

Technical meeting on emerging applications of plasma science and technology

# ML-aided plasma source and process simulation for semiconductor fabrication processes

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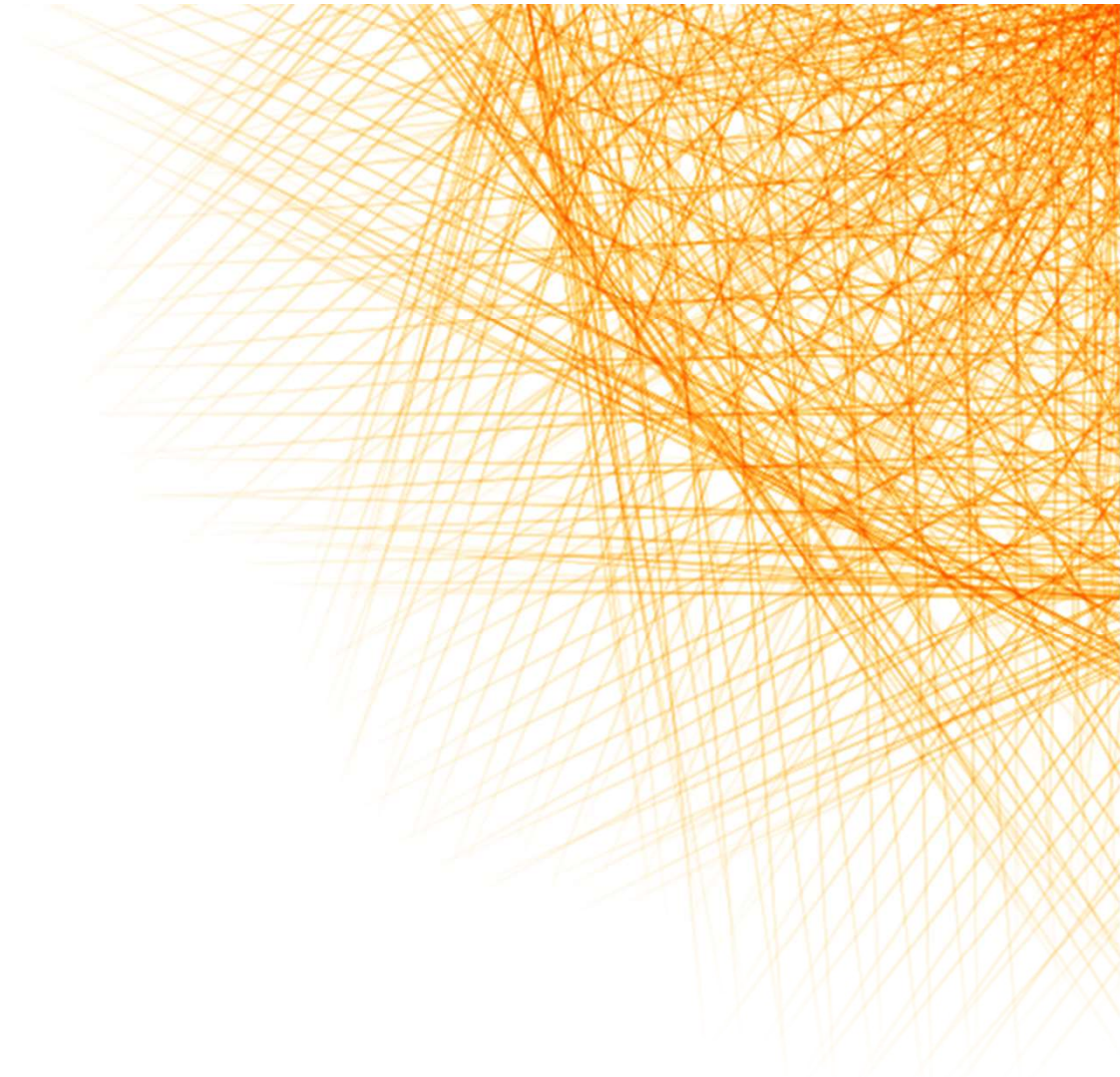
Summary



# 1

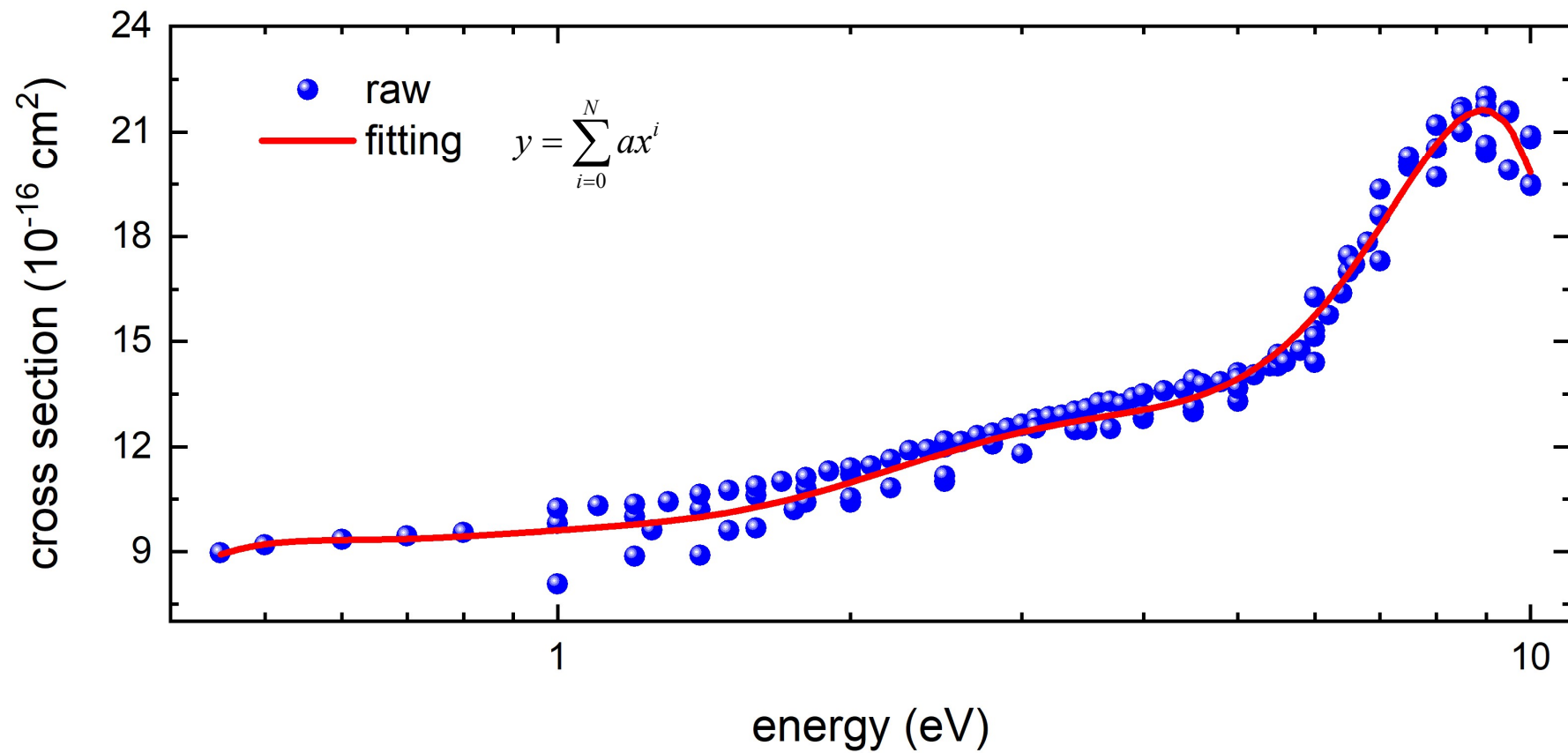
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# Introduction



