

# The Role of MHD in 3D Aspects of Massive Gas Injection

V.A. Izzo,<sup>1</sup> N. Commaux,<sup>2</sup> N.W.  
Eidietis,<sup>3</sup> R.S. Granetz,<sup>4</sup> E.  
Hollmann,<sup>1</sup> G. Huijsmans,<sup>7</sup> D.A.  
Humphreys,<sup>3</sup> C.J. Lasnier,<sup>3</sup> M.  
Lehnen,<sup>7</sup> A. Loarte,<sup>7</sup> R.A. Moyer,<sup>1</sup>  
P.B. Parks,<sup>3</sup> C. Paz-Soldan,<sup>5</sup> R.  
Raman,<sup>6</sup> D. Shiraki,<sup>2</sup> E.J. Strait<sup>3</sup>

<sup>1</sup>UCSD, <sup>2</sup>ORNL, <sup>3</sup>GA, <sup>4</sup>MIT, <sup>5</sup>ORISE,  
<sup>6</sup>UW, <sup>7</sup>ITER IO

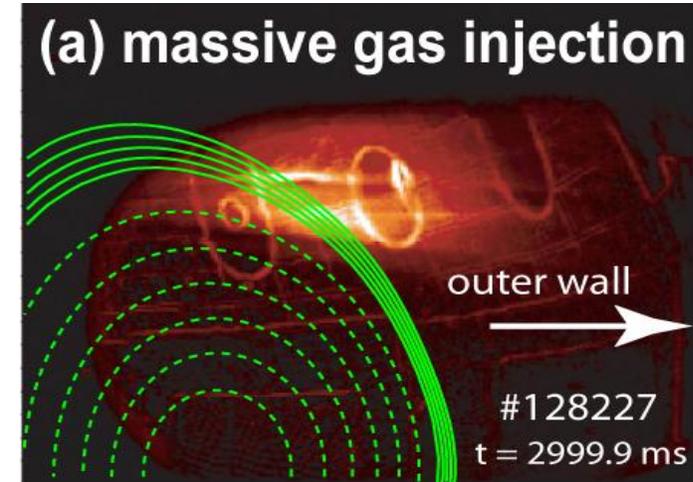


**25<sup>th</sup> IAEA Fusion  
Energy Conference**

**16 October 2014  
TH/4-1**

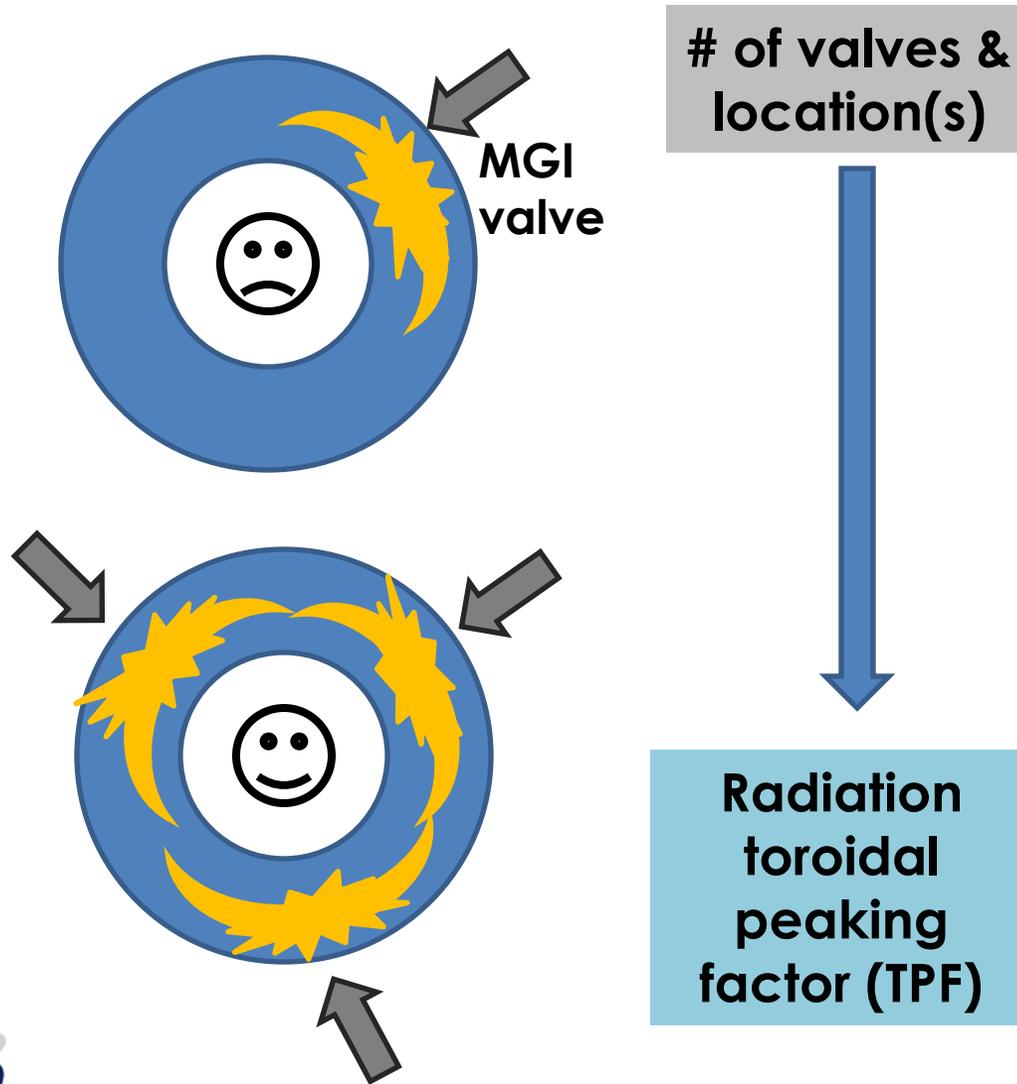
# Massive Gas Injection is a leading candidate for disruption mitigation on ITER

In the event that a disruption is unavoidable, the goal of massive gas injection (MGI) shutdown is to radiate plasma stored energy in order to:

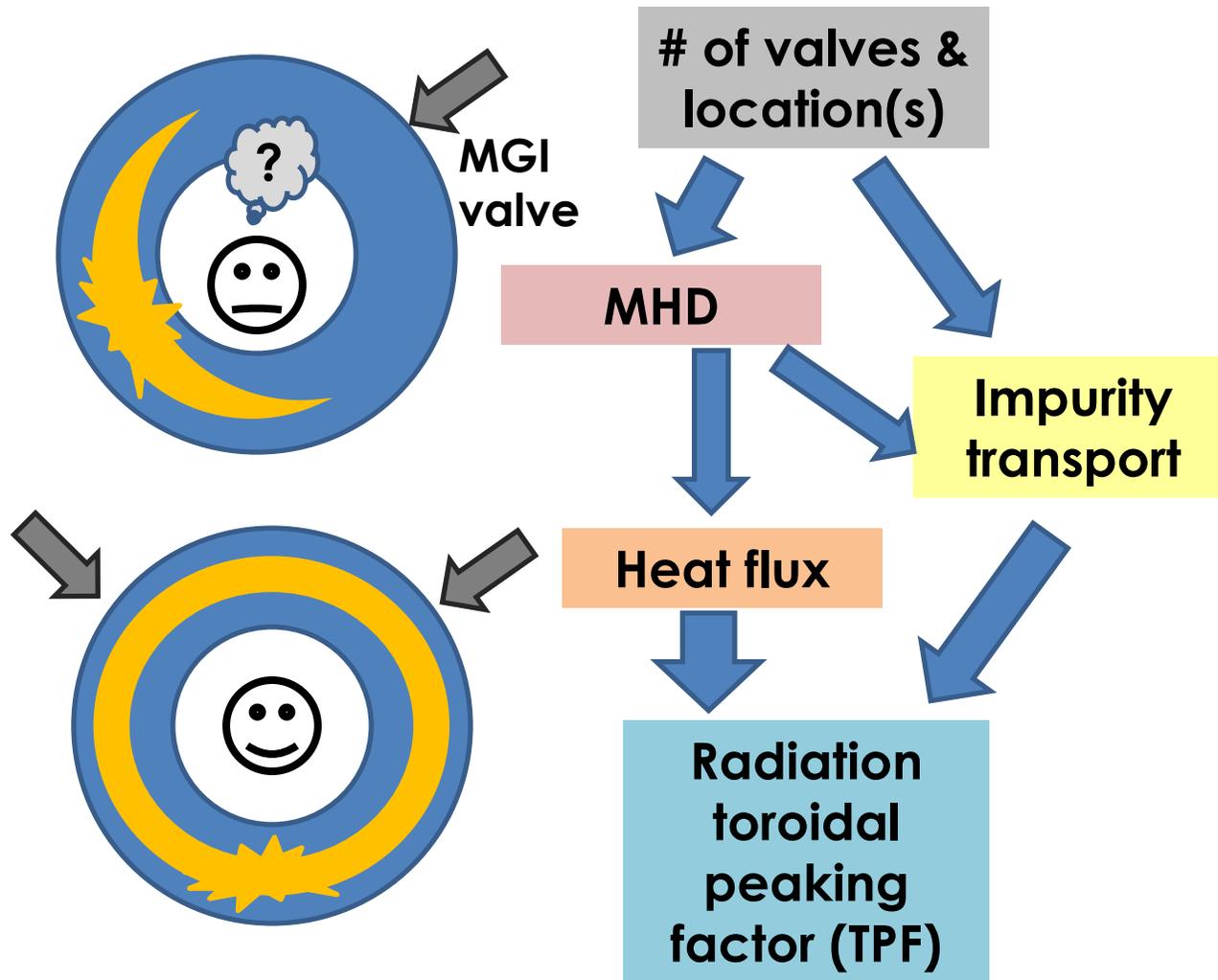


- 1) Avoid conduction of large heat loads to the divertor during the thermal quench (TQ), and ...
- 2) Appropriately tailor the current quench (CQ) time to avoid large vessel forces

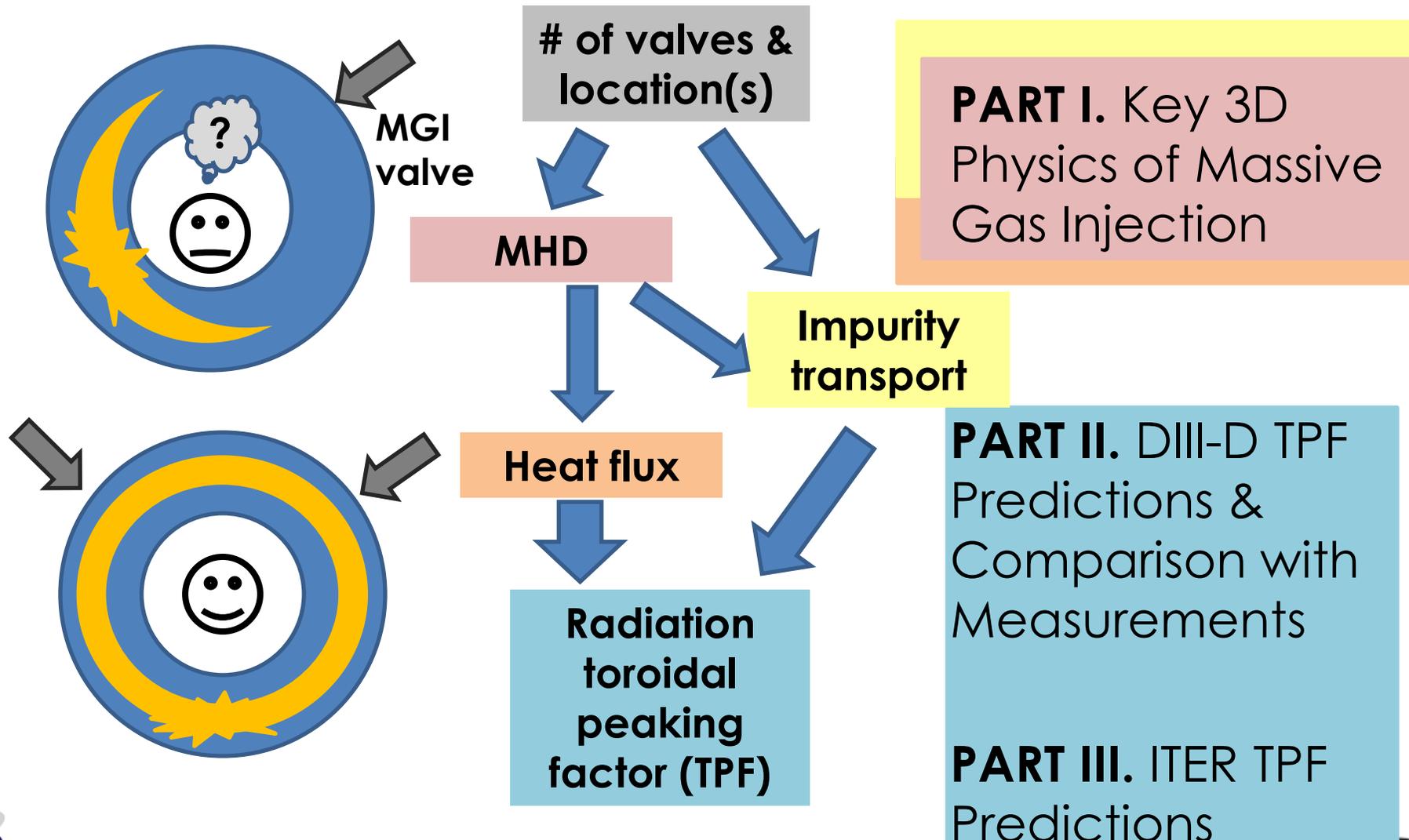
# Goal of massive gas injection is to isotropically radiate plasma stored energy



