



Investigation and qualification of Nuclear Materials for Gen-IV Lead Fast Reactor

IAEA Technical Meeting on Advances and Innovations in Fast Reactor Design and Technology

1° October 2025, IAEA HQ, Vienna

Marco Utili, D. Diamanti, L. Castronuovo, A. Meli, M. Tarantino, L. Silvioli, C. Pudoyer

Nuclear Energy Systems Division (NUC)





























Introduction

- ☐ The investigation and qualification of materials to be used in the Generation-IV Lead Fast Reactor (LFR), in operational and accidental conditions, is a critical issue in the development of the Reactor.
- □ At the Brasimone Research Center, ENEA in partnership with *new*cleo, is working to design, build, and operate Gen-IV Advanced Modular Reactors.
- ☐ To rapidly increase the TRL for the desired nuclear applications towards requirements of corrosion resistance, high temperature strength and thermal stability, a strong qualification roadmap is ongoing with the support of the experimental facilities.



Introduction

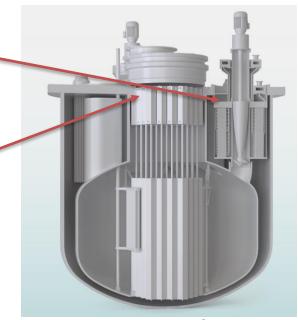
To define the operation limits, plan Restart Limits and major accident limits of the structural materials used in the design of the LFR experimental analysis e investigated with the experimental facilities at **ENEA BRASIMONE**:

- > **SOLEAD:** to investigate <u>chemistry control</u> in the lead in a big pool in standard operation and accidental scenario with interaction between liquid lead and water vapour/air
- ➤ CAPSULE: is used to investigate the <u>corrosion</u> behavior of materials in <u>stagnant</u> conditions with chemistry control in standard operation, transient and accidental conditions
- ➤ **CORE-1**: is dedicated to investigating the <u>corrosion and erosion</u> phenomena in <u>flowing</u> lead temperature range between 400° C and 650° C at 1-10m/s with chemistry control



Chemistry control in Lead in accidental scenario

- 1) Tests, consisting of water/steam injection inside the liquid lead, were carried out with the scope to support the **safety analysis** concerning the consequences of a <u>leak-before-break</u> in a tube of the **steam generator**.
- 2) A test, consisting of water/steam injection inside the cover gas, was carried out to support the safety analysis concerning the consequences of a steam inlet into the cover gas during the fuel handling.
- 3) A test, consisting of **injecting air into the cover gas**, was carried out, with the scope to study the <u>kinetics of oxygen diffusion from the cover gas to the liquid lead</u>.



Newcleo LFR AS:200

These tests had to provide information about the chemistry of lead and its control.



SOLEAD Experimental Facility

- SOLEAD (Solar tOwer LEAd Demo)
 experimental facility has used, in
 collaboration with newcleo, to carry
 out tests of interest for GEN-IV fast
 reactors, LFR type.
- The fields of SOLEAD application are: qualification of large size component, tests in natural circulation of the lead coolant, thermo-hydraulics tests in a big pool, material corrosion tests, lead conditioning and chemistry control tests.





SOLEAD Application

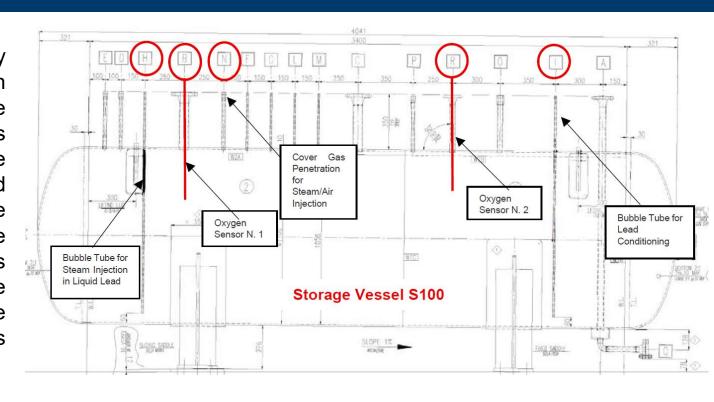
Main Design parameters of SOLEAD facility

