

# Validation of FESTIM Hydrogen Transport Modeling in FLiBe Through HYPERION Permeation Data

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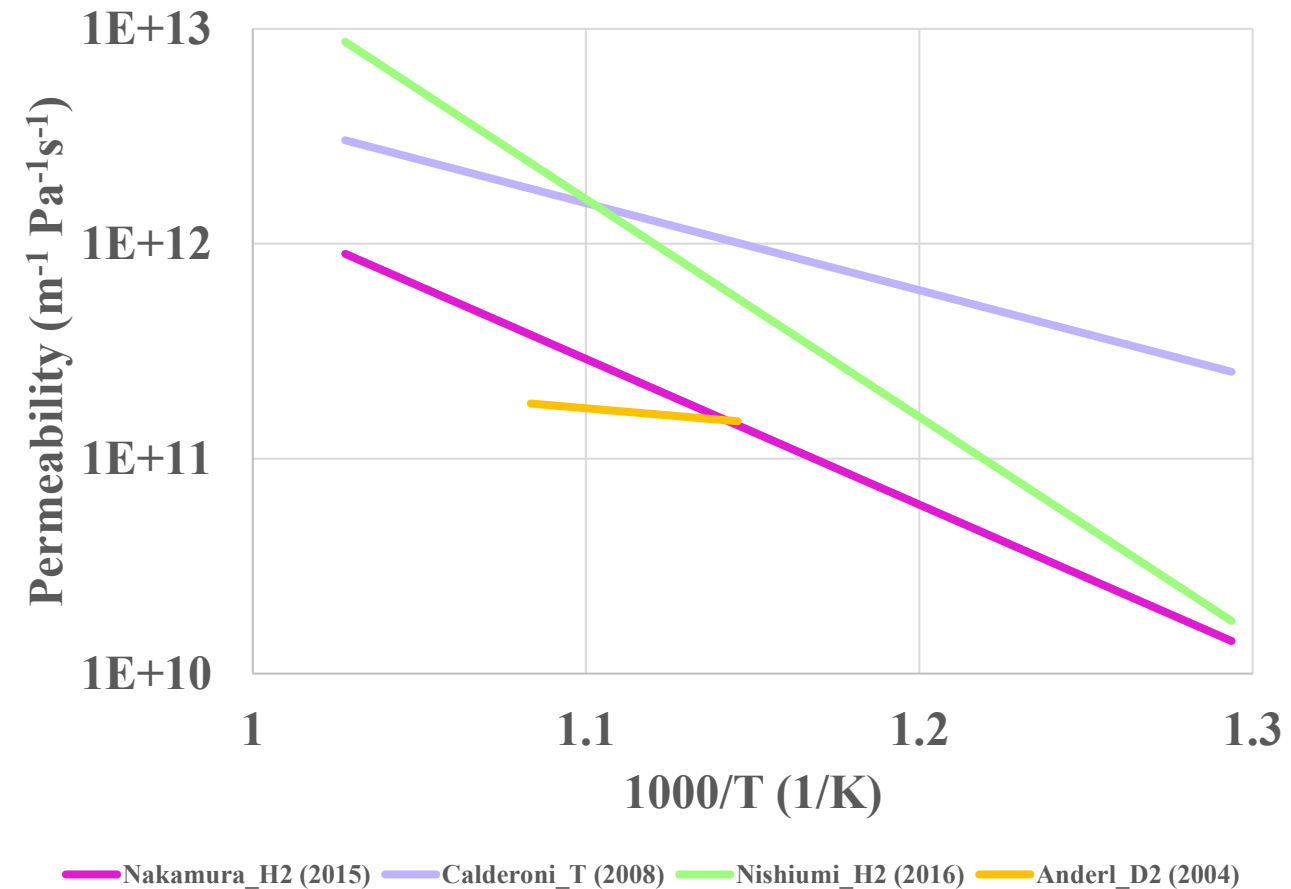
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# Background & Motivation

- FLiBe is a leading molten salt candidate for liquid blankets (MIT LIBRA Project → ARC)
- Tritium control in liquid blankets design requires accurate hydrogen transport models and transport data
- Existing FLiBe permeability data are **scarce & inconsistent**
- Traditional 1D model neglect leakage paths → permeability errors up to order(s) of magnitude



biased permeability leads to **incorrect tritium inventory predictions**

# Background & Motivation

## Goal:

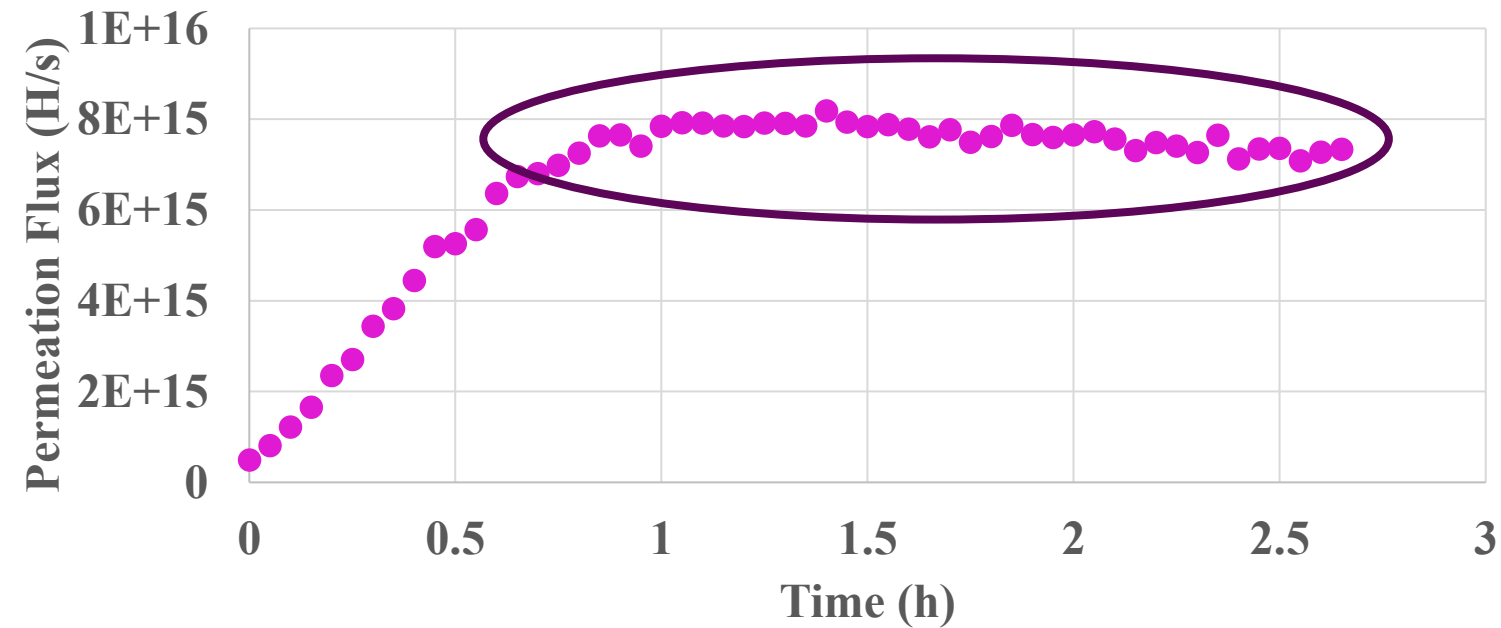
Apply FESTIM to interpret MIT's HYPERION (hydrogen permeation) experiments, accounting for **2D hydrogen transport** and **realistic leakage boundary conditions**, to **extract FLiBe permeability** for liquid blanket design



- **First integrated simulation-experiment framework** for molten-salt permeation, enabling geometry-resolved permeability extraction
- **First direct assessment of sidewall leakage effects** in molten-salt permeation experiment
- Demonstration that **1D models bias permeability** estimations
- **A consistent workflow** to derive Arrhenius-form H-isotope permeability across different materials

# HYdrogen PERmeation (HYPERION) Experiment

- Impose partial pressure of H<sub>2</sub> upstream
- H permeates through the Ni membrane and FLiBe liquid + Ni vessel
- Measure the desorption flux of H downstream
- Repeat at different temperatures



