



First Principles Based Divertor Optimization A Unified MCF Divertor Framework applied to W7-X

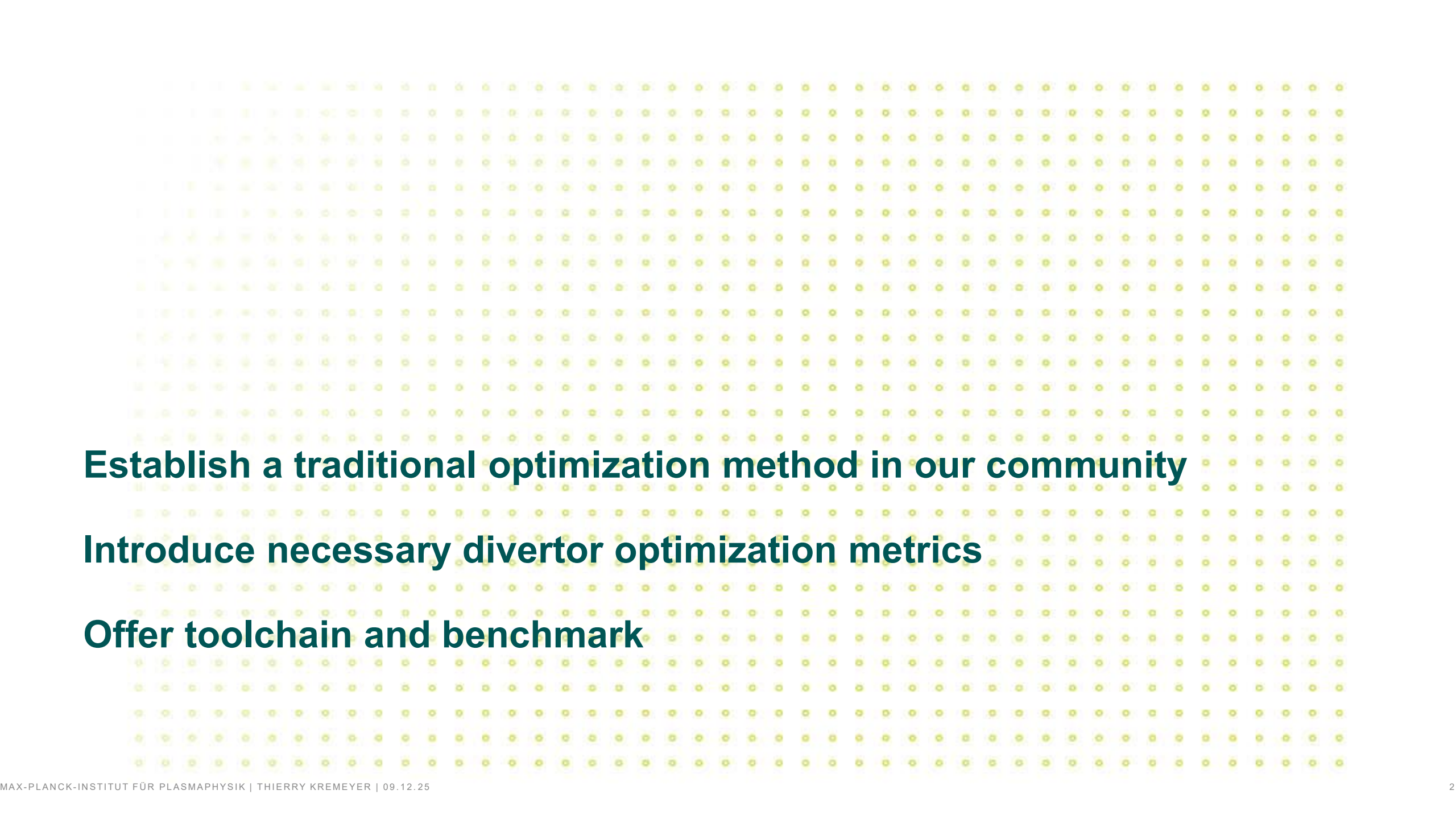
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C.P. Dhard¹, A. Kharwandikar¹, A. Pandey¹, M. Jakubowski¹, and M. Endler¹

¹ Max Planck Inst. for Plasma Physics, 17491 Greifswald, Germany

² University of Wisconsin – Madison, Madison, WI, USA



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Establish a traditional optimization method in our community

Introduce necessary divertor optimization metrics

Offer toolchain and benchmark

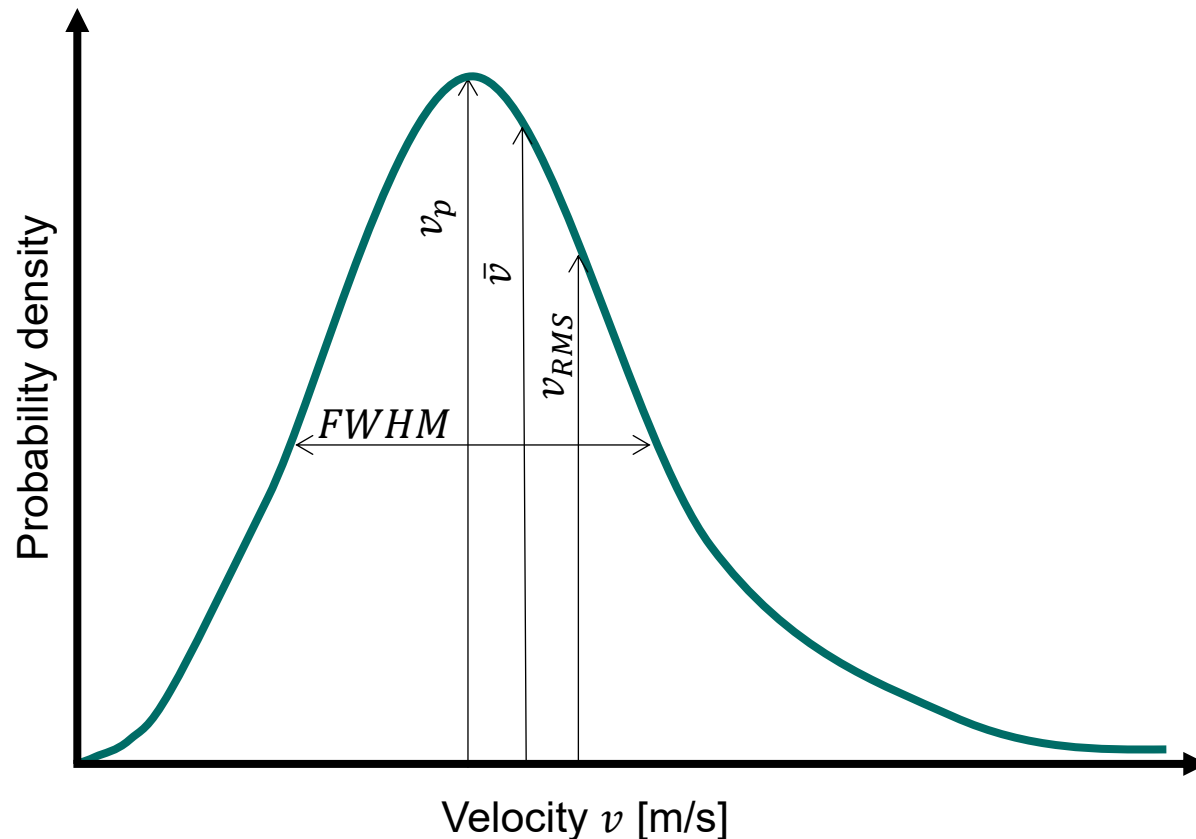
6 σ – Traditional optimization method based on statistical analysis



Plasma physics and nuclear fusion is full of stochastic processes!

How do we quantify them?

Maxwellian Probability Density Function (PDF)



Performance, reliability, & safety of nuclear power plants



Stabilize human/nuclear rated unstable systems
16x B83 (5E+15 J) = 12.5E+9 x ITER (6.4E+6 J)

LOCKHEED MARTIN

NORTHROP GRUMMAN



Design of landing rockets & safety of human rated spacecraft



Continuous quality & process optimization



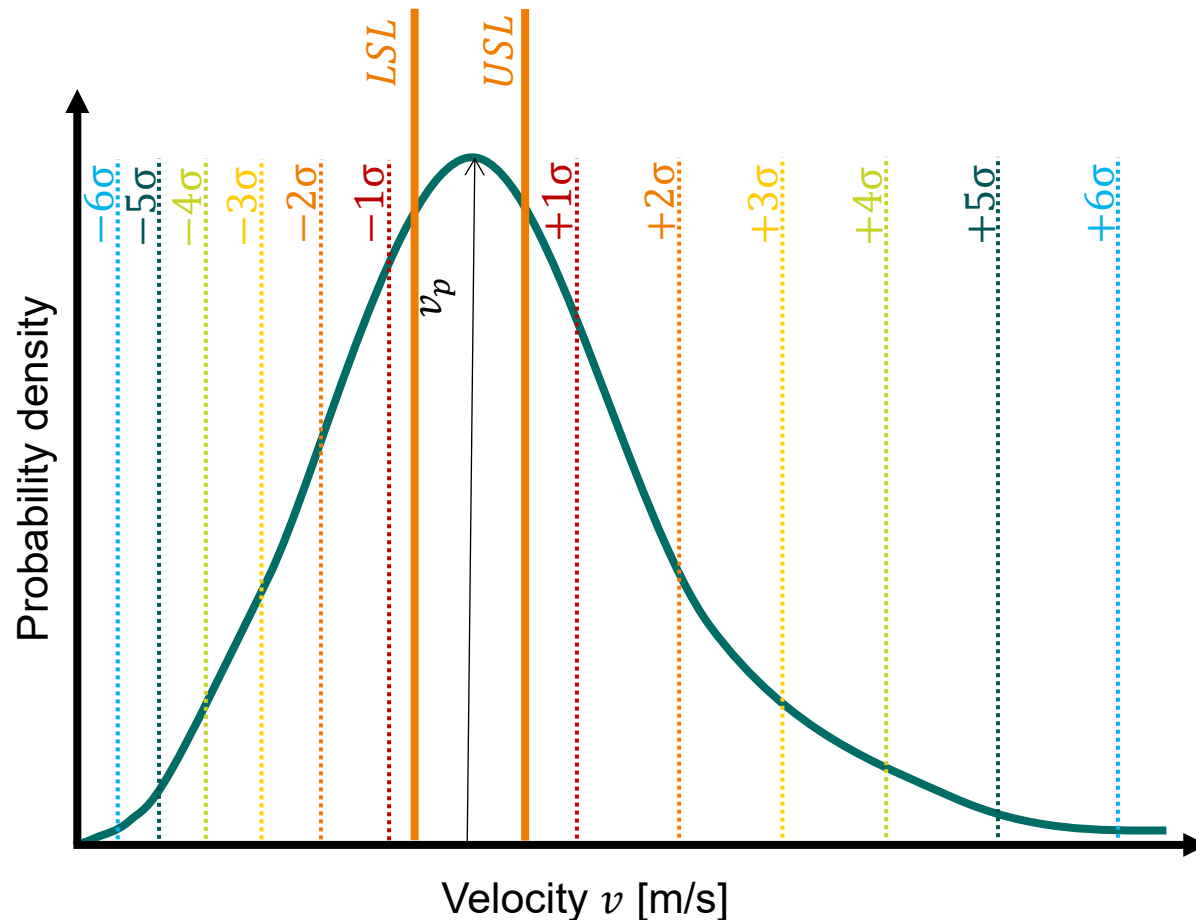
MOTOROLA



General Electric

6 σ – Traditional optimization method based on statistical analysis

Maxwellian Probability Density Function (PDF)



