

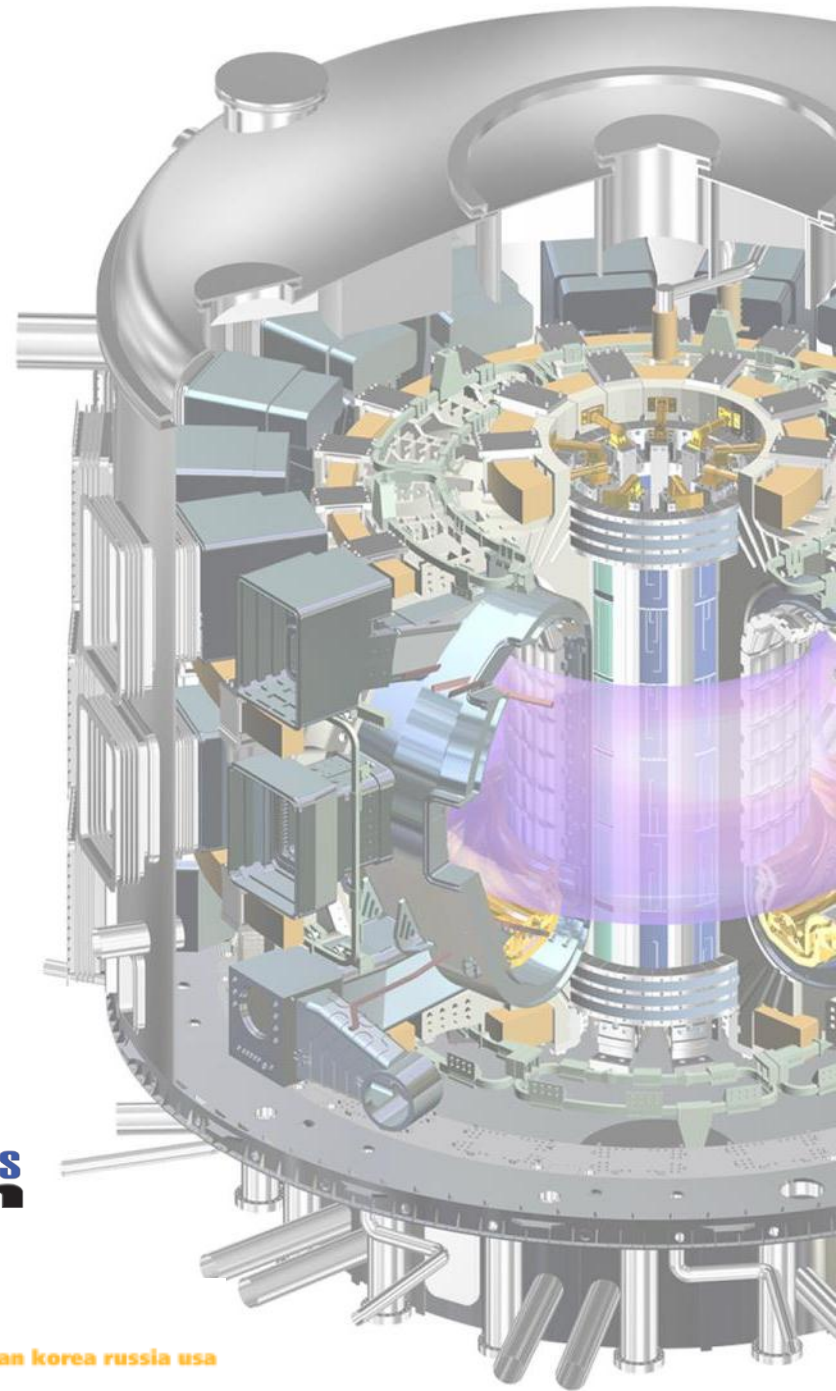
Disruption Mitigation System Developments and Design for ITER

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*25th IAEA Fusion Energy Conference
St. Petersburg, Russia*

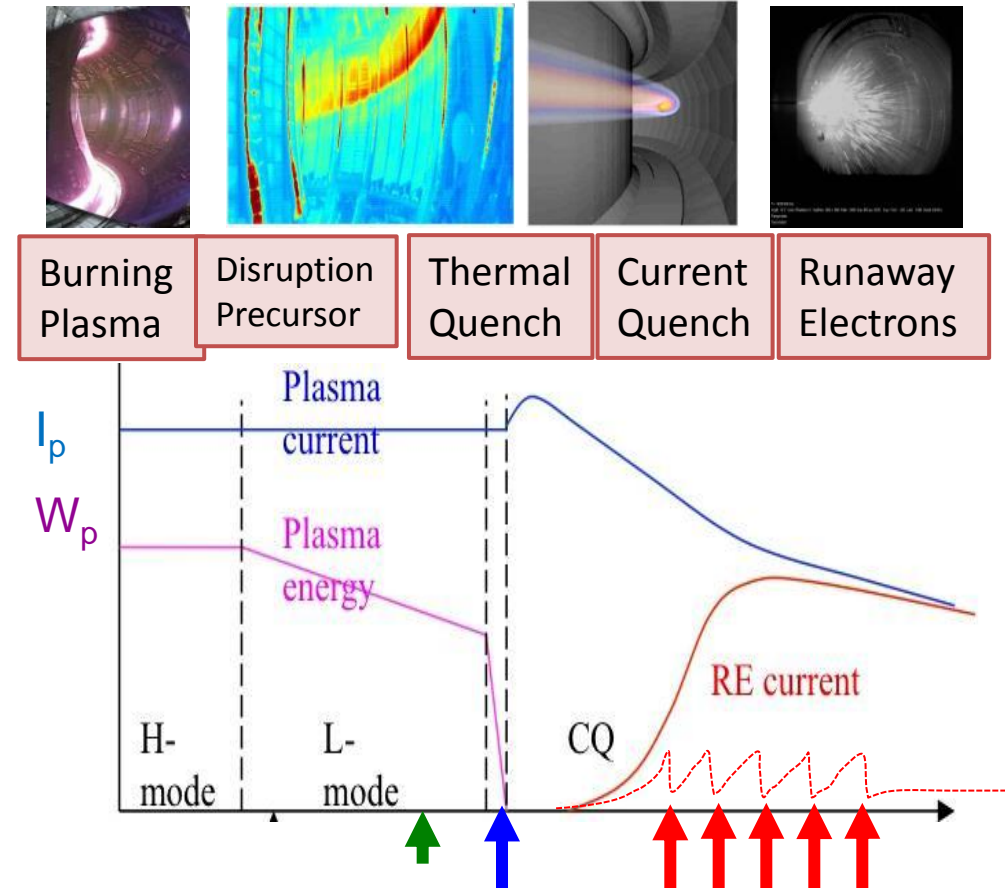


Outline

- DMS Requirements
- DMS Design for ITER
- Design Challenges
- Design Progress-to-Date
- Summary

Mitigation of Disruptions is a Challenge for ITER

- Large Thermal Loads occur during Thermal Quench – **TQ peak heat loads need reduction of > 10 X**
- Large Mechanical Loads on plasma facing components and vessel during Current Quench - **CQ decay time must be controlled within limits of 50-150 ms**
- Runaway electrons can be generated during Current Quench - **RE current must be suppressed or dissipated to less than 2 MA**
- Mitigate with solid and gas injection of deuterium, argon, neon and helium
- Developing tools and techniques for:
 - Massive gas injection (MGI)
 - Shattered pellet injection (SPI)