Data	Value
Lead quantity	37 t
Storage vessel capacity	3640 L
Main vessel capacity	3720 L
Maximum temperature of lead conditioning in storage vessel	500°C
Maximum temperature for tests in main vessel	800°C
Lead conditioning by gas mixture	Ar/H ₂ /Air
Oxygen concentration measurements by Electrochemical Oxygen Sensors	Max. 3 (in storage vessel)



SOLEAD Facility Description

The facility is mainly composed of a main vessel S200, a storage vessel S100 and a gas for panel, the conditioning of the lead and the Ar supply to the the cover gas vessels. For the tests in the described following, the only storage vessel was used





Steam Injection in Liquid Lead

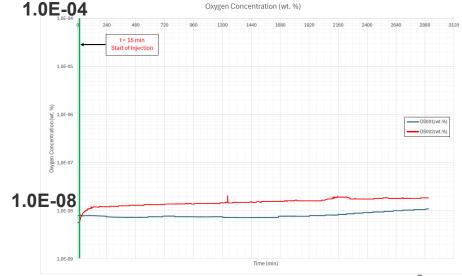
The tests aimed to study if interactions occur when steam is injected into liquid lead and if these
interactions, causing the dissociation of the water, can increase the oxygen dissolved in the liquid metal
bath.

• Different quantities of steam have been injected inside the liquid lead: the minimum amount (**40 g**) of injected water has an oxygen content sufficient to increase its concentration inside the liquid lead from 10⁻⁸

wt% to 10⁻⁴ wt%.

The initial test conditions are the following:

- Lead temperature: 480 ± 2 °C
- Oxygen content in Pb: ~ 10⁻⁸wt. %
- The Figure shows the oxygen concentration measured by the 2 Oxygen Sensors in Pb.
- The measured concentration is far from 10⁻⁴ wt%, value close to oxygen saturation in liquid lead at 480°C.





Steam Injection in Cover Gas

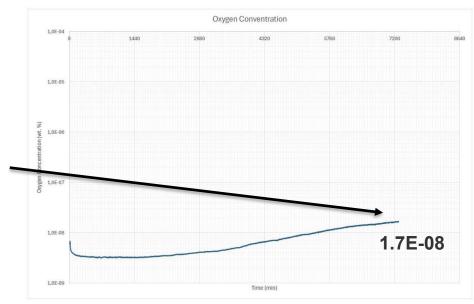
The test aimed to study if interactions occur between **steam injected into the cover gas** and the lead free surface and **if these interactions can cause the dissociation of the water molecules**, with production of oxygen and hydrogen, and diffusion of oxygen into the lead bulk.

The quantity of water that has been injected inside the cover gas is **100 g**. The initial test conditions are the

same of the previous tests.

 The Figure shows the oxygen concentration measured by OS001, during the test.

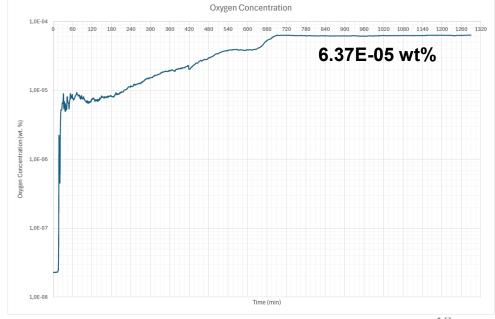
 After the initial transient, the oxygen concentration measured remains approximately constant for a little over a day and then starts to increase, reaching the maximum value, at the end of the test, of approx. 1.7E-08 wt. %.