# 1. Introduction

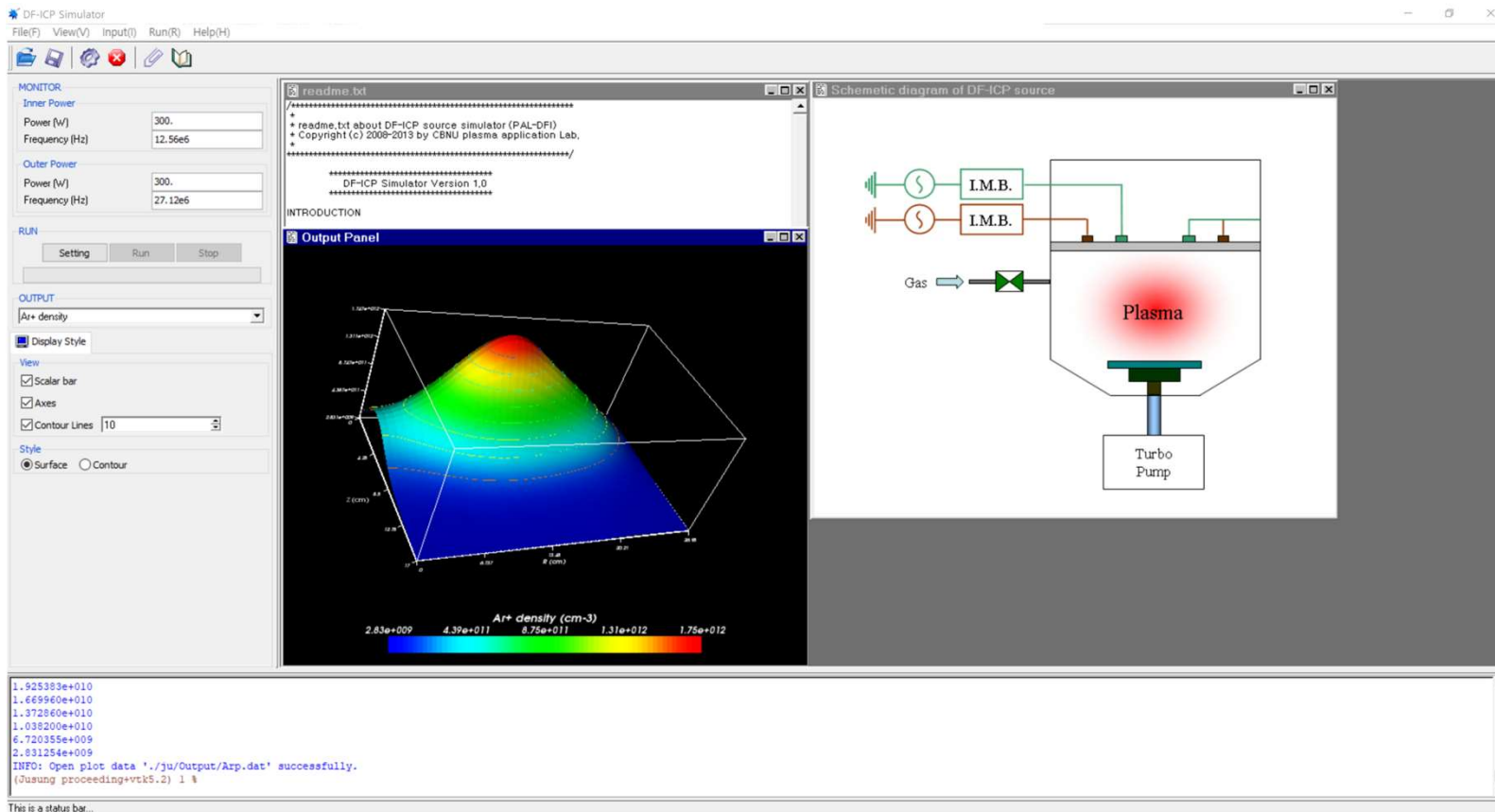
## Motivation & Need for development





# 1. Introduction

## Motivation & Need for development

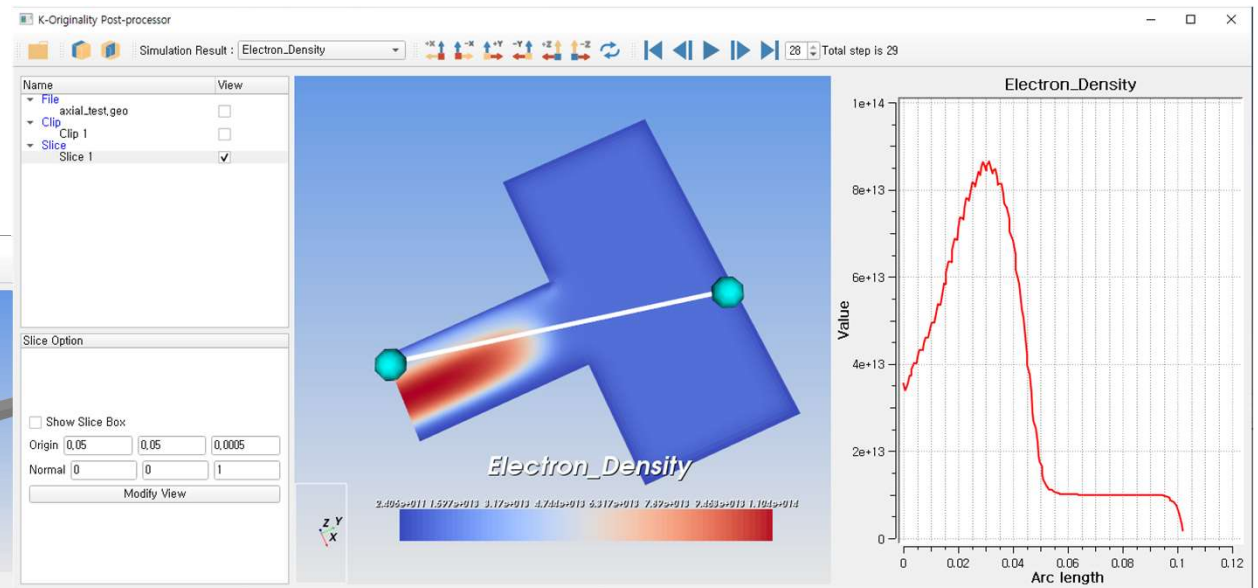
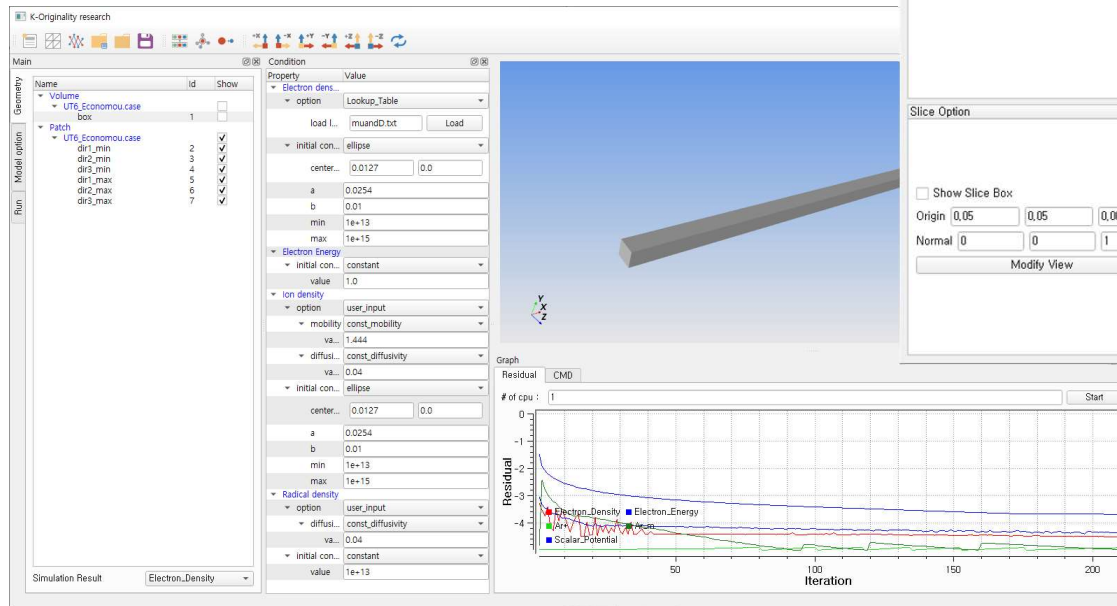


- Language : C, Tcl/Tk, VTK
- Source : TCP/ICP
- Model :
  - Fluid model
  - Non-local heating model
  - Cylindrical 2D geometry
  - Ar plasma

# 1. Introduction

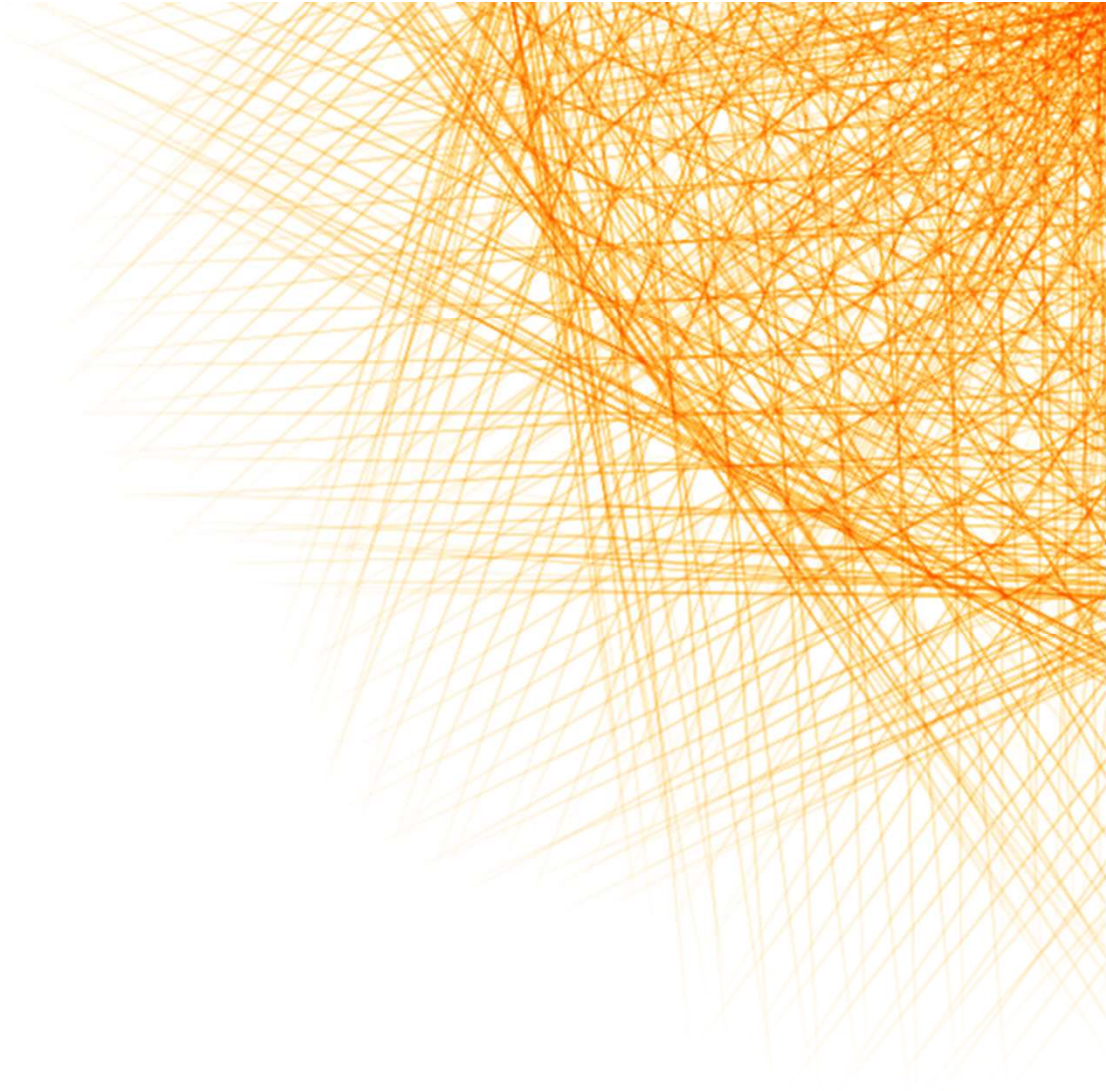
## Developed 3D simulator

- Fluid equation + Boltzmann equation
- 3D Polyhedral mesh
- Finite volume method
- C++, VTK
- Bulk and surface DB



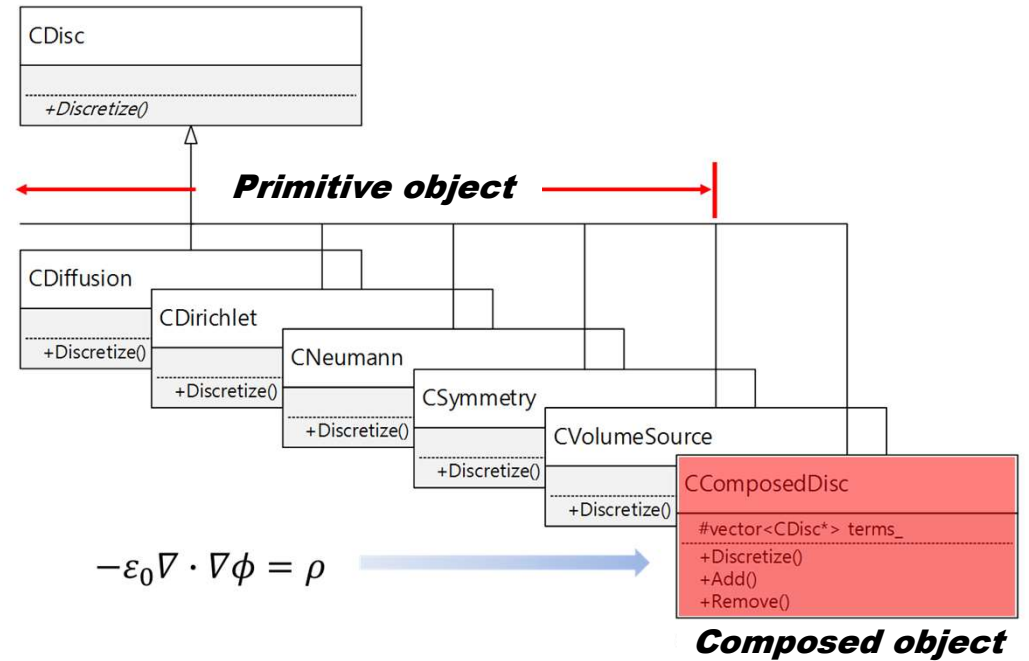
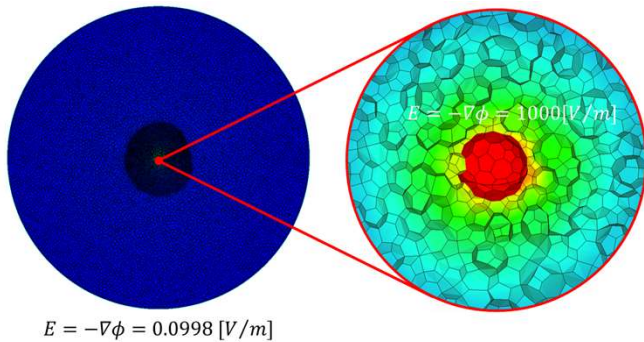
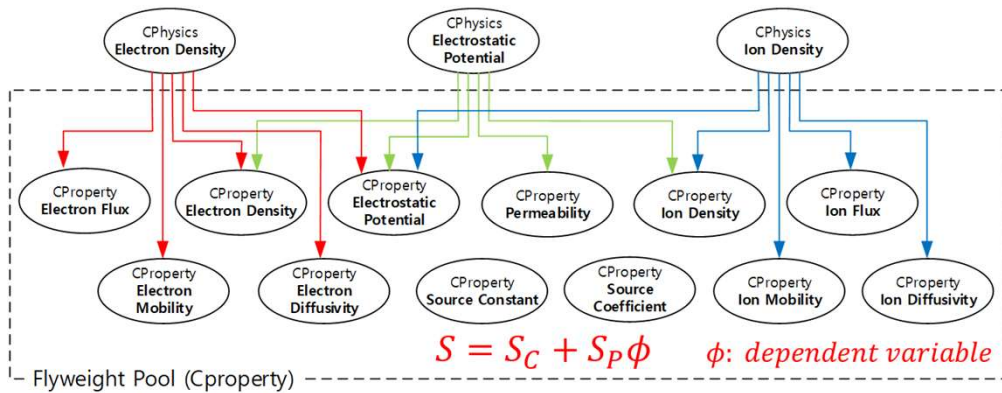
# 2