# NIMROD modeling finds a more complicated relationship

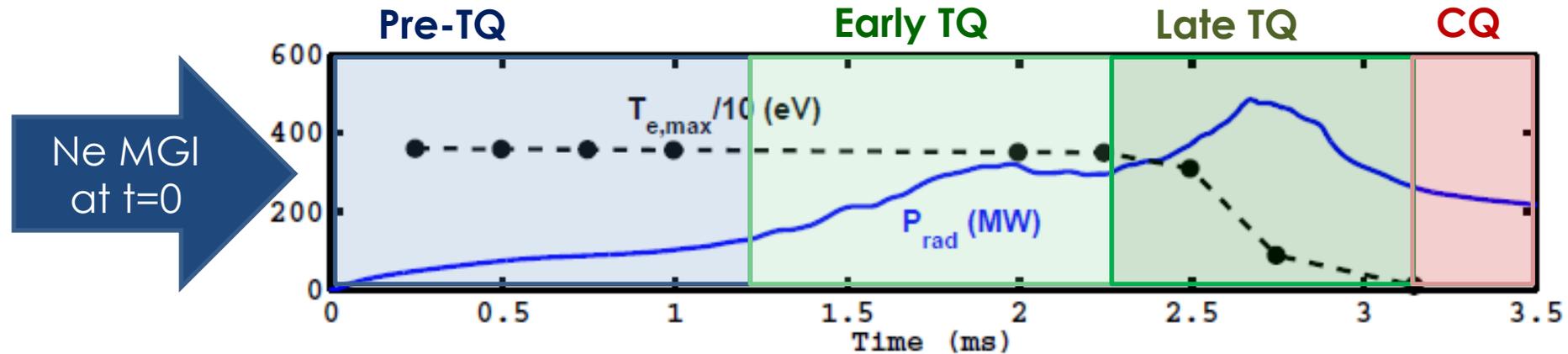


# Outline



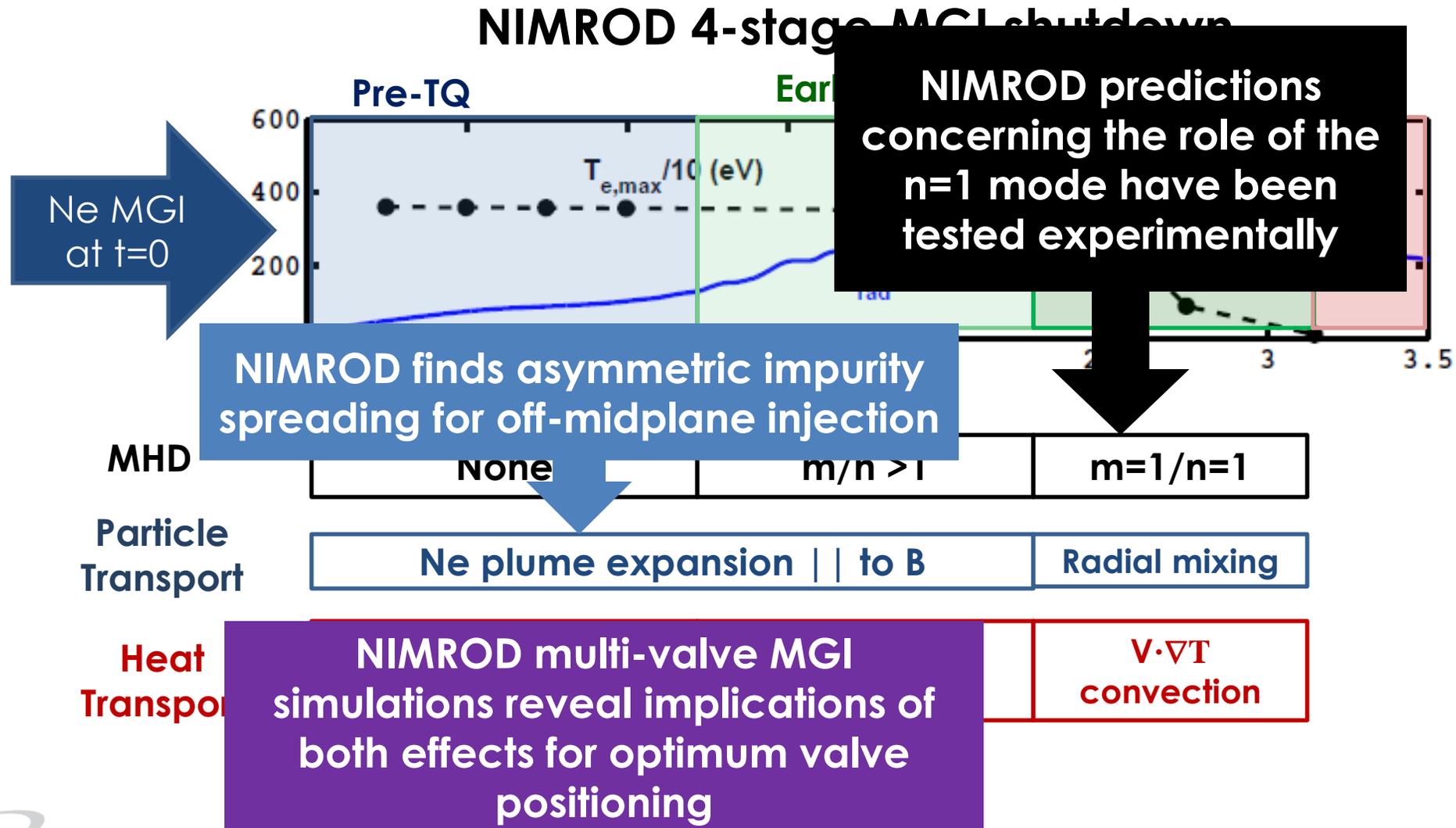
# PART I. Key 3D Physics of Massive Gas Injection

## NIMROD 4-stage MGI shutdown

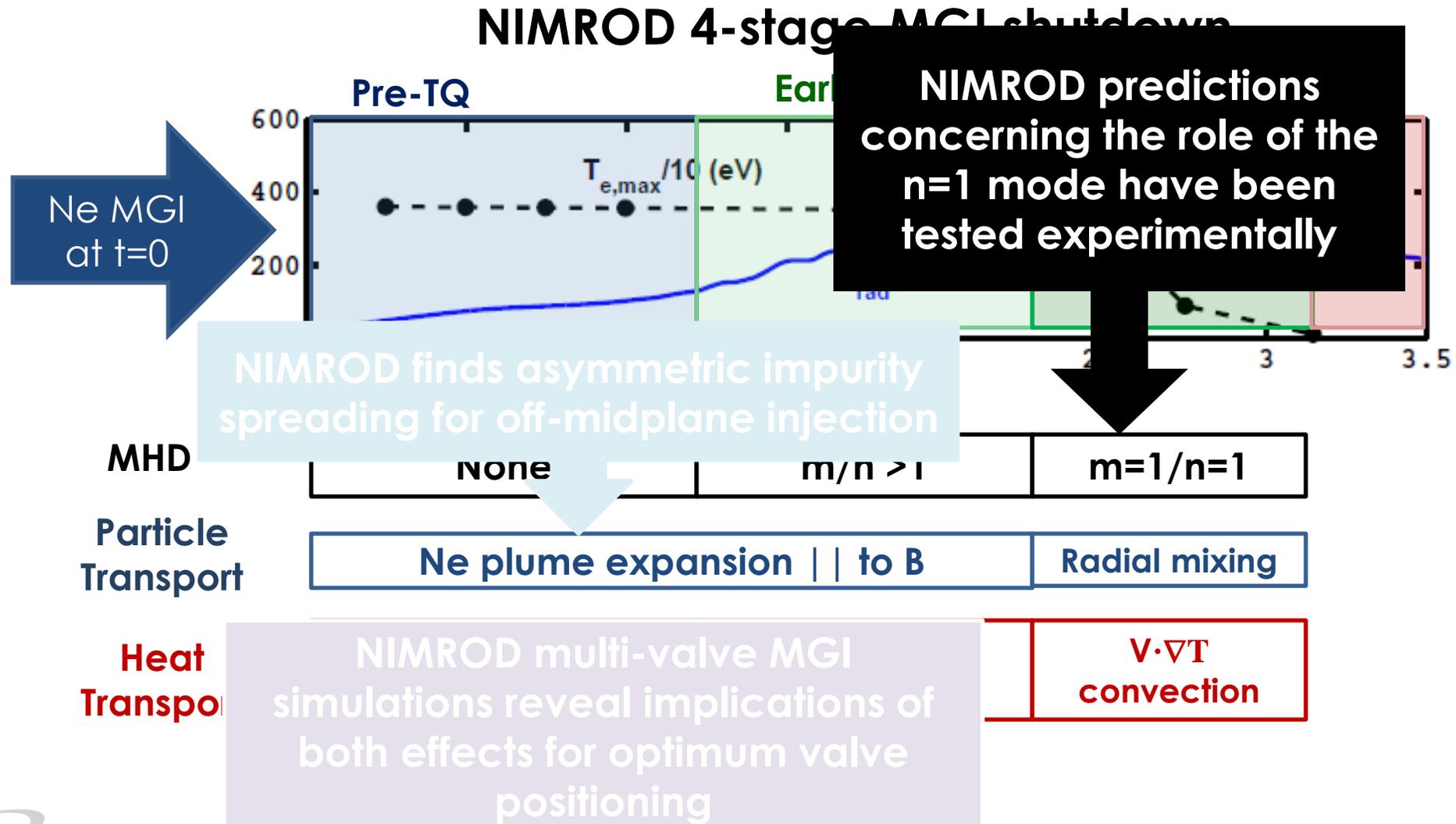


<b>MHD</b>	None	$m/n > 1$	$m=1/n=1$
<b>Particle Transport</b>	Ne plume expansion    to B		Radial mixing
<b>Heat Transport</b>	Slow $\perp$ conduction	Fast    $\delta B_r$ conduction	$\mathbf{V} \cdot \nabla T$ convection

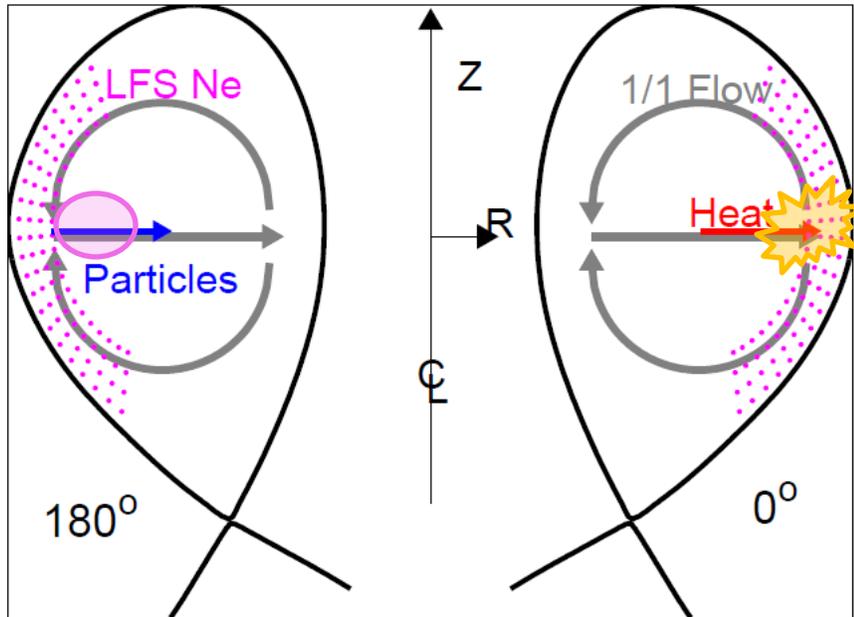
# PART I. Key 3D Physics of Massive Gas Injection



# PART I. Key 3D Physics of Massive Gas Injection

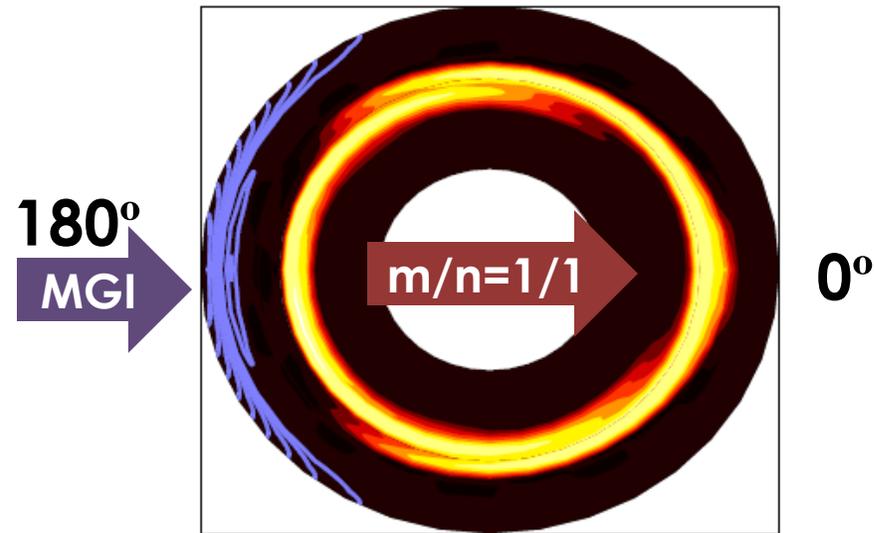


# NIMROD simulations produced two predictions regarding the role of the 1/1 in an MGI TQ\*



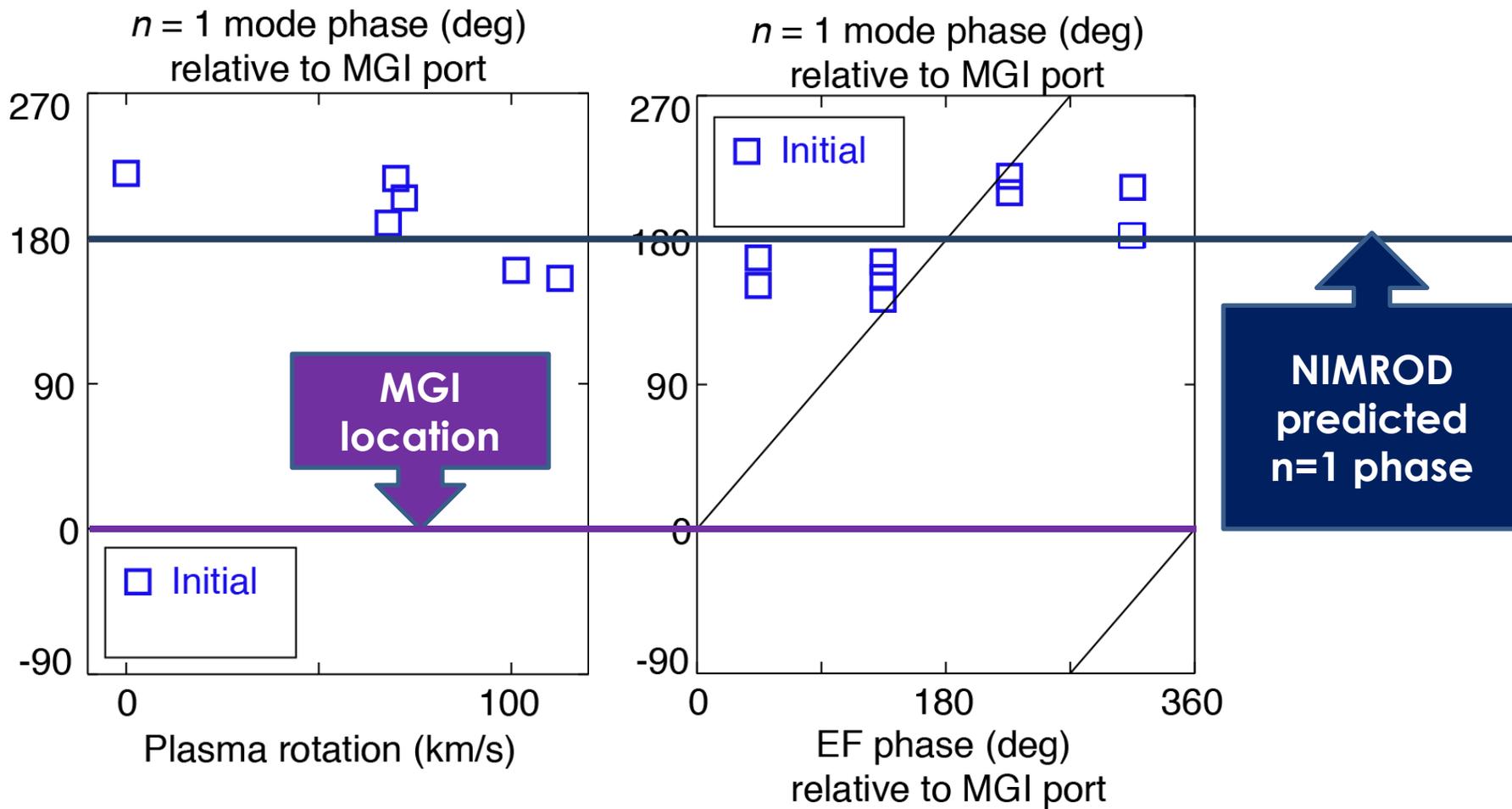
1) 1/1 phase determines location of toroidal radiation peaking due to asymmetric convected heat flux

