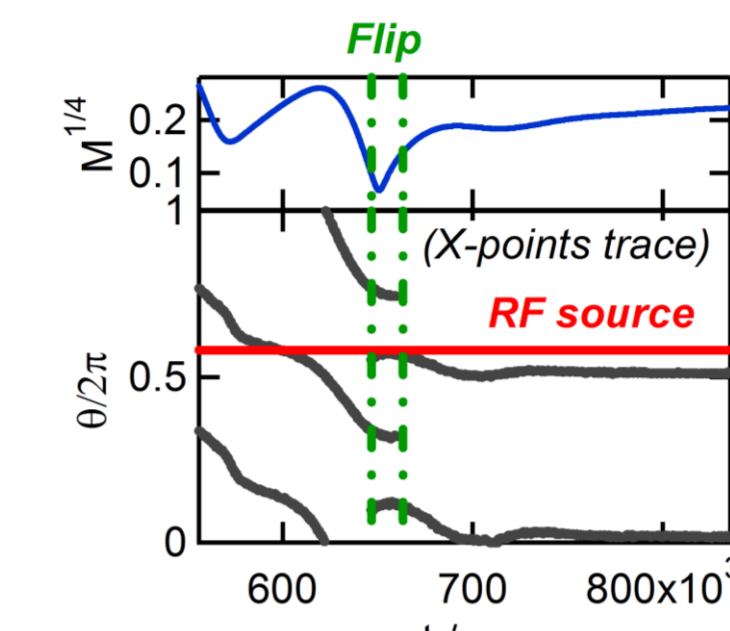


Fig.8 : θ - position of X-points vs time during flip instability.

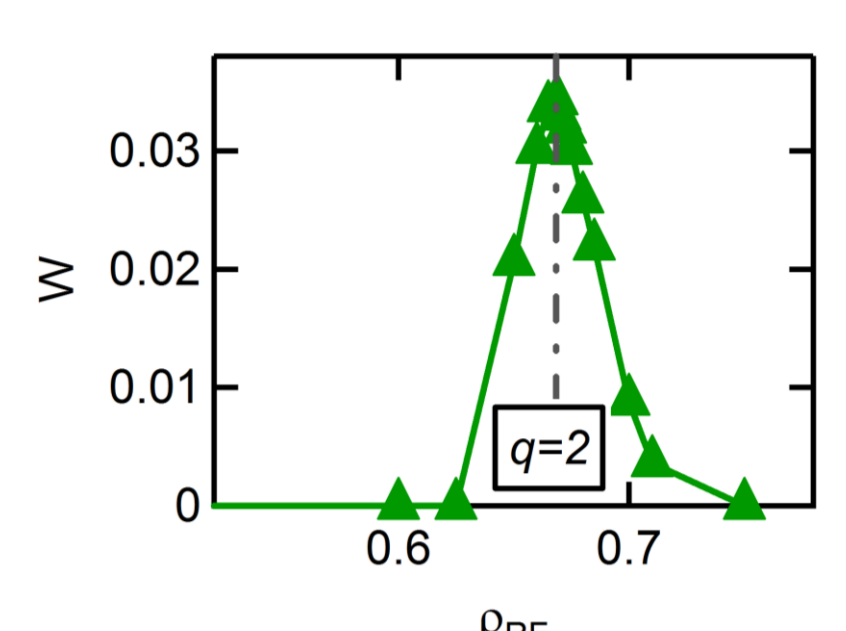


Fig.9 : RF-driven island size vs RF deposition ($I_{RF}/I_p=0.75\%$).