Accuracy

- Relation of most probable outcome on target

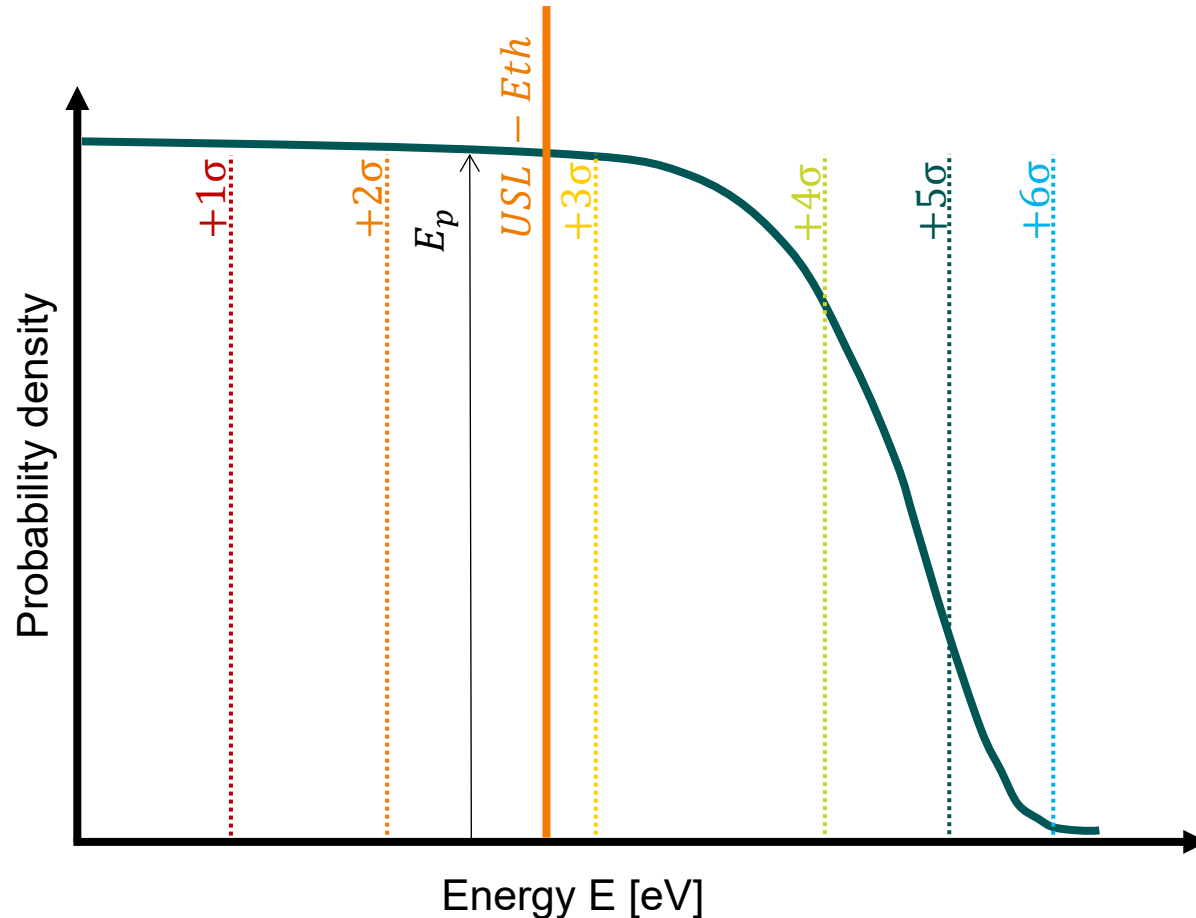
Precision

- Scatter within or around Lower Specification Limit (LSL) & Upper Specification Limit (USL)
- How close are outcomes together

σ -level	DPMO (defects per million opportunities)	Yield %
0	> 691 462	< 31 %
1	691 462	31 %
2	308 537	69 %
3	66 807	93.3 %
4	6 210	99.38 %
5	233	99.977%
6	3.4	99.99966 %

6 σ – Often only an upper or lower limit – Example: Sputtering

Integrated Maxwellian PDF

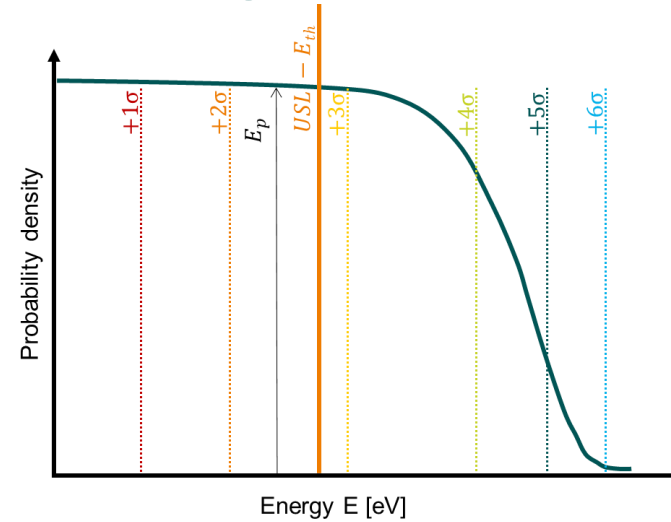


Upper Specification Limit – **USL**

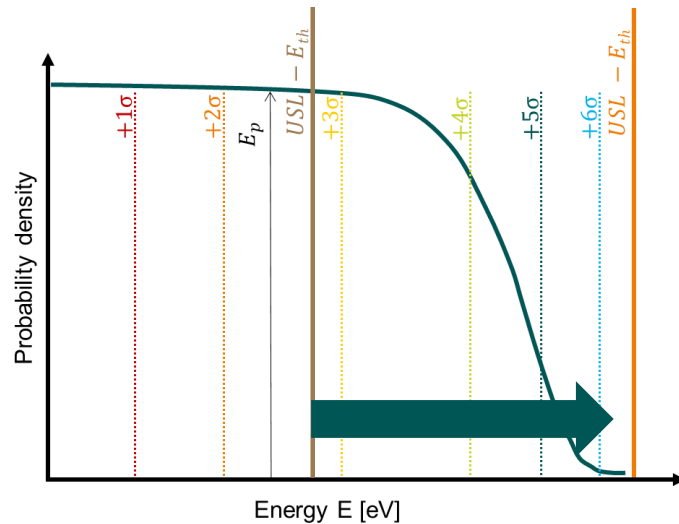
Sputtering Threshold E_{th} [eV]

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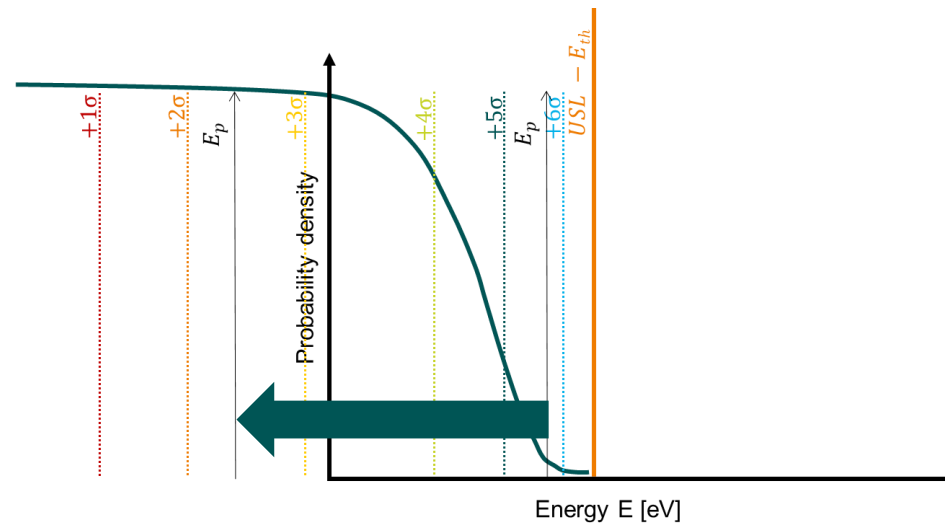
6 σ – Three possible solution strategies