## Plasma Modeling



## 2. Plasma Modeling

### Flyweight pool and composite pattern



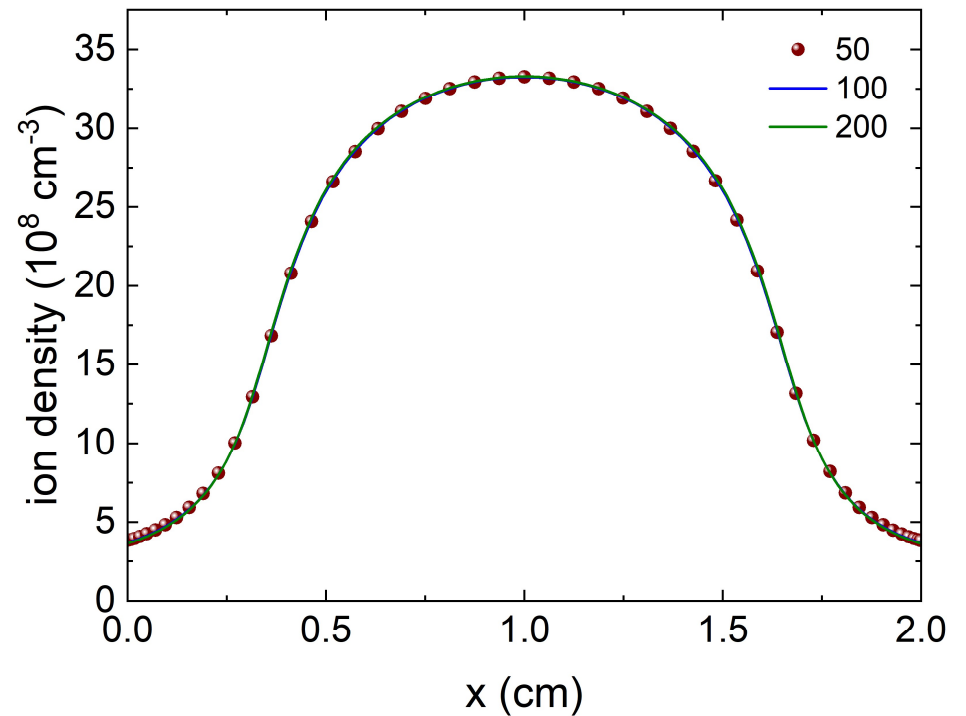
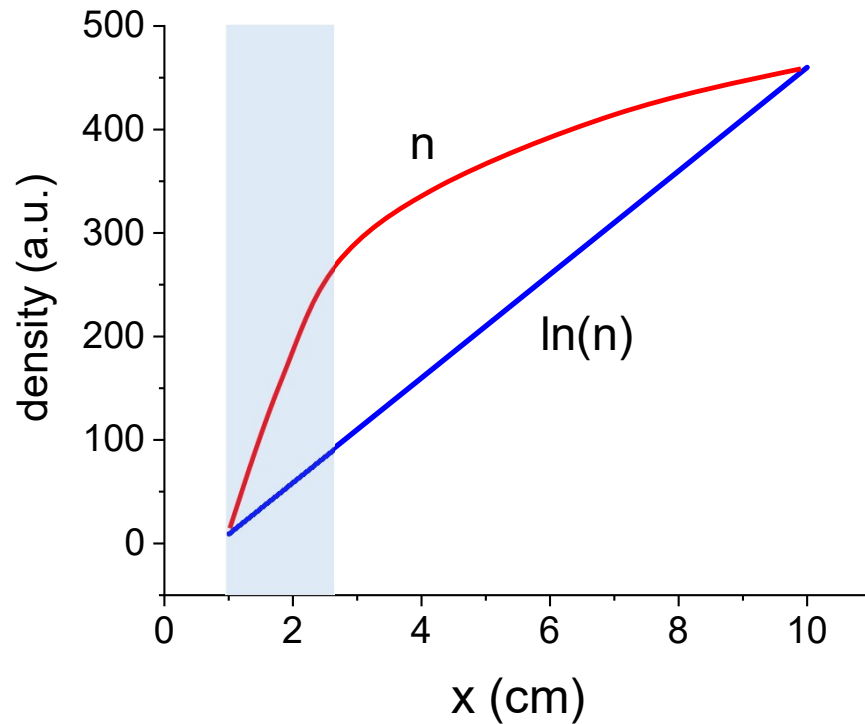


## 2. Plasma Modeling

### Log transformation

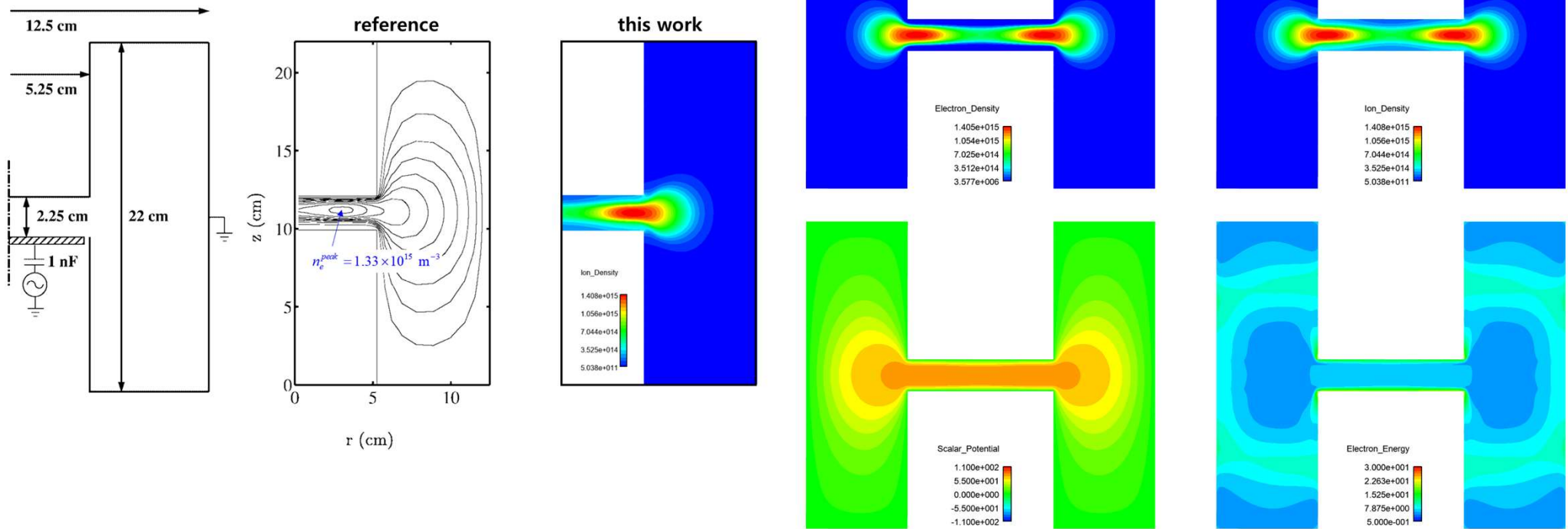
- Improves linearity between independent and dependent variables
- CCP 1D discharge → reduce grid dependence of results

$$\frac{\partial n_e}{\partial t} = \frac{n_e}{n_e} \frac{\partial n_e}{\partial t} = n_e \frac{\partial(\ln n_e)}{\partial t} = n_e \frac{\partial N_e}{\partial t}$$



## 2. Plasma Modeling

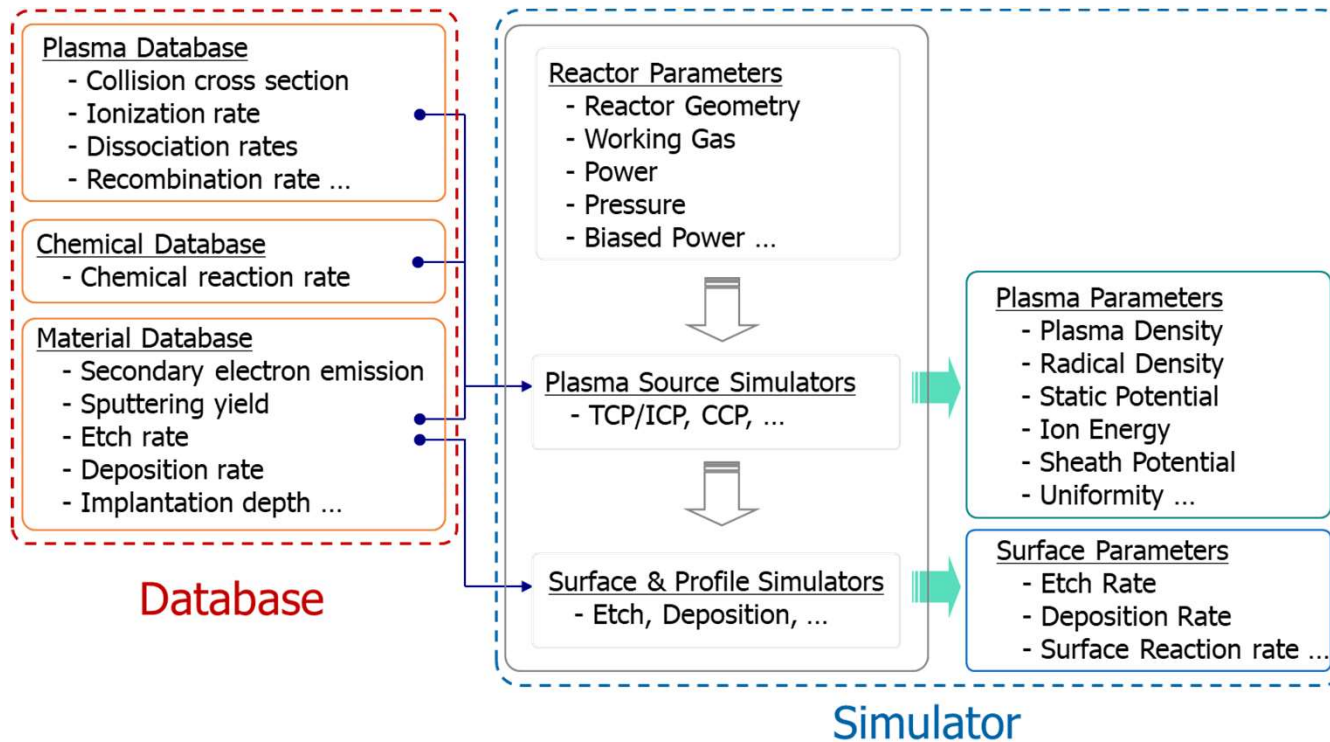
### K-PLASMA unit test



## 2. Plasma Modeling

### Database development

- Bulk and surface chemistry data base (DB) **are necessarily required** to compute the plasma parameters.
- **High reliable DB is closely related with accuracy enhancement of simulations.**



## 2. Plasma Modeling

### Database development

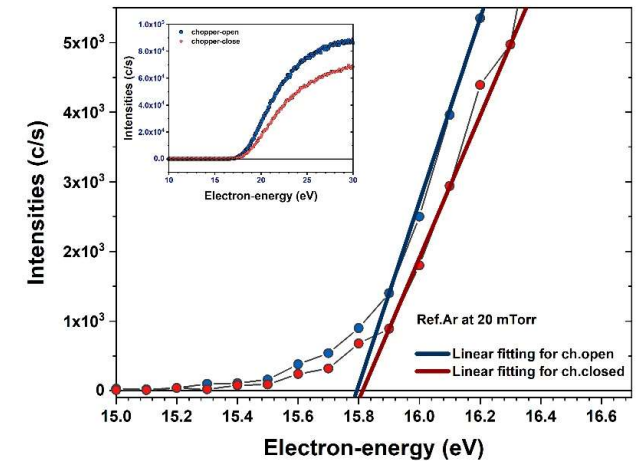
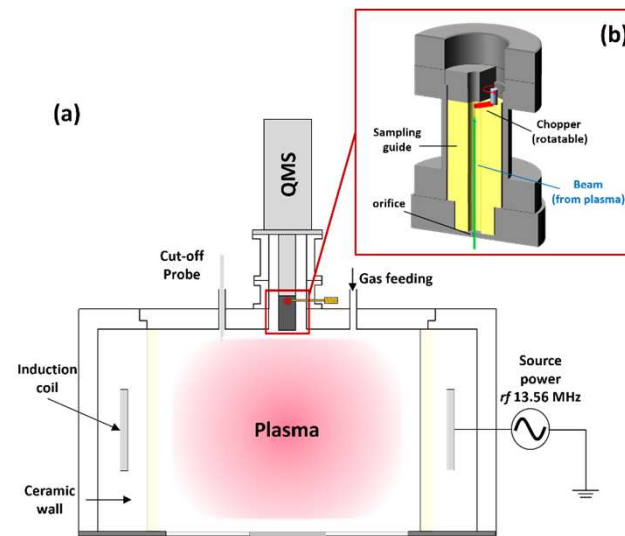
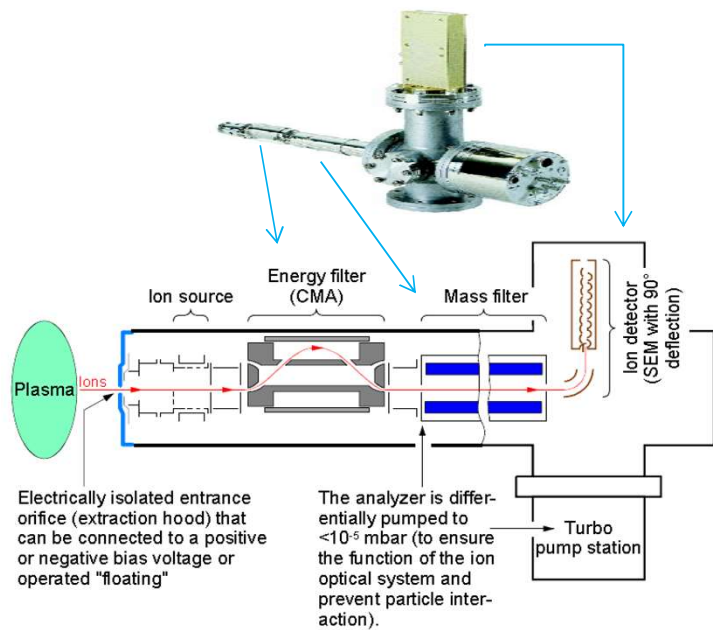
Software	Key DB
<b>CFD-ACE+</b>	Ar, SiH <sub>4</sub> /O <sub>2</sub> /Ar, NF <sub>3</sub> /Ar, C <sub>2</sub> F <sub>6</sub> /O <sub>2</sub> , CF <sub>4</sub> , Cl <sub>2</sub> , He, Ne, N <sub>2</sub> , O <sub>2</sub> , Xe, SF <sub>6</sub> /O <sub>2</sub>
<b>COMSOL</b>	Ar, He, Hg, O <sub>2</sub>
<b>VizGlow</b>	Ar, He, Xe, H <sub>2</sub> , N <sub>2</sub> , O <sub>2</sub> , Ar/O <sub>2</sub> , Ar/O <sub>2</sub> /H <sub>2</sub> , CF <sub>4</sub> , C <sub>2</sub> F <sub>6</sub> , C <sub>4</sub> F <sub>8</sub> , CHF <sub>3</sub> , CF <sub>4</sub> /O <sub>2</sub> /He, C <sub>2</sub> H <sub>2</sub> /Ar, HBr, SiH <sub>4</sub> /N <sub>2</sub> , NF <sub>3</sub> , NH <sub>3</sub> /N <sub>2</sub> /H <sub>2</sub> /Ar, NF <sub>3</sub> , NF <sub>3</sub> /O <sub>2</sub> , SF <sub>6</sub> /O <sub>2</sub> , BF <sub>3</sub> /Ar
<b>QuantemolDB</b>	N <sub>2</sub> /H <sub>2</sub> , Ar/H <sub>2</sub> , O <sub>2</sub> /H <sub>2</sub> , SF <sub>6</sub> /O <sub>2</sub> , CF <sub>4</sub> /O <sub>2</sub> , CF <sub>4</sub> , CF <sub>4</sub> /O <sub>2</sub> /H <sub>2</sub> /N <sub>2</sub> , C <sub>4</sub> F <sub>8</sub> , SiH <sub>4</sub> , SiH <sub>4</sub> /NF <sub>3</sub> , Ar/O <sub>2</sub> , Ar/O <sub>2</sub> /C <sub>4</sub> F <sub>8</sub> , SiH <sub>4</sub> /Ar/O <sub>2</sub> , Ar/Cu, Cl <sub>2</sub> /O <sub>2</sub> /Ar, Ar/BCl <sub>3</sub> /Cl <sub>2</sub> , Ar/NF <sub>3</sub> , CH <sub>4</sub> /H <sub>2</sub> , C <sub>2</sub> H <sub>2</sub> /H <sub>2</sub> , CH <sub>4</sub> /NF <sub>3</sub> , H <sub>2</sub> /O <sub>2</sub> , CF <sub>4</sub> /CHF <sub>3</sub> /H <sub>2</sub> /Cl <sub>2</sub> /O <sub>2</sub> /HBr, SF <sub>6</sub> /CF <sub>4</sub> /O <sub>2</sub> , Ar/Cu/He, Ar/NF <sub>3</sub> , SF <sub>6</sub> /CF <sub>4</sub> /N <sub>2</sub> /H <sub>2</sub>
<b>K-SPEED</b>	C <sub>x1</sub> F <sub>y1</sub> /C <sub>x2</sub> F <sub>y2</sub> /CH <sub>x</sub> F <sub>y</sub> /O <sub>2</sub> /Ar, NF <sub>3</sub> /Ar, SiH <sub>4</sub> /O <sub>2</sub> /Ar



