



Impact of isomeric yield ratios on reactor antineutrino spectra

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Fission Yields in anti-v spectra summation calculations



 $\mathbf{\xi}$ The contribution from the β-decay of each fission product is weighed with its fission yield

FY evaluations -- uncertainties



FY evaluations -- uncertainties



FY evaluations -- uncertainties



FY evaluations -- what's in there?



FY evaluations -- what's in there?



when no measurement is available, independent yields are obtained from Wahl charge-distribution model (errors ~ 32-100%, depending on the yield).

Evaluated yields are obtained normalizing the model prediction to the closest available data points \rightarrow a large error was assumed in these cases.



Isomeric Yield Ratios

- Fission Yields are a key component of the Summation Method
- Isomeric Yield Ratios represent another key component that is difficult to accurately predict, and must be based on experimental data.

$$IYR = \frac{Y_{isom}}{(Y_{isom} + Y_{gs})}$$





Isomers and antineutrino spectra



Isomers and antineutrino spectra



IYRs in current FY evaluation



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It predicts IYR with minimal information on the fission products:

Isomeric ratio is split based on the J_g / J_m assuming a statistical P(J):

 $P(J) = P_0(2J + 1) \exp\left[-(J + \frac{1}{2})^2/\langle J^2 \rangle\right]$

1-parameter (J_{rms}) that fixes the P(J) distribution for all FFs

Experimental Recommended IYRs

Chesk for spoores			Available online at www.sciencedirect.com ScienceDirect						Nuclear Data Sheets			
ER		Nuclear Data Sheets 173 (2021) 118-143						www.elsevier.com/locate/nds				
	Comp	oilation	and Evalu	ation of Is	omer	ic Fi	ission Yiel	ld Rati	05			
. Sea	ars, ^{1,2} A. I	Mattera, ¹ ¹ Nation ² S	^{1,*} E.A. McCu nal Nuclear Dat Bldg. 817, P.C mith College, 1	tchan, ¹ A.A. ta Center, Bro b. Box 5000, U b Elm Street,	Sonzog okhaven Ipton, 1 Northas	ni, ¹ E Natio NY 11 mpton,	D.A. Brown, ¹ onal Laborator 973-5000 MA 01063	and D. F y,	Potemkin ^{1, 3, 4}			
Id	Tgt Name	Proj Name	${f E_{ m inc}} ({ m MeV})$	Fission F Name	rodu J _g	$_{\rm J_m}^{\rm ct}$	IYR (org)	Form	IYR (M/T)	EXFOR	Ref.	Notes
0	U-235	n	2.5×10^{-8}	32-Ge-79	1/2	7/2	0.8(10)	M/T	$[0 \cdots 1]$	22161	[31]	0
1	U-233	n	2.5×10^{-8}	32-Ge-81	9/2	1/2	0.24(7)	M/T	0.24(7)	22798	[34]	
	U-235	n	2.5×10^{-8}	32-Ge-81	9/2	1/2	0.20(6)	M/T	0.20(6)	00161	[91]	
2				02 00 01			0.30(0)	IVI/ I	0.30(0)	22101	31	
$\frac{2}{3}$	U-238	n	1	32-Ge-81	9/2	1/2	0.30(0) 0.46(8)	M/T	0.30(0) 0.46(8)	22334	[31]	
$2 \\ 3 \\ 4$	U-238 Th-232	n p	1 25	32-Ge-81 32-Ge-81	$\frac{9}{2}$ $\frac{9}{2}$	$\frac{1/2}{1/2}$	0.30(0) 0.46(8) 0.920(20)	M/T M/T	0.30(0) 0.46(8) 0.920(20)	22334 O2429	[31] [32] [27]	