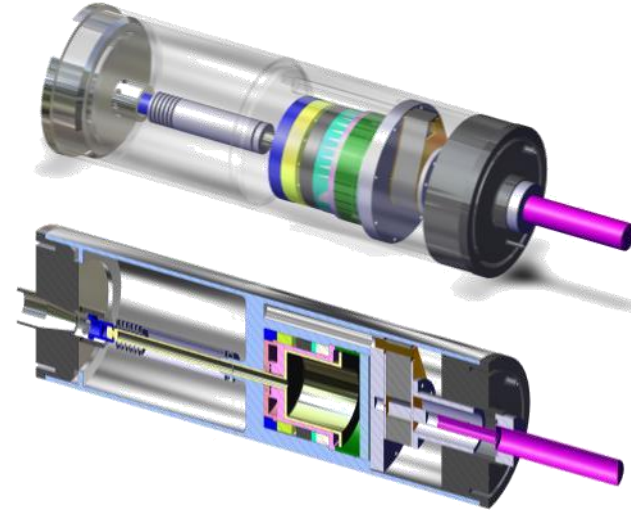
Preventive SPI and MGI of material for
Thermal Mitigation and **Runaway
Electron Suppression**

MGI and SPI **RE Dissipation**

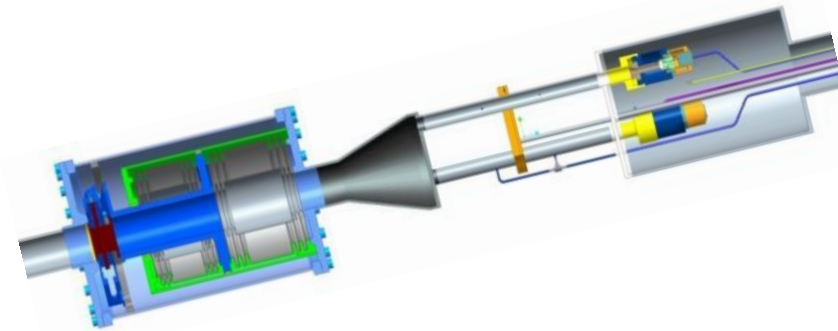
Disruption Mitigation System Material Injection Requirements

DMS Requirements: Deliver rapid shattered pellet and massive gas injection systems to

- Limit impact of plasma disruption thermal and mechanical loads on walls and vacuum vessel – up to 10 kPa-m³ of D₂, Ar, Ne, He in < 20 ms
- Suppress the formation and effects of high energy runaway electrons – up to 100 kPa-m³ in < 10 ms
- Reliability and Maintainability
- Are these requirements compatible?

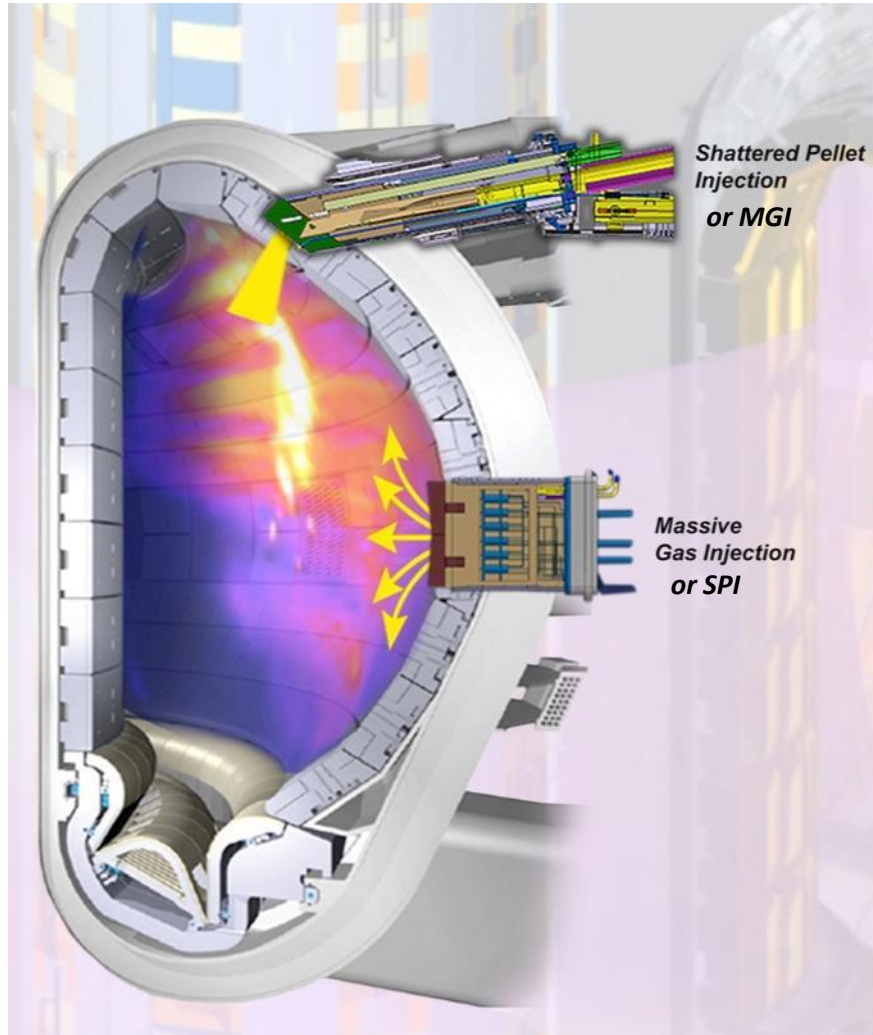


Massive Gas Injection Valve Concept



Shattered Pellet Injector Concept

Disruption Mitigation System Configuration



DMS Configuration:

- Shattered pellet injector (SPI) or Massive gas injection (MGI) located in 3 upper ports with pellet shattered near plasma edge
- SPI has multiple barrels for redundancy and adjusting amount injected – can be used as MGI
- MGI or SPI located in 1 equatorial port for runaway electron mitigation
- Combinations of MGI and SPI are possible

Significant Design and Technical Achievements

- **Requirements defined by IO with input from ITPA and fusion community**
- **Fusion science and technology community workshop**
 - Identification of candidate technologies & techniques for effective mitigation
- **DMS Conceptual Design Review and consideration of viable candidates**
 - Down selection to massive gas injection and shattered pellet injection
- **Technology development in laboratory**
 - Fast massive gas injection valves
 - Production and acceleration of large deuterium and neon pellets
 - Optimization of pellet shatter geometry
- **Technology deployment and demonstration on fusion devices**
 - Initial demonstrations of thermal mitigation and runaway electron dissipation
 - Argon pellet injector deployed for controlled triggering of REs in disruptions
- **Modeling of technology and disruption mitigation experiments**
 - Models of gas flows, pellet fragmentation and assimilation in disruption plasma
 - Modeling of effects of ITER DMS (yet to be achieved)