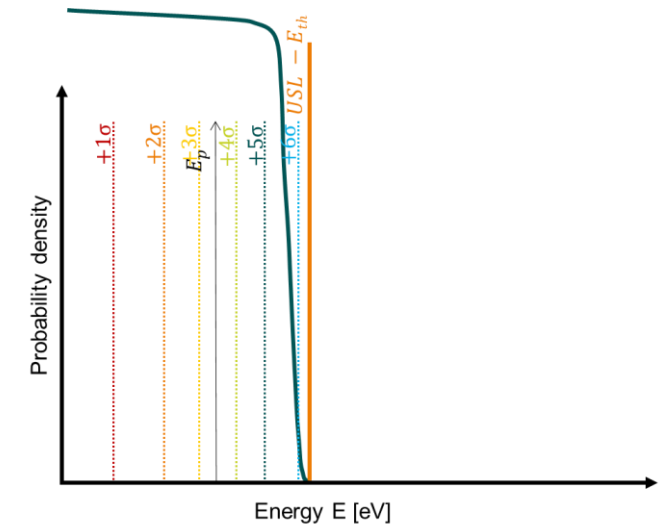
Move USL
Avoid – No solution



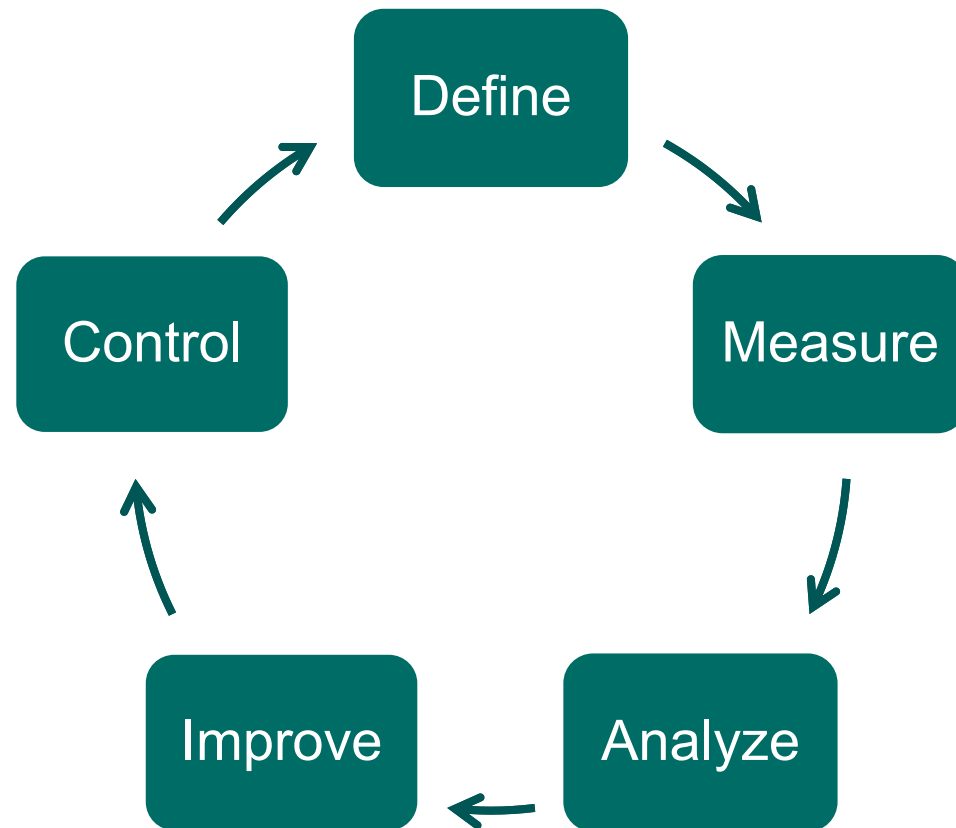
Aim low
Solve – Effective solution



Change PDF
Optimize - Efficient solution



6 σ – DMAIC design cycle to optimize W7-X divertor



Efficient process →

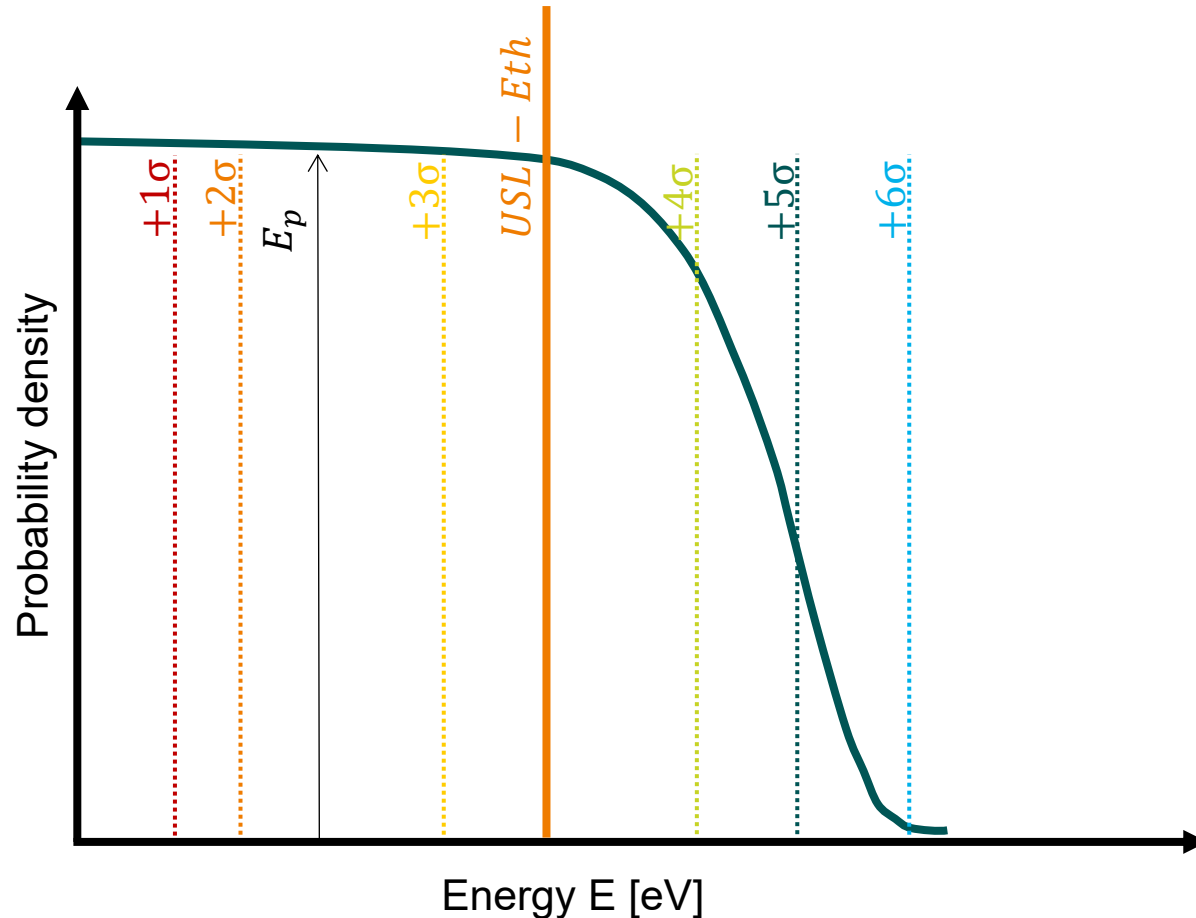
- Quality or performance steps one standard deviation apart
- Ensures efficient step size
 - Too small of step has fixed overhead without gain
 - Too large step might stretch system and bring overwhelming complexity to meet excessive requirements
 - Enables precise definition of boundaries in distributions

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Integrated Maxwellian PDF

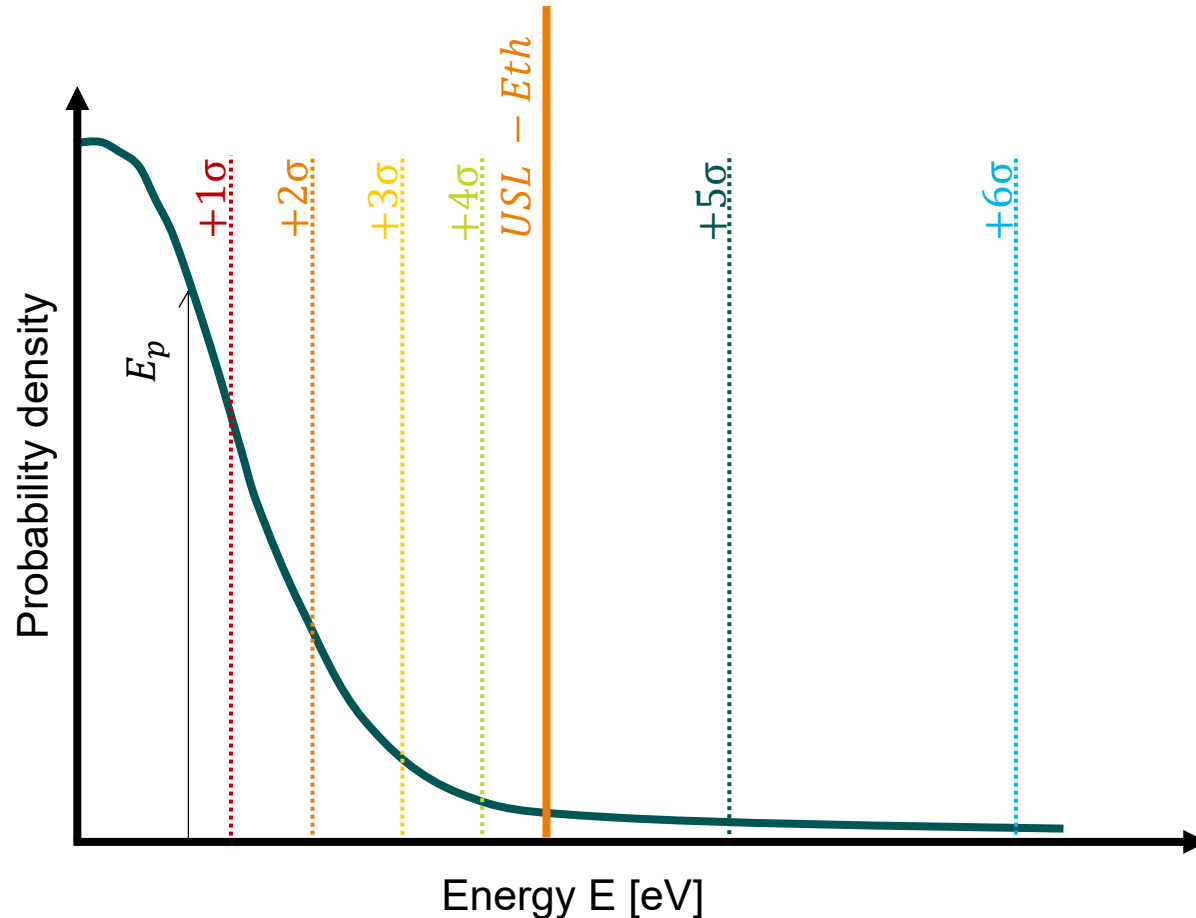


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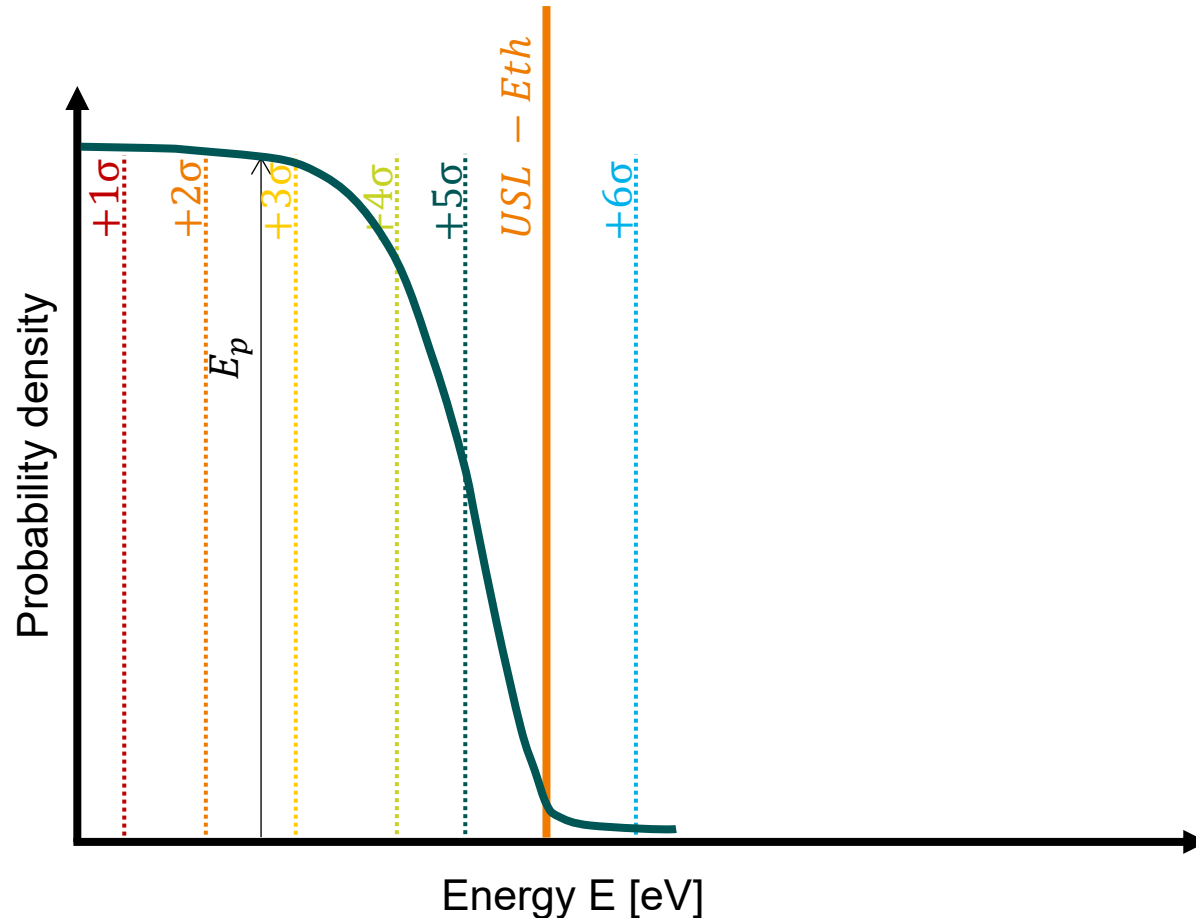