$2 \\ 3 \\ 4 \\ 5$	U-238 Th-232 U-238	n p p	1 25 25	32-Ge-81 32-Ge-81 32-Ge-81	$9/2 \\ 9/2 \\ 9/2 \\ 9/2$	$1/2 \\ 1/2 \\ 1/2 \\ 1/2$	$\begin{array}{c} 0.30(0) \\ 0.46(8) \\ 0.920(20) \\ 0.970(10) \end{array}$	M/T M/T M/T	$\begin{array}{c} 0.30(0) \\ 0.46(8) \\ 0.920(20) \\ 0.970(10) \end{array}$	22334 O2429 O2429	[31] [32] [27] [27]	
$2 \\ 3 \\ 4 \\ 5 \\ 6$	U-238 Th-232 U-238 U-238	n p p p	1 25 25 25	32-Ge-81 32-Ge-81 32-Ge-81 32-Ge-81	9/2 9/2 9/2 9/2 9/2	$1/2 \\ 1/2 \\ 1/2 \\ 1/2 \\ 1/2$	$\begin{array}{c} 0.30(0) \\ 0.46(8) \\ 0.920(20) \\ 0.970(10) \\ 0.975(7) \end{array}$	M/T M/T M/T M/T	$\begin{array}{c} 0.30(0) \\ 0.46(8) \\ 0.920(20) \\ 0.970(10) \\ 0.975(7) \end{array}$	22334 O2429 O2429 O2395	[31] [32] [27] [27] [28]	
$2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7$	U-238 Th-232 U-238 U-238 U-233	n p p n	$ \begin{array}{r} 1 \\ 25 \\ 25 \\ 25 \\ 2.5 \times 10^{-8} \end{array} $	32-Ge-81 32-Ge-81 32-Ge-81 32-Ge-81 33-As-82	9/2 9/2 9/2 9/2 9/2 2	1/2 1/2 1/2 1/2 1/2 5	$\begin{array}{c} 0.30(0) \\ 0.46(8) \\ 0.920(20) \\ 0.970(10) \\ 0.975(7) \\ 0.13(8) \end{array}$	M/T M/T M/T M/T M/T	$\begin{array}{c} 0.30(0) \\ 0.46(8) \\ 0.920(20) \\ 0.970(10) \\ 0.975(7) \\ 0.13(8) \end{array}$	22334 O2429 O2429 O2395 22798	[31] [32] [27] [27] [28] [34]	D
2 3 4 5 6 7 8	U-238 Th-232 U-238 U-238 U-233 U-235	n p p n n	$\begin{array}{c} 1 \\ 25 \\ 25 \\ 25 \\ 2.5 \times 10^{-8} \\ 2.5 \times 10^{-8} \end{array}$	32-Ge-81 32-Ge-81 32-Ge-81 32-Ge-81 33-As-82 33-As-82	9/2 9/2 9/2 9/2 9/2 2 2	$1/2 \\ 1/2 \\ 1/2 \\ 1/2 \\ 1/2 \\ 5 \\ 5$	$\begin{array}{c} 0.30(6)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\end{array}$	M/T M/T M/T M/T M/T M/T	$\begin{array}{c} 0.30(6) \\ 0.46(8) \\ 0.920(20) \\ 0.970(10) \\ 0.975(7) \\ 0.13(8) \\ 0.17(7) \end{array}$	22334 22334 O2429 O2429 O2395 22798 22161	[31] [32] [27] [27] [28] [34] [31]	D D
$ \begin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \end{array} $	U-238 Th-232 U-238 U-238 U-233 U-235 U-235	n p p n n n	$\begin{array}{c} 1 \\ 25 \\ 25 \\ 25 \\ 2.5 \times 10^{-8} \\ 2.5 \times 10^{-8} \\ 1 \end{array}$	32-Ge-81 32-Ge-81 32-Ge-81 32-Ge-81 33-As-82 33-As-82 33-As-82	9/2 9/2 9/2 9/2 2 2 2 2	1/2 1/2 1/2 1/2 5 5 5	$\begin{array}{c} 0.30(0)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\\ 0.08(4) \end{array}$	M/T M/T M/T M/T M/T M/T M/T	$\begin{array}{c} 0.30(6)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\\ 0.08(4) \end{array}$	22334 22334 O2429 O2429 O2395 22798 22161 22334	[31] [32] [27] [27] [28] [34] [31] [32]	D D D
$ \begin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ \end{array} $	U-238 Th-232 U-238 U-238 U-233 U-235 U-238 U-238	n p p n n n p	$\begin{array}{c} 1 \\ 1 \\ 25 \\ 25 \\ 25 \\ 2.5 \times 10^{-8} \\ 2.5 \times 10^{-8} \\ 1 \\ 24 \end{array}$	32-Ge-81 32-Ge-81 32-Ge-81 32-Ge-81 33-As-82 33-As-82 33-As-82 33-As-82	9/2 9/2 9/2 9/2 2 2 2 2 2 2 2	1/2 1/2 1/2 1/2 5 5 5 5	$\begin{array}{c} 0.30(0)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\\ 0.08(4)\\ 0.270(30) \end{array}$	M/T M/T M/T M/T M/T M/T M/T M/T	$\begin{array}{c} 0.30(6)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\\ 0.08(4)\\ 0.213(19) \end{array}$	22334 22334 O2429 O2429 O2395 22798 22161 22334 E1855	[31] [32] [27] [27] [28] [34] [31] [32] [30]	D D D