2) Absent other asymmetries, 1/1 phase is anti-aligned with gas jet

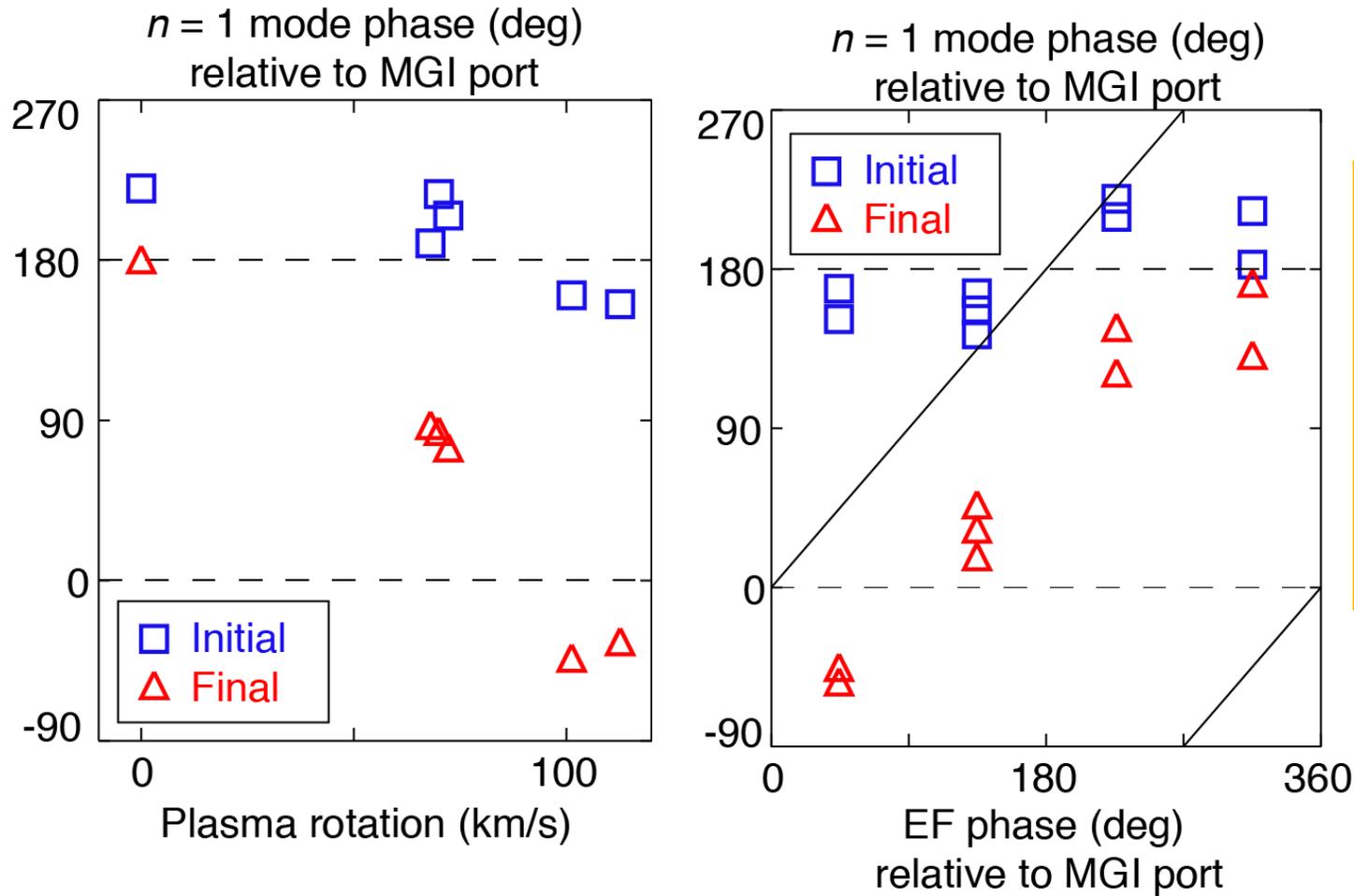


\*IZZO, V.A., Phys. Plasmas **20** (2013) 056107.

# DIII-D experiments: Initial $n=1$ phase corresponds to NIMROD prediction



# DIII-D experiments: $n=1$ phase at TQ influenced by rotation, error fields

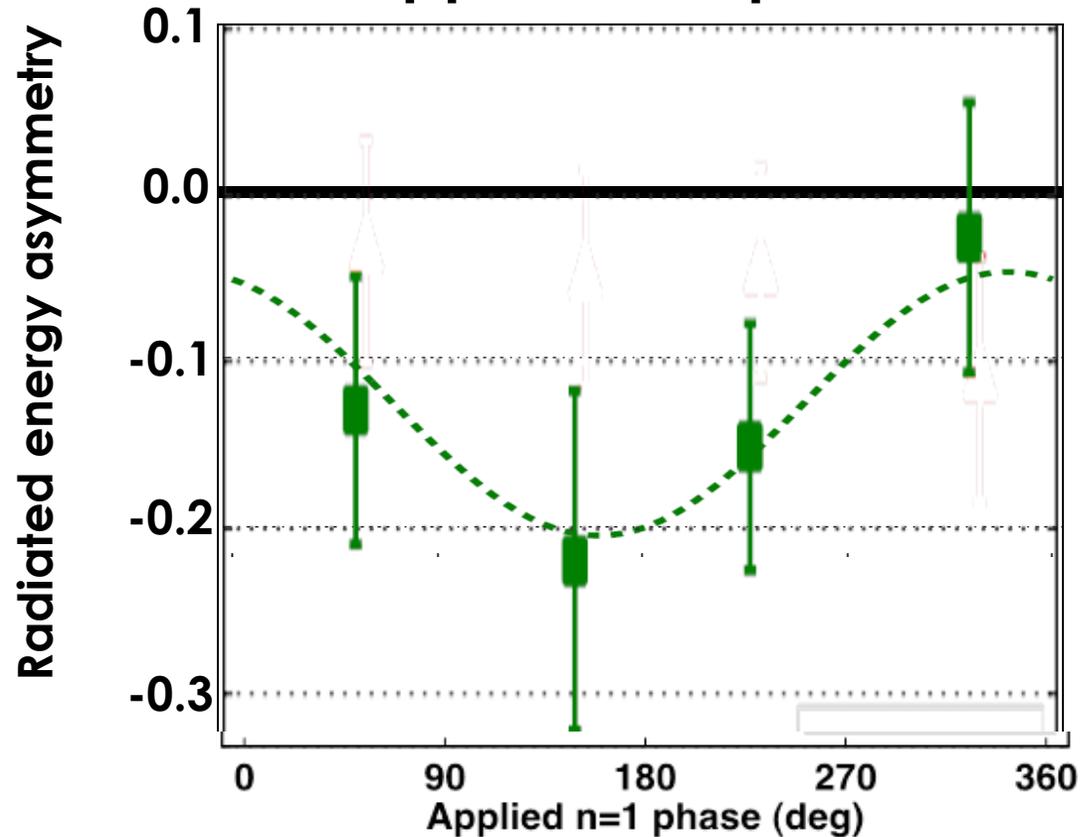


Rotation and error field effects (not in simulations) also determine final mode phase at TQ

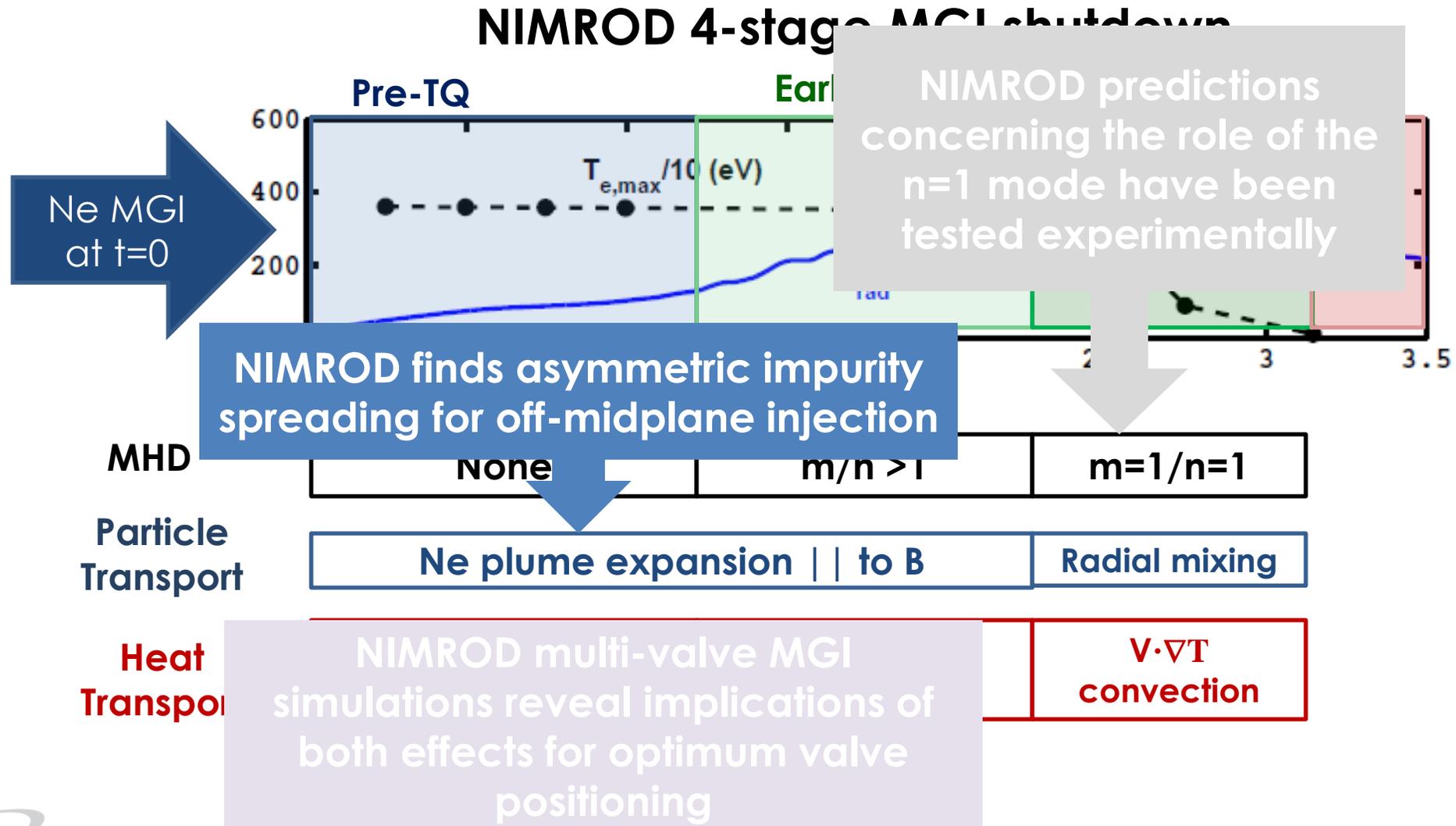
# Experiments verify: the phase of the n=1 mode (relative to the gas jet) affects asymmetry

→ DIII-D experiments:  
Changing phase of applied n=1 fields changes measured radiation asymmetry during TQ

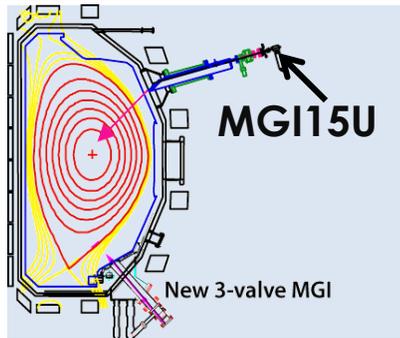
TQ  $W_{\text{rad}}$  asymmetry vs. applied n=1 phase



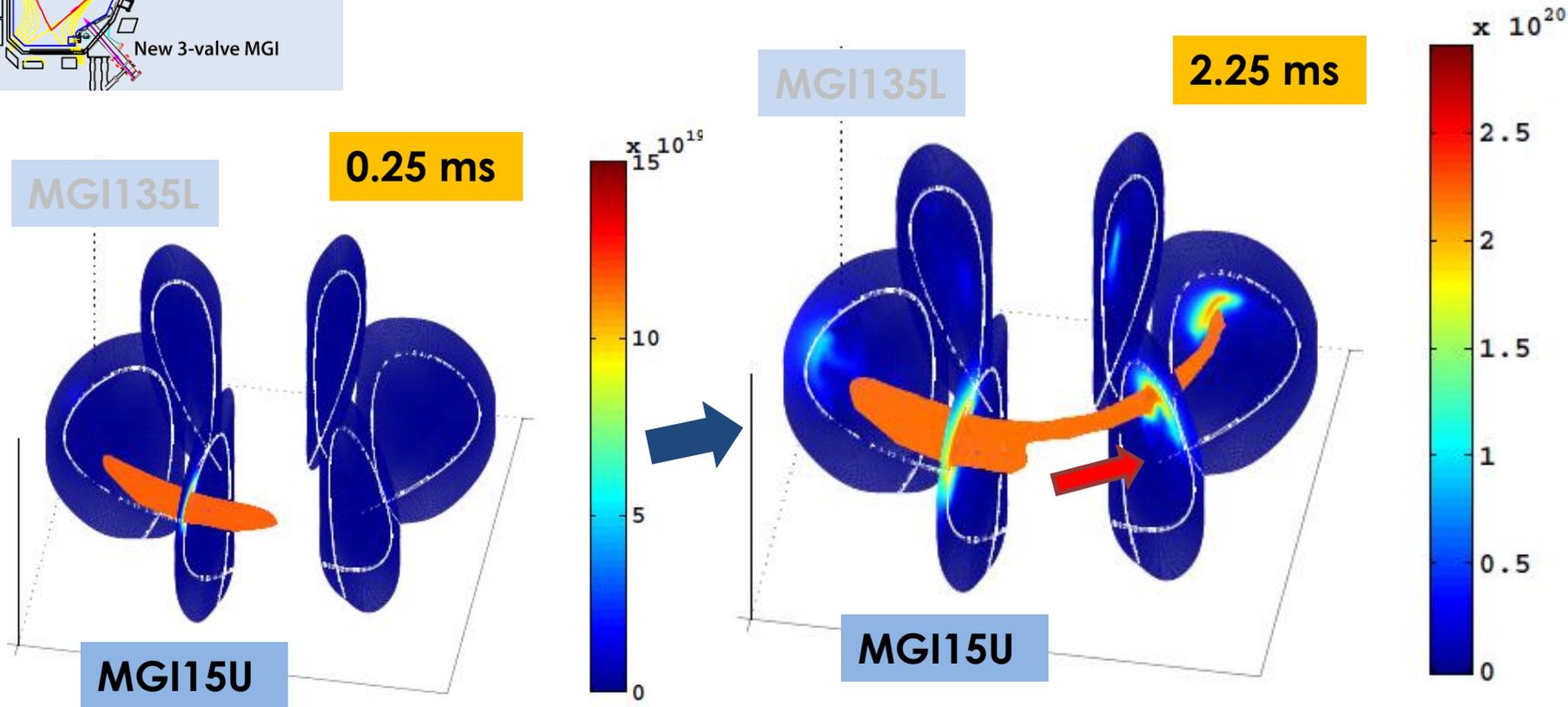
# PART I. Key 3D Physics of Massive Gas Injection