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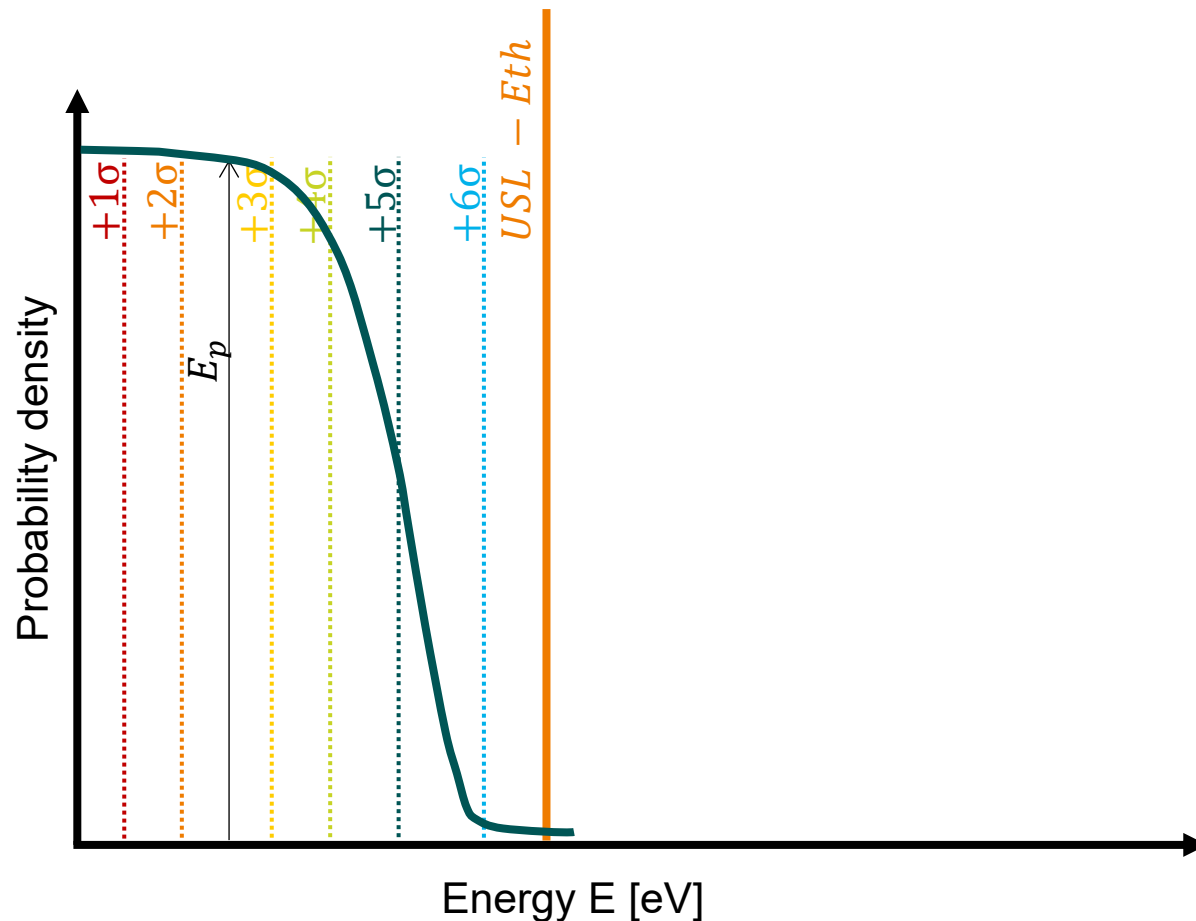


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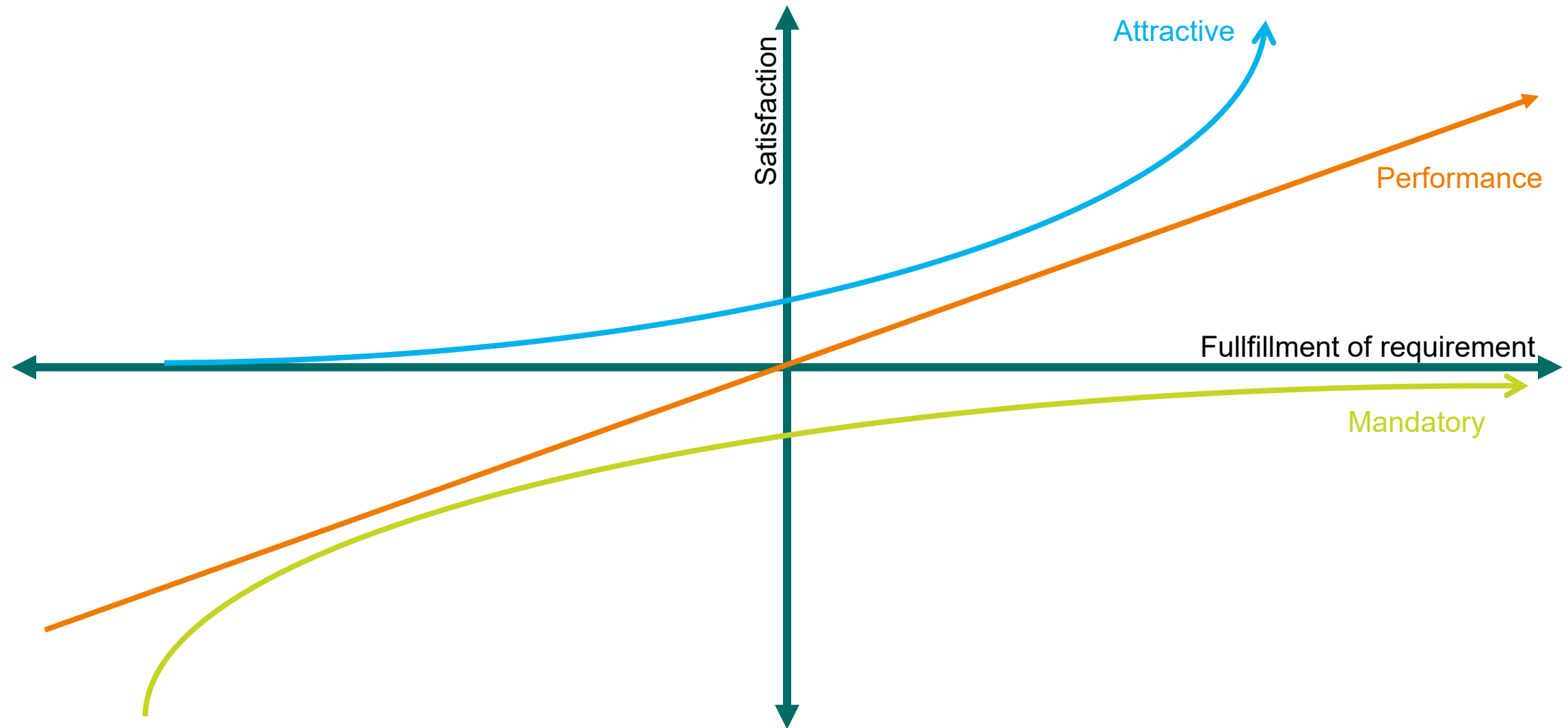
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Kano model to categorize requirements



Understanding Divertor Requirements with the Kano Model

Mandatory (absolute)

- Survive heat
- Survive sputtering
- Survive forces
- Survive neutrons
- Survive ...

Performance (relative)

- Particle exhaust
- Particle retention

Attractive

- High recycling regime
- Power radiation
- Volume recombination
- Tritium Core Recycling

Indifferent

- ?

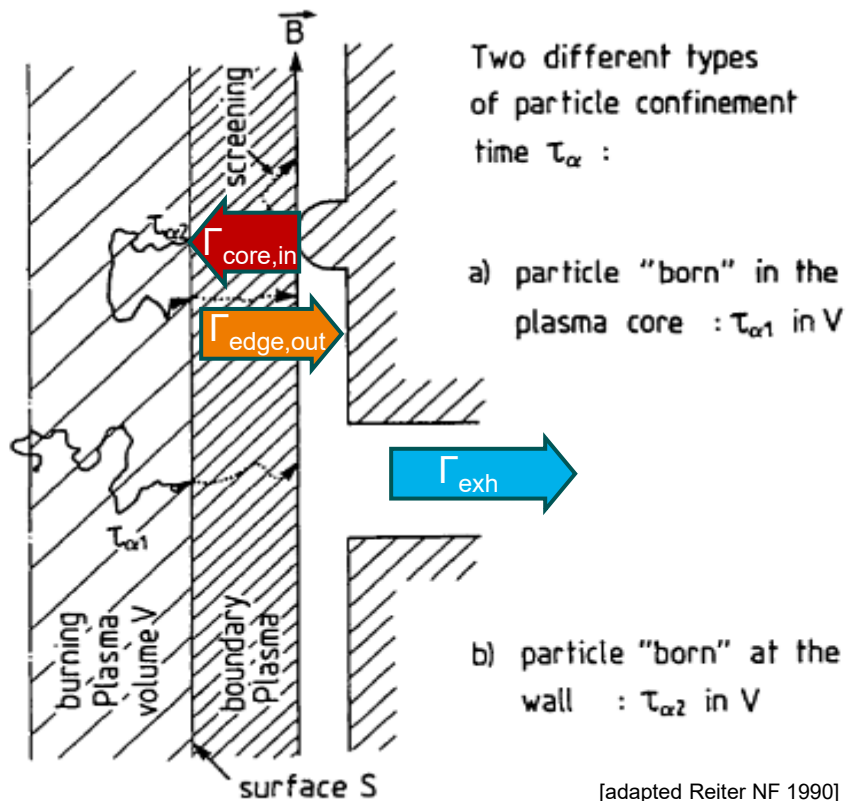
Reverse

- Impurity release



Divertor Reactor performance requirements – He/H exhaust & retention

- $\Gamma_{\text{He,exh}} = \Gamma_{\alpha,1}$ $\Gamma_{\text{H,exh}} = \Gamma_{p,1}$
- Function 1: Exhaust η_{exh} Function 2: Retention η_{ret}
- Exhausted particles do not have to be retained



Function 1:

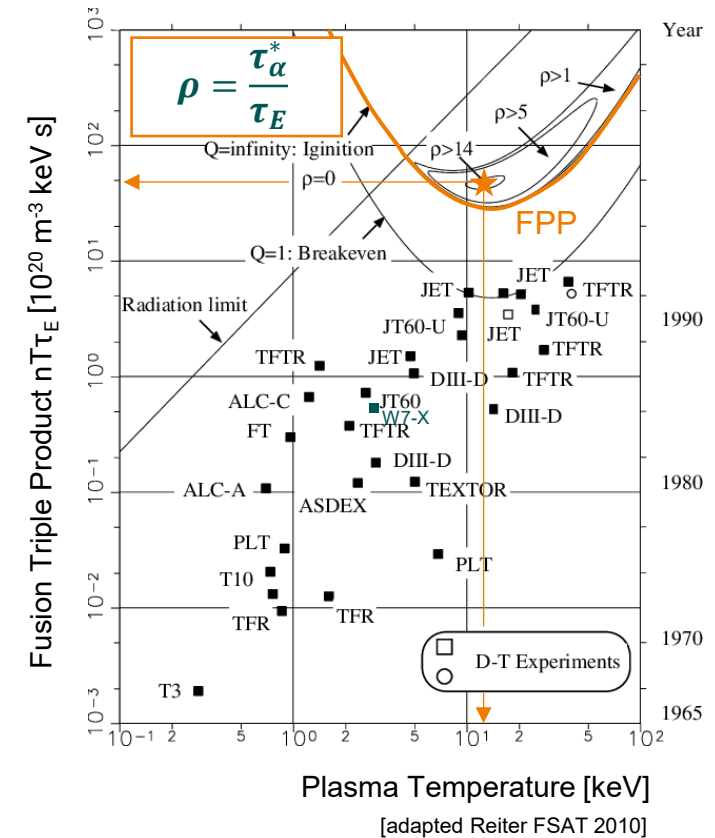
$$\eta_{\text{exh},\alpha} = \frac{\Gamma_{\text{exh}}}{\Gamma_{\text{edge,out}}}$$

Function 2:

$$\eta_{\text{ret},\alpha} = 1 - \frac{\Gamma_{\text{core,in}}}{(\Gamma_{\text{edge,out}} - \Gamma_{\text{exh}})}$$

$$\tau_\alpha^* = \tau_{\alpha 1} + \frac{(1 - \eta_{\text{exh},\alpha}) \eta_{\text{ret},\alpha}}{\eta_{\text{exh},\alpha}} \tau_{\alpha 2}$$