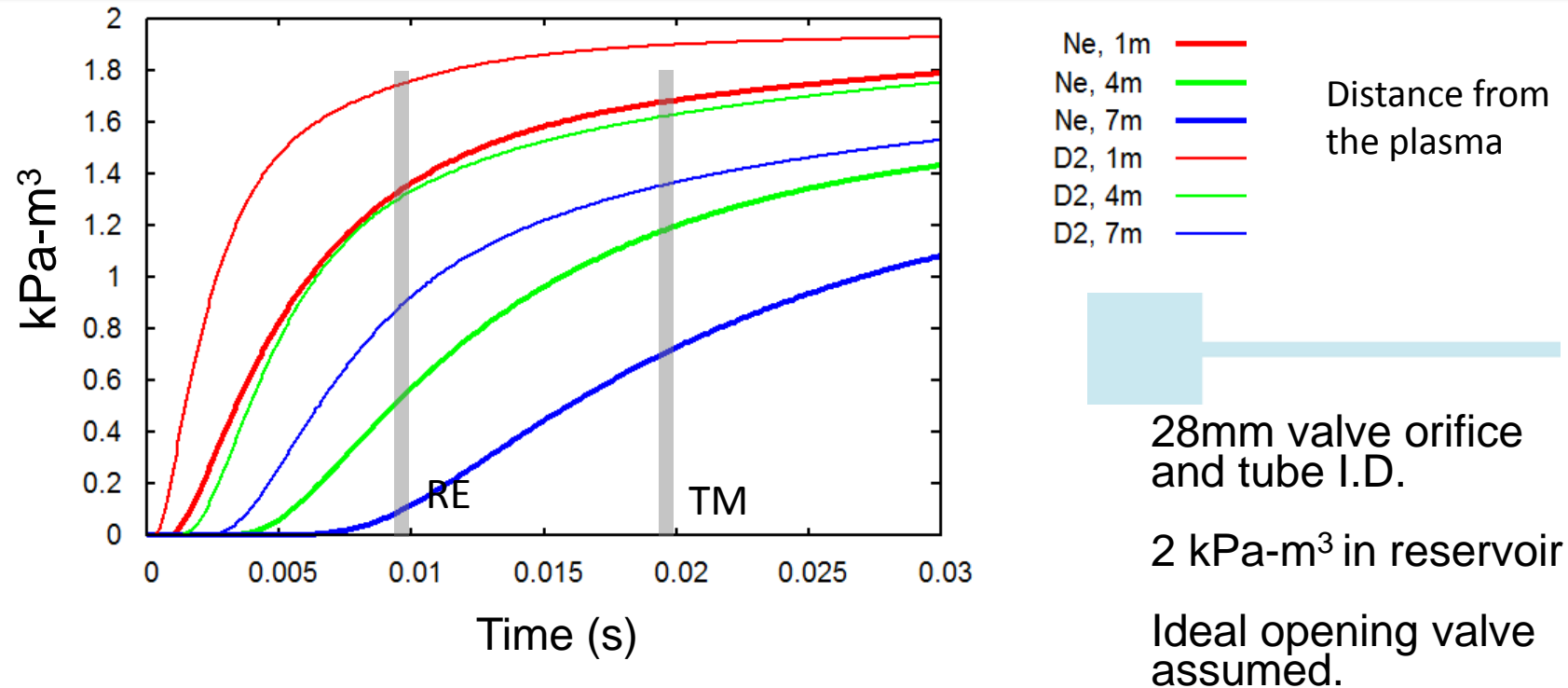
Disruption Mitigation System Design Status and Plans

- CDR complete
- Design underway for
 - Massive gas injection (MGI)
 - Shattered cryogenic pellet injection (SPI)
- Hardware for SPI and MGI subsystems must be tested on fusion experiments to determine effectiveness
 - Experiments are performed by fusion community with their resources
 - Initial tests of DMS techniques and technologies for ITER underway in lab and at DIII-D
 - U.S. ITER and VLT supports SPI and MGI experiments with hardware
 - Simulations to determine effectiveness on ITER are needed

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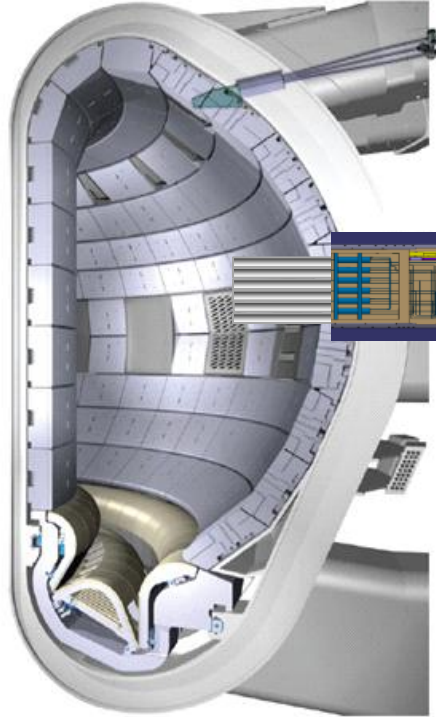
MGI Integrated Mass Flow into Plasma for Different Gases/Distances



- Calculations for Ne and D₂ with a 28mm valve/tube size
- D₂ and Ne at 1m achieves the 90% injection within 20ms – the specified response TM cannot be achieved with neon MGI at 4m, 60% is possible

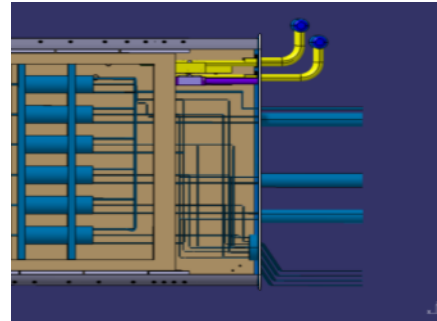
CFD calculations – SonicFOAM

MGI and SPI for RE Suppression/Dissipation Installed Inside Equatorial Port Plug to Meet Injection Time Requirements