Air Injection in Cover Gas

- The aim of the test was to study if interactions occur between air injected into the cover gas and the lead
 free surface and the kinetics of oxygen diffusion inside the lead. The initial test conditions are the same
 of the previous tests. The quantity of air that has been injected inside the cover gas is 120 NL (same atomic
 oxygen content of 40g of water).
- by OS001 shows a sharp increase. Then, the increase becomes less pronounced and, after approximately 675 min from the start of injection, the oxygen concentration remains approx. constant, reaching a maximum value of 6.37E-05 wt%, close to saturation. The arrest of the oxygen concentration growth is due to the decrease of the cover gas pressure and, as consequence, its lower oxygen content.





Test Results – Chemestry control in lead

➤ The results showed that the **steam injection**, both in the lead and cover gas, has had a negligible impact on the coolant chemistry control.

➤ The inlet of **air in the cover gas** has had a quick effect on the oxygen content inside the liquid lead; this fact leads to suppose that the operations of the facility could be compromised if countermeasures are not taken.

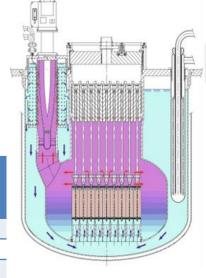


Materials Characterization in Lead

- Structural materials behaviour in lead are analysed at operational, accidental and transient conditions.
- Different product type of the alloy is investigated for each condition: forged bar, seamless pipe, laminated plate, and welded joint.

Component	Acc. Max Temp. ⁽⁰⁾ (°C)	Max. Rad. damage (dpa)	Material (early stages with C _o = 10 ⁻⁶ -10 ⁻⁸ w%)
Fuel cladding	530/750	100	15-15Ti 20% CW (AIM1)
FA Structures	500/750	100	15-15Ti 20% CW (AIM1)
Internal structures	500/700	<2	AISI 316LN (ASTM)
Steam Generator	500/700	0.01	AISI 316LN (ASTM)

Newcleo LFR: AS-200



Power	480 MWth	
Core coolant	Pure lead	
Core coolant temperature	inlet 420°C, outlet 530°C	
Layout	Pool-type	
Circulation	Forced: 6 pumps	
Spectrum	Fast	
Fuel form	Extended-stem fuel assembly	
Fuel	MOX	
Secondary side fluid	Water	
Steam generators	6 spiral-tube SG	
Design life	60 years	
Lifetime capacity factor	94%	



Materials Characterization in stagnat Lead

The material characterisation is performed with 36 standardized modular capsule to carry out the experiments adopting the same device and procedures.

CAPSULES have been in operation since December 2023.

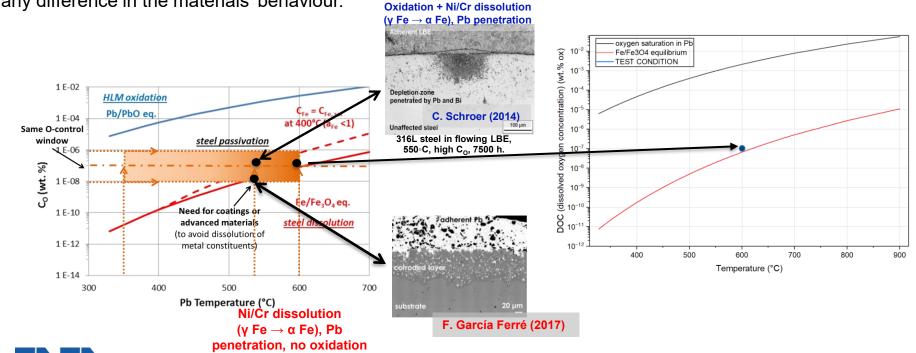
The facility is used to test various kinds of steel, both bare and coated, in stagnant lead under an oxygen-controlled concentration, essentially between 10^-8 and 10^-6 wt%; a temperature range of 450-750 °C is also employed.