## 2. Plasma Modeling

### Database development

- APMS (appearance potential mass spectrometry) method and the microwave cut-off probe
- Reducing the back-ground noise inside the QMS by using a chopper (W. S. Chang et al, **to be published**)



## 2. Plasma Modeling

### Global model

$$\frac{\partial n_i}{\partial t} = \sum_j R_{g,j} + \frac{Q_i}{\Omega} - \sum_j R_{l,j} - n_i \left( \frac{V_{pump}}{\Omega} + \nu_l^i \right)$$

$$\frac{\partial}{\partial t} (N c_p T_g) = \sum_i 3n_e \nu_m \left( \frac{m_e}{m_i} \right) k_B (T_e - T_g) + \sum_j n_e k_j n_j \Delta E_j - \sum_j \Delta H_j - \frac{h_{tc} A}{\Omega} (T_g - T_w)$$

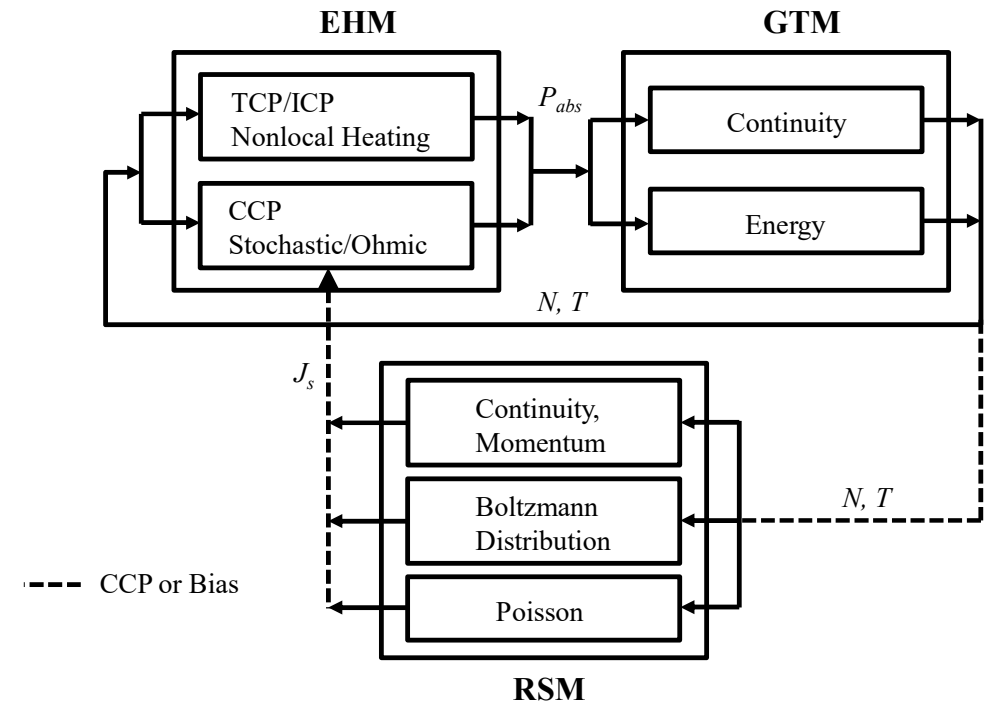
When the EEDF is given,

$$\frac{\partial}{\partial t} \left( \frac{3}{2} n_e T_e \right) = \frac{P_{abs}}{\Omega} - E_e - n_e \varepsilon_l^e \nu_l^e$$

When the EEDF is solved in a self-consistent manner,

$$T_e = \frac{2}{3} \langle \varepsilon \rangle = \frac{2}{3n_e} \int_0^\infty \varepsilon^{3/2} f_0(\varepsilon) d\varepsilon$$

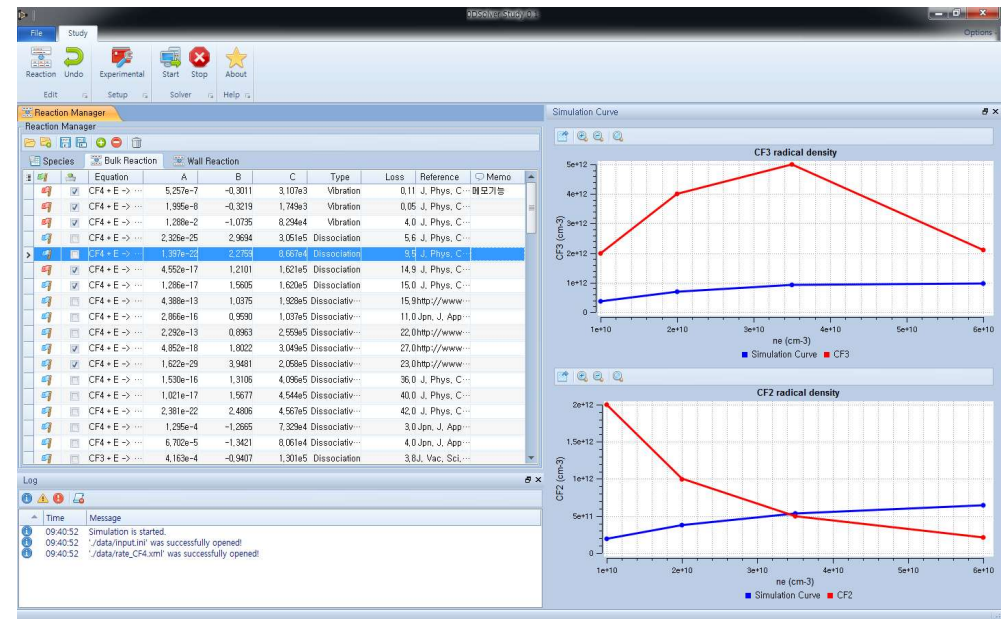
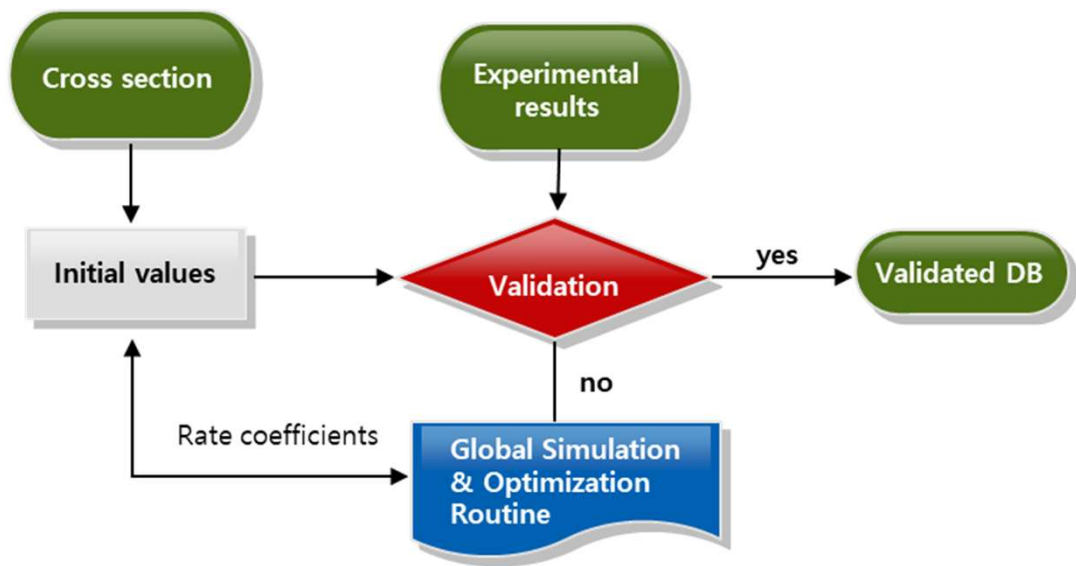
$$k = \int_0^\infty f_0(\varepsilon) \sigma(\varepsilon) \nu d\varepsilon, \quad R = k \times \prod_j n_{r,j}, \quad \nu_l^i = \frac{A_{eff}}{\Omega} \sqrt{\frac{k_B T_e (1 + \alpha_s)}{m_i (1 + \alpha_s \gamma_-)}}, \quad A_{eff} = 2\pi (R_p^2 h_L + R_p L_p h_R)$$



## 2. Plasma Modeling

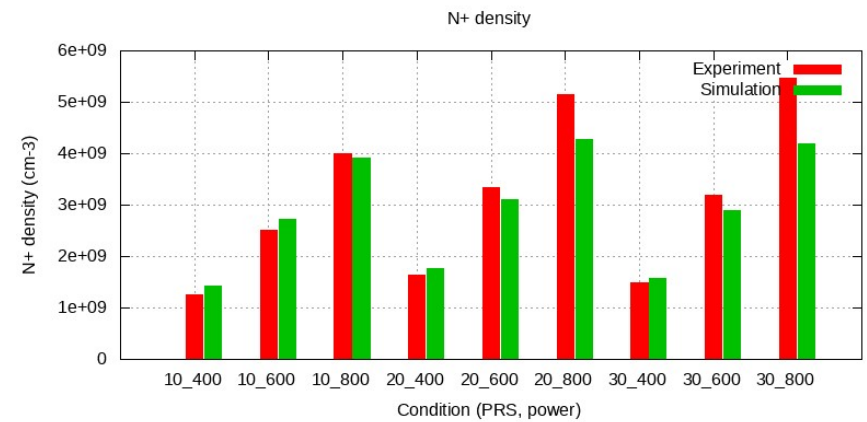
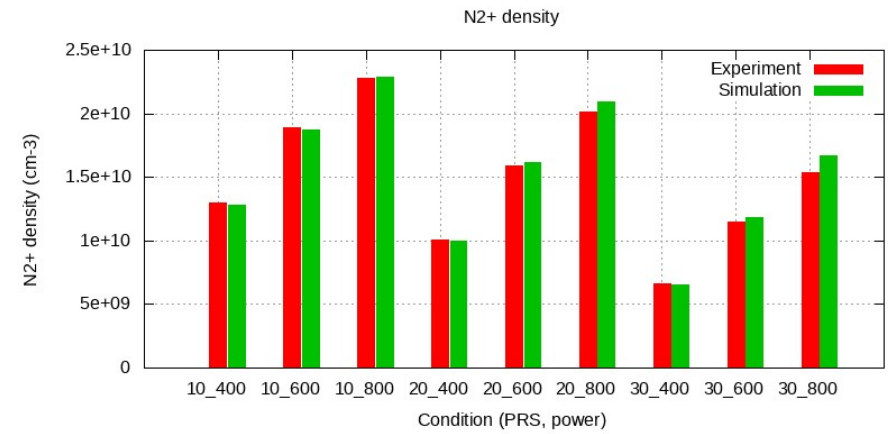
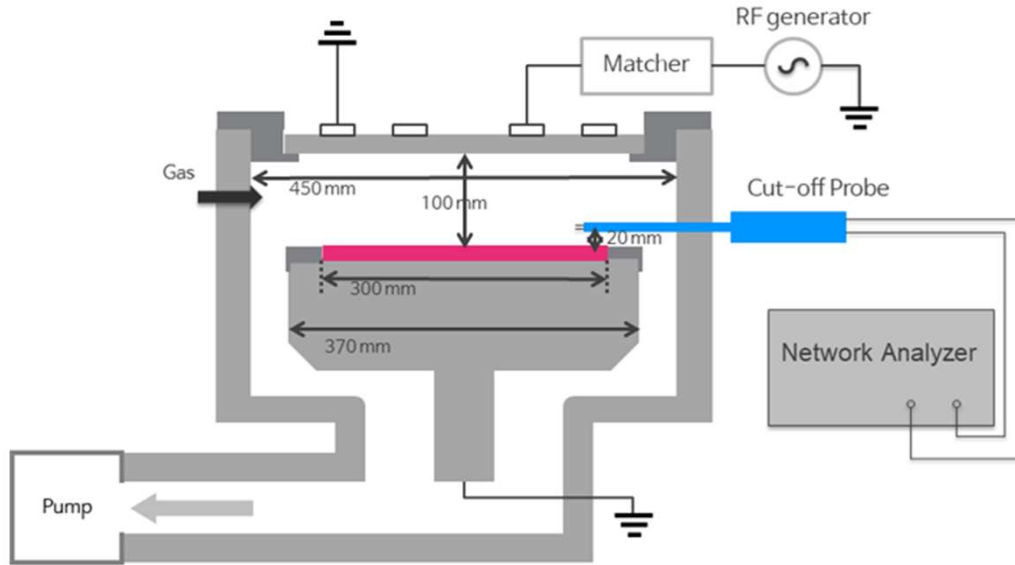
### Global model

