Nuclear Materials and Nuclear Fuel Cycle Center

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Lessons Learned From Operation of A Forced Convection Chloride Molten Salt Loop

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Our Current Research/Capabilities

On-line salt purification/chemistry

- Metal impurity removal
- Non-metal impurity control/removal
- Phase diagram/material solubility
- □ Salt/alloys interactions (Corrosion)
 - Redox potential control
 - > Thermodynamic data measurements
 - Corrosion kinetic data measurements
 - On-line corrosion measurements (flowing and static tests)
 - Graphite degradation in molten salt
- Material separation
 - Oxide reduction
 - Electrochemical separation
 - Liquid/liquid separation
- **Galt Impurity measurement**
 - Metal impurities
 - > O/H impurities
 - > S/C impurities

Model development

- Corrosion model in molten salt loop
- Thermodynamic model for fundamental data
- Electrochemical separation model for salt purification
- Safeguards model for molten salt systems

Measurements of Salt properties

- Liquid salt density,
- thermal conductivity, heat capacity, latent heat
- Materials solubility
- Melting/freezing temperature,
- Phase diagram
- Transport properties, ion diffusion coefficient
- Corrosion kinetics
- Vapor pressure, vaporization rate
- Liquid salt viscosity (method not validated)

VIRGINIA Chloride Molten Salt Advantages and Challenges

Chloride molten salt is the promoted heat transfer fluid (HTF) and thermal energy storage (TES) salt in nuclear and concentrating solar power plants (CSP).

Advantages

✓ Lower melting point

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- Higher boiling point \checkmark
- Lower vapor pressure \checkmark
- Not flammable \checkmark
- \checkmark Low cost
- Non-toxic \checkmark

Background

Good high-temperature thermal \checkmark stability



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Problem Statements



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The Forced Convection Chloride corrosion Loop (FCL)





Flow-induced corrosion

216 holder	wt%	A709	SS316
	Cr	19.93	18-20
Alumina isolator	Ni	24.98	11-14
	Fe	Bal.	Bal.
Alumina spacer \longrightarrow	Mn	0.91	1-2.5
	Мо	1.51	2-3
Test samples -	Si	0.44	0.3-0.65
$ \begin{array}{c} & & \\ & & $	Nb	0.2	-
	Ti	0.04	-
	Cu	-	0.75
	Ν	0.148	-
D: 0.18 inches	С	0.066	0.03
Nimonic 900	Р	0.014	0.03
spring washer	В	0.0045	-
	S	-	0.03

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MSL Specification and Operation Condition

Capability	Parameters
Salt	MgCl ₂ -KCl-NaCl
Flow rate	0.7 L/s
Design temp.	700 °C
Main heater power	15 k W_{th}
Trace1 heater power	10.8 kW_{th}
Trace 2 heater power	$3.6 \text{ kW}_{\text{th}}$
Salt volume	30 L (8 gallons)
Main piping	1-inch sch. 160
Pump	3 HP 0-60 Hz
Loop length	8 m

Experimental Condition

Temperature: 650 °C

Salt weight: 40 kg

Volumetric flow rate: 0.45 l/s

Flow rate at main pipe: 1.25 m/s

Flow rate at test column: 2 m/s

Flow Condition

	Meter V m/s	Flow rate L/s	Loop Re	Test column V m/s	Test column Re
FCL-50	0.5	1.68	5657	0.8	3690
FCL-80	1.25	4.21	14892	2	9225
FCL-100	1.25	4.21	14892	2	9225

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VIRGINIA TECH. **FCL** Operation Transportation Loading Purification Circulation Drainage 1. Cover gas Open vent line of Sto. Preheat the transportation line • 2. Exhaust Open salt Valve #5 and Sto. to 550 °C 3. Heater Flow rate at 7.5 LPM 4. Thermowell 6 a.b.c. purging line Pressurizing Aux. 1.5-2 psi Salt transfer complete at the gas flow suddenly increased to max. Salt transfer direction Storage Tank and Pump Sensor Portals Test Storage tank Column 6h Ultrasonic Flowmeter Auxiliary Tanl Aux. tank

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FCL Operation



Lessons From MSL Operation

Loading

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Purification

Transportation

Results

Circulation

Drainage

Vapor Solidification

- Temperature at the top flange is about 350 °C
- Salt circulation in the Sto. tank generates salt vapor
- Cover gas flow is RT before injecting to Sto. tank
- Cover gas flow rate 0.7 L/min through a half-inch tube
- Solidification occurred and block the inlet



• ORNL loop in 1960s, does not have any values at the circulation path

• Valve is the most complex part that exposed to the flow

Valve leakage

• High-temperature valve leaking is the crucial issue





Conclusions

Lessons From MSL Operation



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Flow





BED images of cross-sections FCL-100-SS316



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The evidence of surface removal on FCL-80-SS316



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Partial removal evidence FCL-100-SS316-S1



Flow Direction



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BED images of cross-sections FCL-100-A709

Flow Direction



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Surface removal evidence FCL-80-A709-S1



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Summary of the Cr depletion depth



- Inner surface underwent typical static corrosion
- Outer surface underwent the FIC and erosion

- The Cr depletion layers thickness are $D_{static} > D_{FIC}$

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Revealing the FIC mechanism in molten salt

In FIC, the significant mass transfer of both corrosion products and oxidant results in the corrosion reaction occurring on the surface at a much higher rate than under static conditions.

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Cr depletion Cr_2O_3 dissolution

Methodologies



Rib turbulator effect



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- Preheating the large loop body is crucial. The quick heat loss can easily block the path.
- The molten salt has the advantage of preventing coolant loss for fuel loss accidents.
- The welding is the best sealing technology in high temperature molten salt application.
- High temperature valve for chloride molten salt needs to be developed.
- Chloride electrolysis incidents are a severe challenge for the testing loop.
- The flow-induced corrosion rate is more significant than static condition tests.
- The flow-induced corrosion process results in server Fe depletion.
- Erosion corrosion happens in the flow-induced condition.

Results

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- Dr. Ting-Leung Sham (Idaho National Laboratory): A709 alloys material
- Dr. Yanli Wang (Oak Ridge National Laboratory) : A709 sample and sample fixture manufacturing

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CARBON NET ZER® Thank You! Questions?