- Specific features with a 3D source : island adjusts its phase to enhance its growth
- Flip instability [6]: the X-point sets in close to the RF source (destabilizing) [fig.8]
- RF-driven island : when close to a resonant surface, the RF current filament forms the X-point of an island [fig.9]

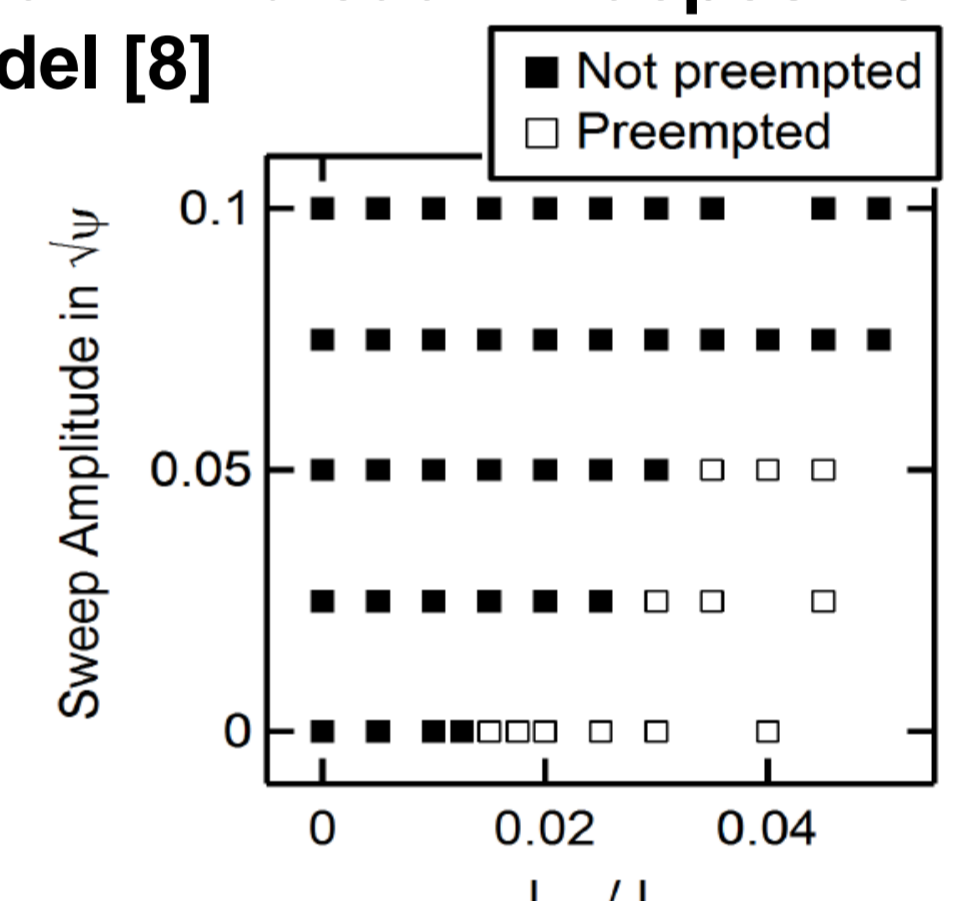
Island control by ECCD: evaluating various strategies

- A basic controller has been implemented for radial sweep and modulation
- Radial sweep aimed at mitigating misalignment risk [7]: successfully tested on TCV and Asdex-Upgrade during the last MST1 campaigns [see overviews, this conf.]
- Modulation aimed at mitigating low efficiency associated with broad RF deposition
- Evaluation of best strategy using the resistive MHD model [8]

Preemption

- Risk due to misalignment [9]: mitigation by radial sweep at the cost of a larger I_{RF} [fig.10]

Fig.10 : Preemption capability as a function of RF current and sweep amplitude



Stabilization (broad source, $\delta_{RF}/W=1.4$) [fig.11]

- Radial sweep : island reduction without misalignment risk, but less efficient than well positioned fixed source
- Combined with modulation : full stabilization obtained
- Alternate modulation with the FADIS (Fast Directional Switch) method uses 2 antennae to obtain a nearly continuous O-point deposition [10]
- Quantification by a gain G and a characteristic time T_{min}

$$G = \frac{W_{sat} - W_{min}}{W_{sat} - W_0}$$

- W_{sat} : island size without control
- W_{min} : minimum width obtained
- W_0 : minimum width for fixed, CW source
- T_{min} : time for reaching W_{min}