Up to 100 kPa-m³ for runaway electron suppression and dissipation

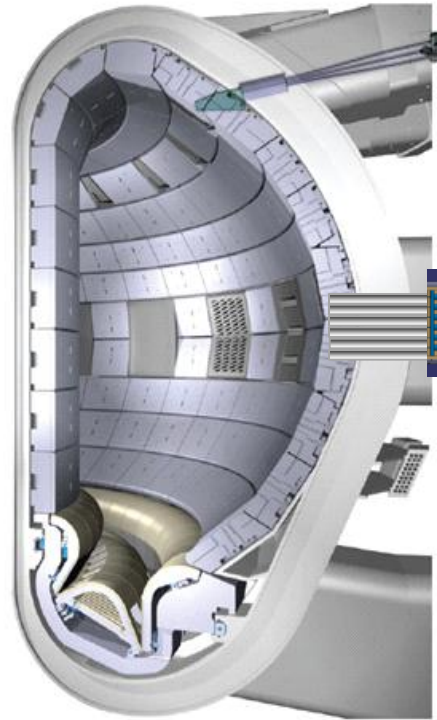
MGI and SPI DMS



MGI fast gas valves use a stainless steel valve seat with Vespel polyimide plugs

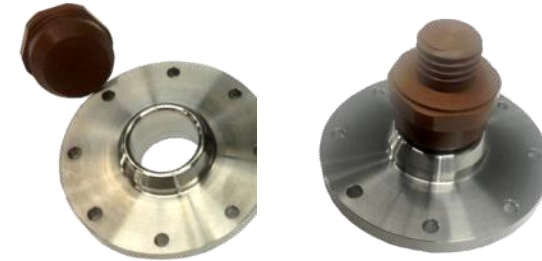
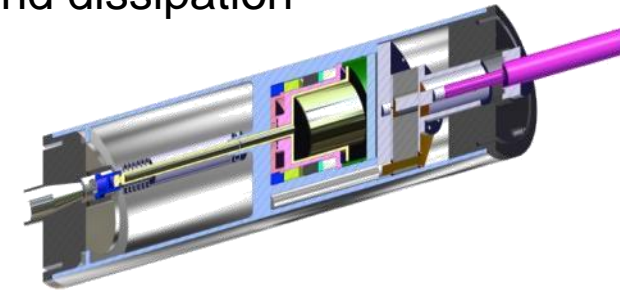
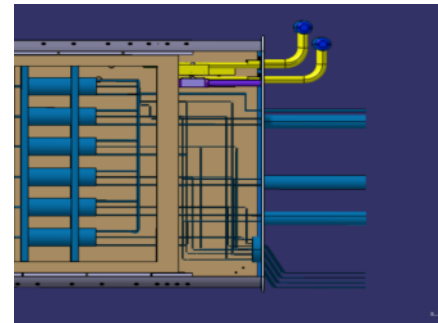
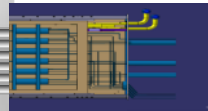
- MGI located in one equatorial port plug for runaway electron suppression/dissipation to meet injection time requirement - limited by sound speed of gas
- Combination of SPI and MGI is possible
- **Design challenges with active MGI components located inside port plug**

MGI and SPI for RE Suppression/Dissipation Installed Outside Equatorial Port Plug for Reliability and Maintainability



Up to 100 kPa-m³ for runaway electron suppression and dissipation

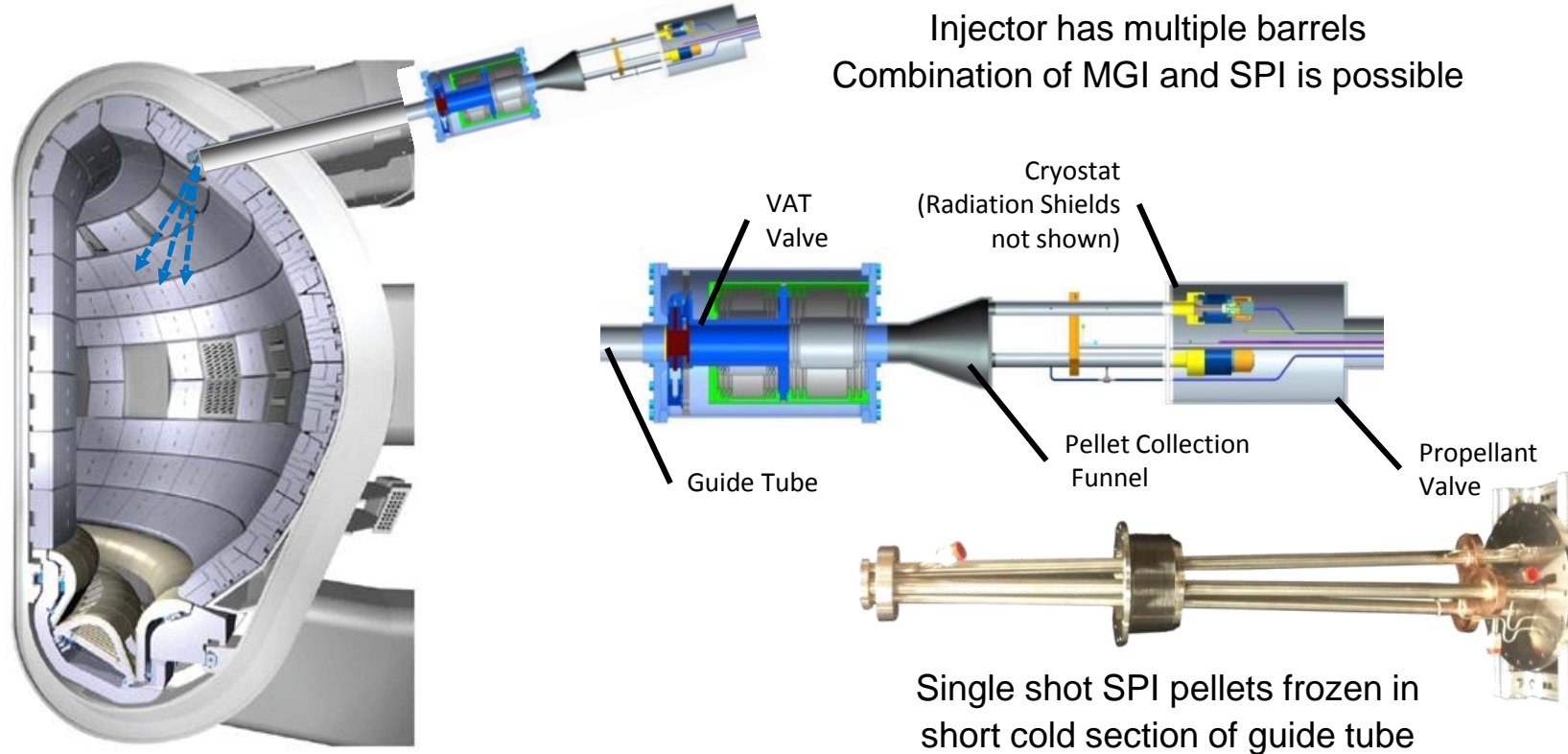
MGI and SPI DMS



Stainless steel valve seat with
Vespel valve plugs

- MGI located in one equatorial port plug for runaway electron suppression/dissipation
- Combination of SPI and MGI is possible
- **Design challenges decrease with active components located outside port plug, but time response is longer**

Shattered Cryogenic Pellet Injection Active Components Installed Outside Upper Port Plugs for Reliability and Maintainability