Material Characterization in Lead-accidental scenario

Screening tests on 316L (N) have been performed in CAPSULE at 500°C and 600°C with oxygen concentration slightly above the passivating one: 10-7wt.%. **Exceeding the operational limits** helps to see any difference in the materials' behaviour.



Material Characterization in Lead –316L Characterization

Three different 316L(N) alloy product types are investigated, all in a solution annealed conditions (RCC-MRx designation, RPS SECTION III, TOME 2):

- RM332-4 forged bar
- RM334-1 seamless pipe
- RM333-1 laminated plate



RM332-4 forged bar

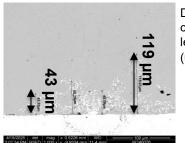


RM333-1 laminated plate



Screening Test in Stagnant Lead - 500h 600°C 1e-7 wt.%

RM 333-1 laminated plate



Deep localized corrosion and lead penetration (up to 119 µm)

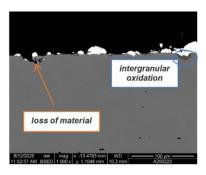
RM 332-4 Forged bar



Deep localized corrosion and lead penetration (up to 241 µm)

Most of the analysed surface not corroded

RM 334-1 seamless pipe

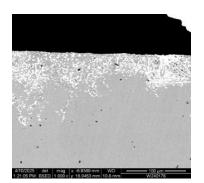


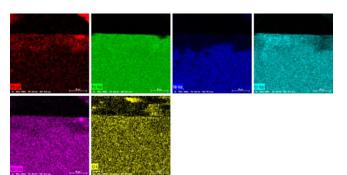
Lead penetration (spots)

Unselective leaching (loss of material)

Internal oxidation

Corrosion layer up to $\sim 20 \ \mu m$





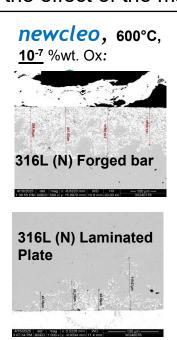
Worst cases for the condition 600°C, 1e-7wt.% are shown for different products:

- Corrosion by selective and/or unselective dissolution, coupled with Pb penetration, observed in all products,
- Worst behaviour in forged part (max 241 µm dissolution depth), best in seamless tube
- · Preliminary results, to be confirmed



Literature review on AISI 316 at 480-600°C Pb exposures

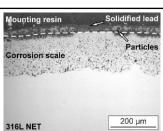
The experimental data are in agreement with the literature data at the same operative conditions; the effect of the manufacturing process has to be investigated:





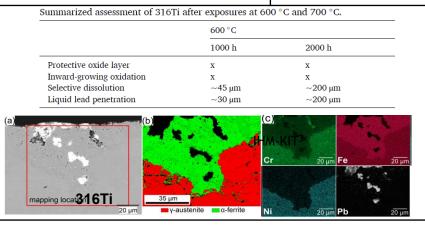
CIEMAT¹- static Pb, 480°C, 2000h, <u>10-7</u> %wt. Ox.

- Fe-Cr oxidation on both austenitic steels
- No Pb penetration
- No significant elemental dissolution



ENEA²- static Pb, **550**°C, 1000h, <u>2*10⁻⁷</u> %wt. Ox. LOM imaging

- Passivation not occur
- Pb penetration & el. Dissolution and ferritization (100-150 µm)



KIT-IHM³ static lead, 600° C, 2×10^{-7} wt% Ox.