Quasi-2D geometry → sidewall becomes an important flux path

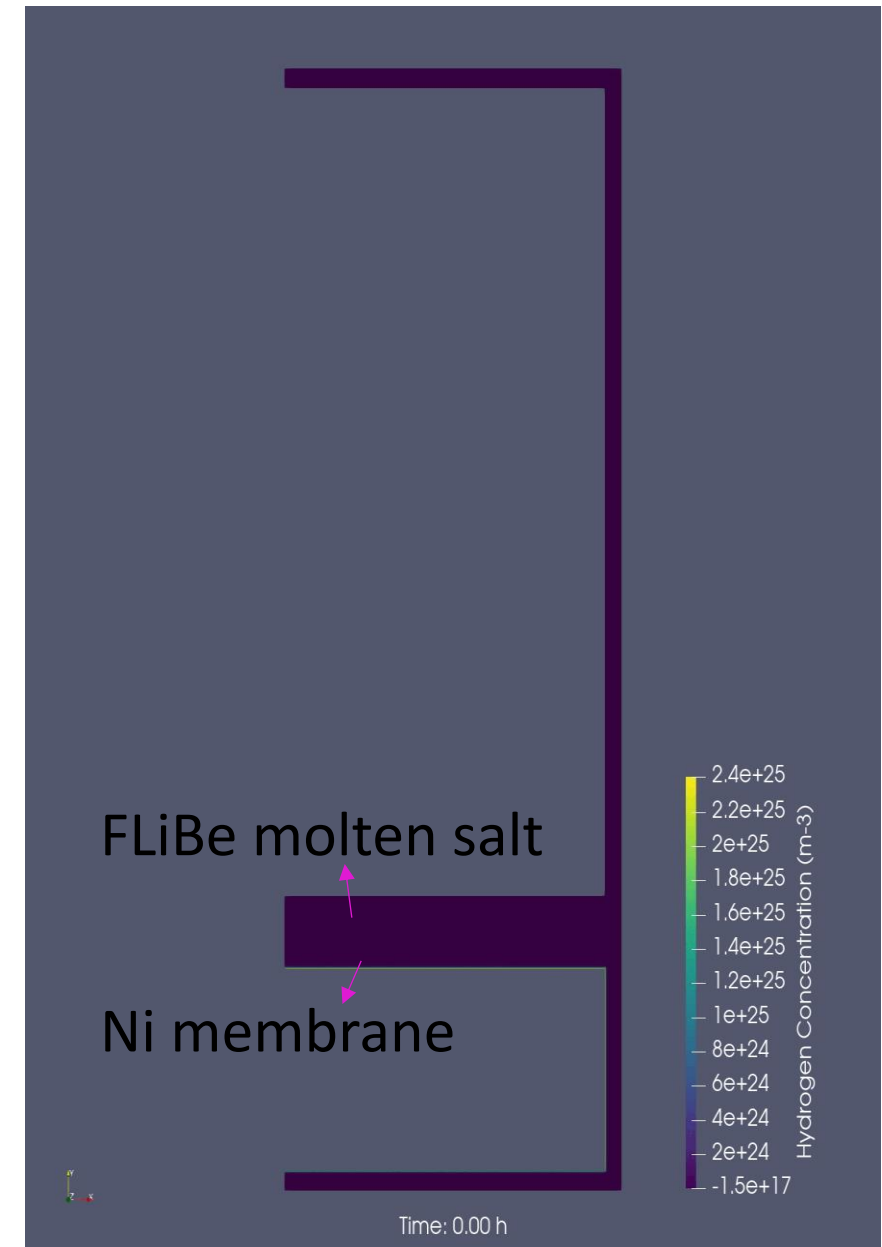
# FESTIM (Finite-Element Simulation of Tritium in Materials)

- Multi-dimension, multi-species (H isotopes) transport
  - Diffusion
  - Trapping and de-trapping
  - Decay
  - Isotope exchange
- Multi-region chemical potential continuities
  - Metal-liquid, metal-metal interfaces
- Heat transfer
- Advection
- **Open-source**

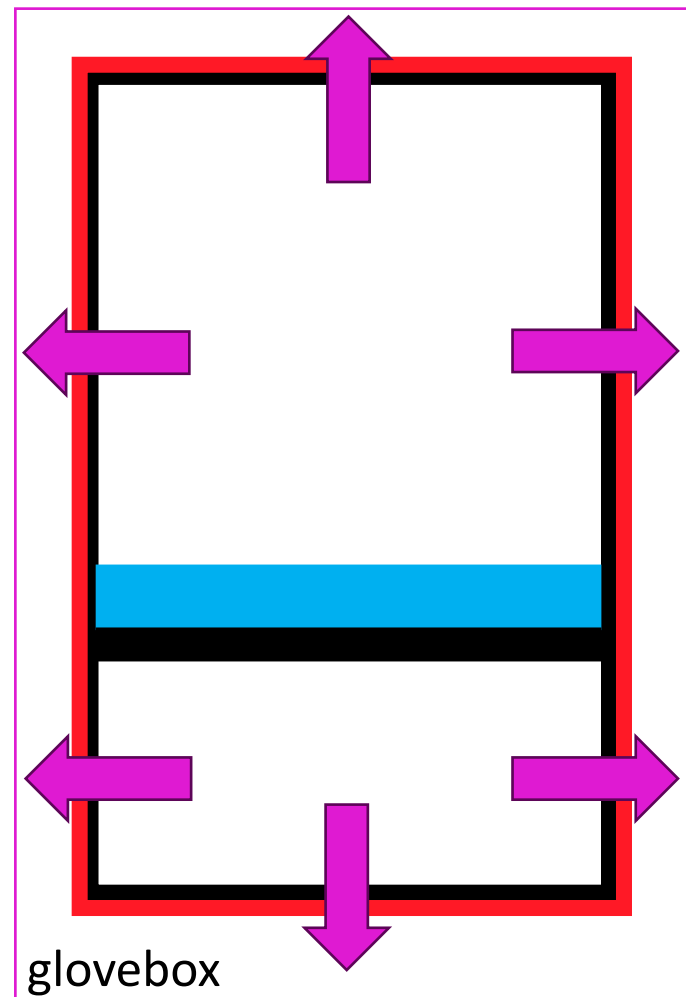


# 2D FESTIM model for HYPERION experiment

- 2D axisymmetric
- H diffusion in Ni membrane + molten FLiBe + Ni vessel
- Potential continuity across the metal-liquid interface
- Sidewall leakage: boundary conditions
- Outputs: spatial hydrogen concentration
- Flux extraction:  $J = -D\nabla c$