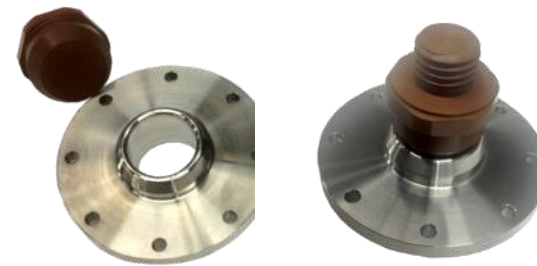
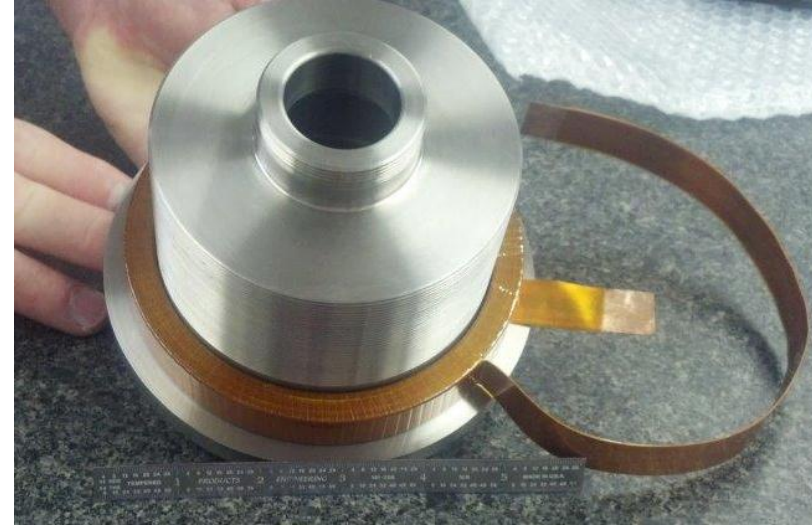
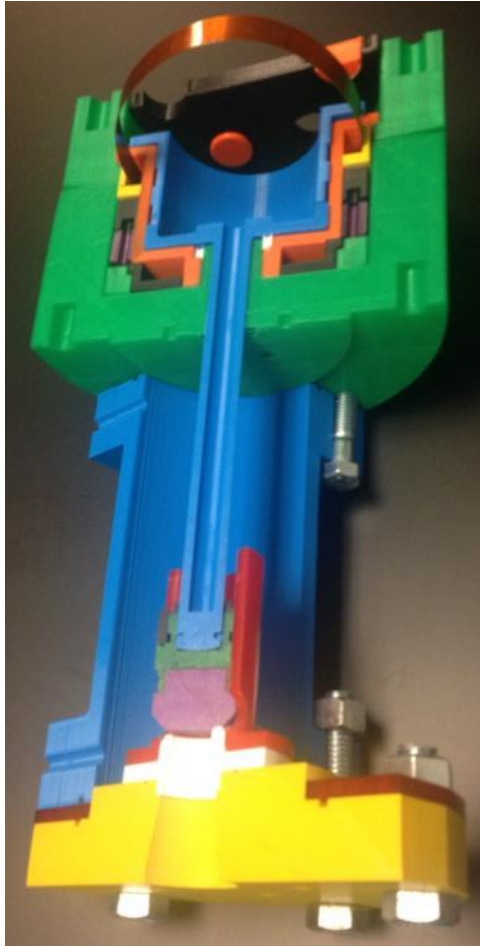


- SPI located in upper port plug(s) with pellet shattered near plasma edge
- Injector has multiple barrels for redundancy and adjusting amount injected – combination of MGI and SPI is possible
- **Challenges decrease with active SPI components located outside port plug**
- **Injection time is marginal to meet 20ms requirement for TM**

Outline

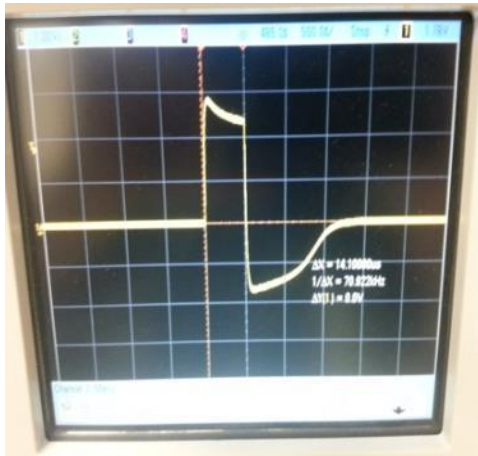
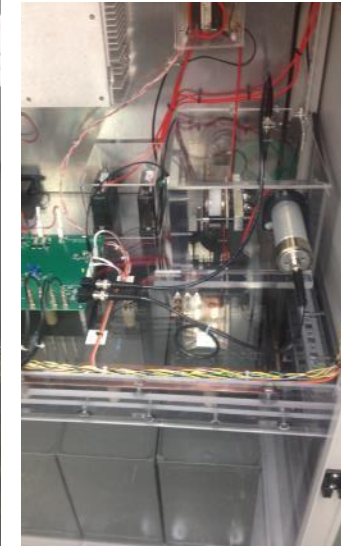
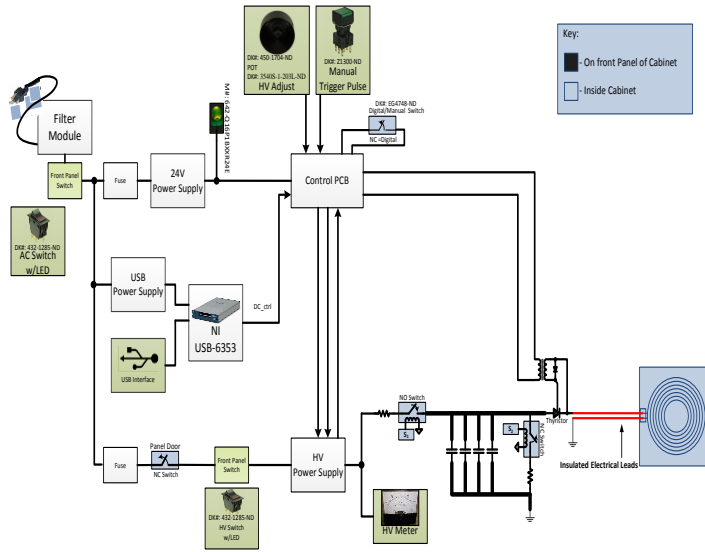
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Massive Gas Injection Valve Prototype



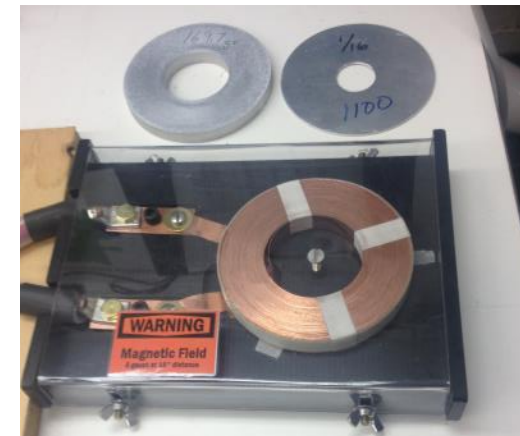
Valve based on a design used on JET, but modified for ITER tokamak environment and injection requirements. MGI Valve uses Flyer Plate to Achieve Fast Opening Time and incorporates T compatible components