- Optimized the rate coefficients for heavy particle reactions excluding electron collisions.
- Numerical optimization (Random sampling, Newton, Secan, Broyden-Fletcher-Goldfarb-Shanno, etc.)



## 2. Plasma Modeling

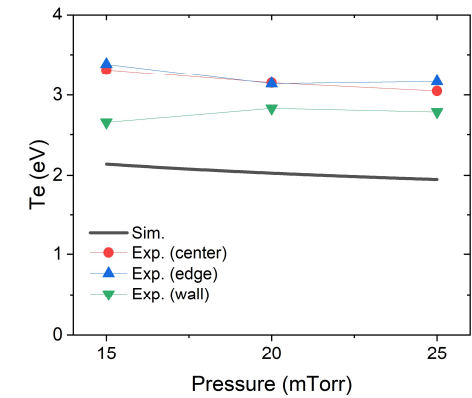
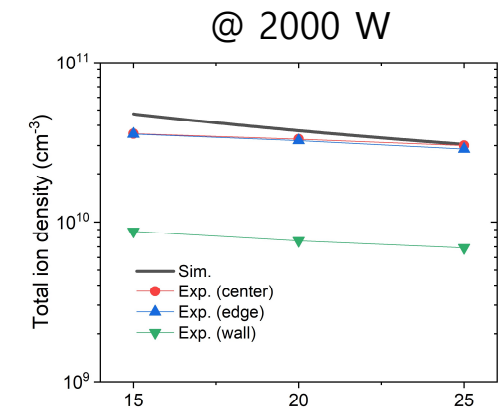
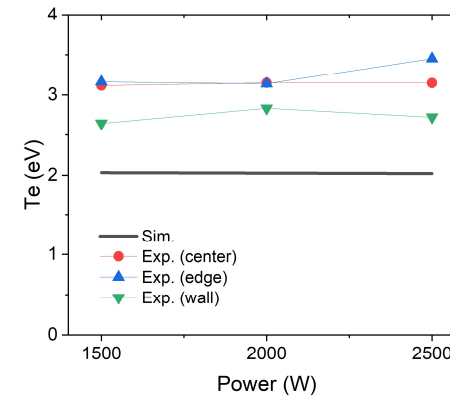
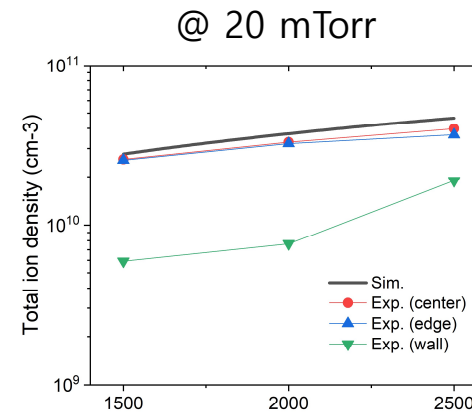
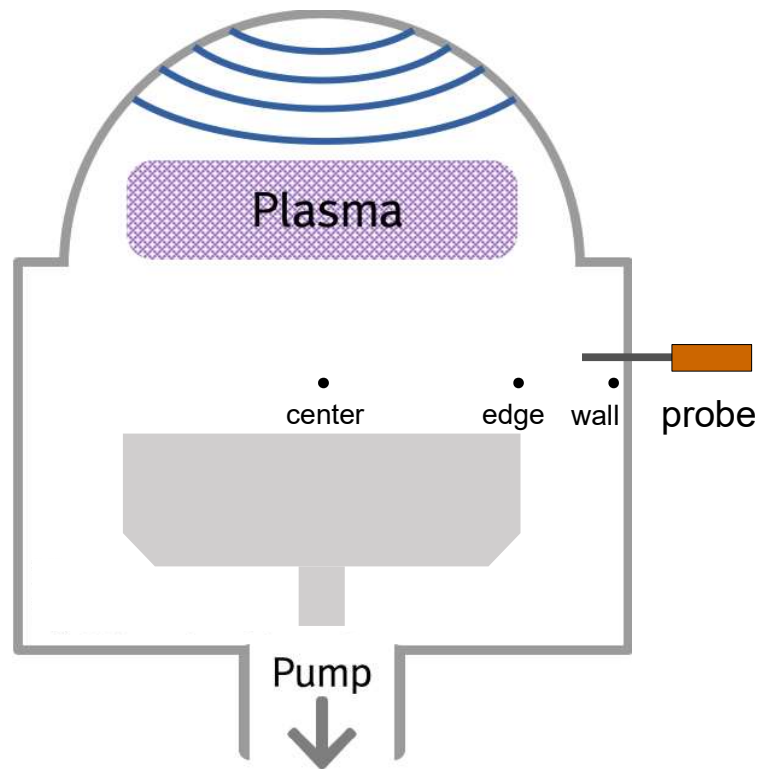
### Global model @ N<sub>2</sub> discharges





## 2. Plasma Modeling

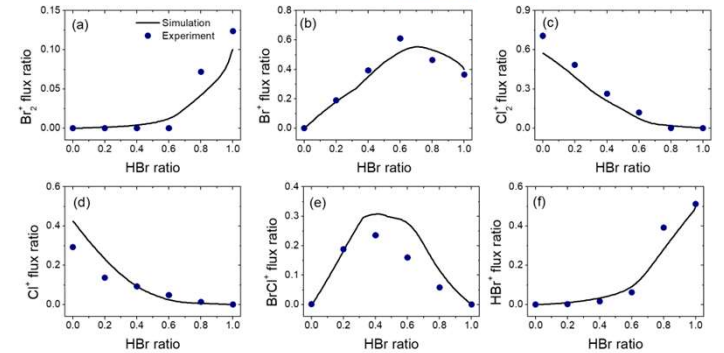
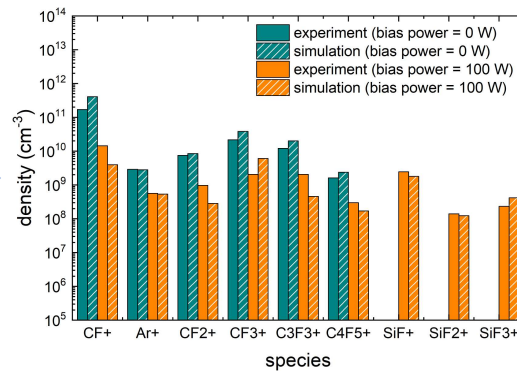
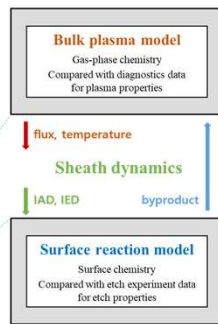
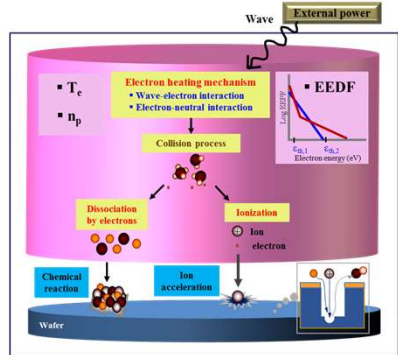
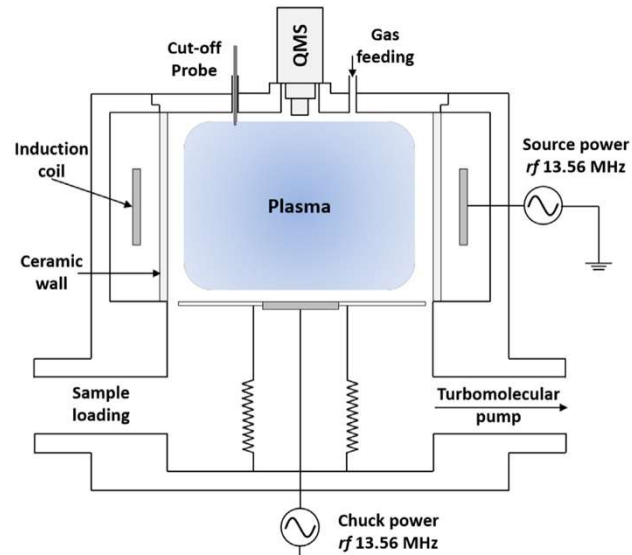
### Global model @ commercial source