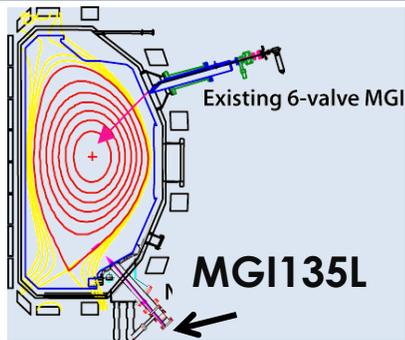
# Injected Ne plume spreads along B-field in one direction toroidally $\rightarrow$ toward HFS poloidally



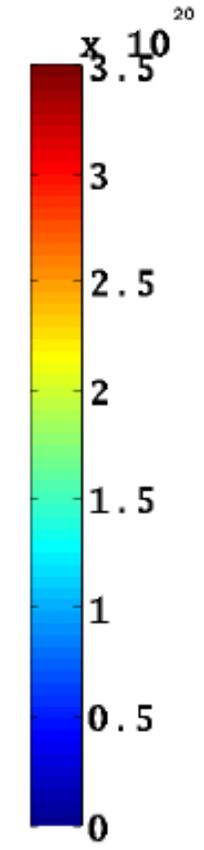
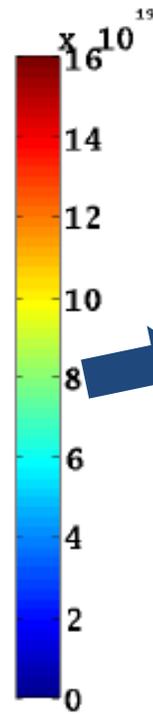
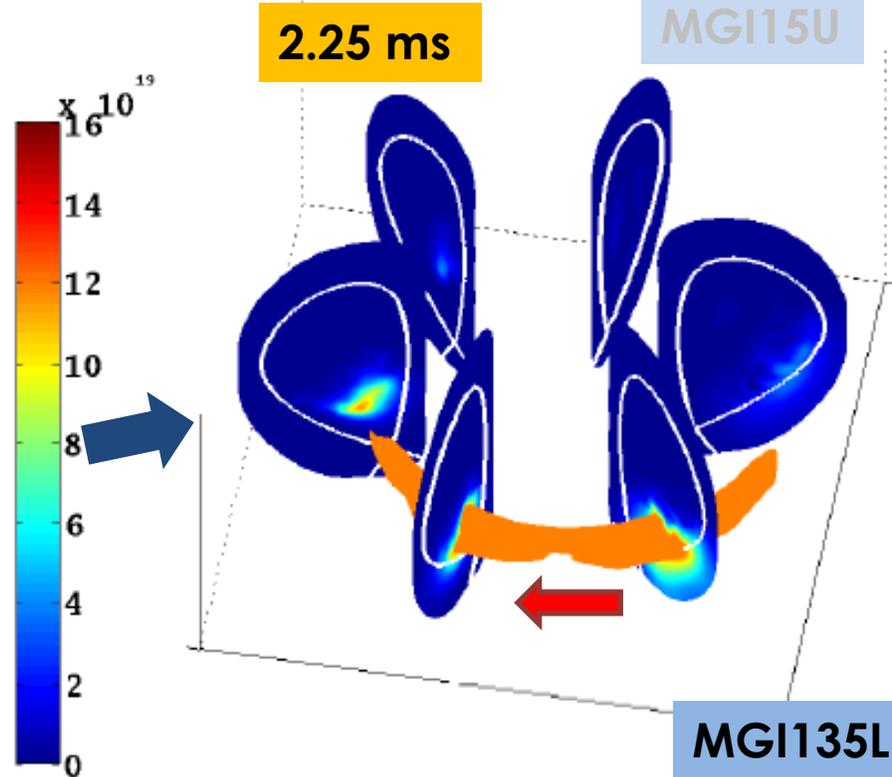
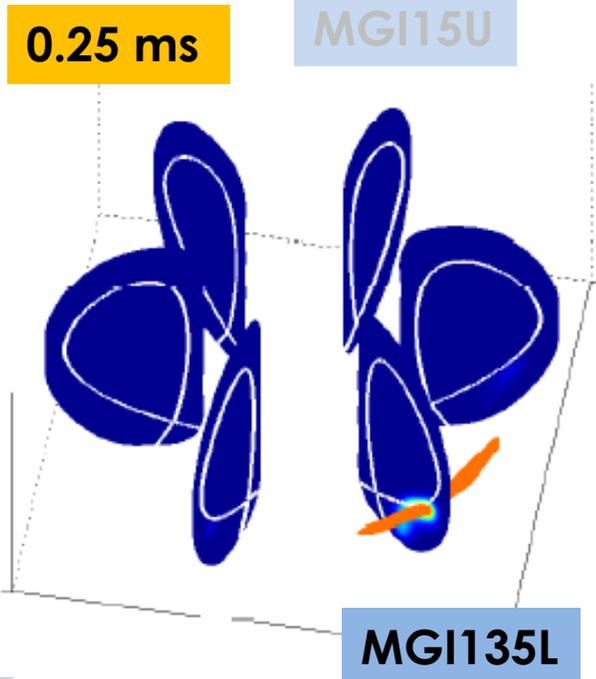
Contours/isosurface of ionized Ne density