- Overview of stabilization strategies [fig.12]
- Island control achieved without misalignment risk
- Large gain for modulation techniques
- Control time scale reduced with the FADIS alternate modulation scheme

Thin RF source ($\delta_{RF}/W=0.7$) : results qualitatively similar, but no advantage to use modulation techniques ($G \sim 1$) (see [8])

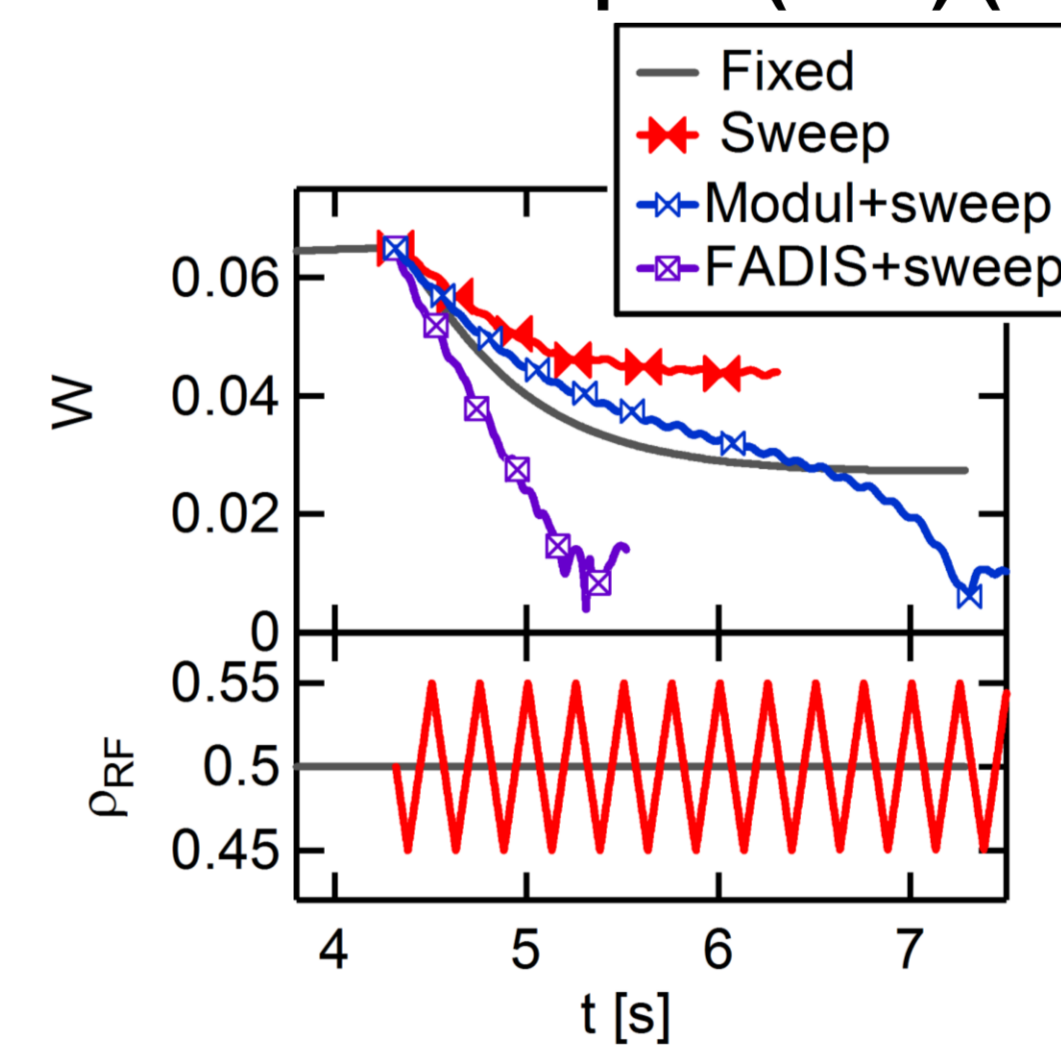


Fig.11 : Island width evolution following different strategies (top); RF deposition during the sweep (bottom).