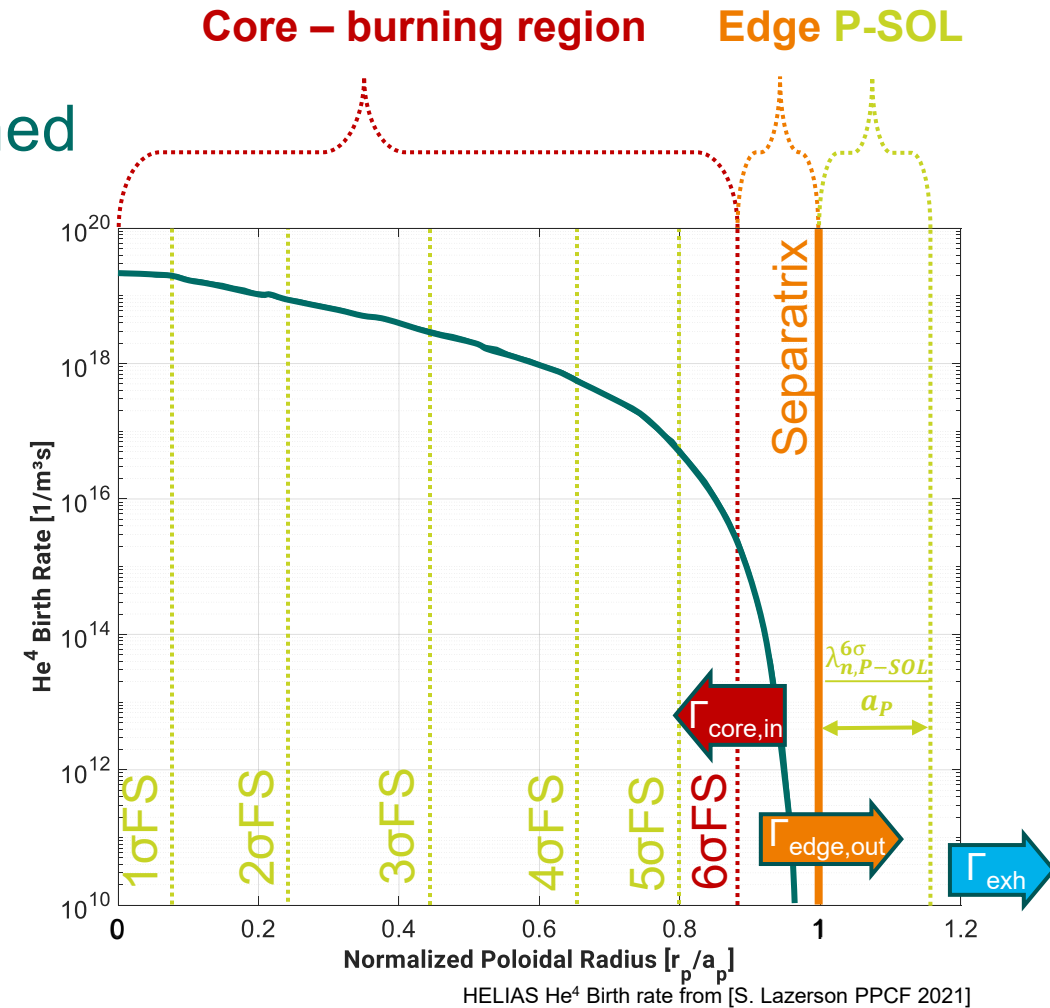
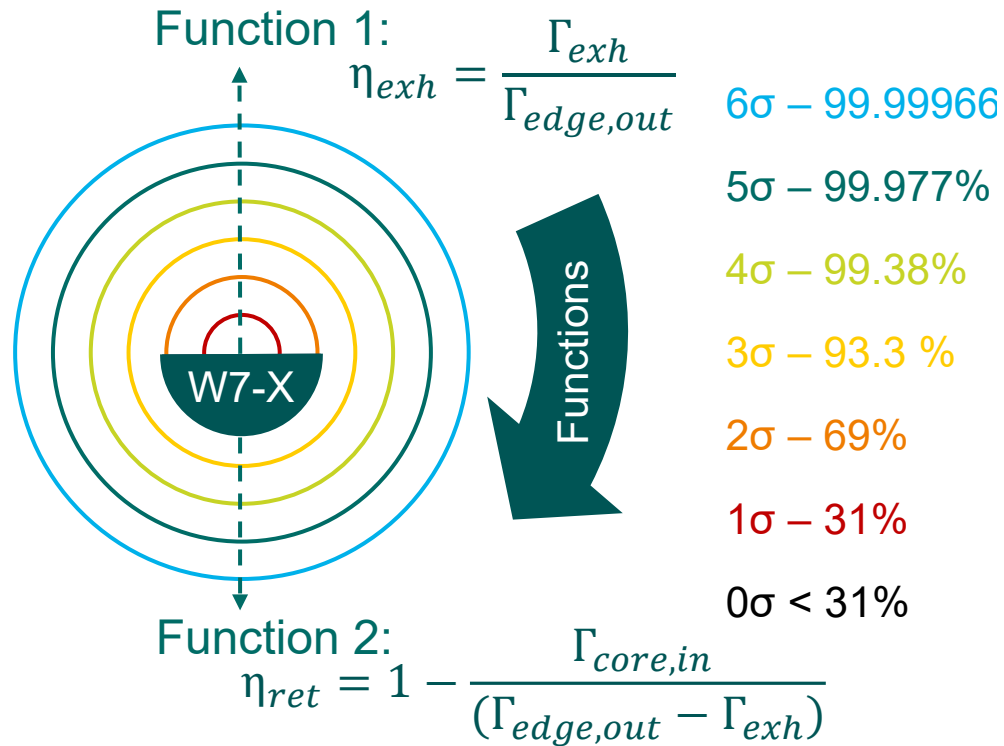
[adapted Reiter NF 1990]





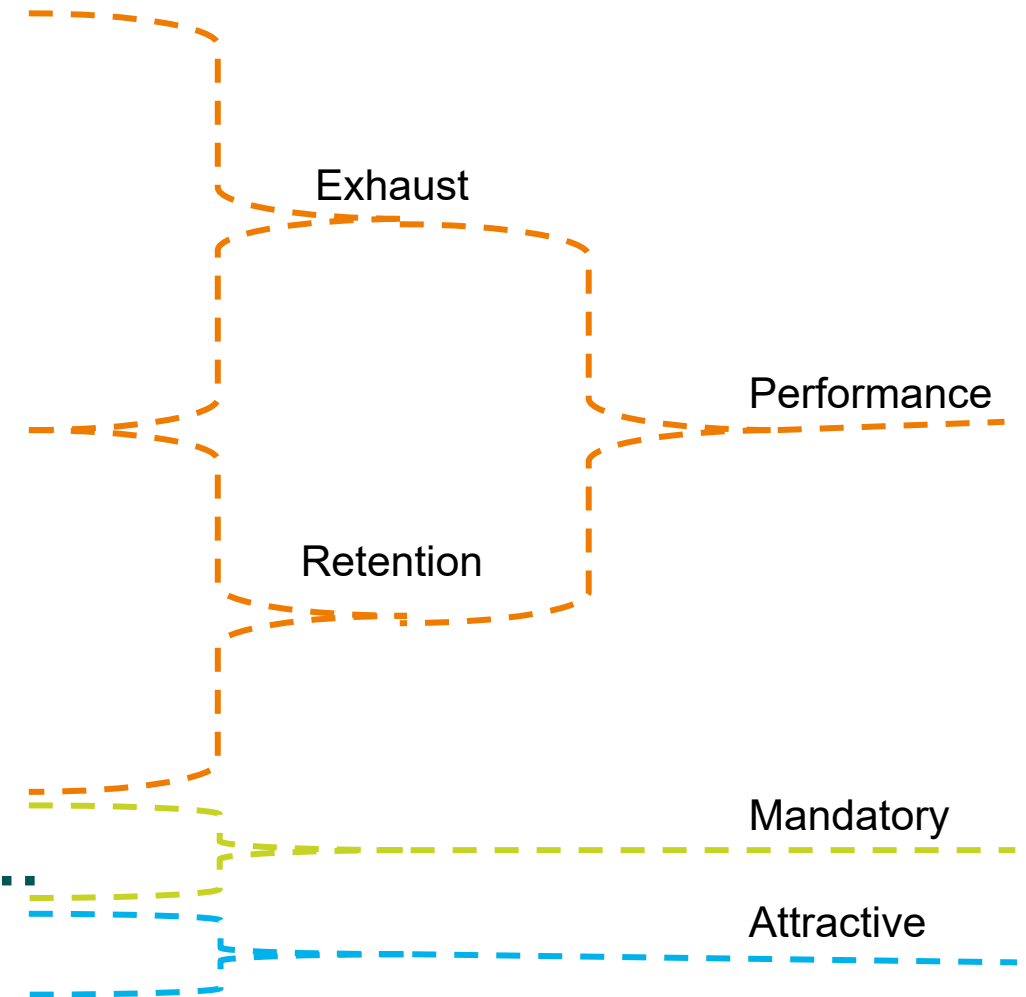
Divertor Reactor performance requirements – He/H exhaust & retention

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- Function 1: η_{exh} Function 2: η_{ret}
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A priori first principle divertor functions

1. Divert plasma particles
2. Neutralize plasma particles
3. Collect neutral particles
4. Remove neutral particles
5. Contain particles in sub-divertor
6. Recycle neutrals in divertor
7. Plug particles in divertor
8. Screen impurity particles from core
9. Survive – Heat, Sputtering, Forces,...
10. Cost/Time function



A-priori first principle Design Metrics

Performance Function 1: Particle exhaust

$$\eta_{\text{exh}} = \Gamma_{\text{exh}} / \Gamma_{\text{edge,out}}$$

$$= \eta_{\text{diversion}} \eta_0 \eta_{\text{coll}} \eta_{\text{removal}}$$

1.1 Particle diversion

$$\eta_{\text{diversion}} = \Gamma_{\text{div,in}} / \Gamma_{\text{edge,out}}$$

1.2 Particle neutralization

$$\eta_0 = \Gamma_0 / \Gamma_{\text{div,in}} = \eta_{0,\text{surf}} + \eta_{0,\text{vol}}$$

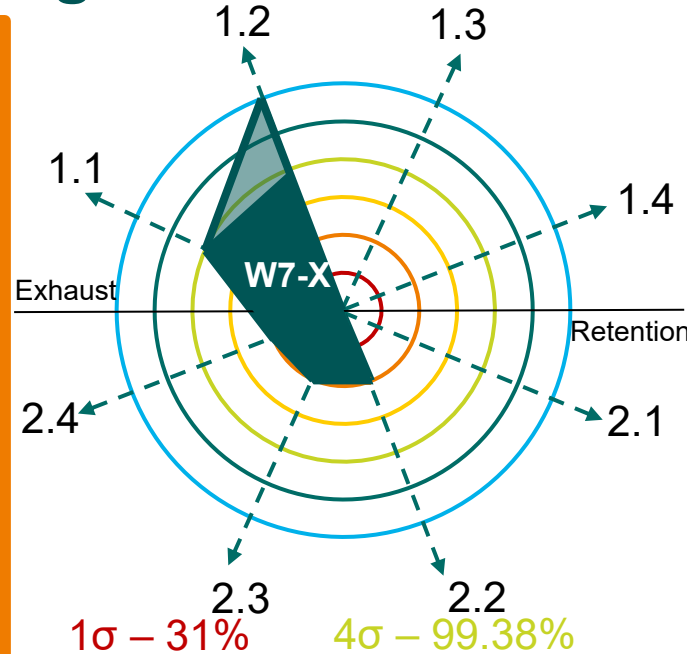
$$\eta_{0,\text{surf}} = \Gamma_{0,\text{surf}} / \Gamma_{\text{div,in}}$$