# Boundary conditions

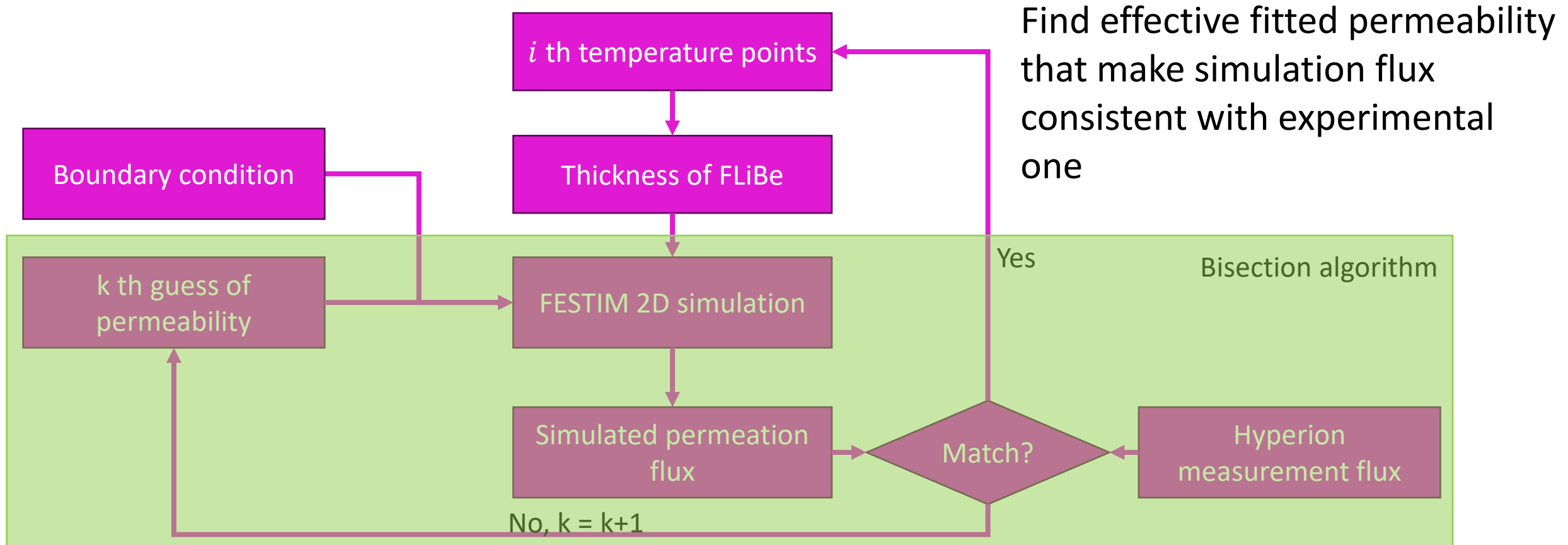


## Two extreme cases

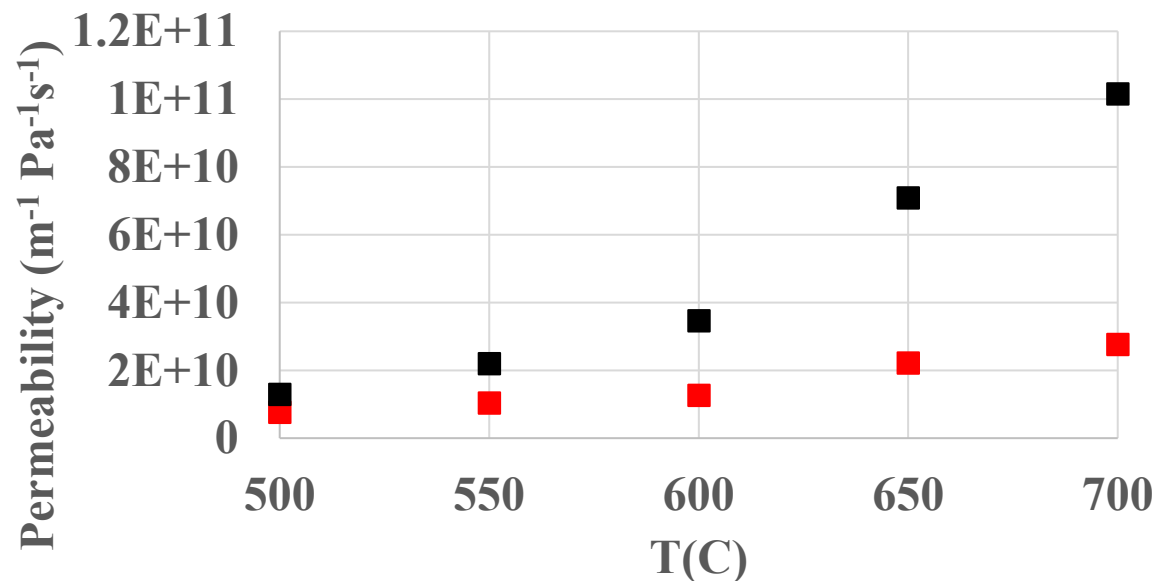
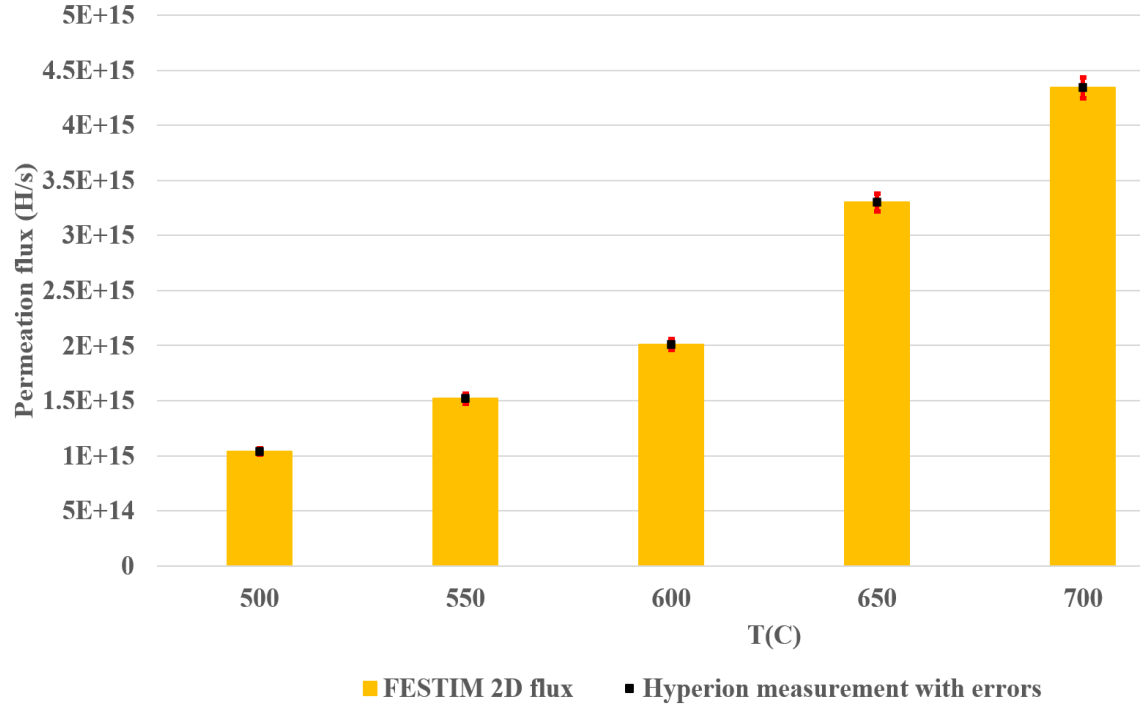
- Ideal coating → sealed vessel → no H leakage to glovebox
  - Basic assumption used in traditional 1D interpretation
- No coating → full leakage → H free release to the glovebox
  - Real experiment (partial coating) lies between these limits

# FESTIM-Hyperion Workflow

Temperature  $\rightarrow$  Compute salt thickness  $\rightarrow$  Setup BC  $\rightarrow$  Guess **permeability**  $\rightarrow$  Run 2D FESTIM  $\rightarrow$  Compared to experiment  $\rightarrow$  **Bisection update**







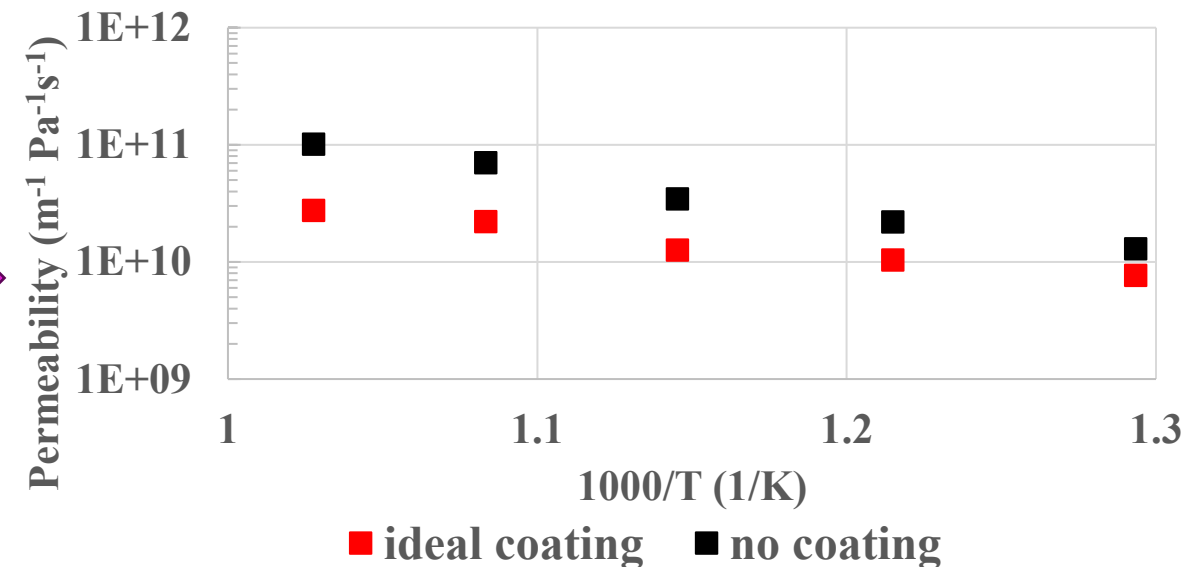
Permeability properties can be expressed as Arrhenius format:

$$P = P_0 \exp\left(-\frac{E_P}{k_B T}\right)$$

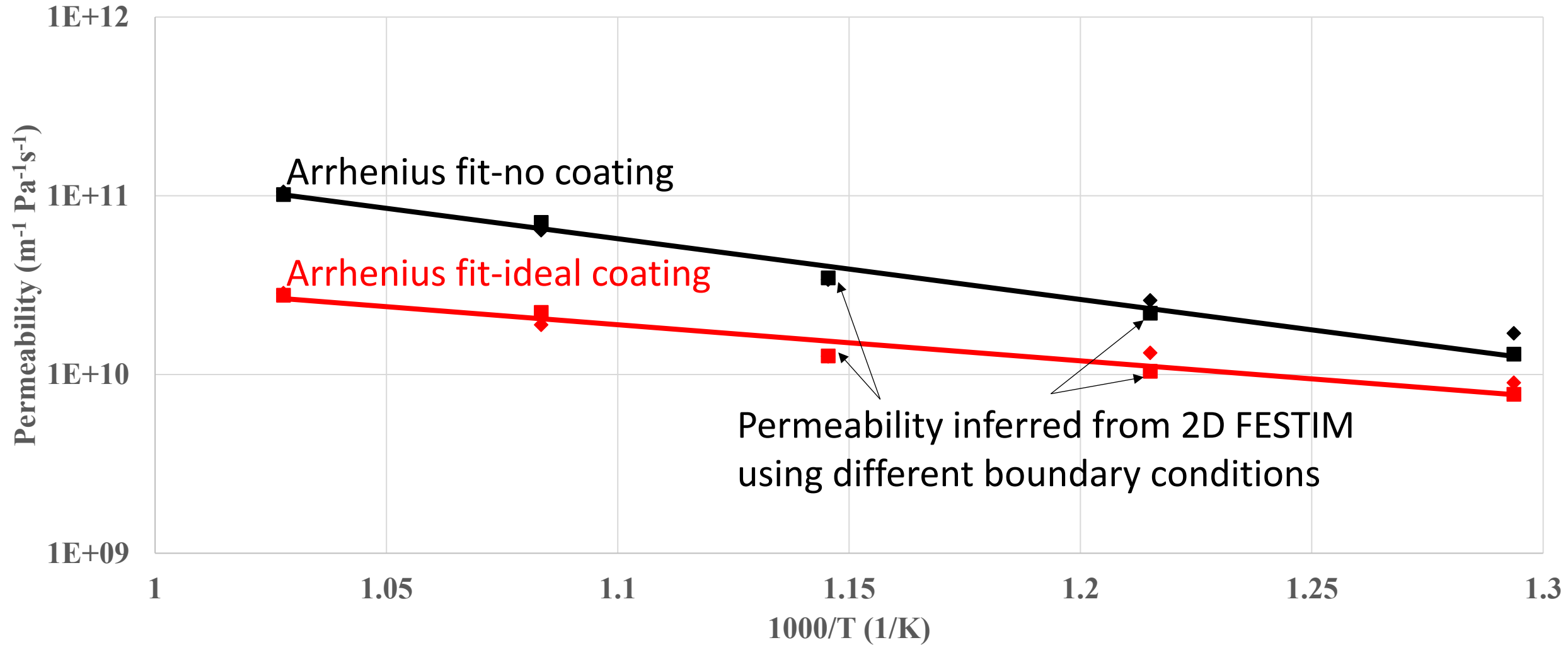
$$\ln P = \ln P_0 - \frac{E_P}{k_B T}$$

Weighted linear fitting,  $w_i = \frac{1}{\sigma_{\ln P_i}^2}$ , with

$\ln P_i$  relevant measurement uncertainty

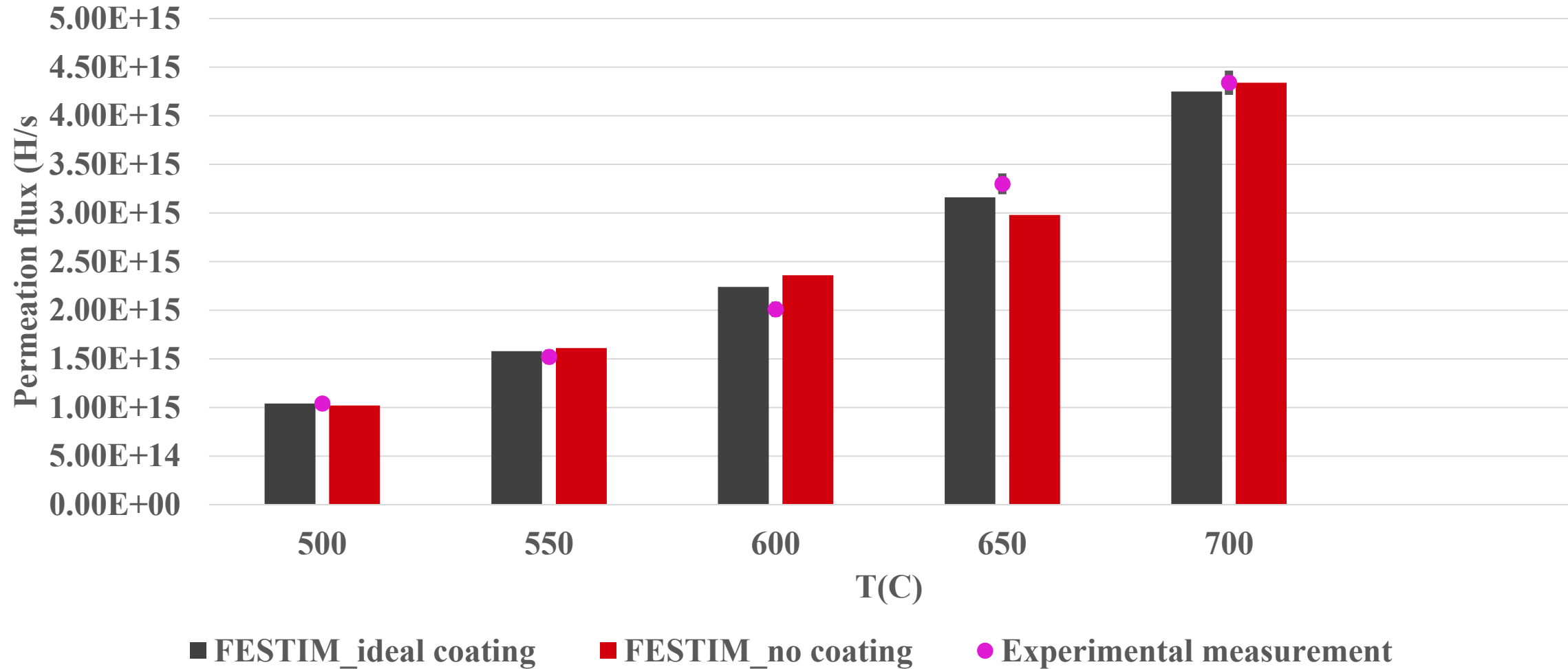


# Fitting permeability



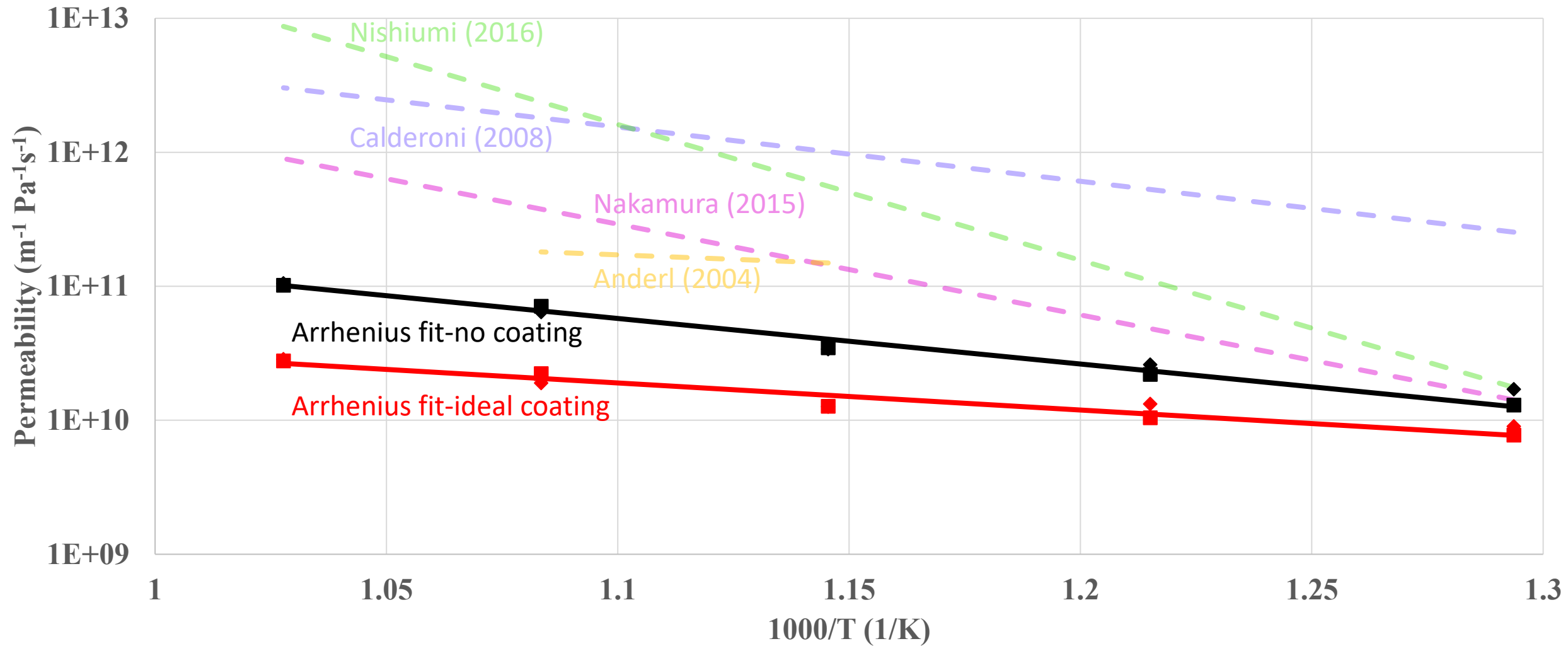
FLiBe permeability lies between  $3.17 \times 10^{12} \exp\left(-\frac{0.401}{k_B T}\right) \sim 3.16 \times 10^{14} \exp\left(-\frac{0.675}{k_B T}\right)$