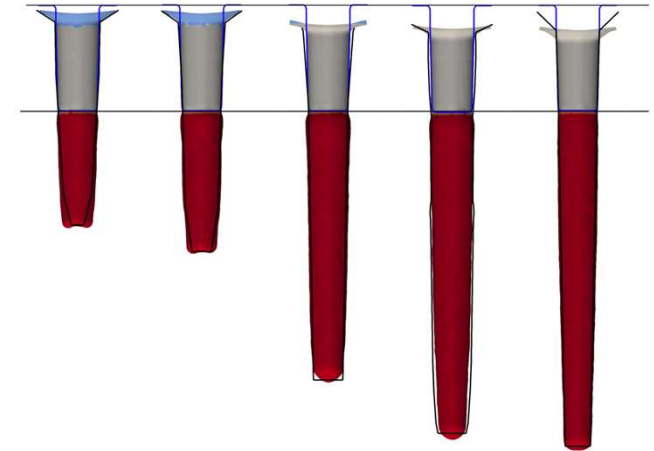
# 2. Plasma Modeling

## Global model

6 inch oxide wafer



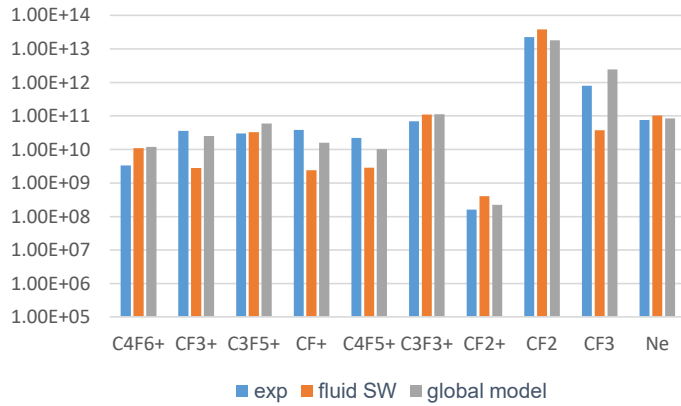
Cl2	0	10	20	30	40
HBr	40	30	20	10	0



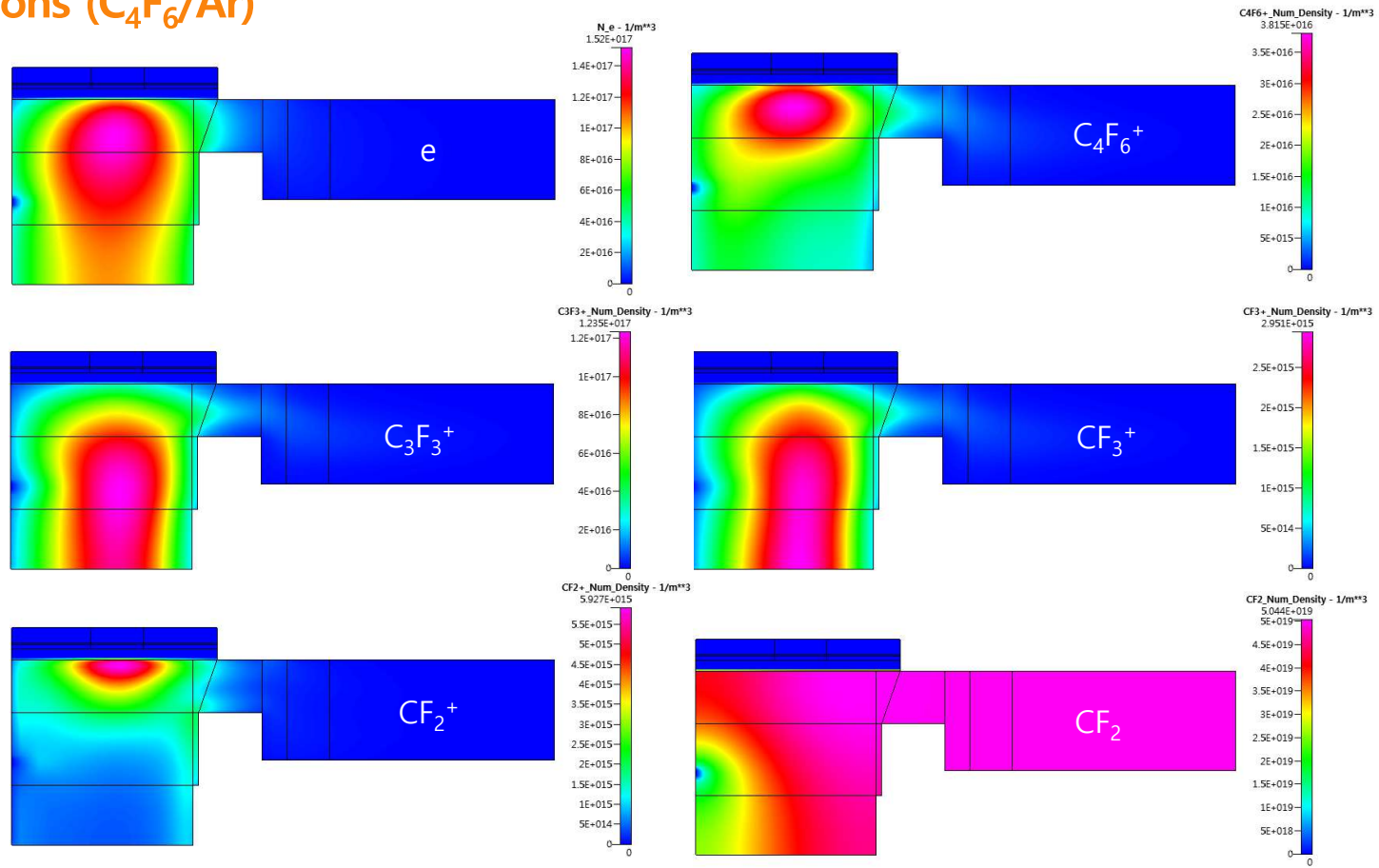
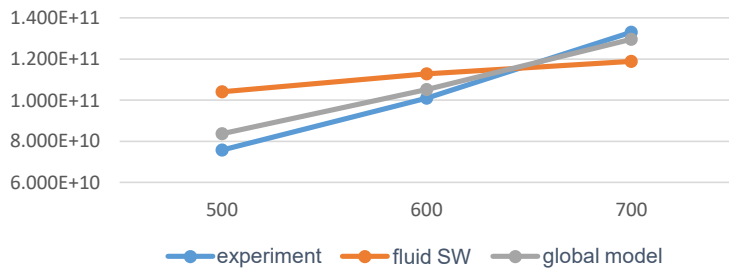
# 2. Plasma Modeling

## Comparison with 2D simulations ( $C_4F_6/Ar$ )

20 mTorr, 500 W



Plasma Density



## 2. Plasma Modeling

### Developed bulk databae

Gas	DB	experiment	validated
C <sub>4</sub> F <sub>6</sub> /Ar	0	0	0
C <sub>4</sub> F <sub>6</sub> /Cl <sub>2</sub> /Ar	0	0	0
C <sub>4</sub> F <sub>8</sub> /Ar	0	0	0
C <sub>4</sub> F <sub>6</sub> /C <sub>4</sub> F <sub>8</sub> /Ar	0	0	0
C <sub>4</sub> F <sub>6</sub> /O <sub>2</sub> /Ar	0	0	0
C <sub>4</sub> F <sub>6</sub> /C <sub>4</sub> F <sub>8</sub> /O <sub>2</sub>	0	0	0
C <sub>4</sub> F <sub>6</sub> /C <sub>4</sub> F <sub>8</sub> /CH <sub>2</sub> F <sub>2</sub> /O <sub>2</sub>	0	0	0
C <sub>4</sub> F <sub>6</sub> /C <sub>4</sub> F <sub>8</sub> /CH <sub>2</sub> F <sub>2</sub> /O <sub>2</sub> /Ar	0	0	0
C <sub>4</sub> F <sub>6</sub> /C <sub>4</sub> F <sub>8</sub> /CH <sub>2</sub> F <sub>2</sub> /Ar	0	0	0
C <sub>4</sub> F <sub>6</sub> /C <sub>4</sub> F <sub>8</sub> /CHF <sub>3</sub> /Ar	0	0	0
C <sub>4</sub> F <sub>6</sub> /C <sub>4</sub> F <sub>8</sub> /CH <sub>3</sub> F/Ar	0	0	0
C <sub>4</sub> F <sub>6</sub> /C <sub>4</sub> F <sub>8</sub> /C <sub>3</sub> F <sub>8</sub> /Ar	0	0	0
CHF <sub>3</sub> /Ar	△	X	△
C <sub>2</sub> HF <sub>5</sub> /Ar	0	0	0
CH <sub>2</sub> F <sub>2</sub> /Ar	0	0	0
SiH <sub>4</sub> /Ar	0	0	0
SiH <sub>4</sub> /NH <sub>3</sub> /Ar	0	0	0

Gas	DB	experiment	validated
N <sub>2</sub>	0	0	0
Ar	0	0	0
CF <sub>4</sub> /O <sub>2</sub>	0	△	0
CF <sub>4</sub> /Cl <sub>2</sub>	△	X	△
PF <sub>3</sub>	△	X	△
SF <sub>6</sub>	△	X	△
WF <sub>6</sub>	△	X	△
Kr	△	X	△
Xe	△	X	△
CBr <sub>2</sub> F <sub>2</sub>	△	X	△
NF <sub>3</sub> /O <sub>2</sub> /Ar	0	0	0
HBr/Cl <sub>2</sub>	0	△	0
C <sub>4</sub> F <sub>8</sub> /CHF <sub>3</sub> /Kr	0	0	0
C <sub>4</sub> F <sub>8</sub> /CH <sub>2</sub> F <sub>2</sub> /O <sub>2</sub> /Xe	0	0	0
C <sub>4</sub> F <sub>8</sub> /CH <sub>2</sub> F <sub>2</sub> /O <sub>2</sub> /Ar(Kr)	0	0	X
SiH <sub>4</sub> /H <sub>2</sub> /Ar	0	0	X
Etc	△	△	△





# 3

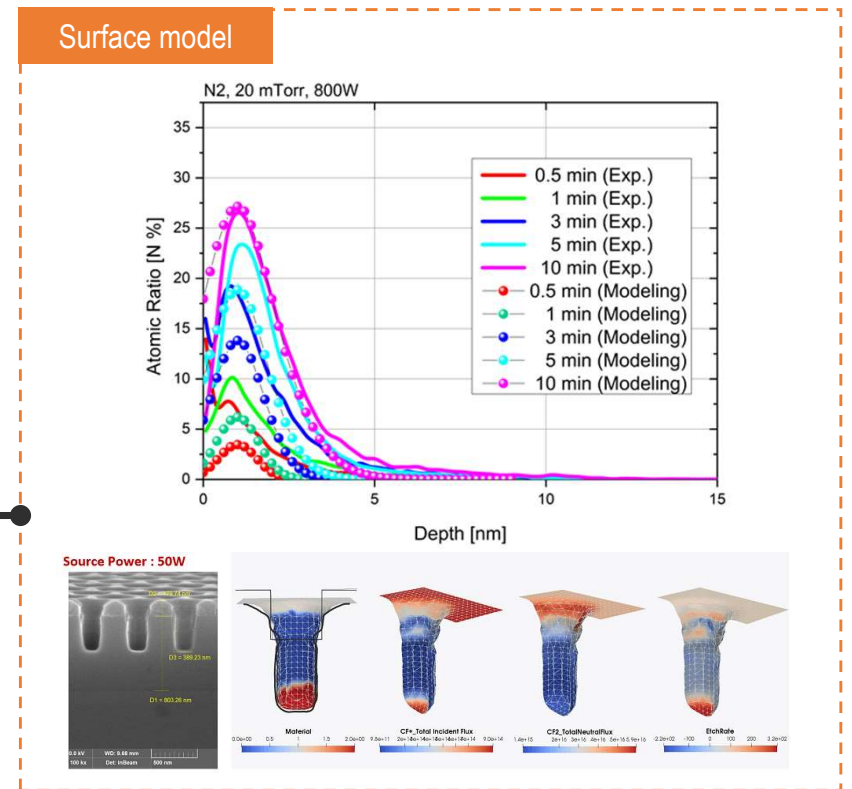
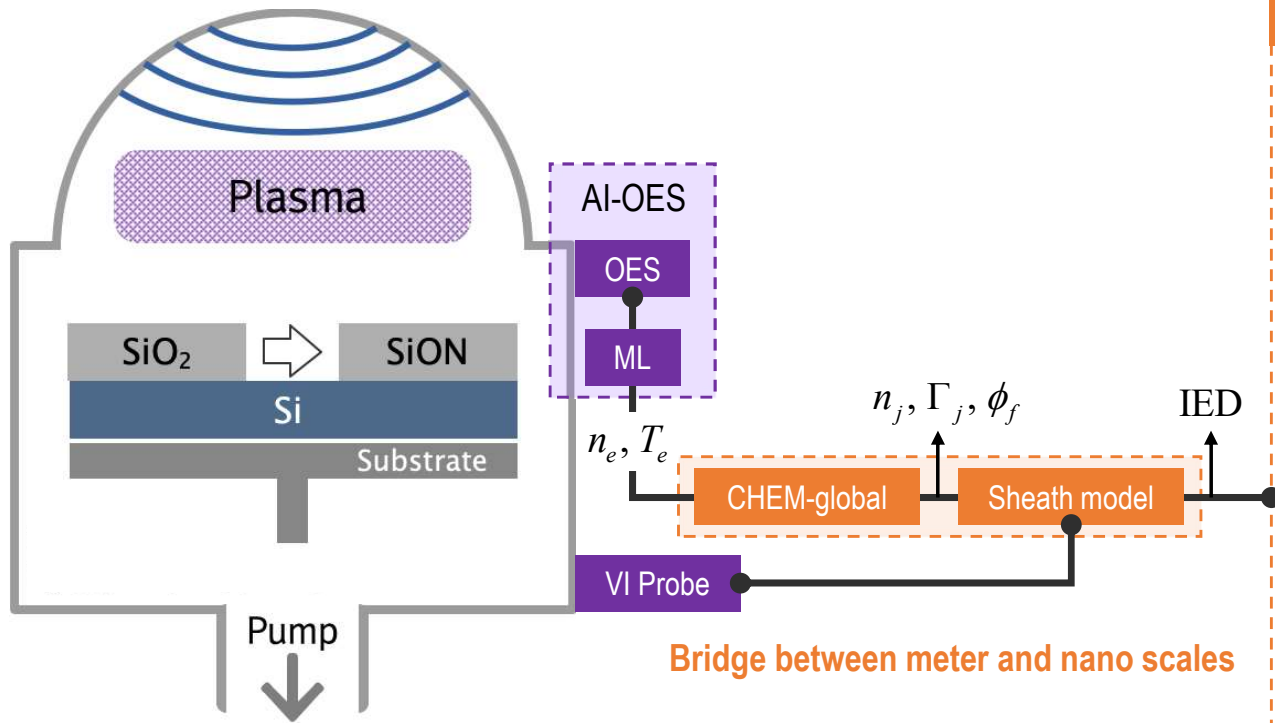
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## ML-aided Modeling



# 3. ML-aided Modeling

## Sensor-bulk-surface coupling model



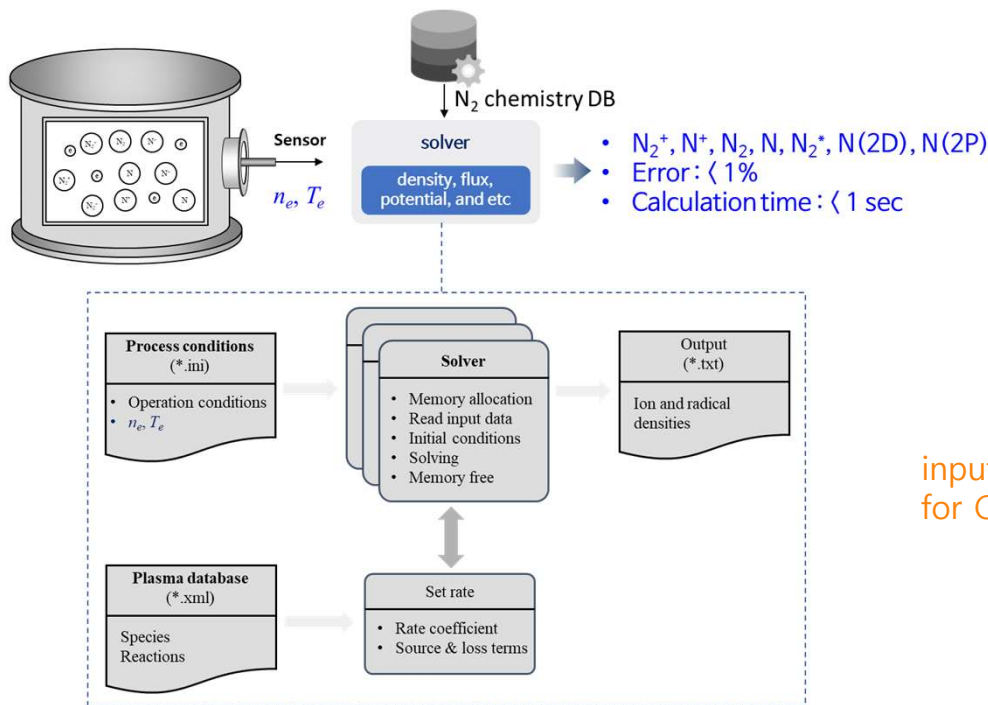
# 3. ML-aided Modeling

## CHEM-global (chemical reaction analyzer using a global model)

### Quasi-neutrality

Assuming the quasi-neutrality, the continuity equation is solved using the electron density and temperature.