$2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11$	U-238 Th-232 U-238 U-238 U-233 U-235 U-238 U-238 U-235	n p p n n n p n	$\begin{array}{c} 1 \\ 25 \\ 25 \\ 25 \\ 2.5 \times 10^{-8} \\ 1 \\ 24 \\ 2.5 \times 10^{-8} \end{array}$	32-Ge-81 32-Ge-81 32-Ge-81 32-Ge-81 33-As-82 33-As-82 33-As-82 33-As-82 33-As-82 33-As-82	9/2 9/2 9/2 9/2 2 2 2 2 2 9/2	1/2 1/2 1/2 1/2 5 5 5 5 1/2	$\begin{array}{c} 0.30(0)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\\ 0.08(4)\\ 0.270(30)\\ 0.11(7) \end{array}$	M/T M/T M/T M/T M/T M/T M/T M/G M/T	$\begin{array}{c} 0.30(6)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\\ 0.08(4)\\ 0.213(19)\\ 0.11(7)\end{array}$	22101 22334 O2429 O2395 22798 22161 22334 E1855 22161	[31] [32] [27] [27] [28] [34] [31] [30] [31]	D D D
$ \begin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ \end{array} $	U-238 Th-232 U-238 U-238 U-233 U-235 U-238 U-238 U-235 U-238	n p p n n n p n p	$\begin{array}{c} 1 \\ 25 \\ 25 \\ 25 \\ 2.5 \times 10^{-8} \\ 2.5 \times 10^{-8} \\ 1 \\ 24 \\ 2.5 \times 10^{-8} \\ 24 \end{array}$	32-Ge-81 32-Ge-81 32-Ge-81 32-Ge-81 33-As-82 33-As-82 33-As-82 33-As-82 33-As-82 33-As-82 34-Se-83 34-Se-83	9/2 9/2 9/2 9/2 2 2 2 2 2 2 9/2 9/2 9/2	1/2 1/2 1/2 1/2 5 5 5 1/2 1/2 1/2	$\begin{array}{c} 0.30(0)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\\ 0.08(4)\\ 0.270(30)\\ 0.11(7)\\ 8(4) \end{array}$	M/T M/T M/T M/T M/T M/T M/T M/G M/T G/M	$\begin{array}{c} 0.30(6)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\\ 0.08(4)\\ 0.213(19)\\ 0.11(7)\\ 0.11(6) \end{array}$	22101 22334 O2429 O2429 O2395 22798 22161 22334 E1855 22161 E1855	[31] [32] [27] [27] [28] [34] [31] [32] [30] [31] [30]	D D D
$ \begin{array}{c} 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ \end{array} $	U-238 Th-232 U-238 U-238 U-233 U-235 U-238 U-238 U-238 U-235 U-238 Th-232	n p p n n p n p γ	$\begin{array}{c} 1\\ 1\\ 25\\ 25\\ 25\\ 2.5\times 10^{-8}\\ 1\\ 2.5\times 10^{-8}\\ 1\\ 24\\ 2.5\times 10^{-8}\\ 24\\ 8.5\end{array}$	32-Ge-81 32-Ge-81 32-Ge-81 32-Ge-81 33-As-82 33-As-82 33-As-82 33-As-82 33-As-82 34-Se-83 34-Se-83 35-Br-84	9/2 9/2 9/2 2 2 2 2 2 2 9/2 9/2 9/2 2	1/2 1/2 1/2 1/2 5 5 5 1/2 1/2 1/2 6	$\begin{array}{c} 0.30(0)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\\ 0.08(4)\\ 0.270(30)\\ 0.11(7)\\ 8(4)\\ 0.28(4) \end{array}$	M/T M/T M/T M/T M/T M/T M/T M/G M/T G/M M/G	$\begin{array}{c} 0.30(6)\\ 0.46(8)\\ 0.920(20)\\ 0.970(10)\\ 0.975(7)\\ 0.13(8)\\ 0.17(7)\\ 0.08(4)\\ 0.213(19)\\ 0.11(7)\\ 0.11(6)\\ 0.219(24) \end{array}$	22101 22334 O2429 O2429 O2395 22798 22161 22334 E1855 22161 E1855 G4028	[31] [32] [27] [27] [28] [34] [31] [30] [31] [30] [41]	D D D