# Below midplane jet spreads in the opposite toroidal direction, also toward HFS

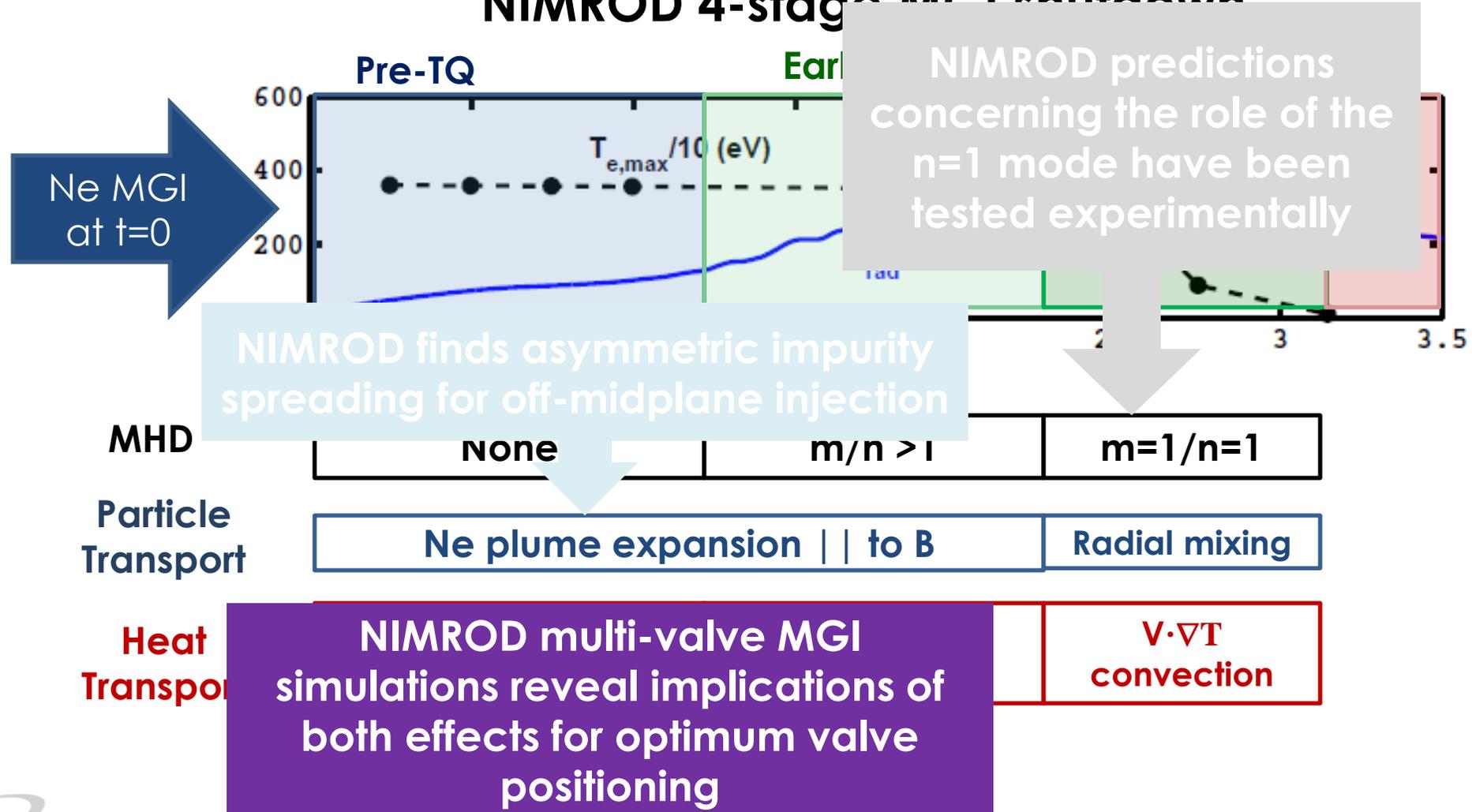


Contours/isosurface of ionized Ne density

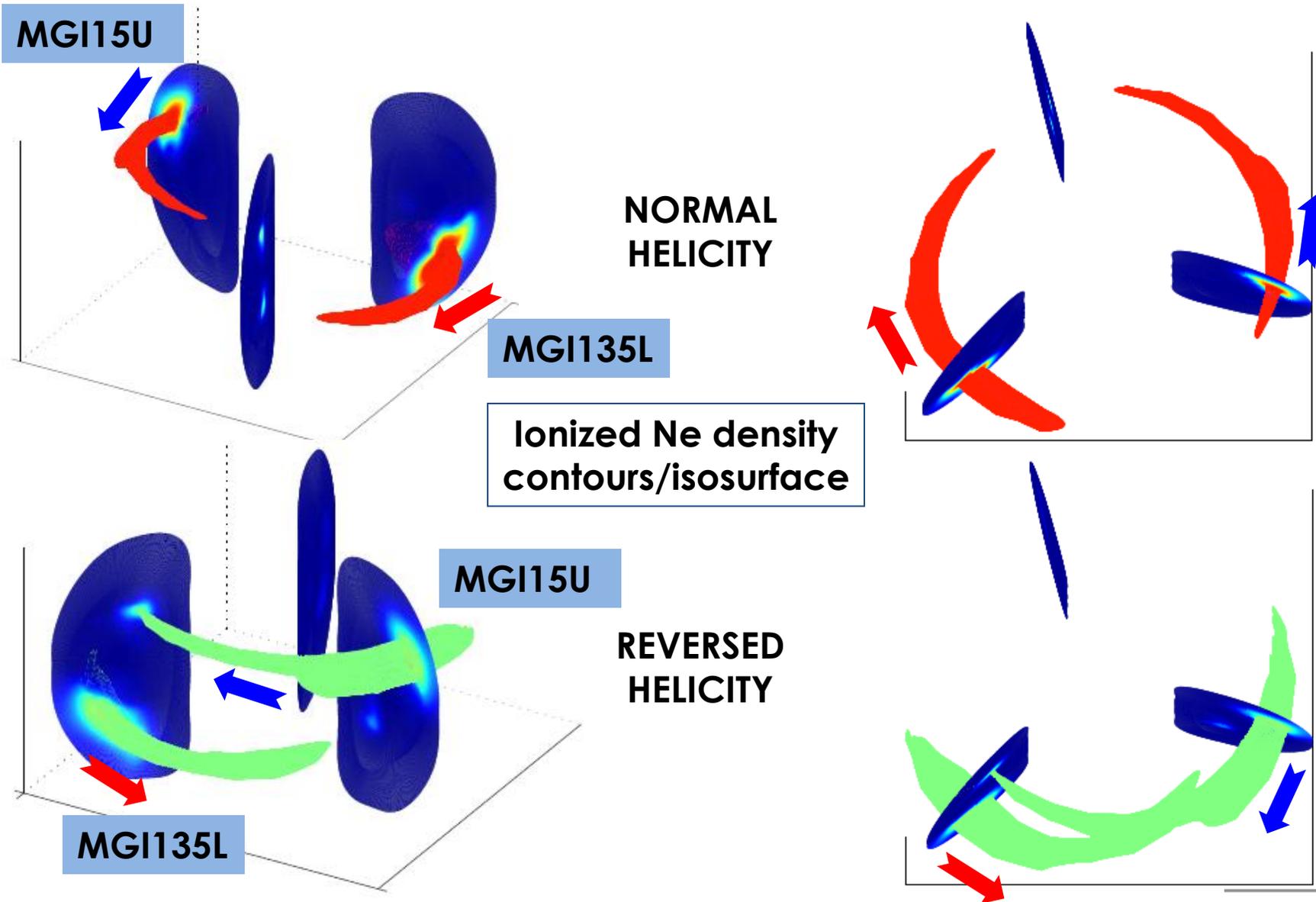


# PART I. Key 3D Physics of Massive Gas Injection

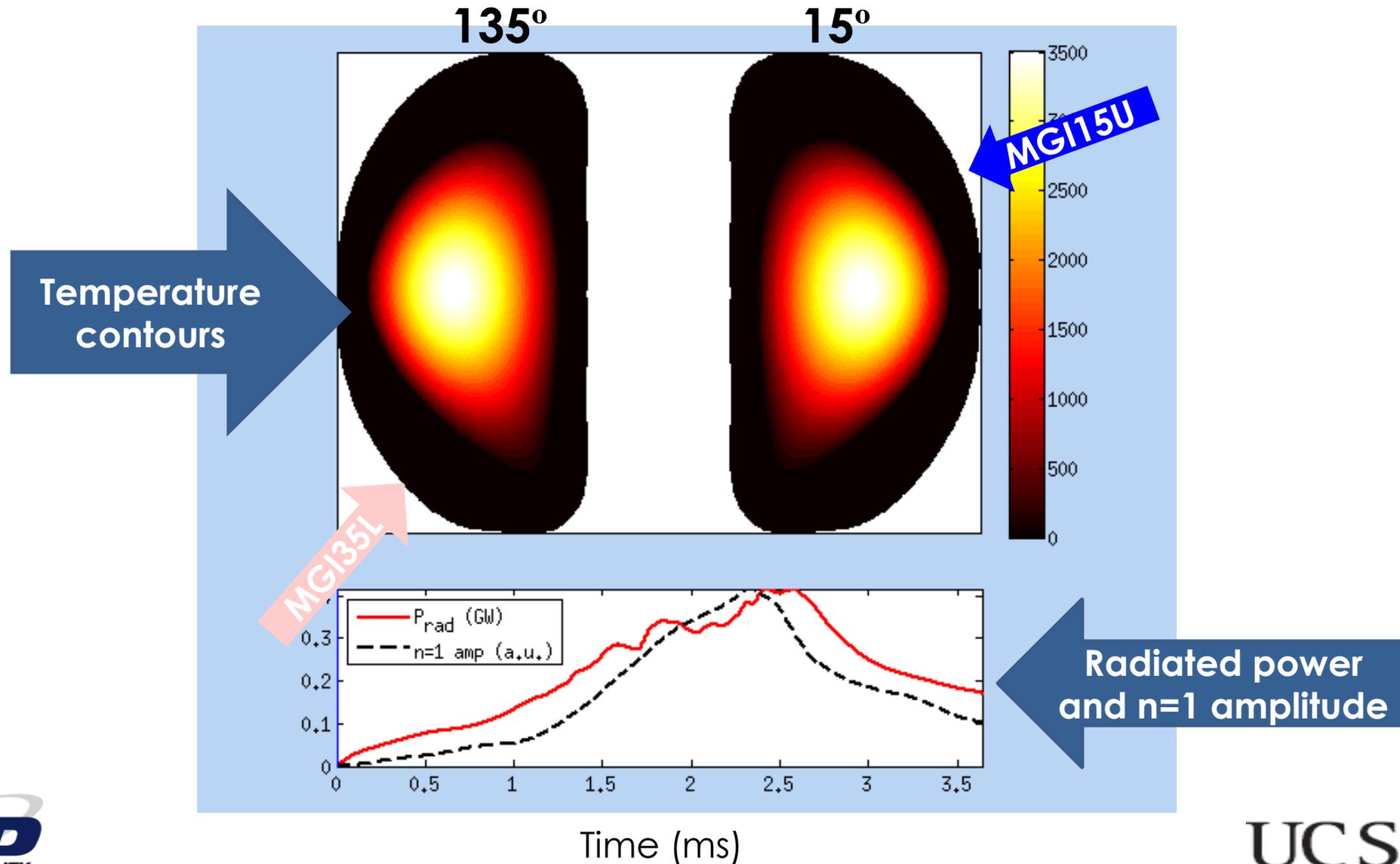
## NIMROD 4-stage MGI shutdown



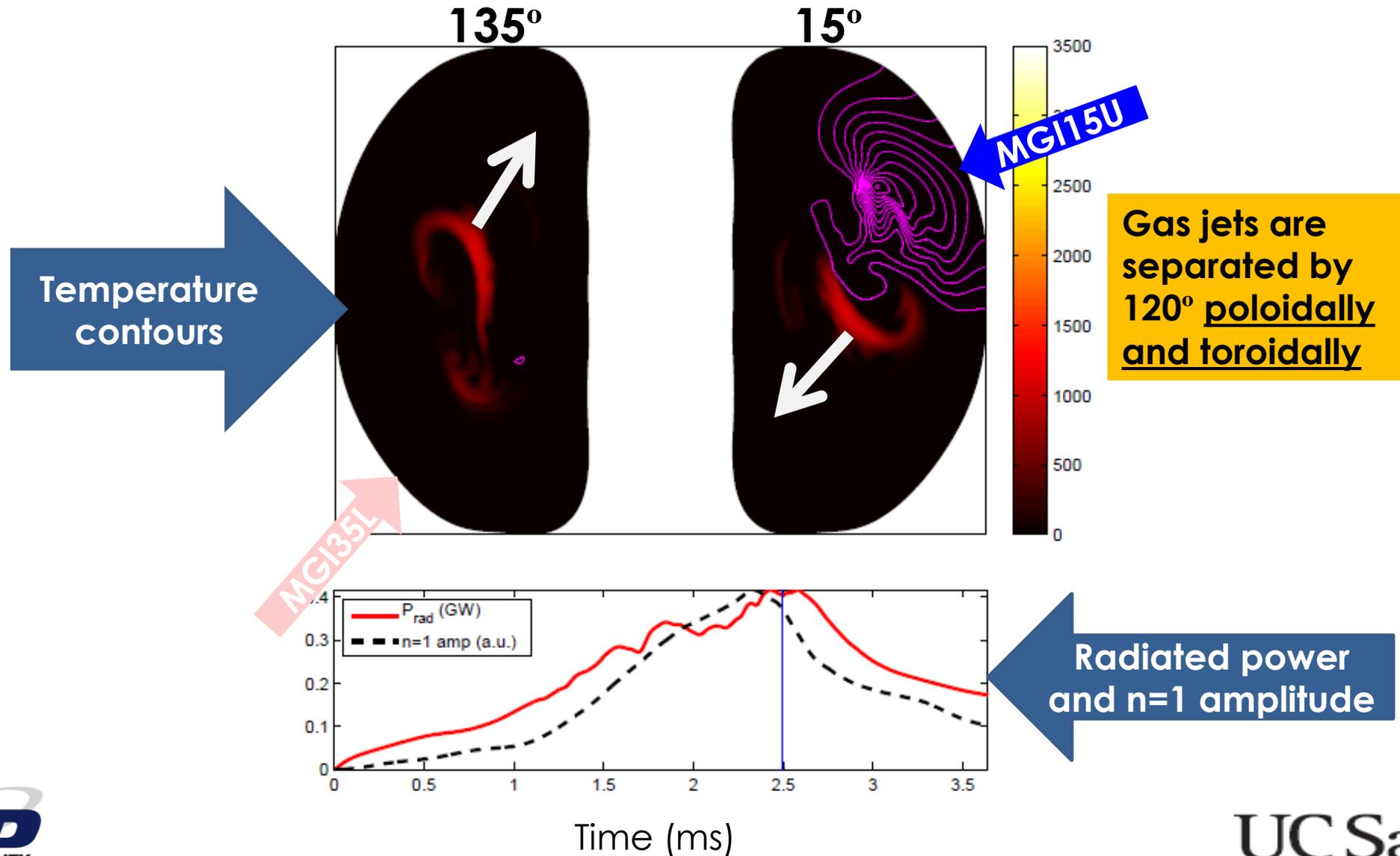
# NIMROD: $I_p$ direction affects direction of impurity spreading



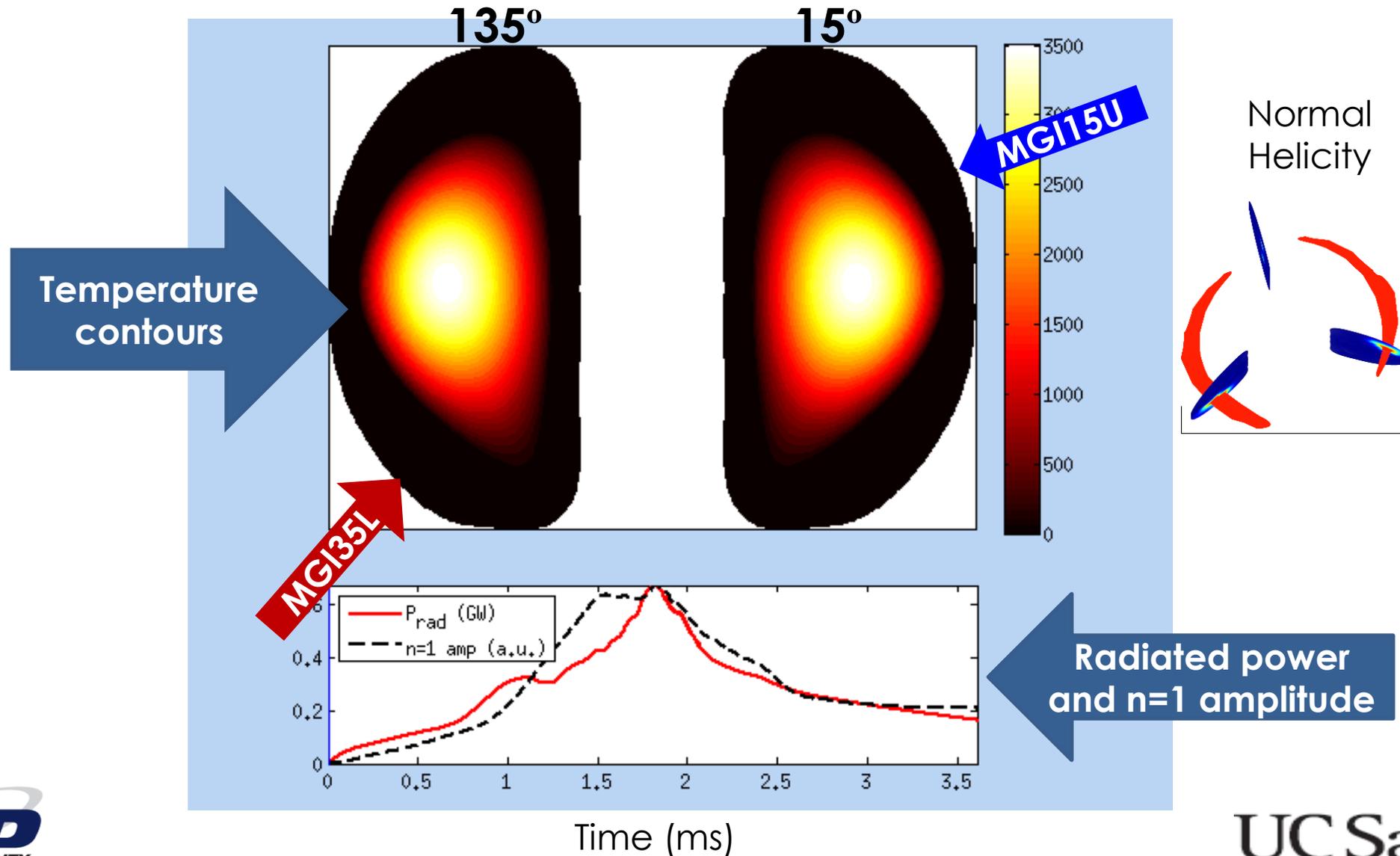
# Relative spacing of gas valves affects interaction with 1/1 mode



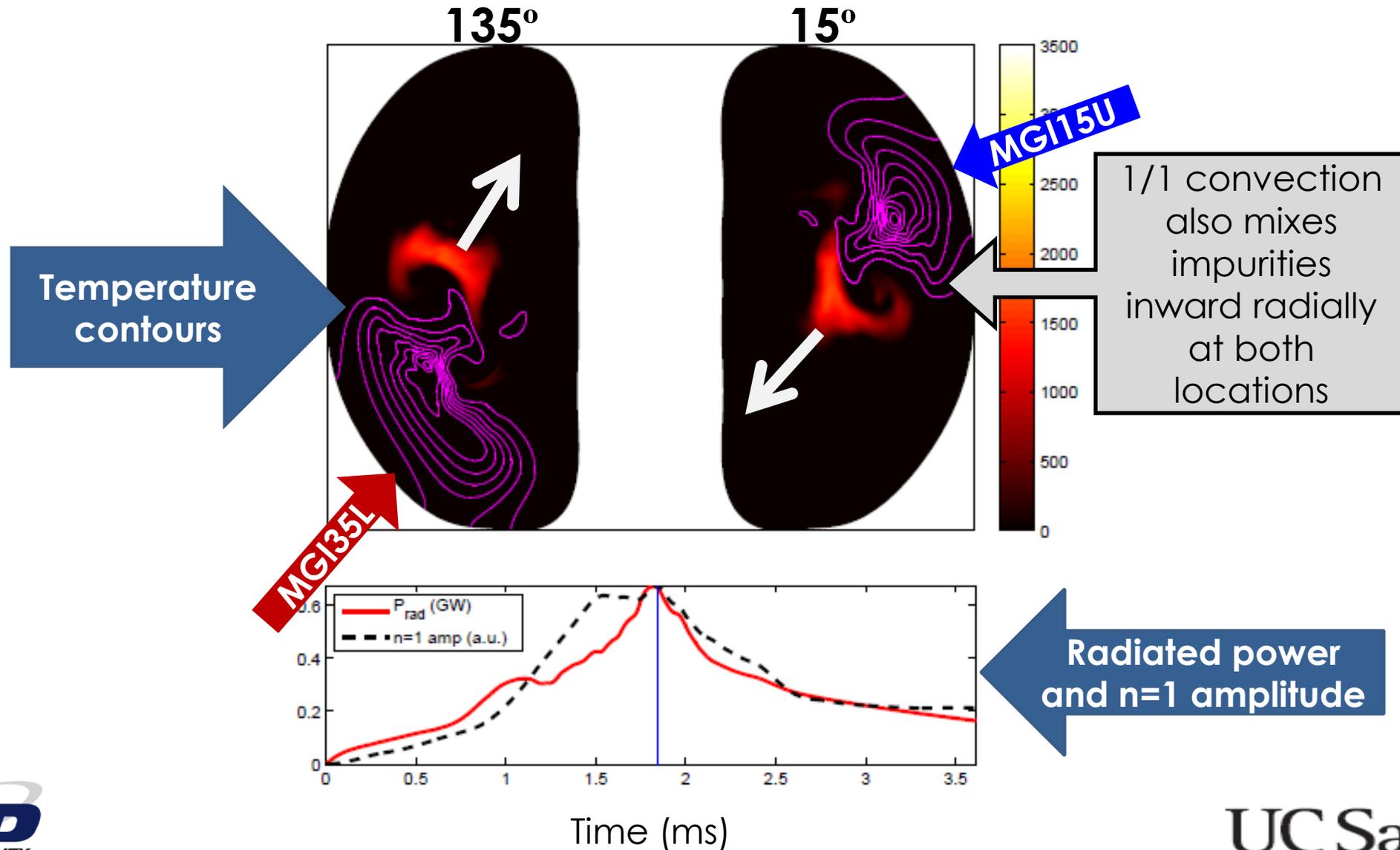
# MGI15U and MGI135L will tend to drive the same 1/1 mode phase