Design, Fab and Test of MGI Power Supply Completed

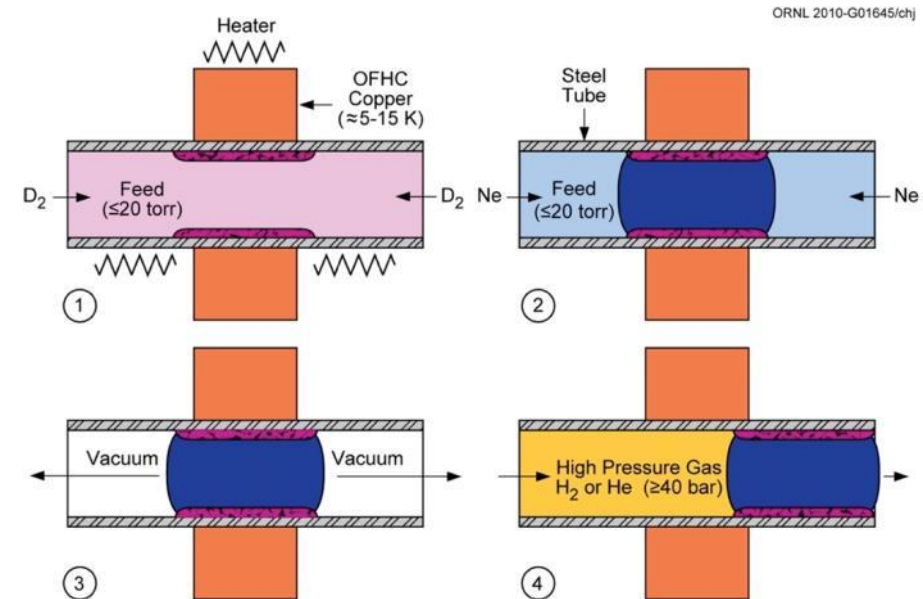
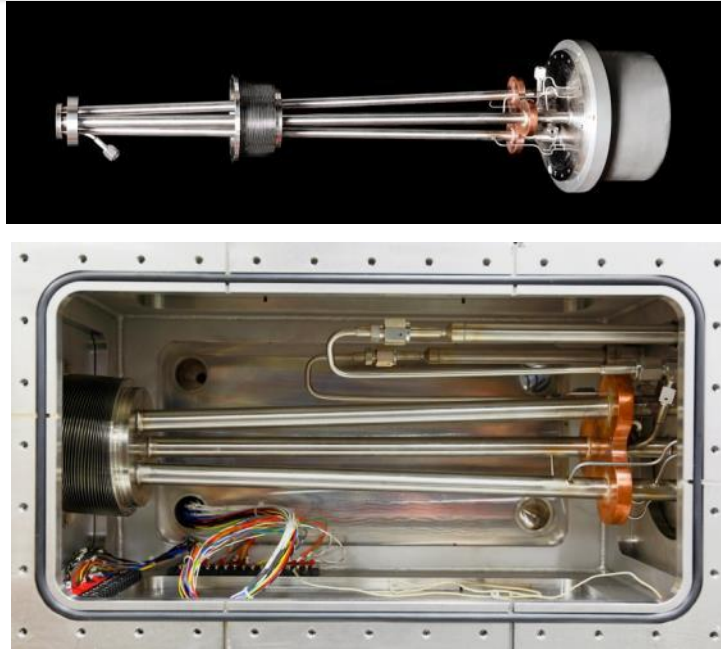


SCR Triggering Requirements:

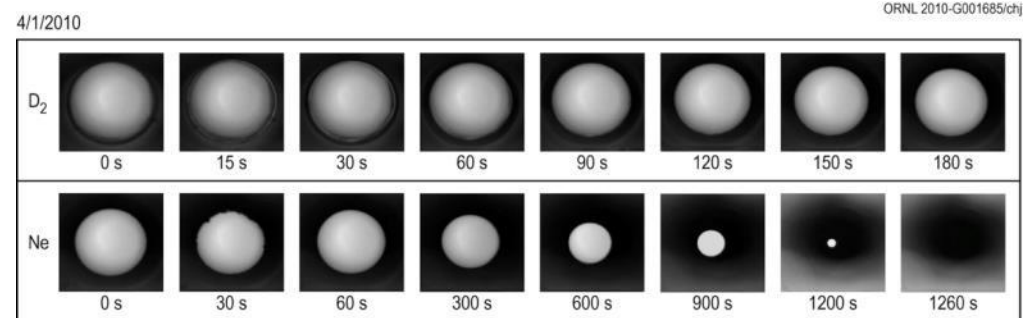
- $\sim 5V$, $\sim 300mA$, $\sim 100\mu s$ duration
- $\sim 15\text{ ohm}$ load



SPI 3-Barrel Prototype Completed



- Barrel inner diameter increased to 24.4 mm (from 16 mm diameter) in order to study scaling of D_2 and neon pellet formation/acceleration.
- SPI uses MGI valves to accelerate pellets and can be used as MGI system when no pellet is formed.



View of freezing process from end of barrel

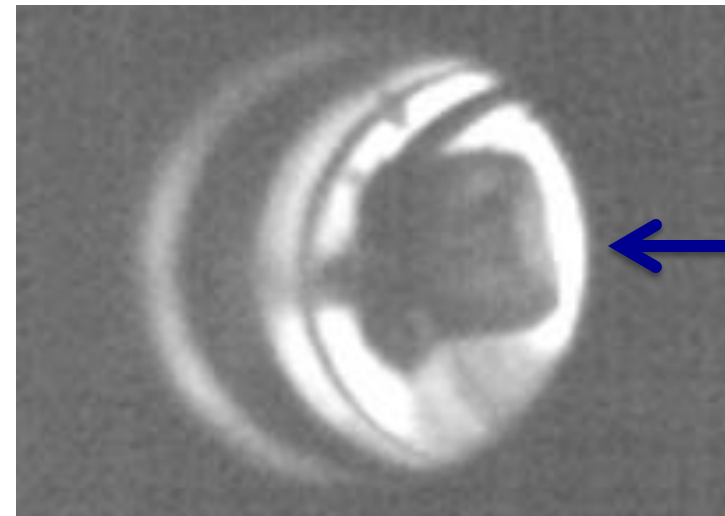
25 mm D₂ and Neon Pellets Formed and Accelerated from 3 Barrels



- 3 ea. ~ 25 mm pellets formed and accelerated to 330 m/s
- 1.5 kPa-m³ of deuterium each. 2 pellets exceed the requirement of 2 kPa-m³ for thermal mitigation
- Future testing planned for 34mm diameter pellets for RE suppression



25 mm
neon



25 mm
D₂

Disruption Mitigation – Laboratory Testing of Neon Pellet Shattering



Plume of the shattered neon pellet after passing through bent tube



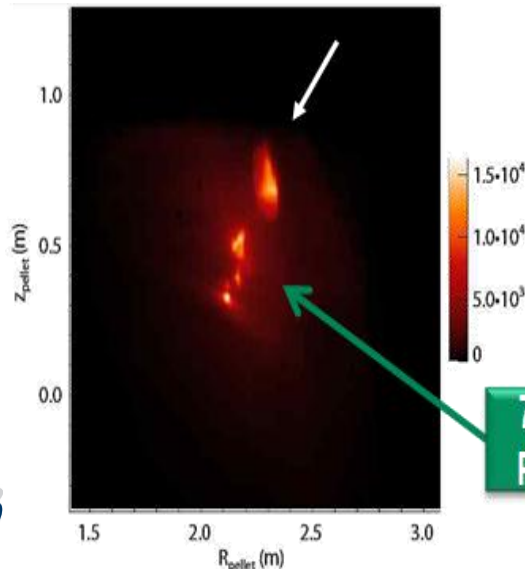
Disruption Mitigation – Field Testing of Neon Shattered Pellet



- Additional pumping capacity added eliminates issues with leading edge propellant

SPI Injection
Line Pumping

Disruption mitigation experiments carried on DIII-D in 2014 – results presented at APSDPP 2014