# Fitting performance



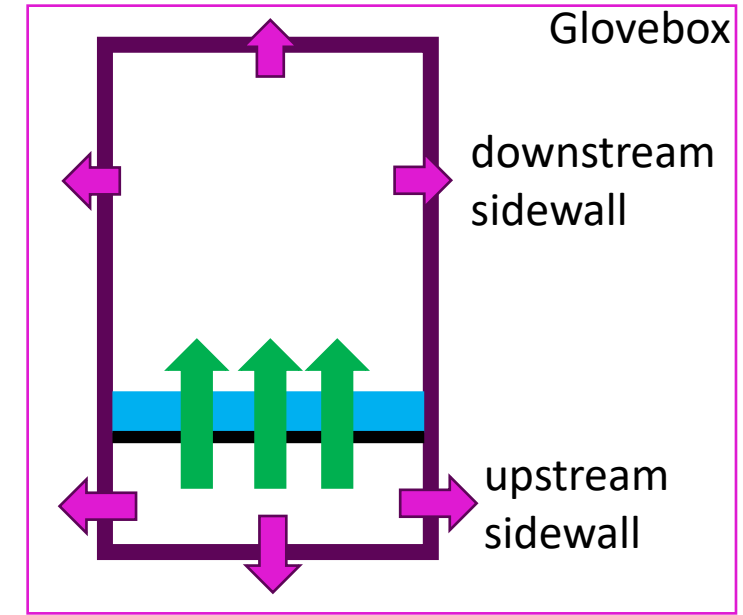
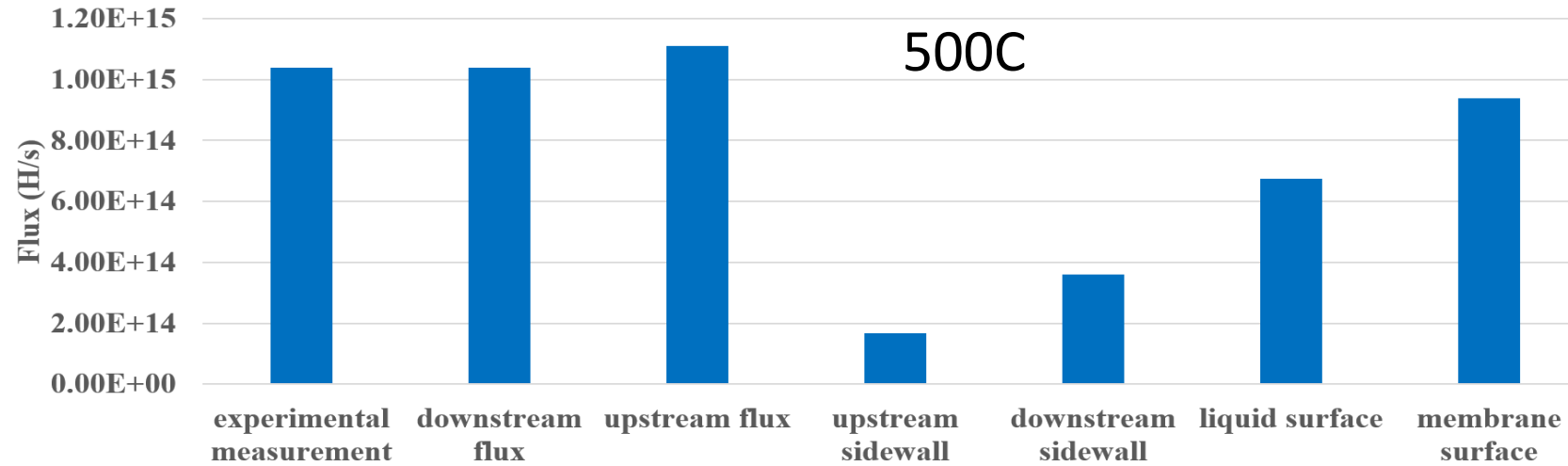
- Simulation match experiment
- Different inferred permeability, similar fluxes, **ONLY due to boundary condition choice**

# Fitting permeability



FLiBe permeability lies between  $3.17 \times 10^{12} \exp\left(-\frac{0.401}{k_B T}\right) \sim 3.16 \times 10^{14} \exp\left(-\frac{0.675}{k_B T}\right)$