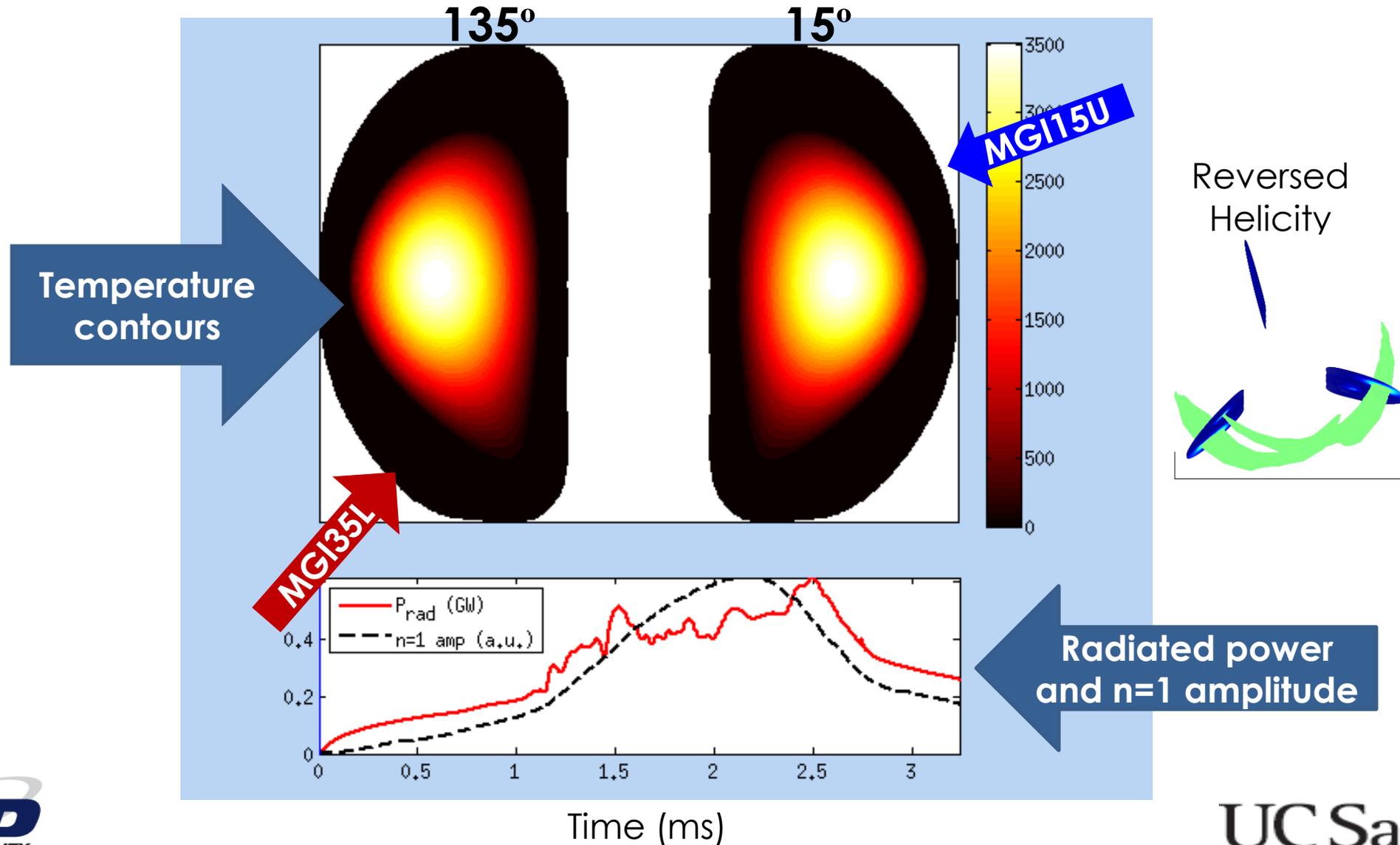
# Simulation with both gas jets drives same mode phase as single jet



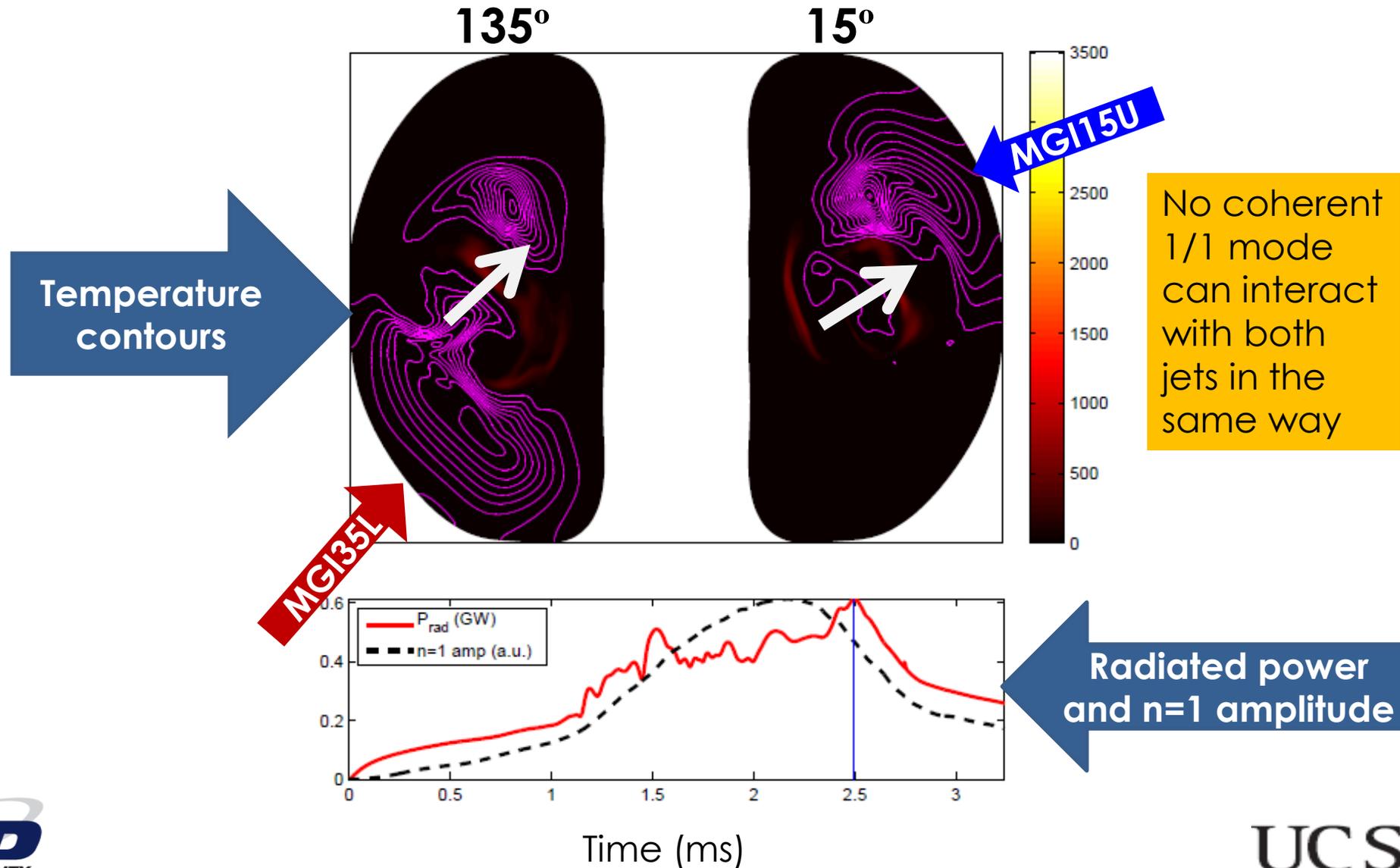
# Heat flux due to 1/1 convection is simultaneously away from both jets



# In reversed helicity, spacing of two jets no longer coheres with 1/1 symmetry



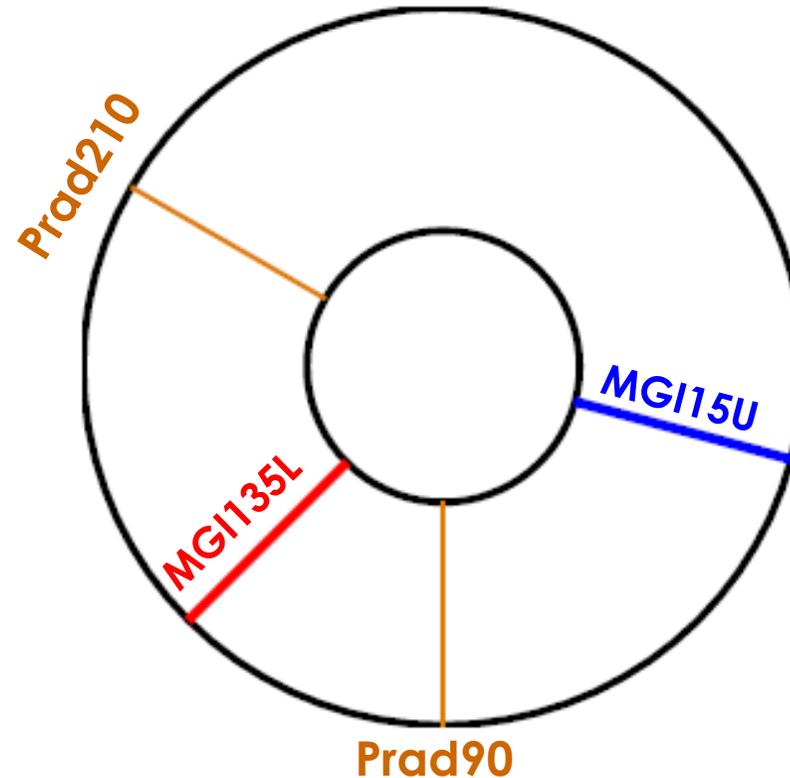
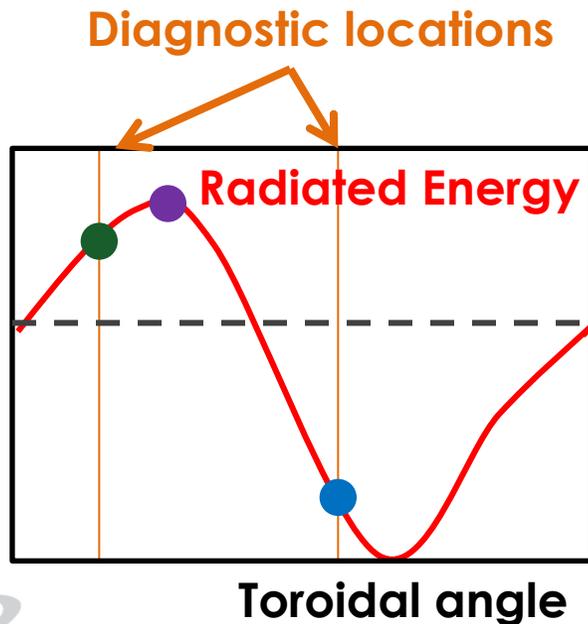
# Interaction of 1/1 mode with each of the two impurity plumes is very different