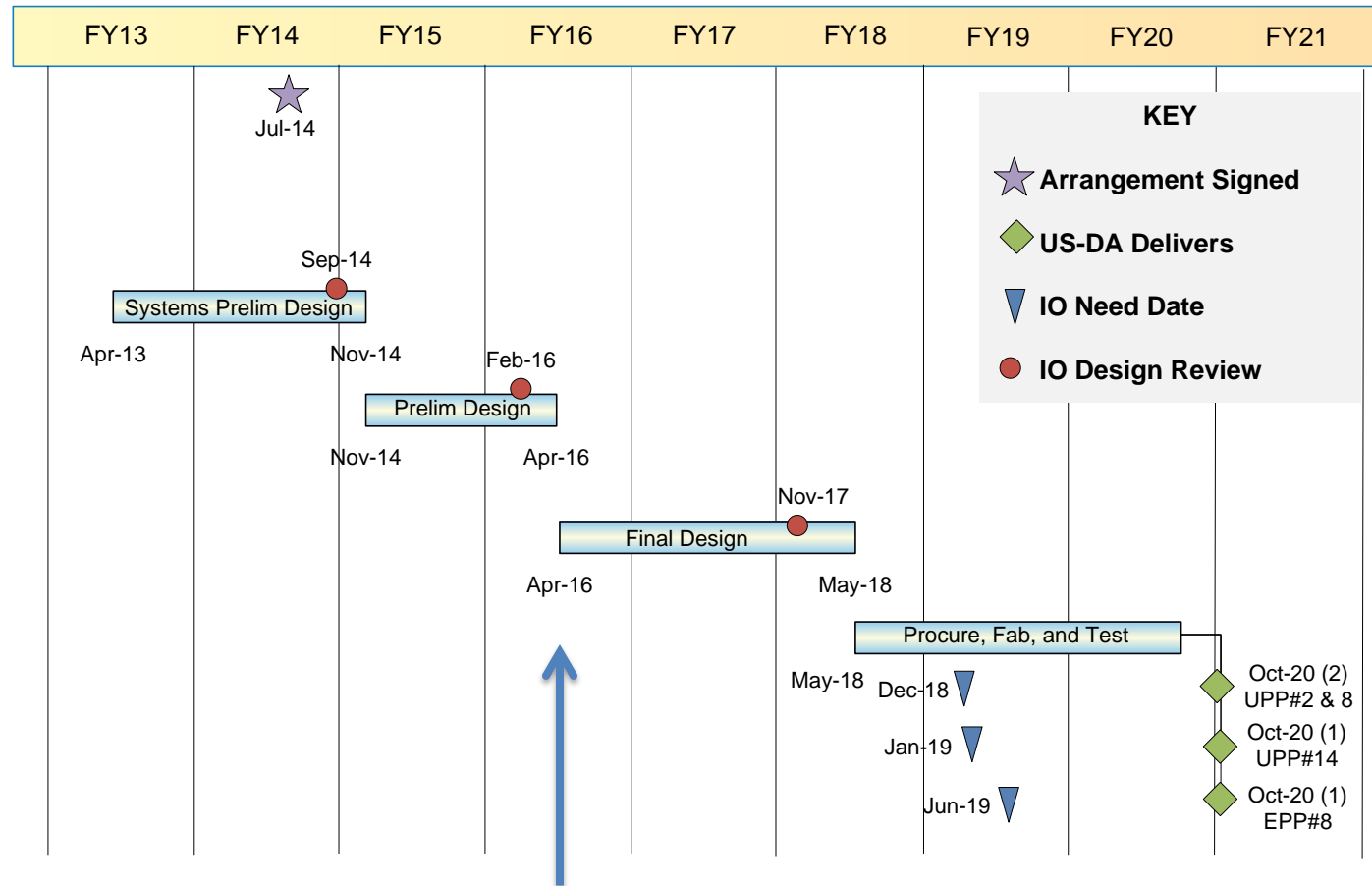


- Barrel diameter downscaled to 7 mm for thermal mitigation testing on DIII-D

7 mm Neon Shattered
Pellet in DIII-D Plasma

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N. Commaux, B. Dannels, A.R. Horton,
D. Shirake, L.R. Baylor*

Disruption Mitigation Summary Schedule (based on detailed schedule with 321 activities)



Schedule Drivers:

- Final design of components that meet response time and interface requirements
- Fabrication durations for specialized components
- Requires experimental time on DIII-D, JET, etc. to deploy and qualify DMS components
- Critical path
 - Test program

Summary

- DMS scope and schedule are well defined and being executed
 - CDR Complete
 - Down selection to SPI and MGI following December 2012 CDR
 - Hardware for candidate SPI and MGI being designed, fabricated and tested
 - International fusion community is actively engaged
 - Design and qualification integrated with DMS research partners
- Present Challenges - Injection response vs Reliability
 - Harsh port plug environment and reliability requirements
 - Minimum response time for runaway electron suppression and dissipation
- **More simulation and modeling needed to resolve requirement issues**
 - Needed for Final Design of DMS

Disclaimer:

The views and opinions expressed in this paper do not necessarily reflect those of the ITER Organization.

Thank you

BACKUP ONLY

Milestone: Complete Disruption Mitigation System PDR (November 2014)