1.3 Particle collection

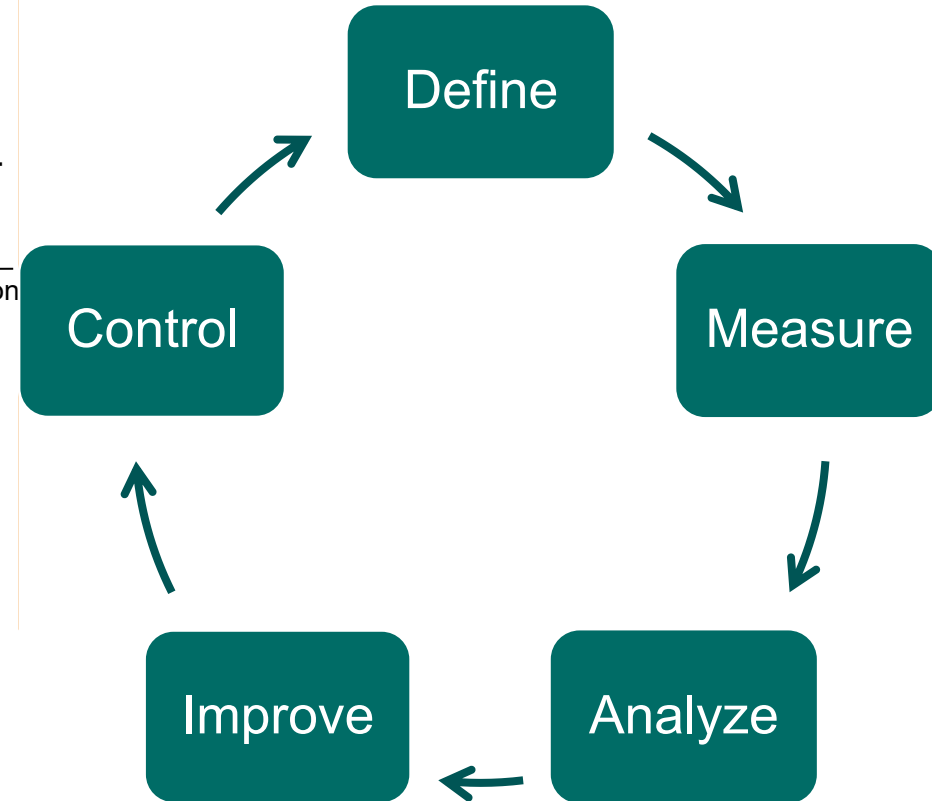
$$\eta_{\text{coll}} = \Gamma_{\text{coll}} / \Gamma_0$$

1.4 Particle removal

$$\eta_{\text{removal}} = \Gamma_{\text{exh}} / \Gamma_{\text{coll}}$$



1σ – 31% 4σ – 99.38%
2σ – 69% 5σ – 99.977%
3σ – 93.3 % 6σ – 99.99966 %



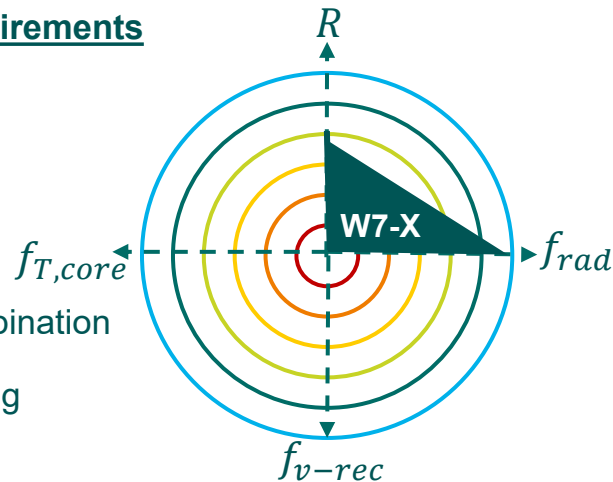
Attractive requirements

Recycling

Radiation

Volume Recombination

T-Core Recycling



Mandatory Requirement	Heatload	Sputtering	Mechanics	Neutrons
Metric	$FOS = \frac{\dot{q}_{\text{max}}}{\dot{q}_{\text{div}}}$	$\eta_{\text{sptr,resist}} = 1 - Y$	$FOS = \frac{\text{yield stress}}{\text{working stress}}$	DPA
W7-X	1.67	?	> 1	?

Control Models

Parametric Design

- Target maker
 - ~ Hours – by hand
 - 5-30 min – parametric on field line tracer
 - 300 ms – parametric on gordon
- **Baffle maker – in development**

EMC3Lite

- 30 s

COMSOL

- 2 h setup – newbie
- 20 min setup – experienced
- 15-30 min $\eta_{\text{collection}}$
- 4-5 h η_{removal}

Mercury

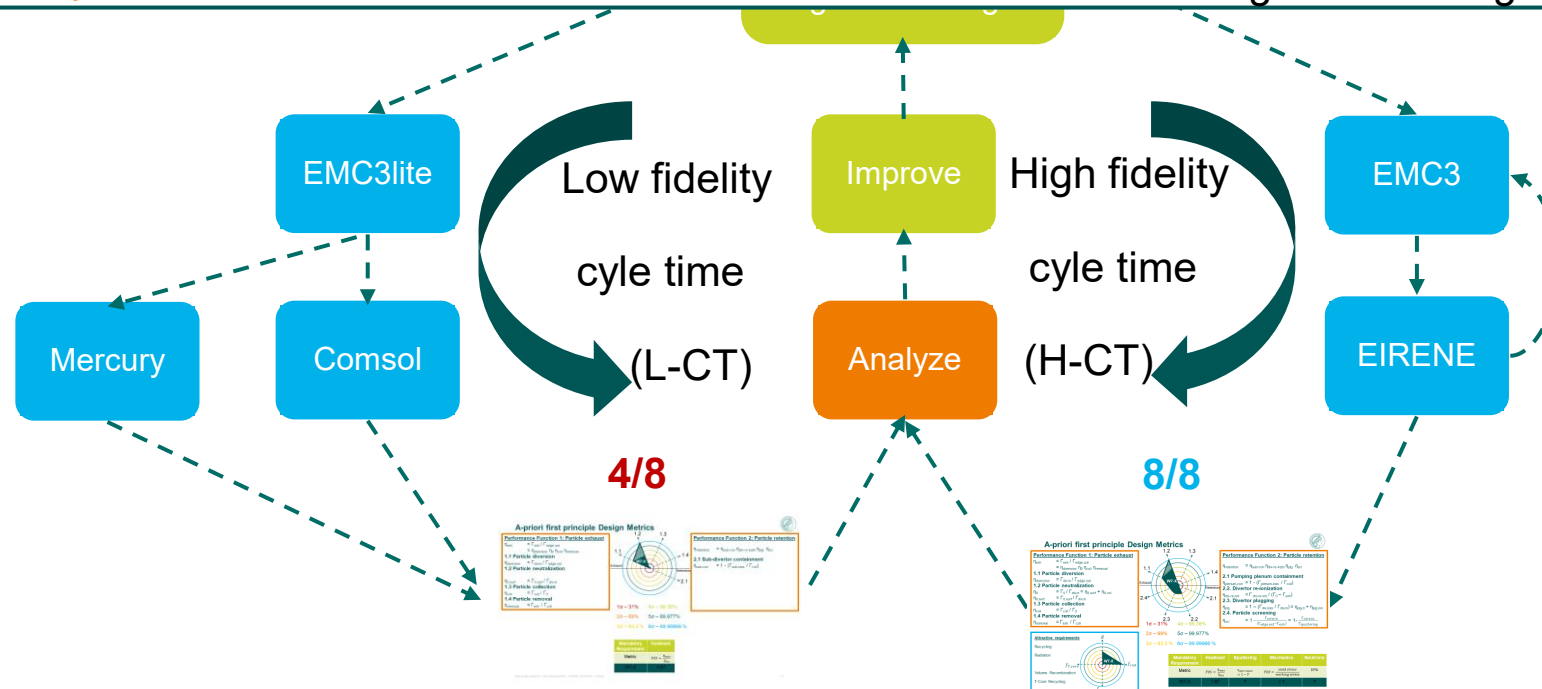
- 2 min setup
- Parallelisation:
- Now 15-45 min $\eta_{\text{collection}}$
 - from 90 min $\eta_{\text{collection}}$

Further reduction through coarsening of grids

Plasma code

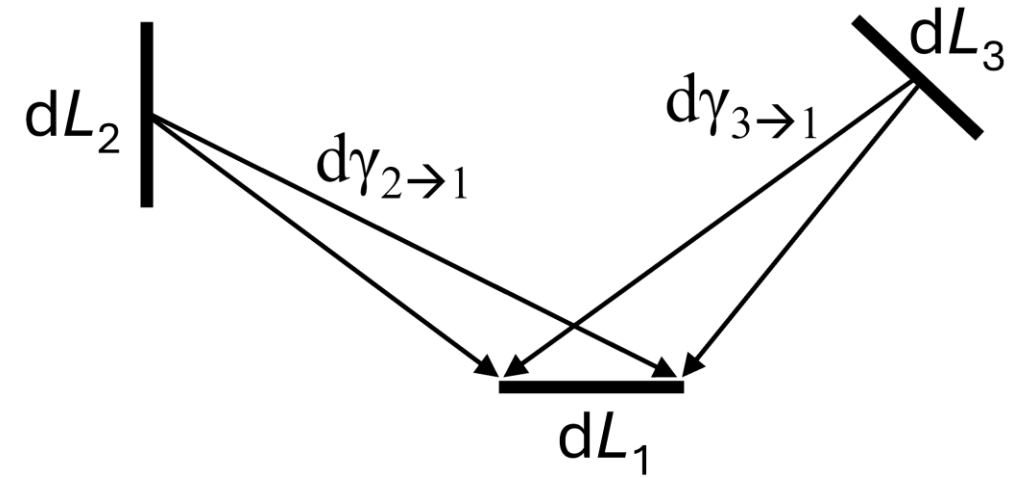
Neutral code

Performance result



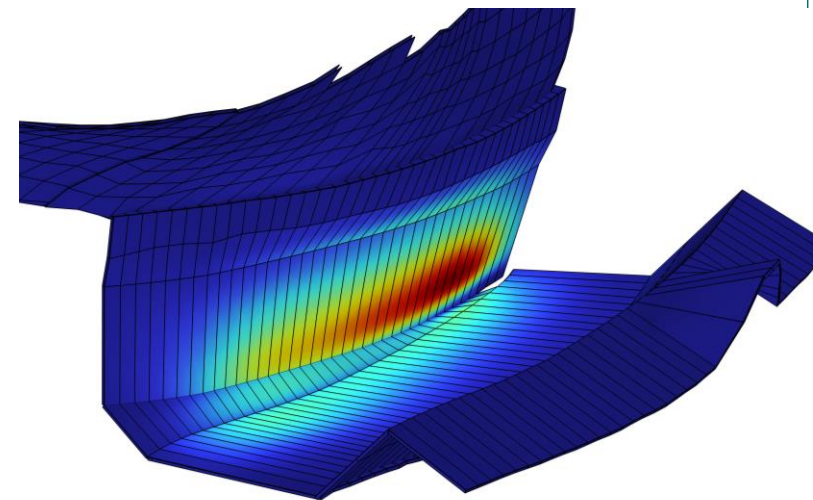
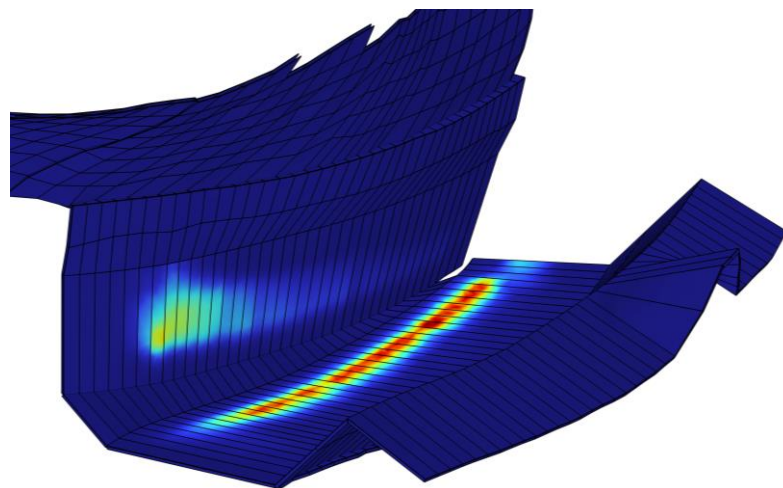
Understanding the AC method for the molecular flow regime