# Hydrogen permeation behavior investigation



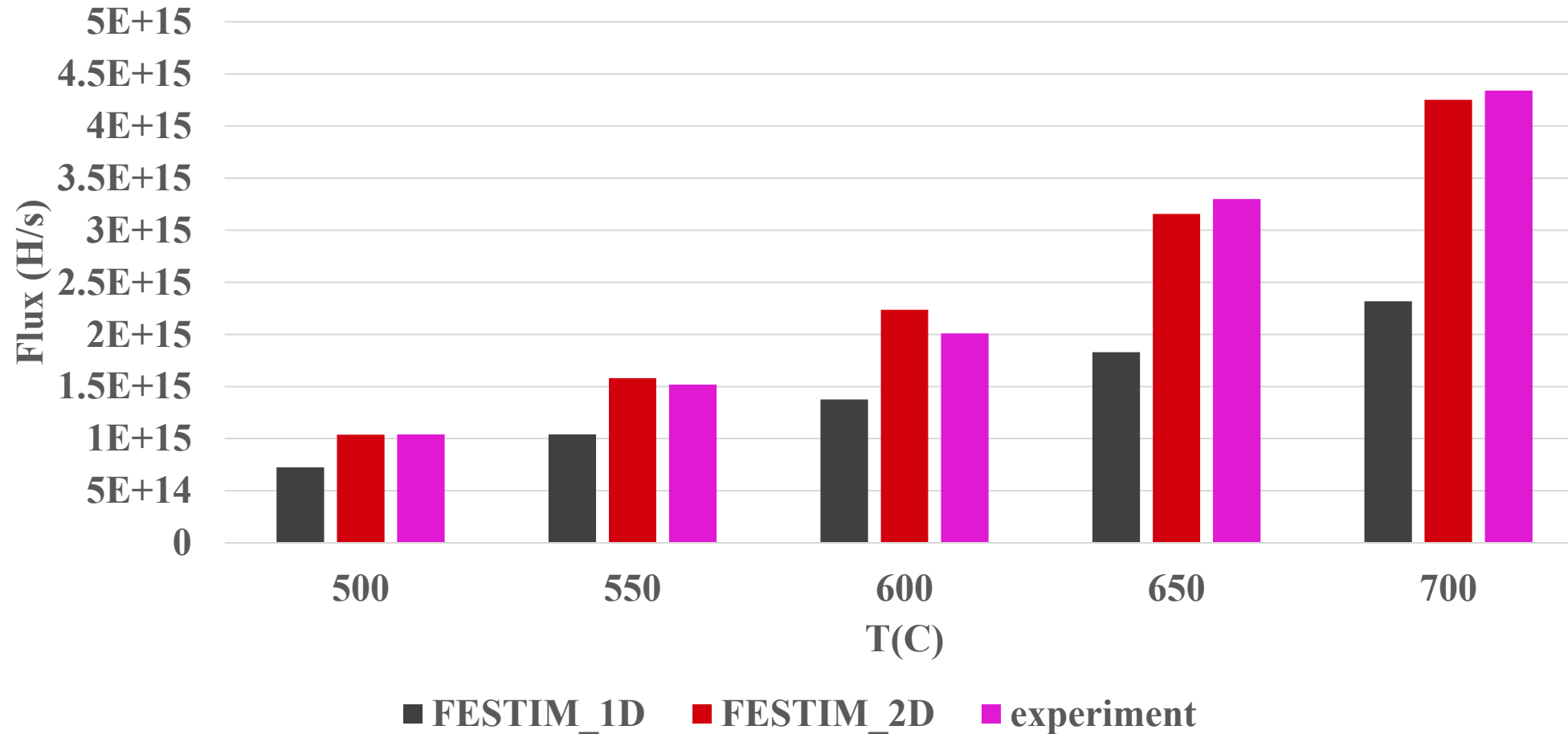
500-700C

Case	Upstream sidewall share Relative to upstream flux	Downstream sidewall share Relative to downstream flux
Ideal coating	15% - 21%	35% - 53%
No coating	~94%	13% - 61%

Sidewall transport contribution increases with temperature

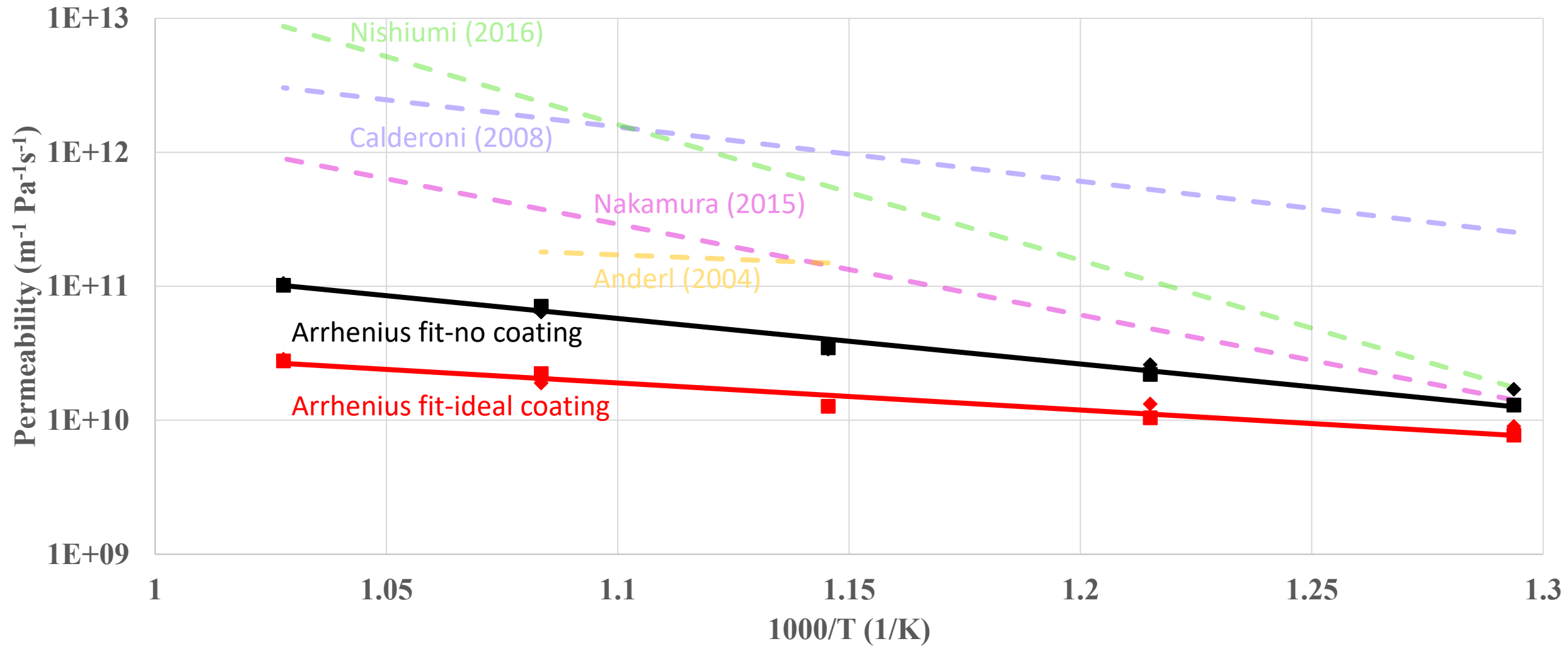
**Geometric effects are non-negligible**, should be modeled explicitly

# 1D vs 2D simulation result comparisons



- 1D models **underestimate** flux (~ 50% at 700C) → forces all H permeate through the shortest path and ignores real leakage geometry
- Extracted permeability from 1D is **artificially high**, especially at high temperature

# Fitting permeability



FLiBe permeability lies between  $3.17 \times 10^{12} \exp\left(-\frac{0.401}{k_B T}\right) \sim 3.16 \times 10^{14} \exp\left(-\frac{0.675}{k_B T}\right)$

# Conclusions & Takeaways

- Geometry strongly biases inferred FLiBe permeability
  - Neglecting sidewall leakage in 1D models leads to systematic **overestimation of permeability**, with the error growing at high temperature
- **First 2D, coating-condition-aware interpretation** of molten-salt permeation experiment using FESTIM

$$3.17 \times 10^{12} \exp\left(-\frac{0.401}{k_B T}\right) \sim 3.16 \times 10^{14} \exp\left(-\frac{0.675}{k_B T}\right)$$

- Direct impact on **tritium inventory & safety margins**
- **A transferable digital-twin framework** for permeation analysis
  - Applicable across molten salts, structural metals, and permeation test configurations



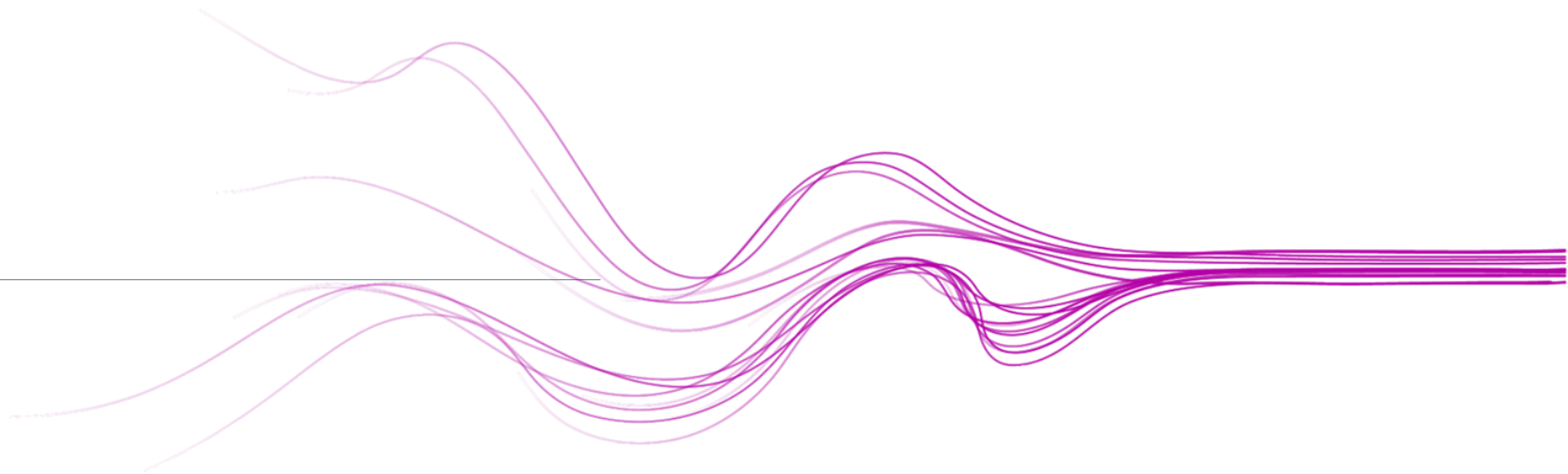
# Future direction

- **Interfacial bubble formation** has been observed at the metal-FLiBe interface, modifying the effective hydrogen permeability
- This introduces a **three-phase coupled transport problem**: solid-liquid-gas
- **Next step**: develop and integrate a **bubble nucleation, growth, and retention model** into FESTIM
- Swap configuration experimental data will be used to **quantify and interpret** the bubble-induced transport effects