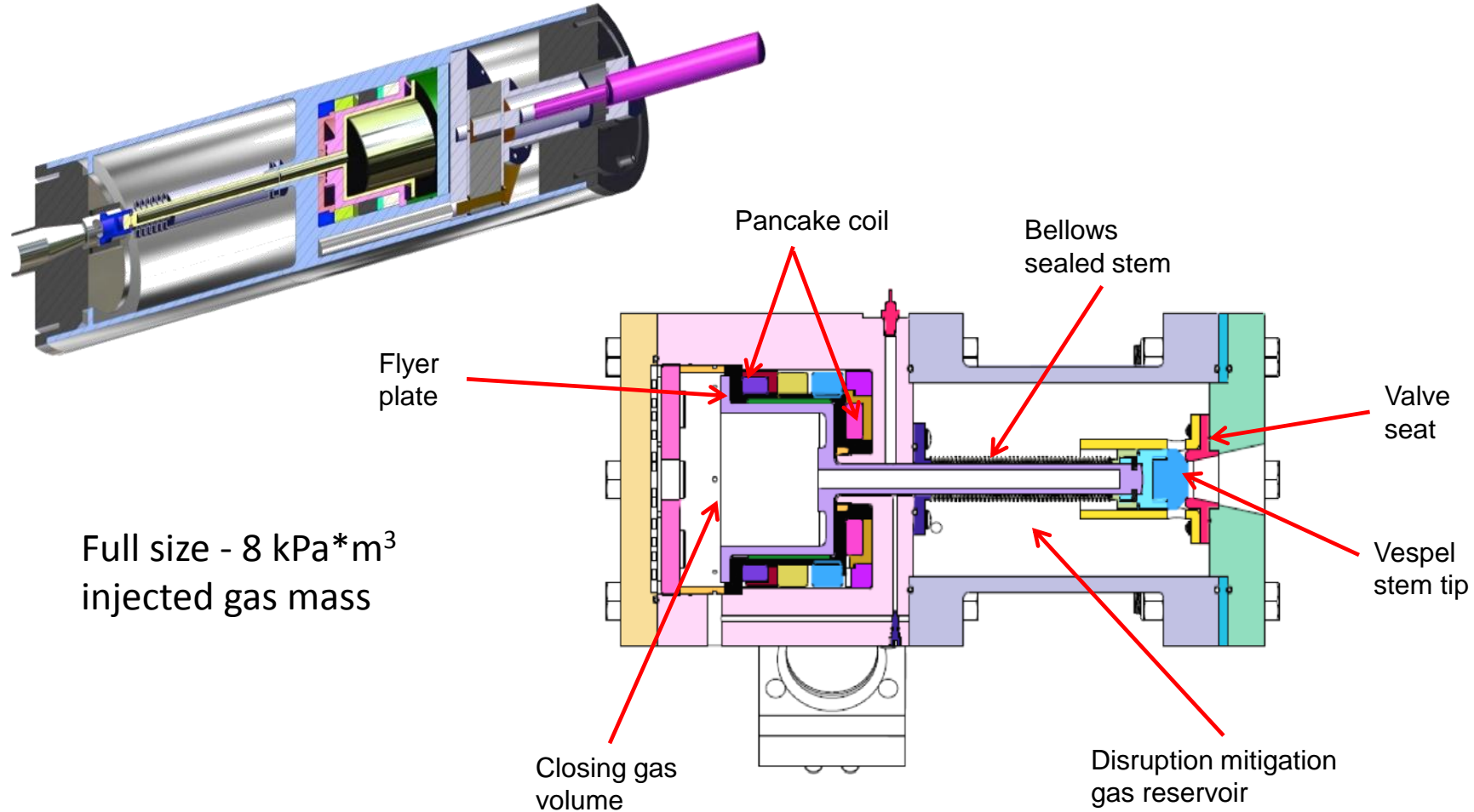
Pre-SPDR tasks and responsible parties

- IO completes physics studies to determine maximum allowable response time
- IO completes PCR to reserve space for outside of the port plug location
- Tokamak experiments and IO analysis provide guidance on MGI vs SPI material assimilation, TQ, CQ and RES effectiveness and need for multiple toroidal and/or poloidal injection locations
- US completes P&IDs for MGI and SPI options
- US performs 3-barrel injector tests
- US determine the maximum obtainable pellet speed
- US completes the design, fabrication and initial testing of the MGI valve
- US completes the design and fabricate MGI valve firing electronics

SPDR Outcomes

- Most promising DM technology identified at SPDR becomes basis for remaining PD and port plug interfaces
- Backup DM technology design placed on hold and minimum hardware and design needed for associated port plugs
- Update Systems Requirements to reflect latest physics and hardware understanding

Massive Gas Injection Valve Prototype

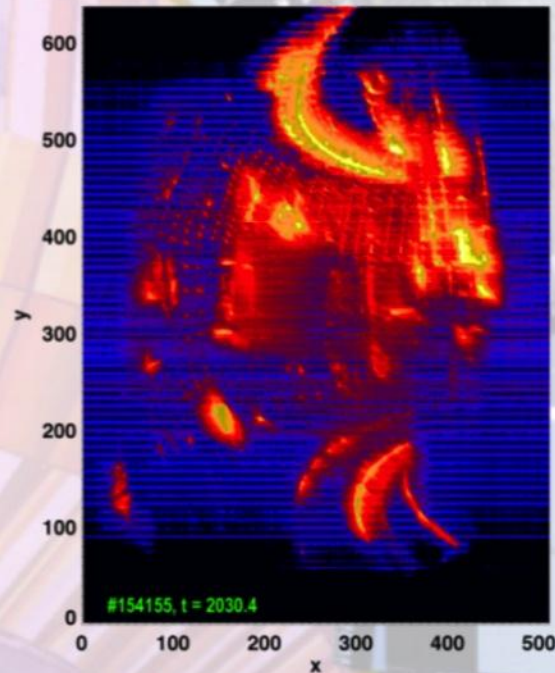


Valve based on a design used on JET but modified for ITER tokamak environment and injection rate requirements. Modified Valve uses Flyer Plate to Achieve Fast Opening Time and incorporates T compatible components

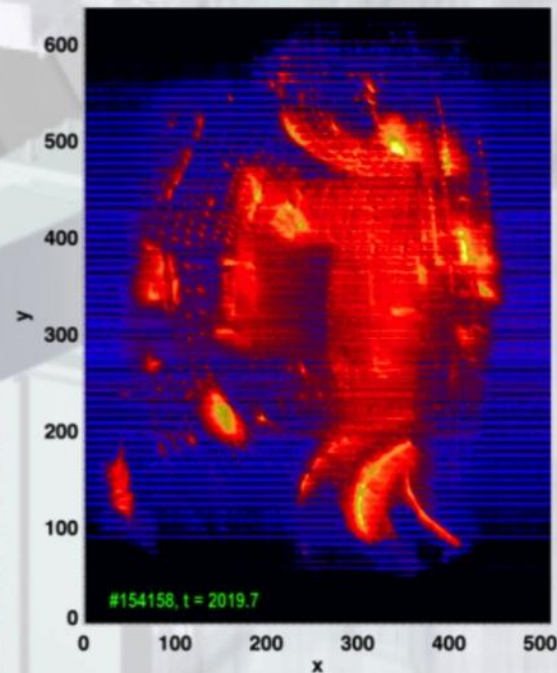
Massive Gas Injection on DIII-D

Experimental Progress

Effective mitigation of thermal quench with massive gas injection has been demonstrated on JET, DIII-D, ASDEX-U and C-MOD tokamaks. Mitigation with shattered pellet injection has also been demonstrated on DIII-D.



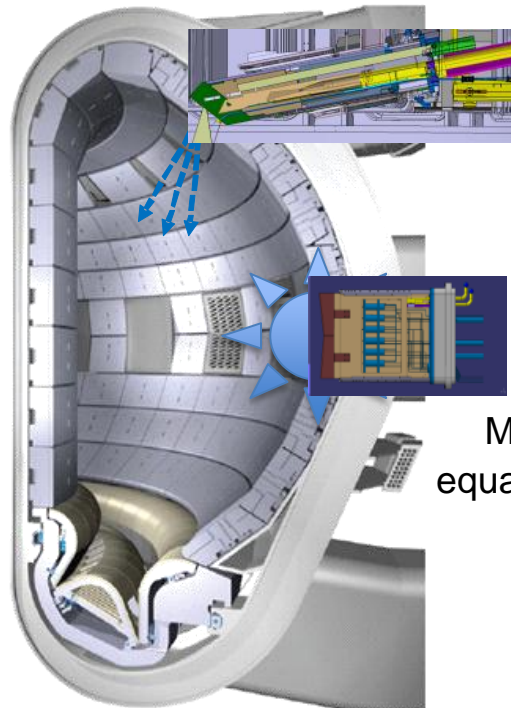
Unmitigated Upward
Vertical Displacement
Event on DIII-D



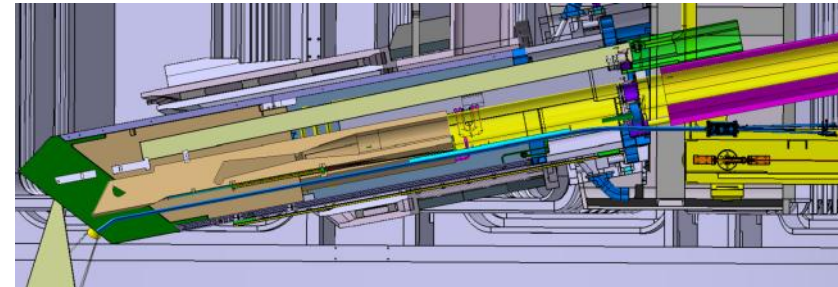
Mitigated Upward
Vertical Displacement
Event on DIII-D

Disruption Mitigation Includes Injection of Pellets Shattered at Plasma Edge and Gas Injection through Delivery Tubes

- **Mitigate impact of the disruption thermal and current quench**
 - Use large shattered pellets composed of neon with a deuterium shell
- **Suppress and dissipate runaway electrons**
 - Use massive gas or shattered pellet injection



SPI located in upper port plugs with pellet shattered near plasma edge



MGI located in equatorial port plugs