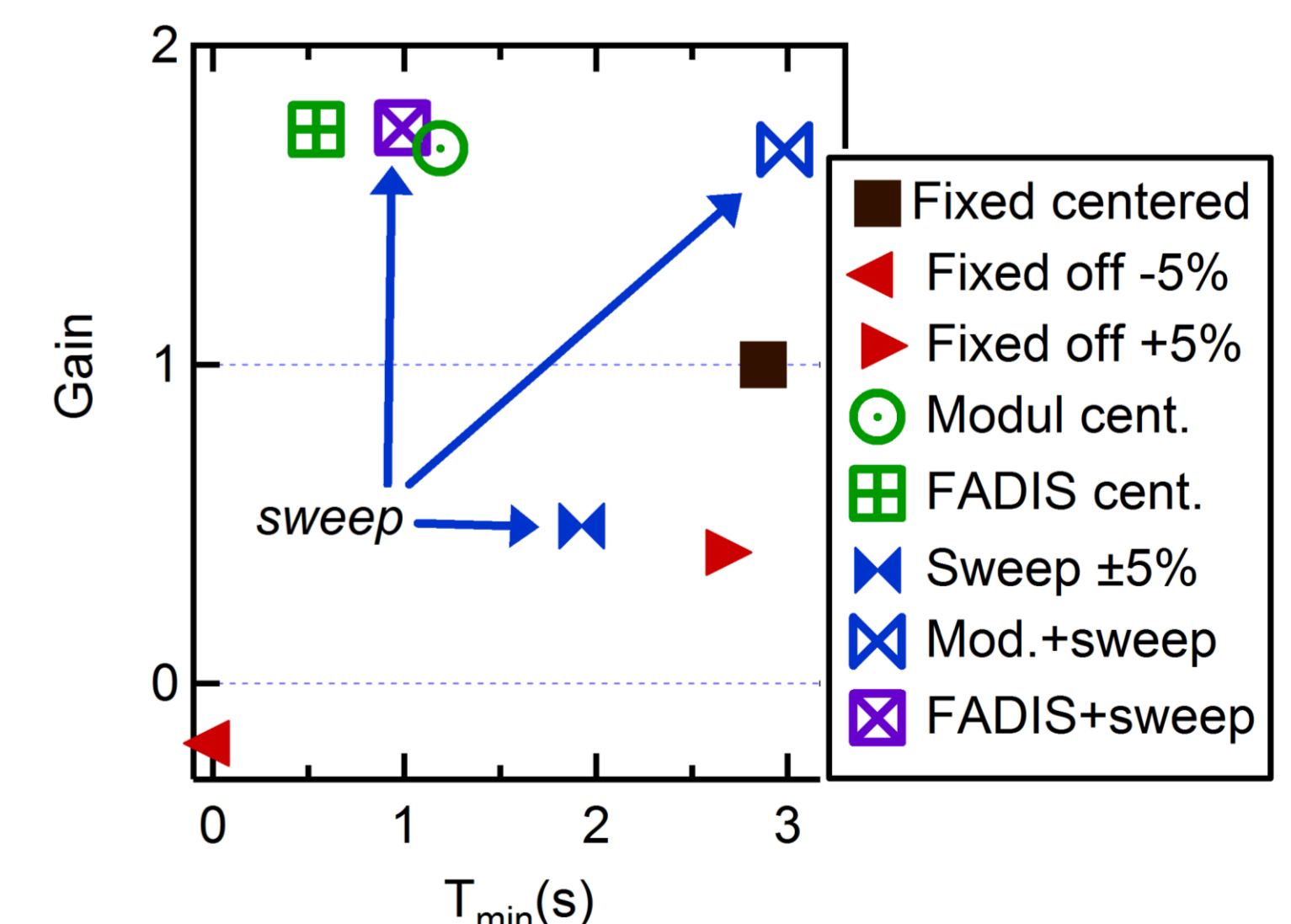


Fig.12 : Gain as a function of characteristic control time T_{min} .

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