# Acknowledgement

- This work is supported by the U.S. National Science Foundation (NSF) through the POSE Phase II program under Award No. 2449339.
- Experimental support
  - Abhishek Saraswat and Dr. Weiyue Zhou for conducting Hyperion permeation experiment
- Modeling & code development
  - FESTIM development team
- Collaborations
  - LIBRA project collaboration

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## Key parameters

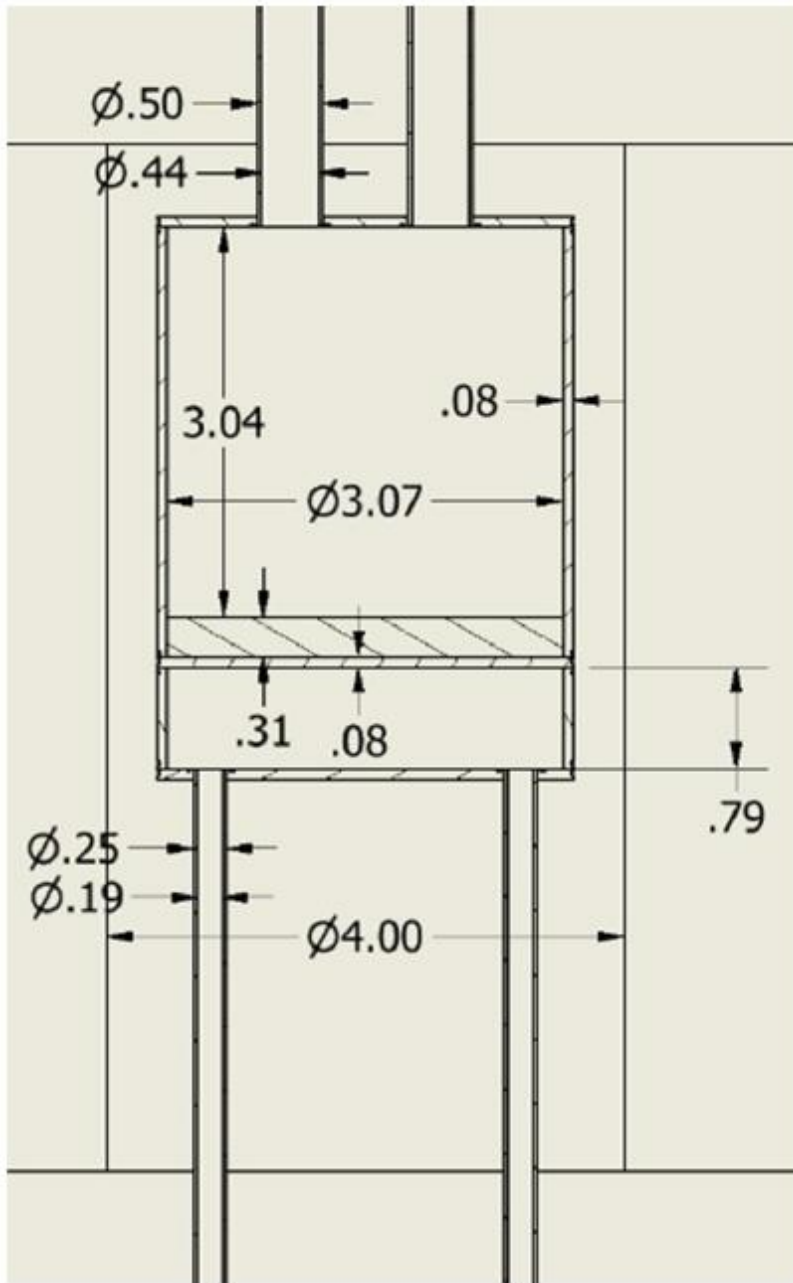
- Ni membrane: 0.002 m
- FLiBe thickness:

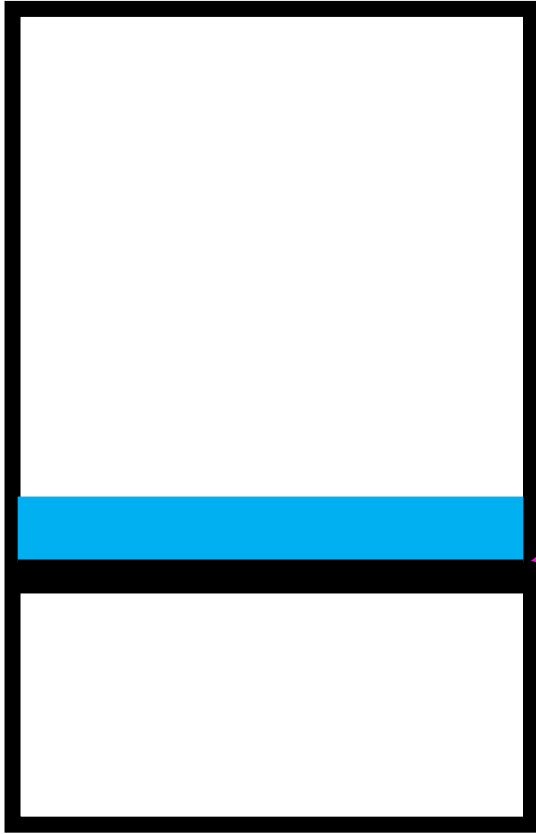
Salt layer thickness	m
Thickness @ 500C	0.005139858
Thickness @ 550C	0.005194021
Thickness @ 600C	0.005249337
Thickness @ 650C	0.005305845
Thickness @ 700C	0.005363582

- Repeat the measurement, each temperature repeat twice
- T=500-700C

## Experimental condition

- Normal:  $P_{\text{upstream}} \sim 1e5 \text{ Pa}$ ,  $P_{\text{down}}: 5\text{-}20\text{Pa}$