Raytracing (Computer Graphics) $\longrightarrow$ AC method

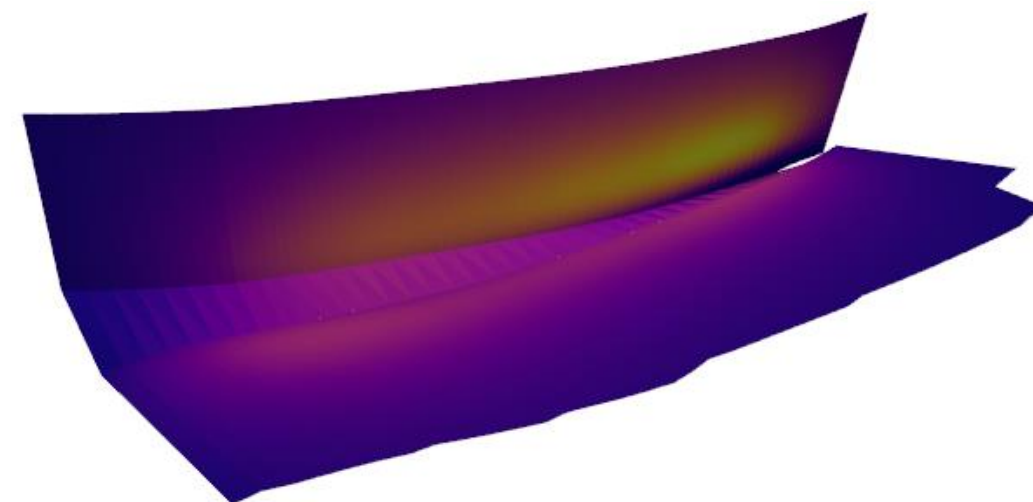
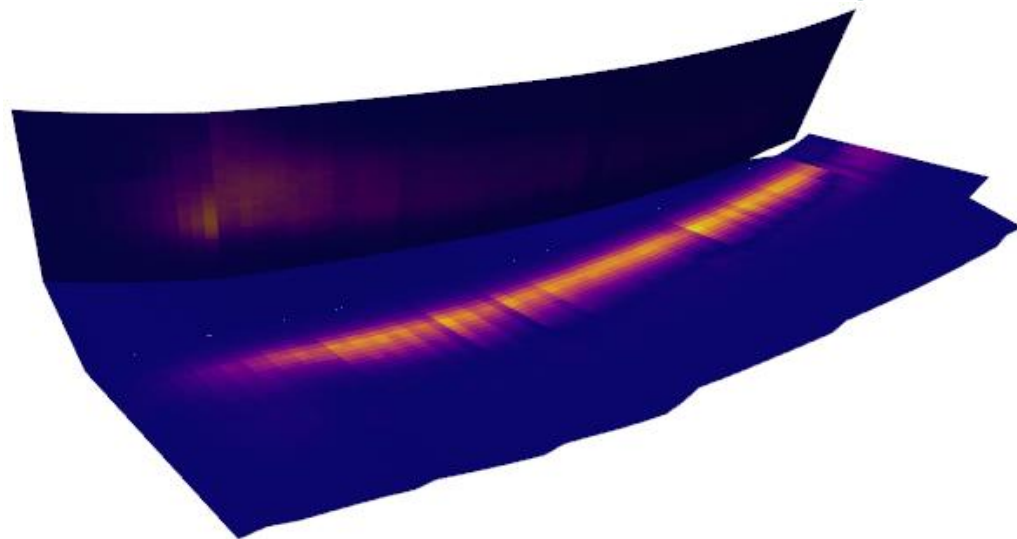


- Calculates probability densities instead of particle dynamics
- No discretisation of phase space

Solution with COMSOL Multiphysics



Solution with EMC3-Mercury



Location of neutralisation

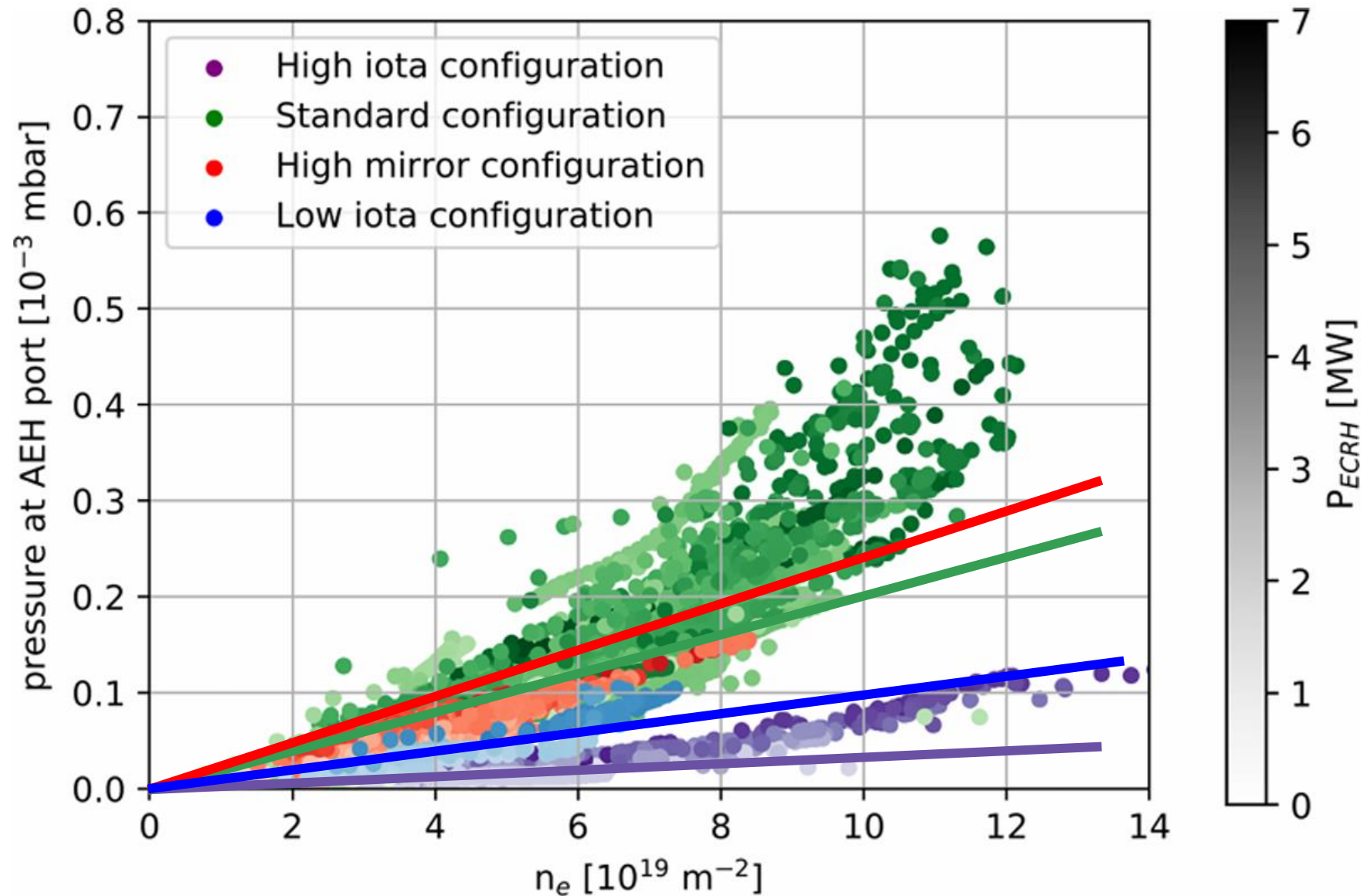
Neutral particle distribution

Benchmark



Performance metric	Standard 5/5	High-Mirror 5/5	High-lota 5/4	Low-lota 5/6
Particle diversion ✗	99.86 %	99.94 %	99.71 %	99.93%
Particle collection ✗	2.94 %	3.32 %	3.83 %	1.01 %
Particle removal =	2.99 %	3.45 %	2.84 %	3.14 %
Particle exhaust	0.084 %	0.113 %	0.108 %	0.032 %

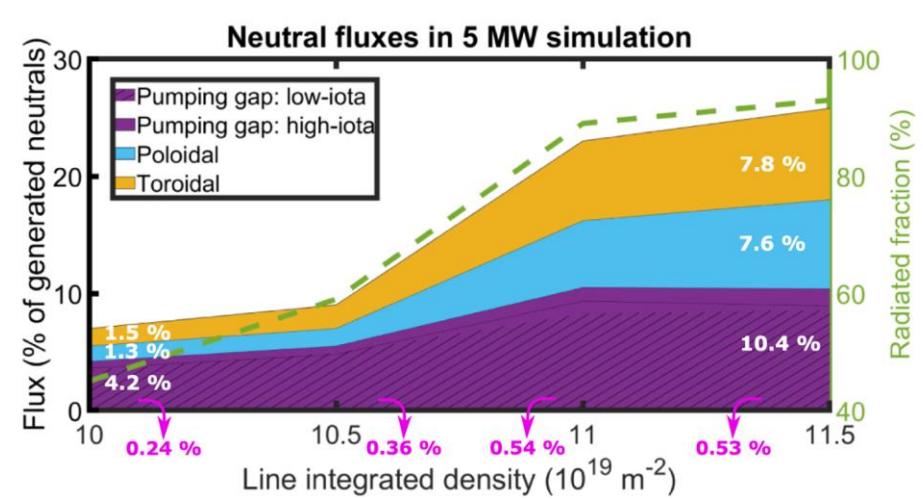
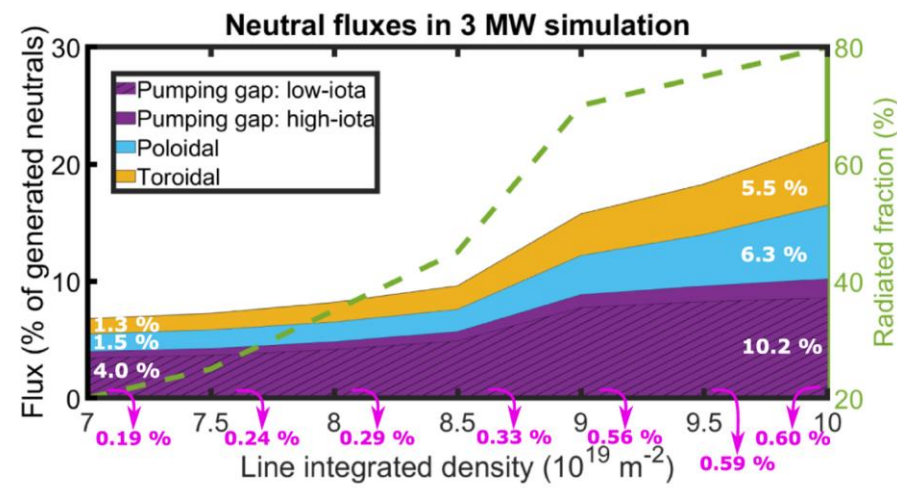
Experimental validation: Pressure at AEH port



Particle collection: Comparison to high-fidelity model



	AC method	EMC3-Eirene	(Wenzel et al., NF 2024)
Particle collection (Standard configuration)	2.83 %	4.0 % - 10.4 %	0.69 % ± 0.28 %