@ N<sub>2</sub> 80 SCCM, 15 mTorr, 500 W



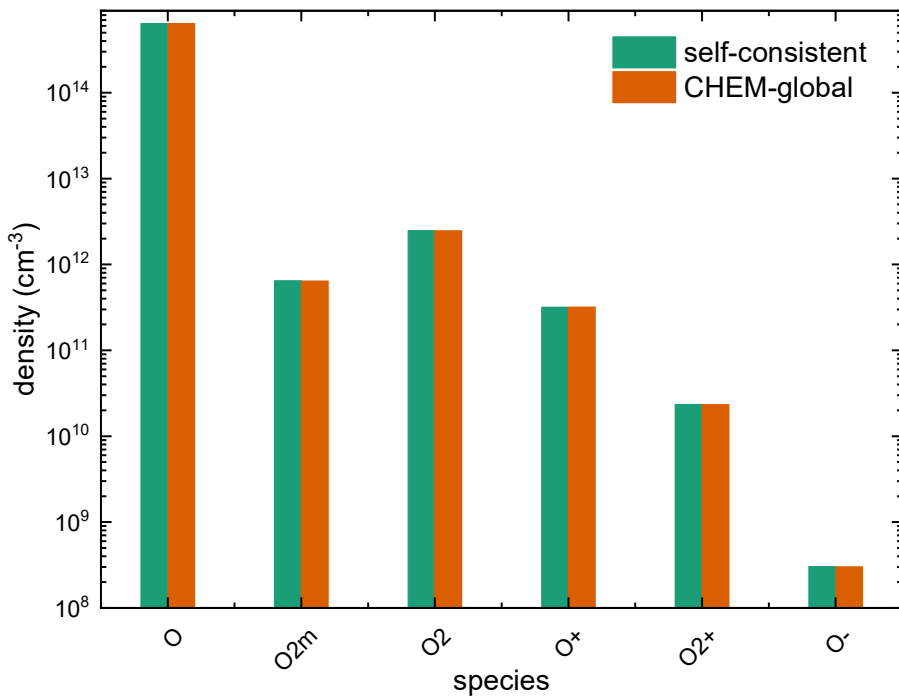
species	Self-consistent	CHEM-global
N	1.5166×10 <sup>13</sup> cm <sup>-3</sup>	1.5164×10 <sup>13</sup> cm <sup>-3</sup>
N <sub>2</sub> <sup>*</sup>	7.3827×10 <sup>12</sup> cm <sup>-3</sup>	7.3815×10 <sup>12</sup> cm <sup>-3</sup>
N <sub>2</sub>	4.6440×10 <sup>14</sup> cm <sup>-3</sup>	4.6432×10 <sup>14</sup> cm <sup>-3</sup>
N(2P)	6.9623×10 <sup>11</sup> cm <sup>-3</sup>	6.9603×10 <sup>11</sup> cm <sup>-3</sup>
N(2D)	1.3143×10 <sup>12</sup> cm <sup>-3</sup>	1.3141×10 <sup>12</sup> cm <sup>-3</sup>
N <sub>2</sub> <sup>+</sup>	6.0594×10 <sup>10</sup> cm <sup>-3</sup>	6.0595×10 <sup>10</sup> cm <sup>-3</sup>
N <sup>+</sup>	2.4852×10 <sup>9</sup> cm <sup>-3</sup>	2.4850×10 <sup>9</sup> cm <sup>-3</sup>
e	6.3080×10 <sup>10</sup> cm <sup>-3</sup>	
T <sub>e</sub>	2.9531 eV	
Calculation time	161 sec	0.001 sec

input parameters for CHEM-global

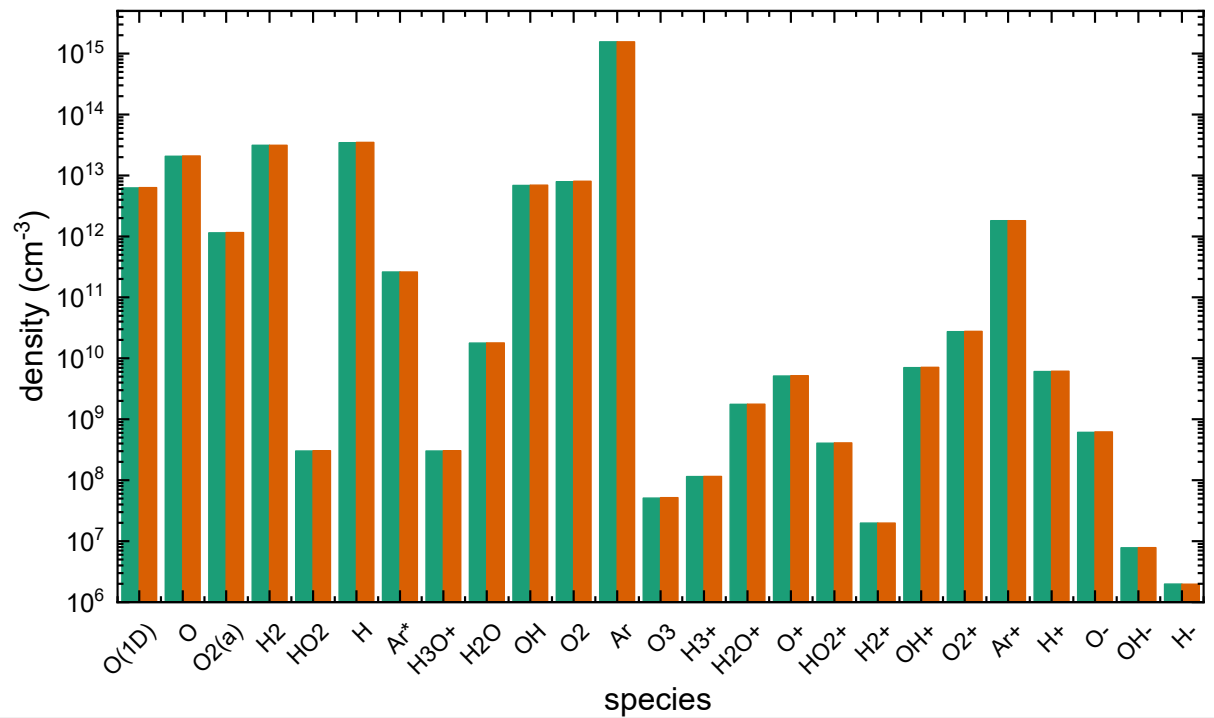
# 3. ML-aided Modeling

## CHEM-global

- ▶ O<sub>2</sub> plasma
  - > 7 species and 25 reactions
  - > O<sub>2</sub> 80 SCCM, 10 mTorr, 500 W → 0.5% mean error

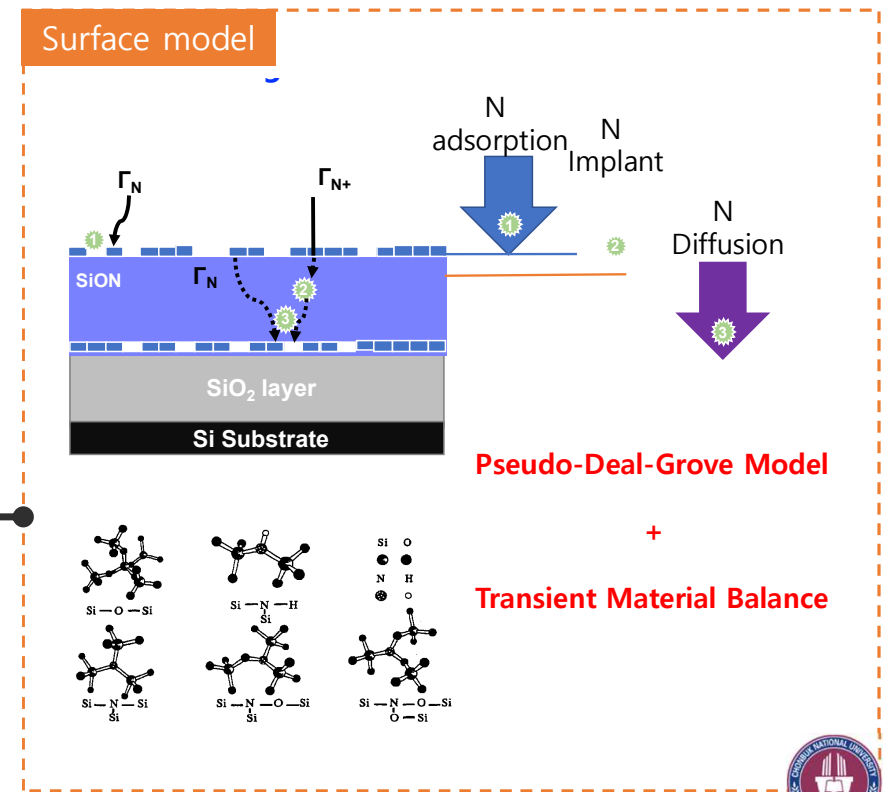
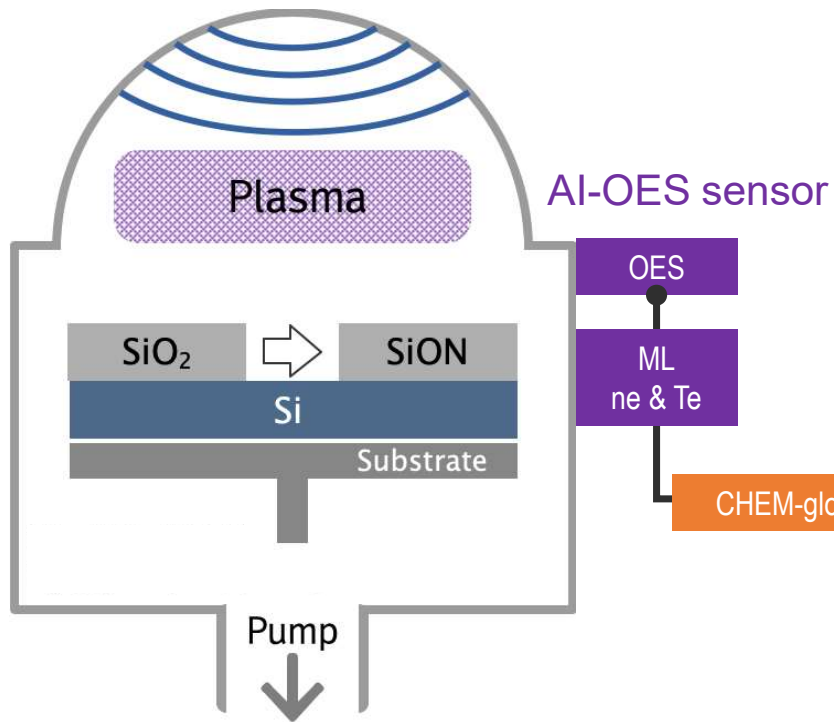


- ▶ H<sub>2</sub>O/Ar plasma
  - > 26 species and 153 reactions
  - > H<sub>2</sub>O 1 SCCM, Ar 30 SCCM, 50 mTorr, 1500 W → 0.8% mean error