# PART II. NIMROD asymmetry predictions and comparison with DIII-D measurements

→ DIII-D has two fast radiated power measurements

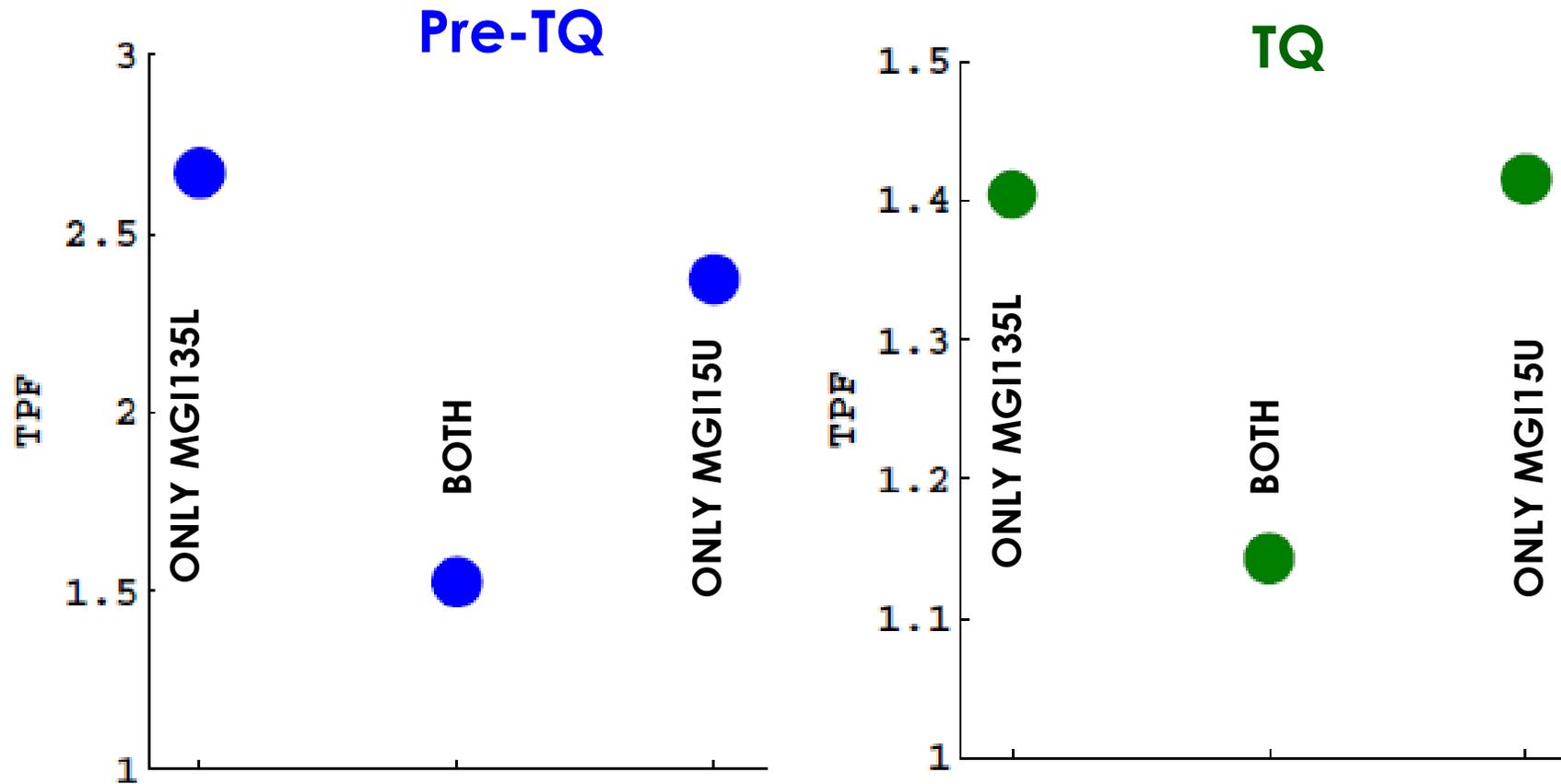
→ Both jets are closer to Prad90



$$\text{TPF} = \text{Max}(W_{\text{rad}}) / \text{Mean}(W_{\text{rad}})$$

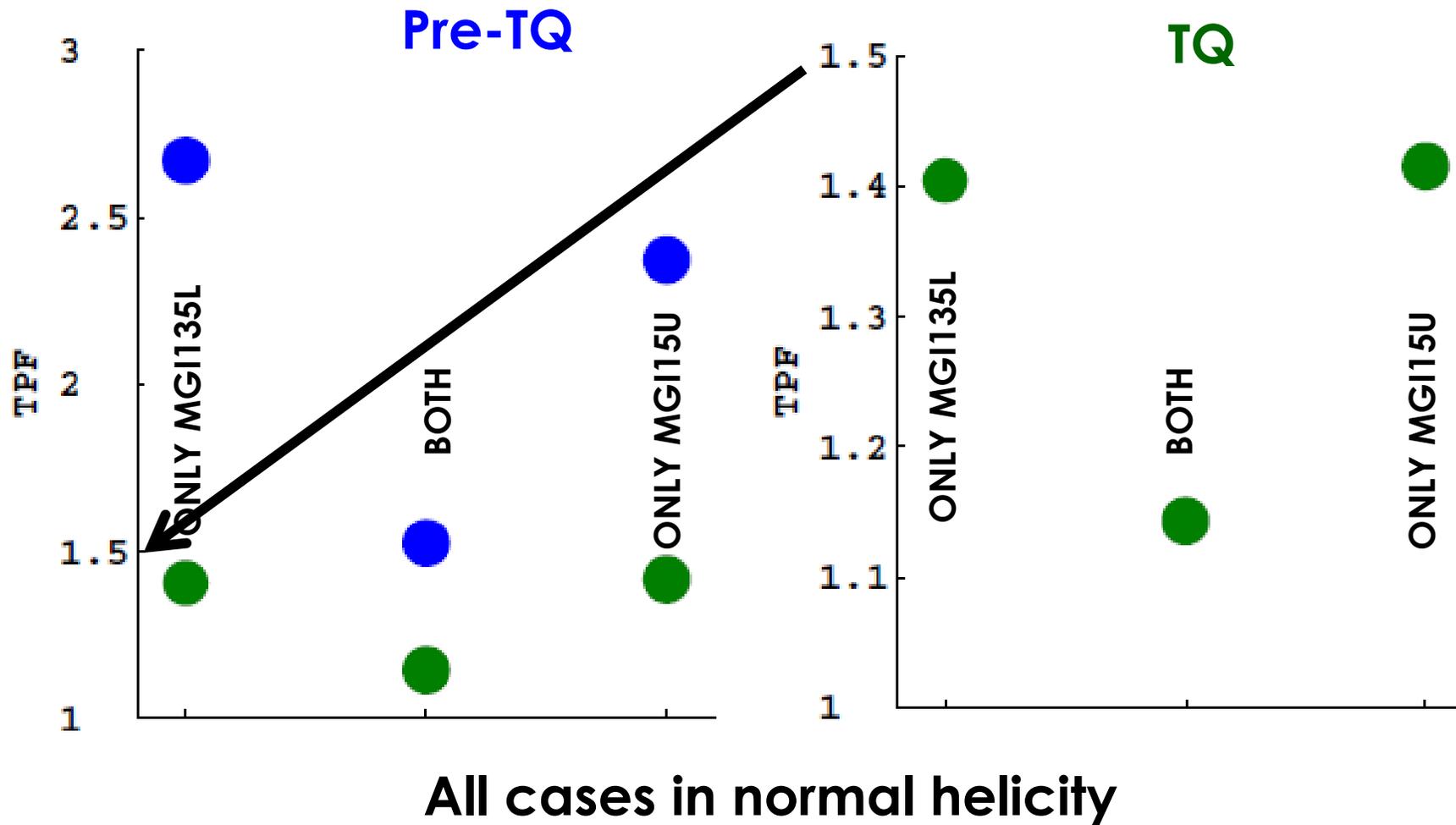
Clearly, asymmetry calculated from 2 measurement locations is an approximation...

# NIMROD predicts improved symmetry when both DIII-D jets are used



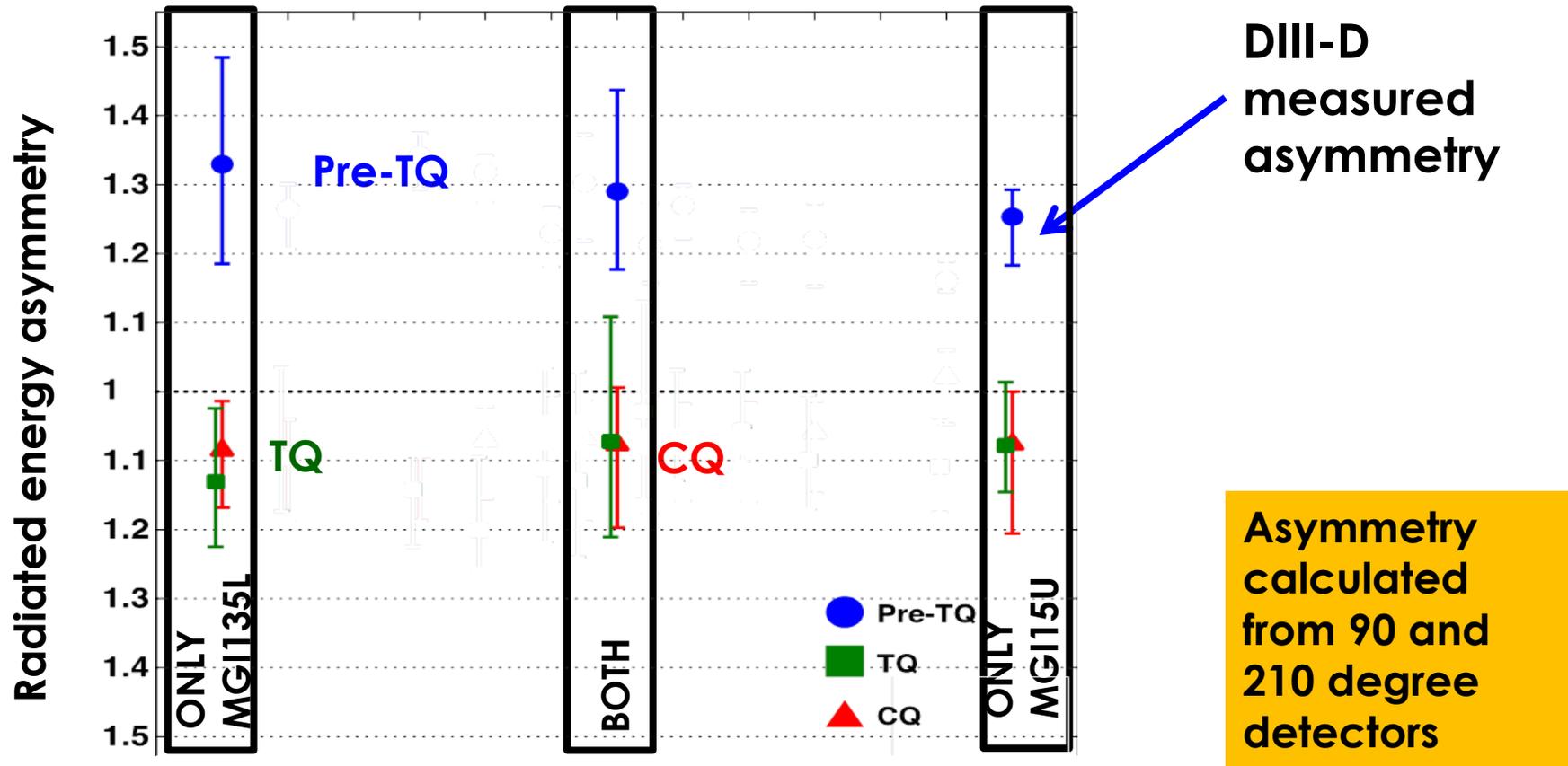
All cases in normal helicity

# NIMROD predicts improved symmetry when both DIII-D jets are used

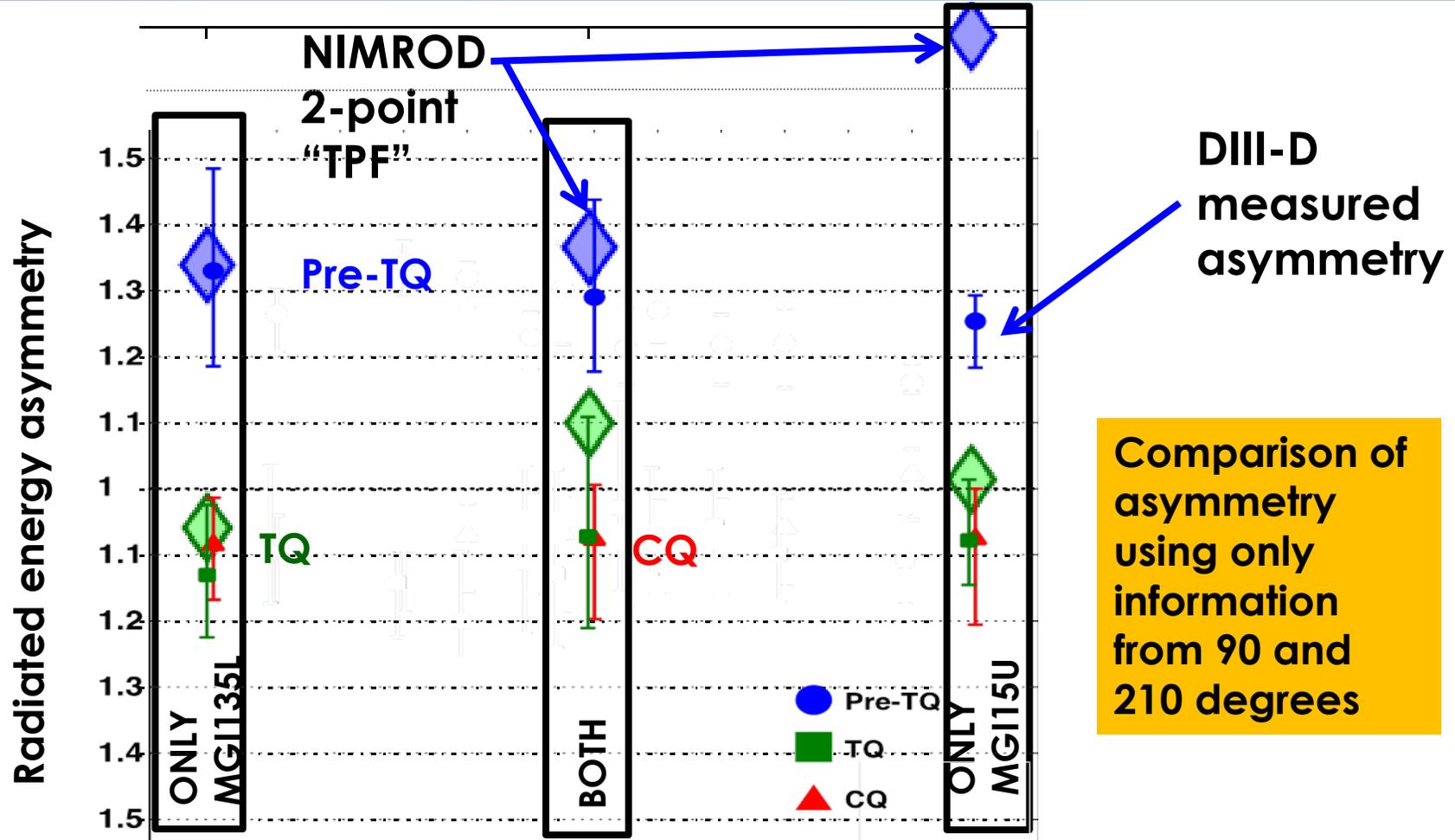


All cases in normal helicity

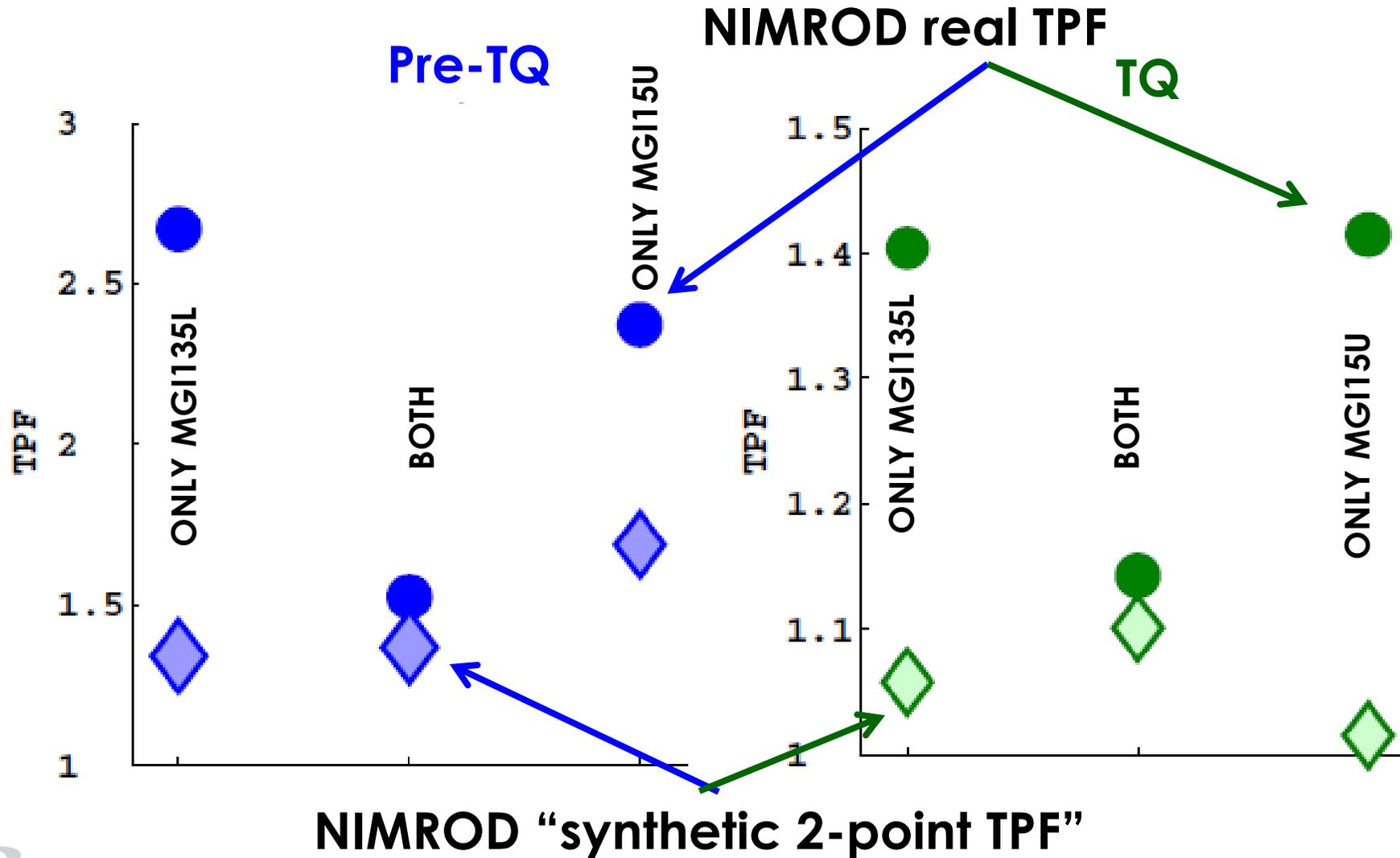
# DIII-D finds little or no variation in the asymmetry for one vs two gas jets