$$\frac{\partial c}{\partial t} = \nabla \cdot (D \nabla c)$$

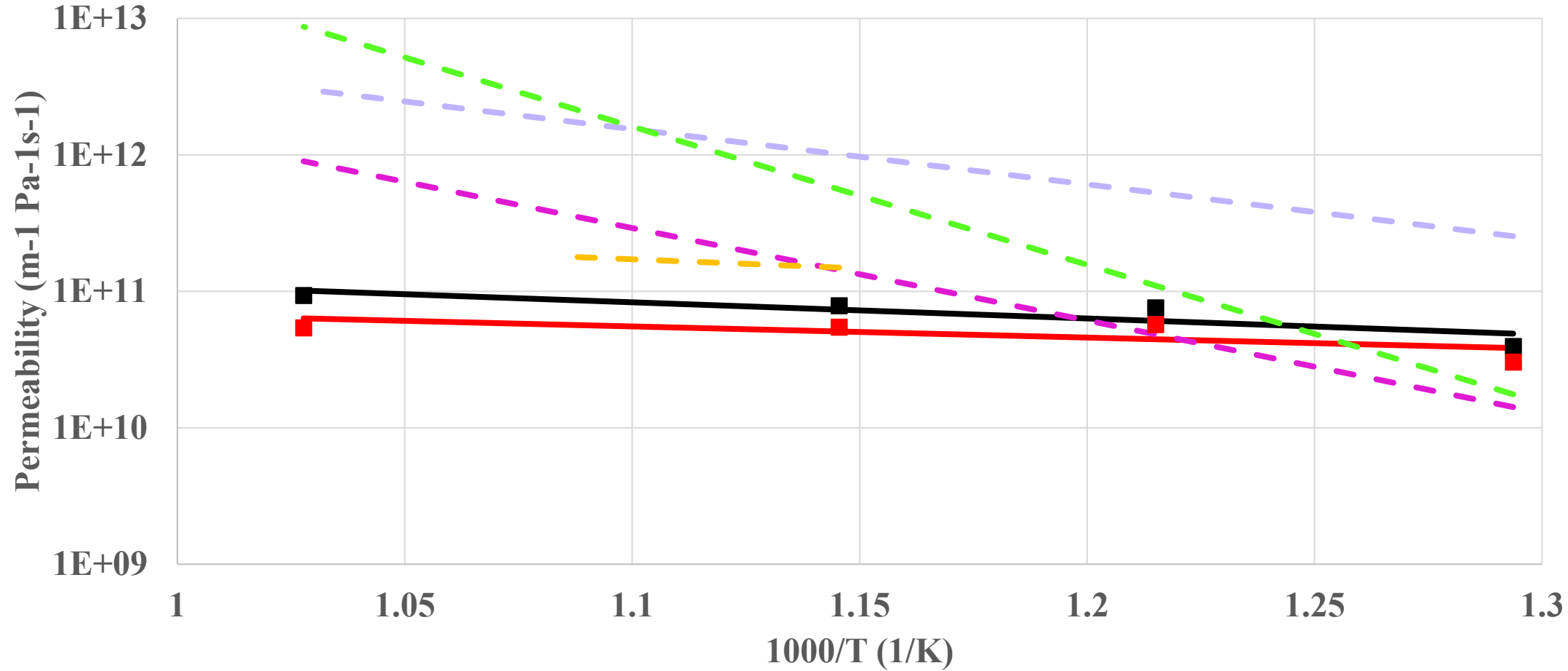
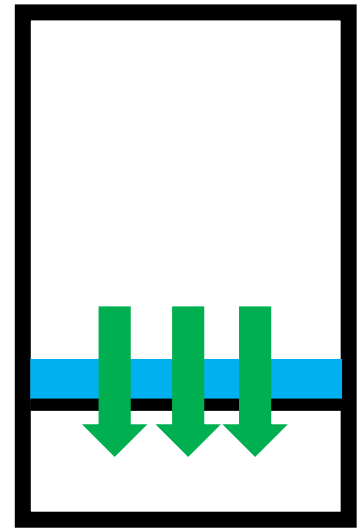
$$\left( \frac{c_{Ni}}{K_{s,Ni}} \right)^2 = \frac{c_{FLiBe}}{K_{H,FLiBe}}$$

$$J = -D \nabla c$$

# Uncertainty

- Mesh uncertainty almost negligible, mesh independence study has done
- Relative system error from gas chromatograph (GC):  $u_s = \frac{\Delta \text{PPM}_{\text{GC}}}{\text{PPM}_{\text{GC}}} \approx 1.00011\%$
- Measurement error  $u_r$ :
  - N steady state measurement data  $y_i, i = 1 \dots N$
  - Average:  $\bar{y}$
  - Standard deviation:  $std = \sqrt{\frac{\sum_{i=1}^N (y_i - \bar{y})^2}{N-1}}$
  - Standard uncertainty of the mean:  $u_r = \frac{std}{\sqrt{N}}$
- Combined standard uncertainty  $u_c = \sqrt{(u_s \bar{y})^2 + u_r^2}$
- Expanded uncertainty at 95% confidence:  $U = 2 u_c$

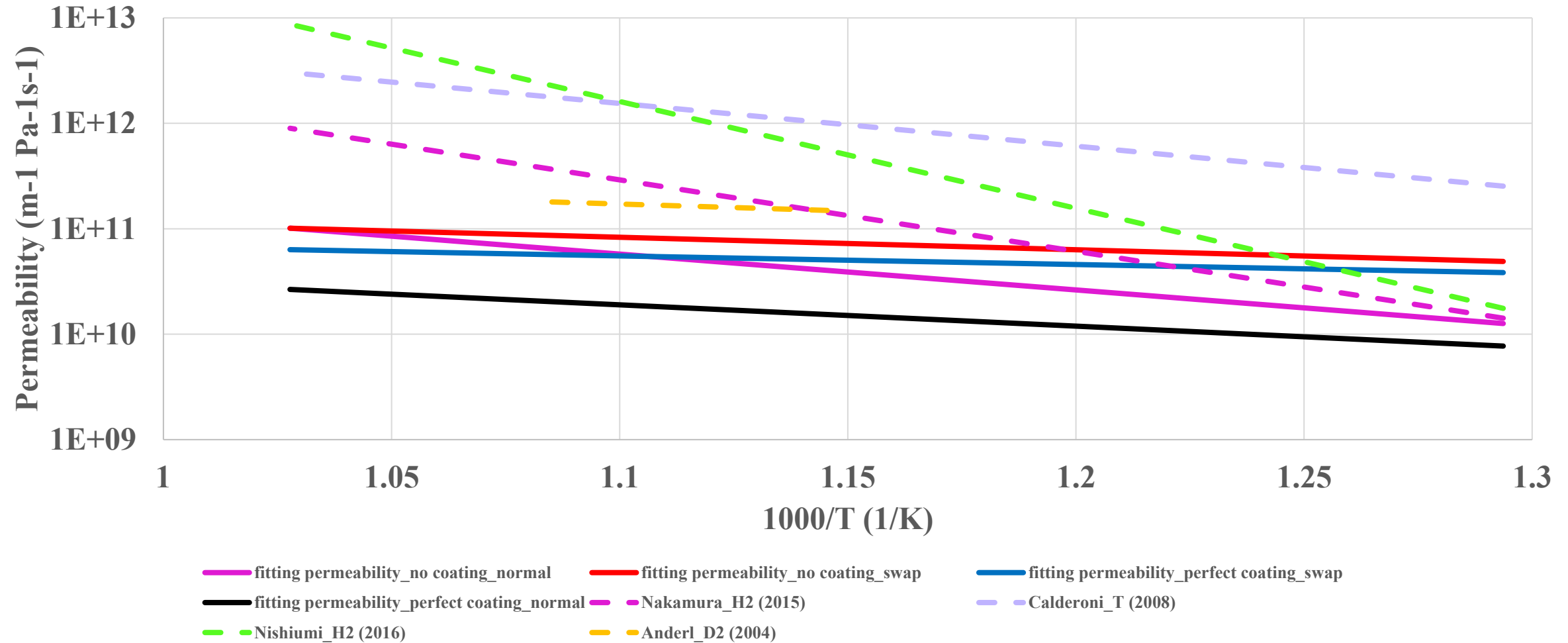
# Fitting of permeability: swap configuration liquid side as upstream



■ artificial permeability\_no coating\_exp 1    — fitting permeability\_no coating\_1    ■ artificial permeability\_ideal coating\_exp 1  
 — fitting permeability\_ideal coating\_1    - - Nakamura\_H2 (2015)    - - Calderoni\_T (2008)  
 - - Nishiumi\_H2 (2016)    - - Anderl\_D2 (2004)

$$4.38 \times 10^{11} \exp\left(-\frac{0.162}{k_B T}\right) \sim 1.67 \times 10^{12} \exp\left(-\frac{0.235}{k_B T}\right)$$

# Fitting of permeability





# FLiBe details

LiF–BeF<sub>2</sub> molten salt (typically 66–34 mol%)

Originally developed at ORNL (MSRE)

## ➤ Excellent Neutron Performance

- Lithium enables efficient tritium breeding
- Beryllium acts as a neutron multiplier
- Supports compact, high-performance blanket designs

## ➤ High Thermal Stability

- Operating range: ~500–900 C
- Low vapor pressure → compatible with near-vacuum systems
- Excellent heat transfer capabilities

## ➤ Chemical & Radiological Stability

- Low swelling under irradiation
- No violent boiling under off-normal conditions
- Chemically stable fluoride system

## ➤ Liquid Blanket = Self-Healing & Reconfigurable

- No radiation damage accumulation like solid blankets
- Salt can be purified, reprocessed, and reused online

Property	<b>FLiBe (LiF–BeF<sub>2</sub>)</b>	<b>FLiNaK (LiF–NaF–KF)</b>	<b>PbLi (Liquid Metal)</b>
Tritium breeding	✓	✓	✓
Neutron multiplier	✓	✗	✓
Phase	Molten salt	Molten salt	Liquid metal
Operating temp.	~500–900 C	~450–900 C	~500–800 C
Vapor pressure	Very low	Very low	Very low
Electrical conductivity	Low (good for MHD)	Low	High (severe MHD issues)
Chemical safety	Stable fluorides	Stable fluorides	Reactive with air/water
Radiation damage	Self-healing (liquid)	Self-healing	Self-healing
Tritium leakage risk	Moderate–High	Low–Moderate	High
Data availability	Sparse & inconsistent	Moderate	Extensive