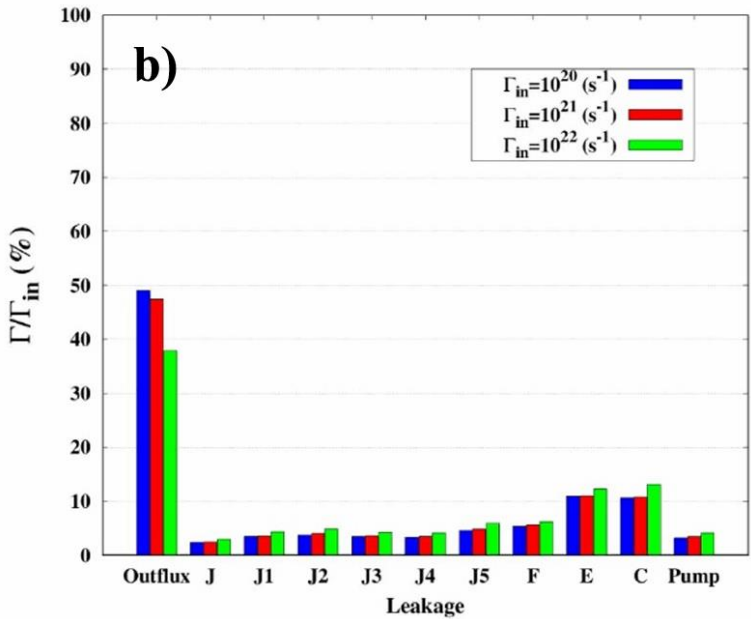
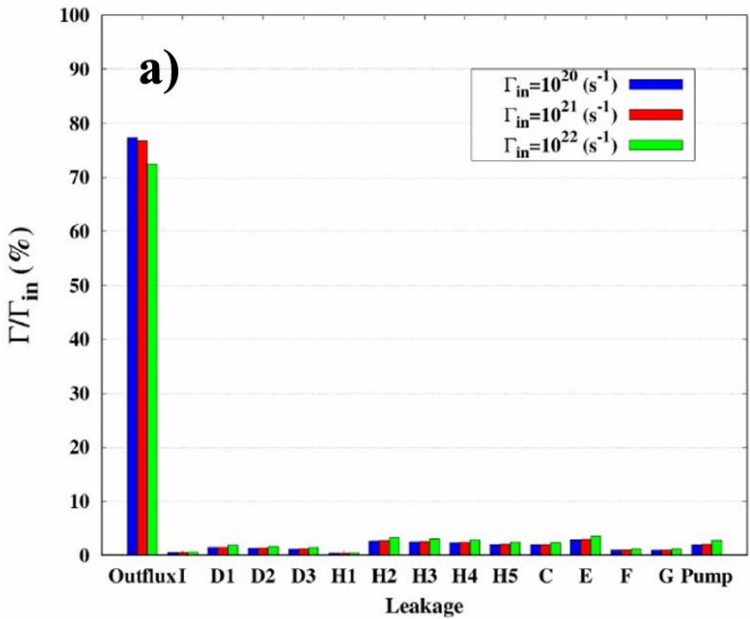


[D. Boeyaert, PPCFET 2024]

Particle removal: Comparison to high-fidelity model



	AC method		DIVGAS		EMC3-Eirene
Divertor section	Low-lota	High-lota	Low-lota	High-lota	Low-lota
Particle removal	2.99 %	2.84 %	1.9 % - 2.7 %	3.0 % - 4.0 %	4.75 % - 5.88 %

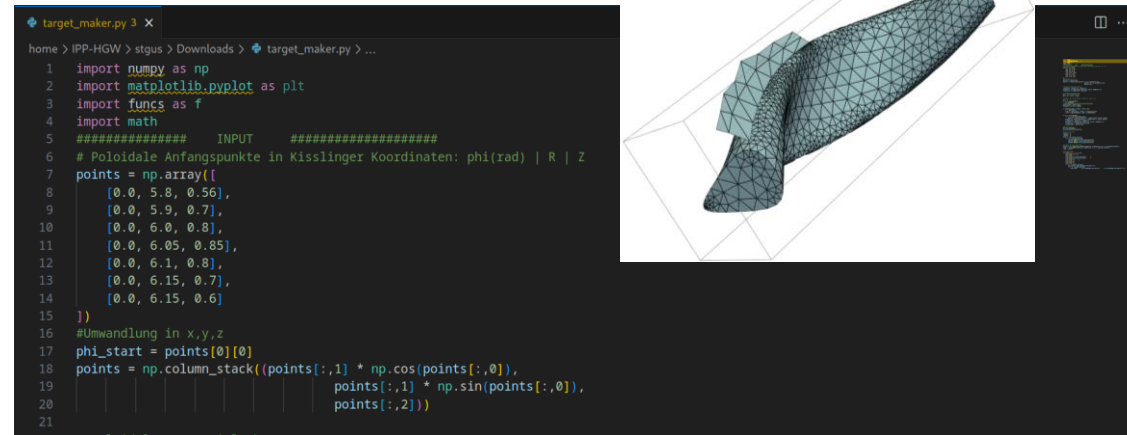


[S. Varoutis, NF 2024]

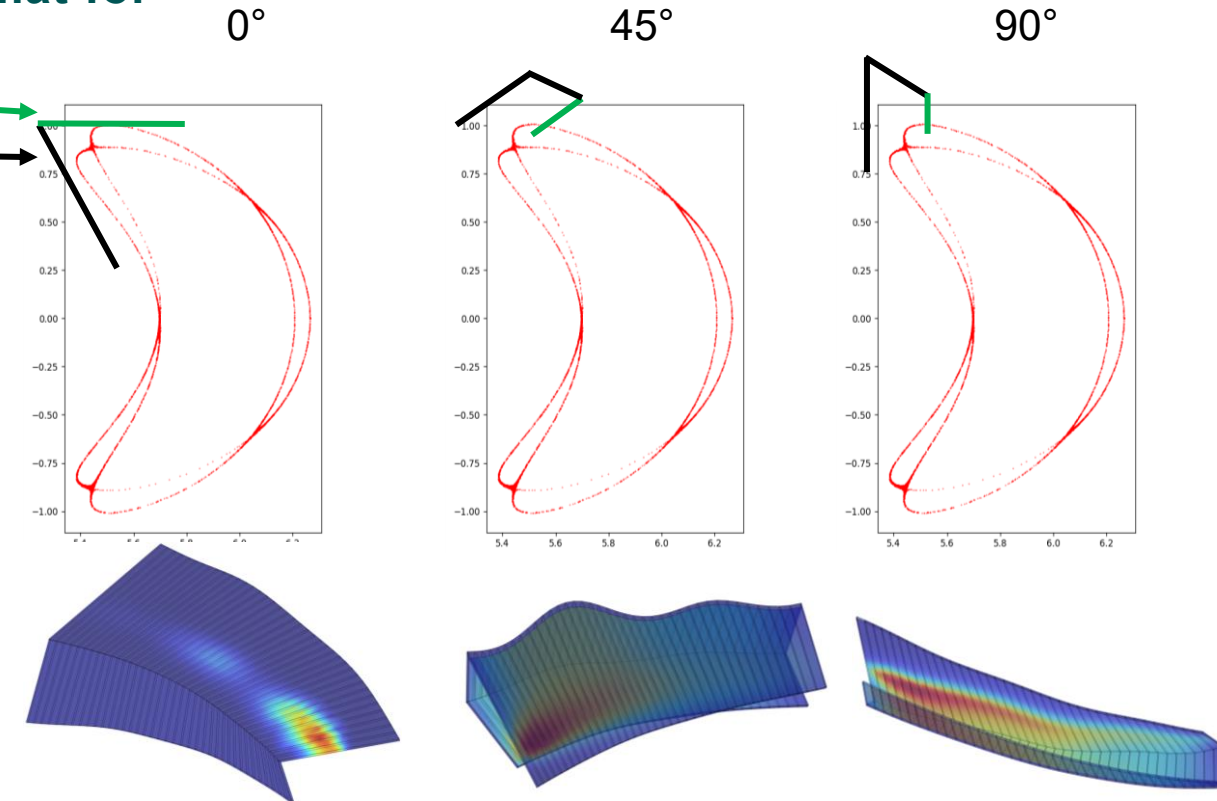
Parametric Divertor Chamber Maker

Field aligned, parametric design in Kisslinger format for

- Target maker
- Pump opening maker
- Baffle maker – under development



Target – Separatrix angle



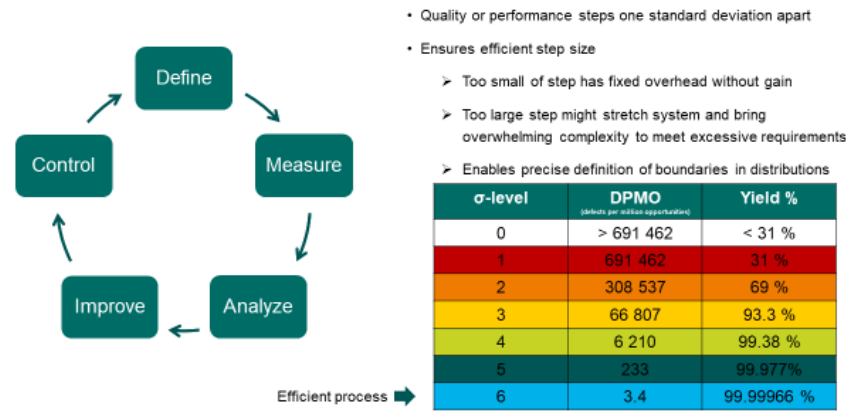
Low fidelity particle collection efficiency

1.7%

76.8%

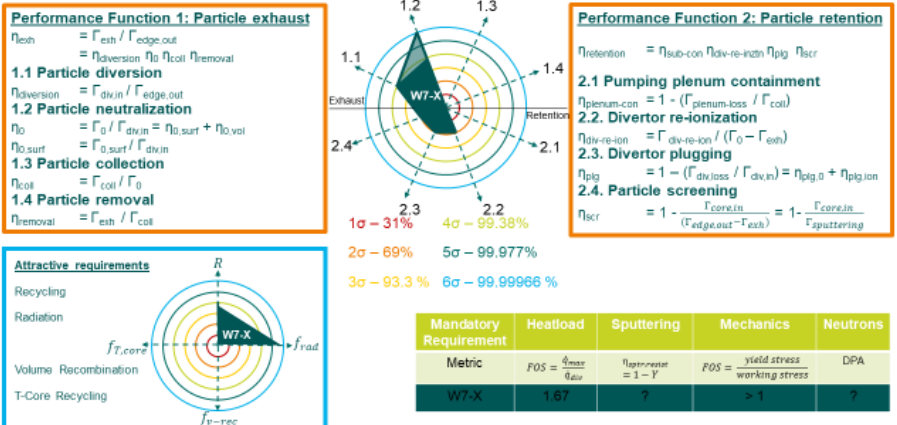
64.1%

6σ – DMAIC design cycle to optimize W7-X divertor



MAX-PLANCK-INSTITUT FÜR PLASMAPHYSIK | THIERRY KREMEYER | 11.07.24

A-priori first principle Design Metrics



36

Control Models

Core and Edge field up to LCFS

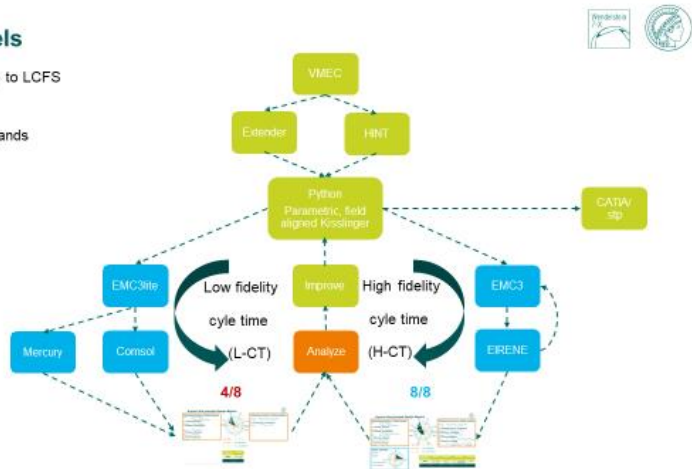
Diverted field lines / islands

Divertor chamber

Plasma code

Neutral code

Performance result



MAX-PLANCK-INSTITUT FÜR PLASMAPHYSIK | THIERRY KREMEYER | 01.08.20

Solution with COMSOL Multiphysics