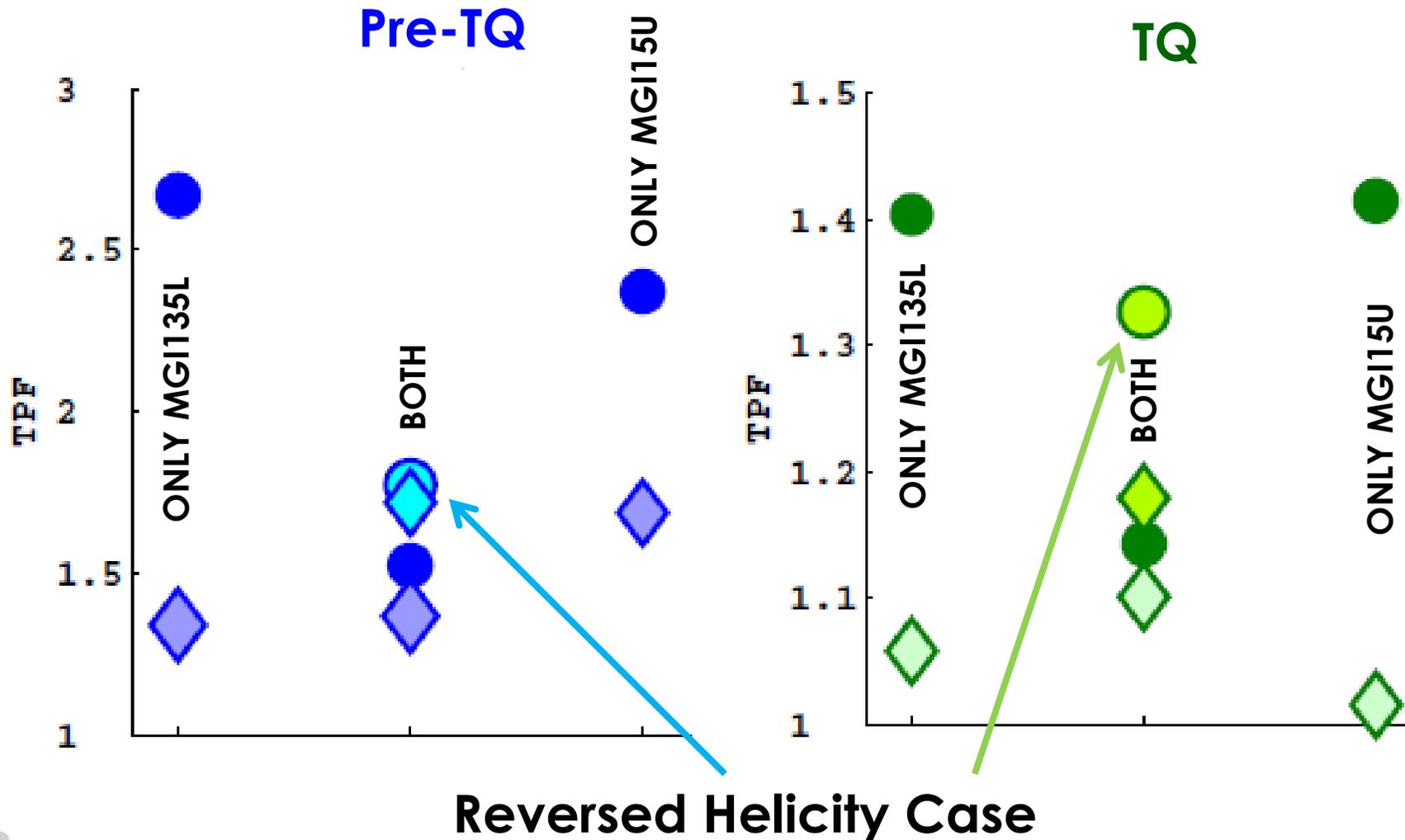
# NIMROD synthetic asymmetry diagnostic largely reproduces missing trend in DIII-D data



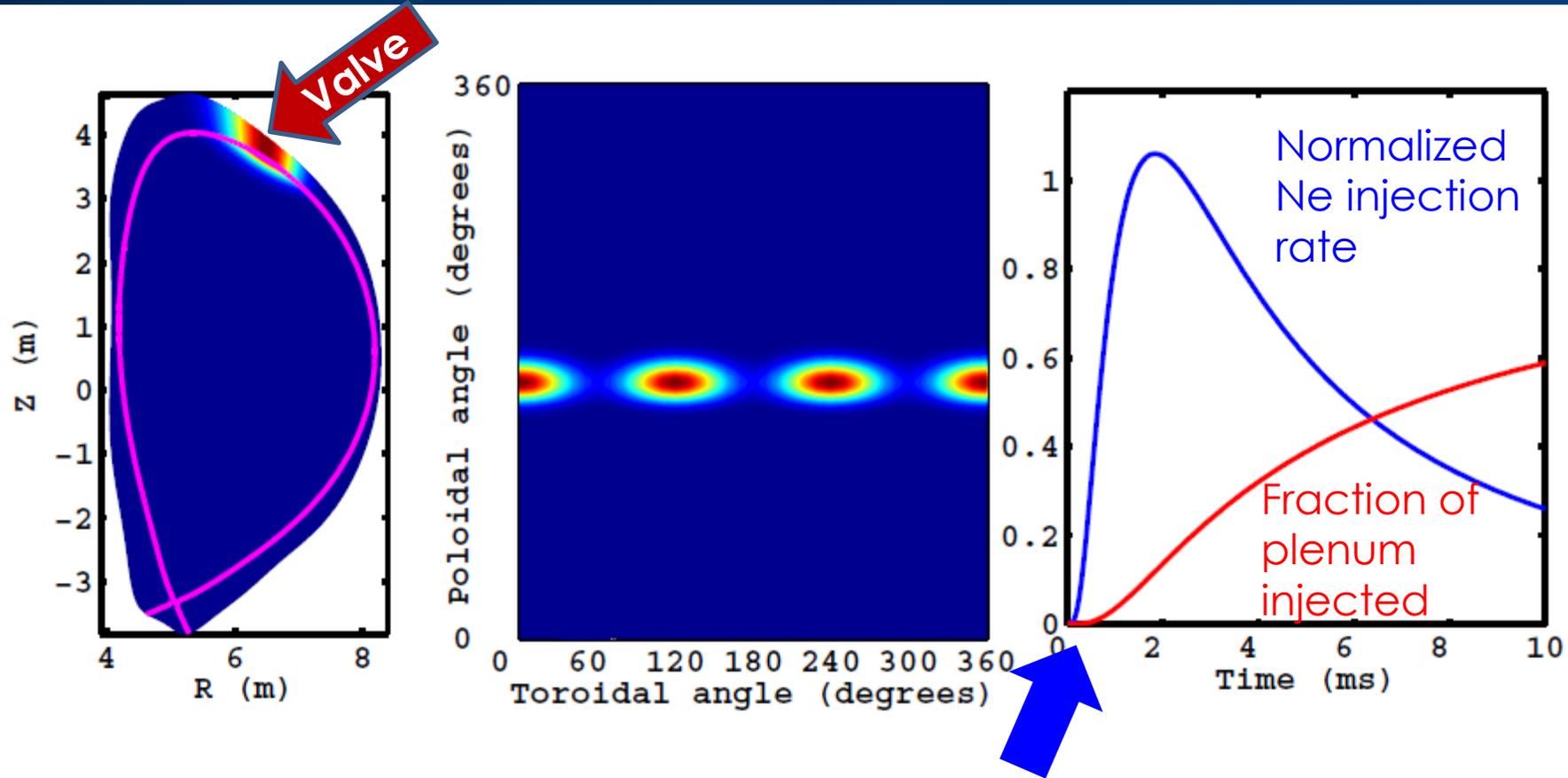
# NIMROD: 2-point "TPF" does not capture real trend in TPF



# NIMROD: reversing helicity increases TQ TPF with 2 jets



# Part III. ITER simulations use three upper ports allocated for TQ mitigation part of DMS



Total particle injection rate vs. time based on FLUENT calculations

→ Assumes 1 m delivery tube: unrealistically short!

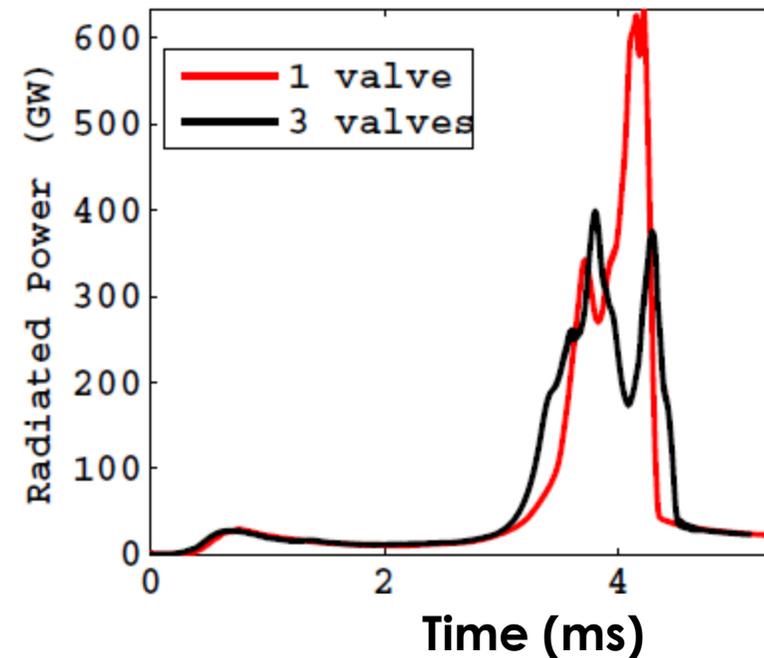
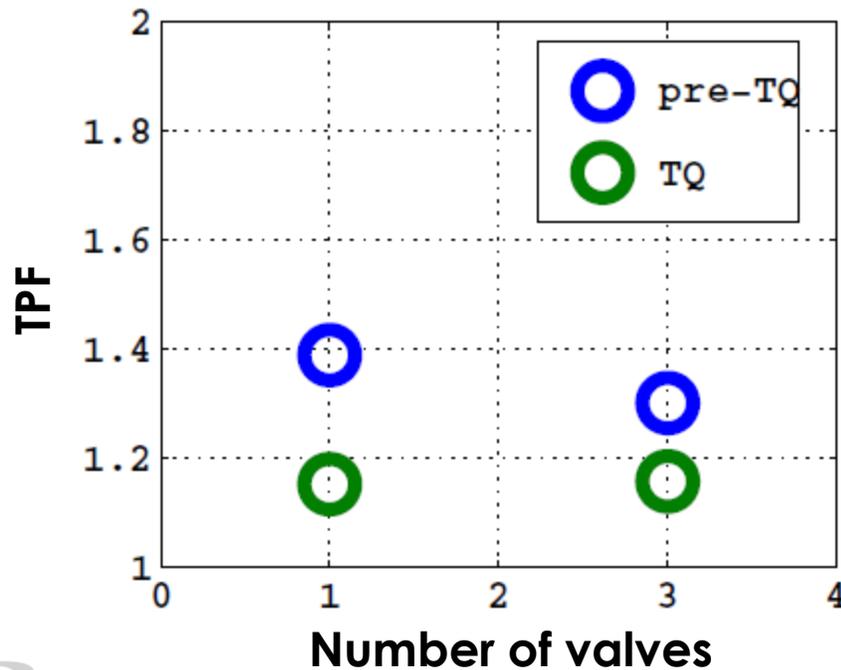
# 3-valves and 1-valve have same TPF, different TQ durations

- Slight decrease in TPF during pre-TQ with 3 valves

- Virtually no change in TPF during TQ

- Single valve has higher maximum Prad

- Three valve has longer TQ duration



# NIMROD modeling provides new physics insights into MGI with single or multiple gas valves

NIMROD predicts that DIII-D 2-valve configuration reduces TPF, but increased diagnostic resolution is needed to capture trend, validate model

On ITER, 3 upper valve configuration is not found to reduce TPF compared to single upper valve during TQ

→ Single jet TPF during the thermal quench is not very severe in DIII-D or ITER

# NIMROD modeling provides new physics insights into MGI with single or multiple gas valves

NIMROD predicts that DIII-D 2-valve configuration reduces TPF, but increased diagnostic resolution is needed to capture trend, validate model

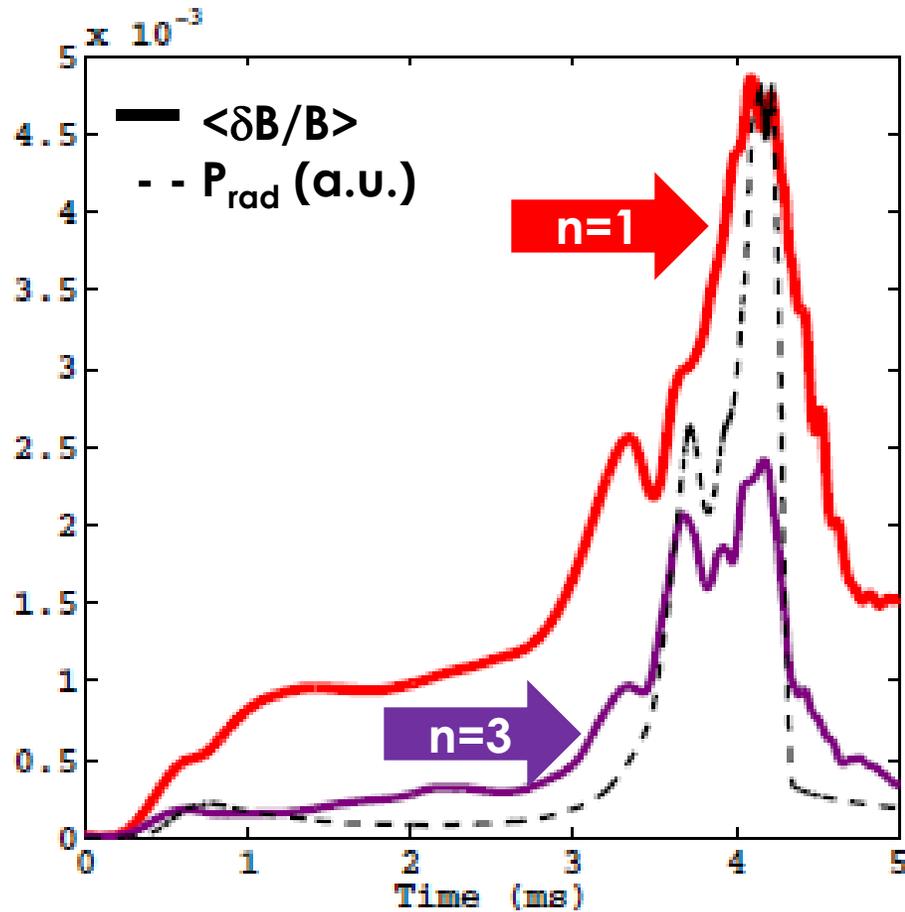
On ITER, 3 upper valve configuration is not found to reduce TPF compared to single upper valve during TQ

→ Single jet TPF during the thermal quench is not very severe in DIII-D or ITER

THANK YOU!

# # of valves $\rightarrow$ MHD Mode # $\rightarrow$ TQ duration?

1 valve  $\rightarrow$  n=1 dominant



3 valves  $\rightarrow$  n=3 dominant