TABLE II: Recommended IYR values for all low-energy thermal to 2 MeV) n-induced fission reactions on any issionable target. The recommended yield ratios are expressed in the M/T form. The number of data points in orackets represents the number of values excluded from he average because considered statistical outliers.

Fission Product	$egin{array}{c} { m Recomm.} \\ { m IYR} \\ { m (M/T)} \end{array}$	Nr. of data points
32-Ge-81	0.32(4)	3
34-Se-83	0.11(7)	1
37-Rb-90	0.526(30)	3(1)
41-Nb-95	0.248(29)	1
39-Y-97	$0.695(14)^{\dagger}$	1
39-Y-98	0.139(6)	2
41-Nb-99	0.83(17)	1(1)
45-Rh-102	0.44(14)	1
47-Ag-120	0.86(4)	2(1)
49-In-120	0.21(20)	1
19-In-120 M2	0.27(25)	1
48-Cd-121	0.89(11)	1
49-In-122	0.24(10)	1
9-In-122 M2	0.48(20)	1
48-Cd-123	0.65(6)	2
49-In-123	0.07(7)	1
48-Cd-125	0.85(5)	2
49-In-126	0.30(5)	3
49-In-127	0.185(31)	3
49-In-128	0.30(7)	1
51-Sb-128	$0.463(16)^{\dagger}$	14
49-In-129	0.42(6)	2
50-Sn-129	0.47(4)	3
49-In-130	0.25(5)	1
9-In-130 M2	0.41(7)	1
50-Sn-130	0.089(7)	4
51-Sb-130	$0.499(17)^{\dagger}$	18

(see text for details).

J_{rms} is not constant - M&E model is too simplistic



Evaluated IYRs

- of the ~150 isomeric yields that are included in the ND libraries, 42 have exp. data at low energy.
- In about half the cases where data is available, the libraries contain a value that doesn't agree with the measurements



Sears, C.J., et al. "Compilation and Evaluation of Isomeric Fission Yield Ratios." Nuclear Data Sheets 173 (2021): 118-143.



Impact of experimental values on anti-v spectra

- Spectrum shown as a ratio of the benchmark (JEFF-3.3 yields and IYRs)
- Virtually no difference below 5 MeV
- Overall increase elsewhere:

up to + 5% at 6 MeV up to +60% at 8 MeV





Some isomers are more equal than others...



$$IYR_{th} = 65\% \rightarrow IYR_{exp} = 50\%$$

$$CFY \approx 5\%$$
B
National Laboratory

В

$$\begin{array}{c} \text{IYR}_{\text{th}} = 81\% \rightarrow \text{IYR}_{\text{exp}} = 14 \ \% \\ \text{CFY} \approx 3 \ \% \end{array}$$

A broader sensitivity study

- Analysis of all fission products with a known isomer included in ENDF (many without published IYR data)
- Varied the value within physical boundaries
- Identified a fission products whose IYR affects the antineutrino spectra (e.g., Sb-134, Nb-100, La-146, Rb-90)





Summary and Outlook

- New evaluated isomeric ratios result in an increased antineutrino flux compared to the current FY libraries up to 60% for specific energies and fissile targets.
- Experimental data on IYRs exist only for a fraction of the fission products
- A sensitivity study shows that a number of other isomers could considerably affect the antineutrino spectrum, especially at high energies



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Evaluation of Isomeric Yield Ratios

There are ~200 fission products with a known long-lived isomer

 $IYR = \frac{Y_{isom}}{(Y_{isom} + Y_{gs})}$

The Madland & England model, loosely based on data from 40 yrs ago, is **used in all evaluated data libraries** as the basis to split Independent FYs between the GS and the IS based on the levels J_{rms}





Outline

- The "bump" in antineutrino spectra
- Fission yields and isomers in antineutrino summation calculations
- Impact of newly evaluated recommended isomeric yields
- A broader sensitivity study
- Outlook



Reactor antineutrino spectra and "the bump"

- km-baseline experiments measured the antineutrinos from β⁻-decay of fission products
- 5% deficit of the total number of antineutrinos (RAA)
- Excess of antineutrinos between
 5-6 MeV → "The Bump"