¹Bassini et al. GEMMA conference 2023 ²Bassini et al. Deliverable 4.2 GEMMA

³Purwitasari et al., 2025



Material Characterization: accidental and accidental conditions

- ☐ The next step is the testing in **accidental conditions** just on the material type that showed the **worst** resistance in the screening tests.
- □ Accidental, transient and cumulative/integral durations of accidents, transients and accidents throughout the anticipated lifetime of the relevant components and systems are studied. Three different temperatures are selected to simulate the behaviour of the materials, exceeding:
 - Operational limit (Design Basic Condition (DBC)-1, 550°C, corrosion layer under 144 μm in 1,000 hours with an oxygen content of 10⁻⁷ wt.%)
 - Plant Restart limit (DBC-2 &3, 650°C, 10-2 > f > 10-4 y-1)
 - Major Accident limit (DBC-4 & DEC-A, 750°C, corrosion runaway threshold, f > 10⁻⁴ y⁻¹)

Two exposure durations - 100 h and 500 h - are selected at each temperature to simulate both a single accident (lasting more than 72 hours) and the cumulative effect of multiple accidents. During these tests, the oxygen concentration is maintained near the lead oxide equilibrium (10⁻⁴ wt.%) and below the magnetite formation threshold (10⁻⁸ wt.%, ensuring no passivation).

Subsequent tests under **normal operating conditions** are conducted by varying temperature (440°C and 480°C), oxygen content (10⁻⁸ wt.% - 10⁻⁵ wt.%), and exposure time (500 - 8000 hours). A sensitivity analysis is performed to evaluate the effects of time, oxygen content, and temperature on corrosion and passivation layer development, using SEM and EDS analyses on cross-sections of the tested samples.



Material Characterization in Flowing Lead

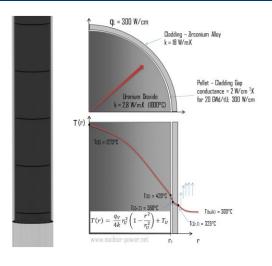
CORE-1

Loop-type facility to test various kinds of steel, bare and coated, in fluent lead under oxygen-controlled concentration, essentially between 10-8 and 10-6 wt %; temperature in the corrosion test section 650 °C and velocity 1 m/s; in the erosion test section the temperature is 520 °C and the velocity 10 m/s. It will also be used to test the effectiveness of cold traps and mechanical filters





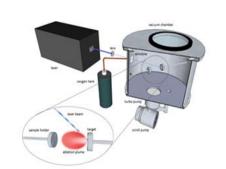
Coating Technologies

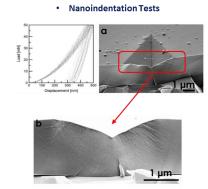


- □ Alumina-based coating manufacturing by Pulsed Laser Deposition (PLD) technology was selected as one of the most promising for Fuel cladding coating manufacturing thanks to the metal-like behaviour under plastic strain
- □ 1:1 scale PLD facility was designed and will be installed in 2026-2027 in ENEA Brasimone to validate the process at an industrial scale

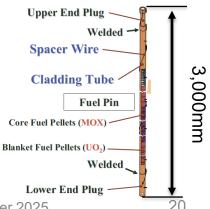
The facility will be able to:

- Manufacture the coating on pipes characterised by a length of 3,000mm, and a diameter in the range between 6 and 13mm
- ☐ Manufacture the coating on 1000 pipes per year.





metal-like behavior under plastic strain



Conclusion

- Experimental characterization of <u>chemistry control in lead</u> in standard operation and in accidental scenario are ongoing in SOLEAD facility, the facility will be upgraded in 2026-2028 to integrate the Remote Handling system and analyze full-scale operational scenario;
- <u>Structural material characterization</u> tests exceeding the operational limits in stagnant and flowing lead are ongoing: Design Basis Conditions, Design Extension Condition, transient and cumulative/integral durations of accidents and transients of the relevant components and systems are studied;
- A <u>database for the analysis of corrosion rate</u>, lead penetration in the materials with different manufacturing processes, surface status, and welding techniques is under development starting from the data available in the literature and European projects (MATTER, GEMMA, CONNECT – NM);
- <u>Coating</u> technologies R&D is ongoing to increase the TRL of the technology available at laboratory scale and demonstrate in 2026-2027 the applicability at industrial scale of PLD technique.



Thank you for the attention!



Marco Utili marco.utili@enea.it