# 3. ML-aided Modeling

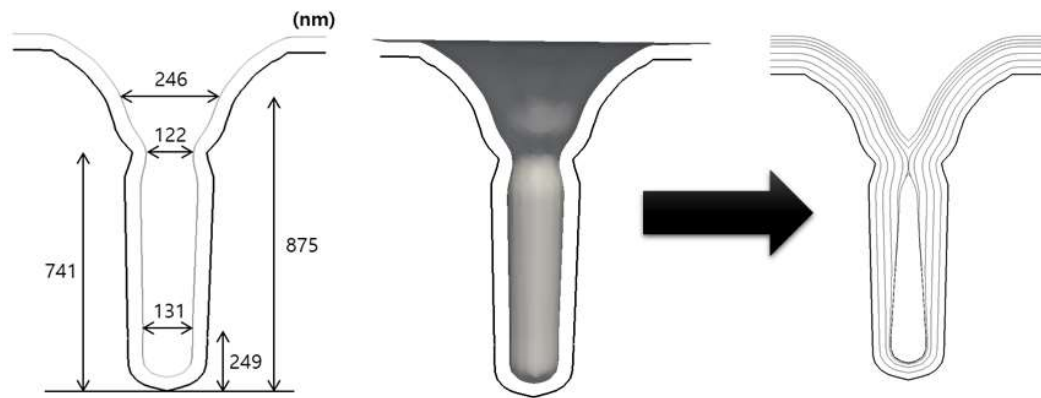
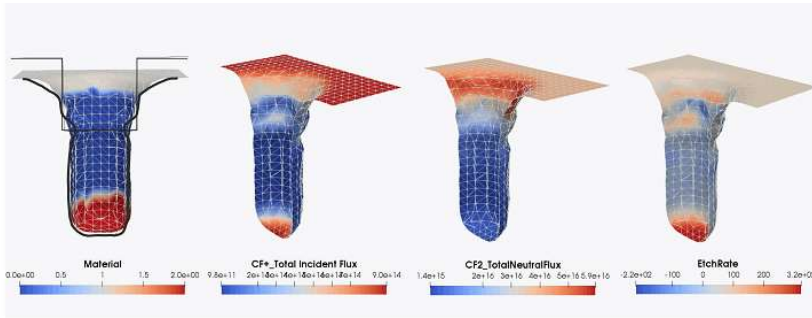
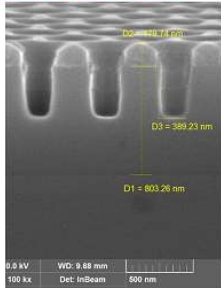
## Bulk-surface coupling model



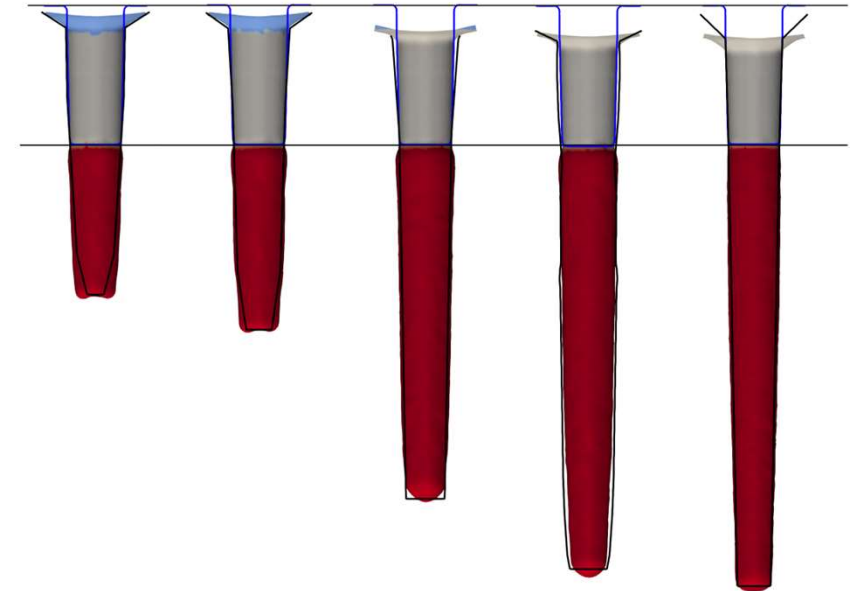
# 3. ML-aided Modeling

## Bulk-surface coupling model

Source Power : 50W



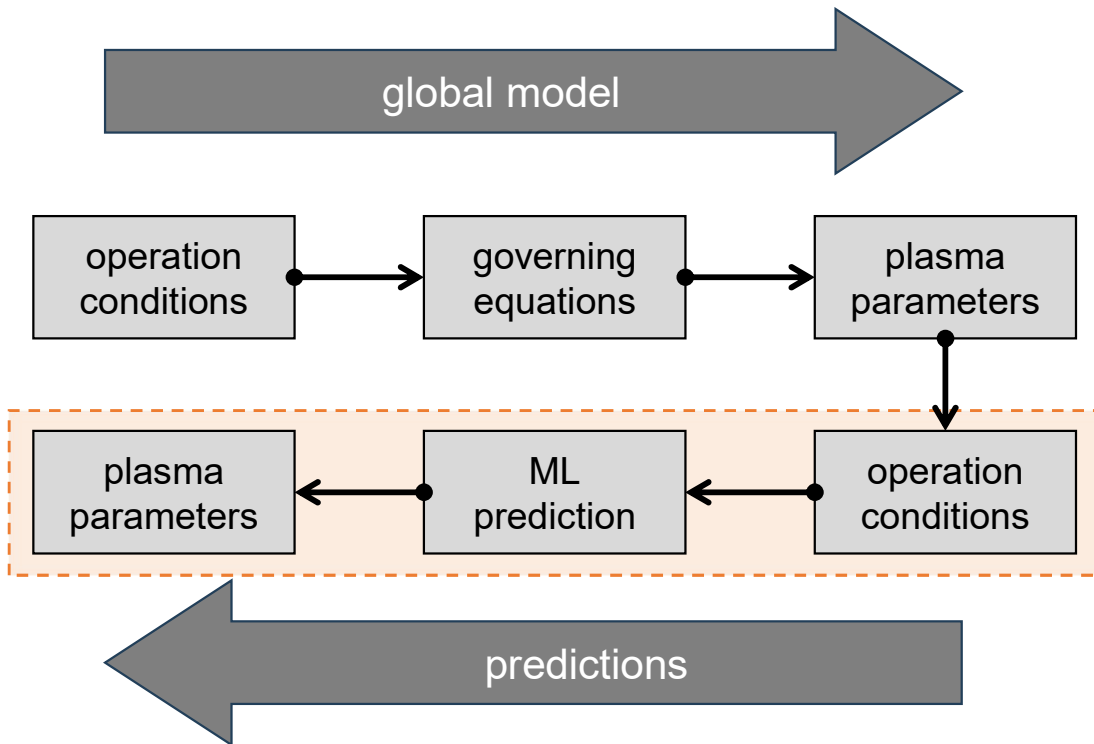
CI2	0	10	20	30	40
HBr	40	30	20	10	0



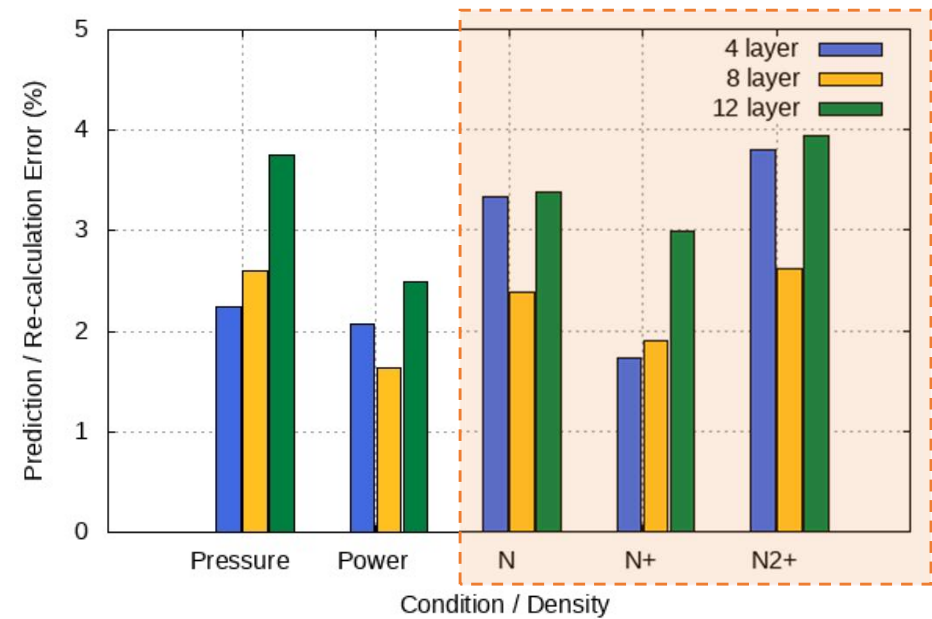


### 3. ML-aided Modeling

#### Global model + Machine learning

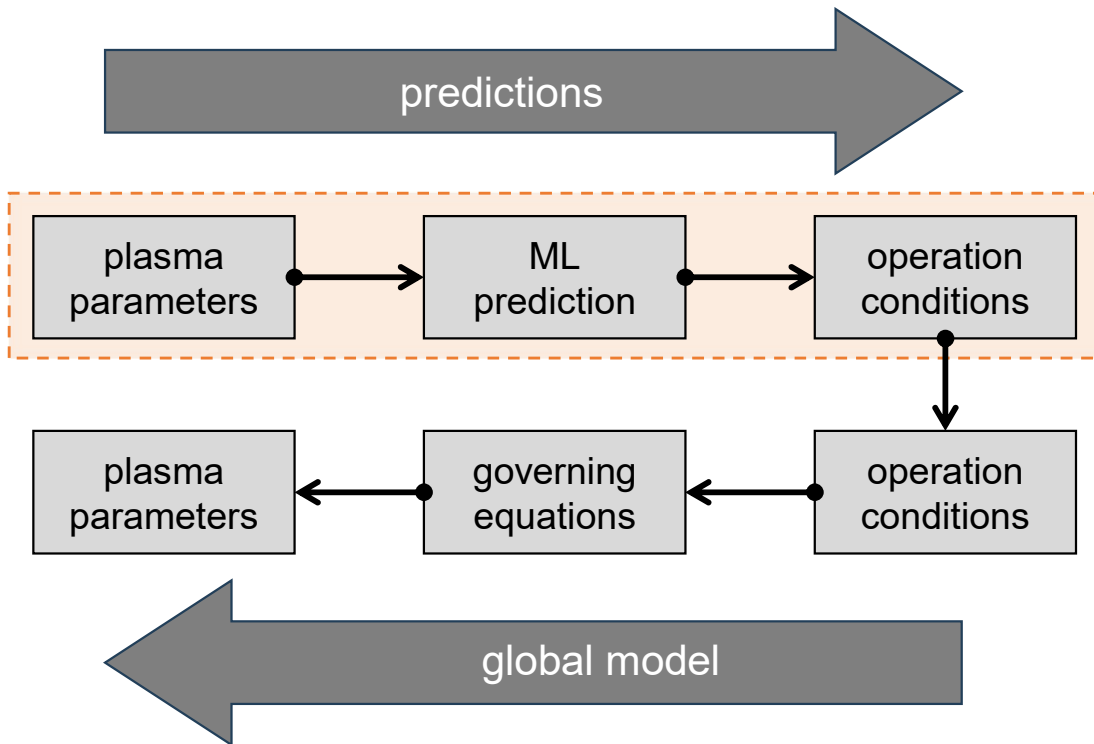


- Training plasma parameters on operations → prediction of plasma parameters
- Accuracy is not always proportional to the number of hidden layers

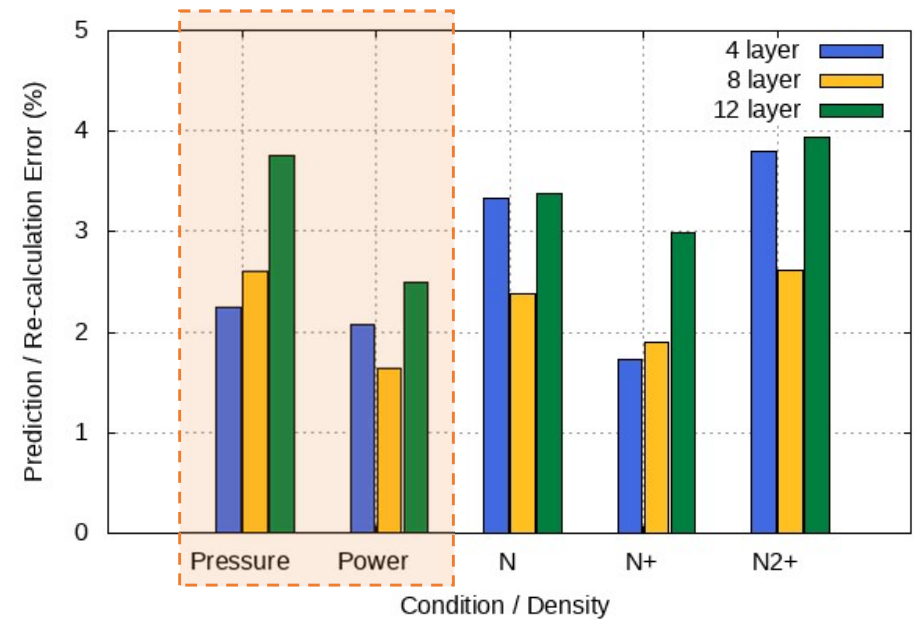


### 3. ML-aided Modeling

#### Global model + Machine learning



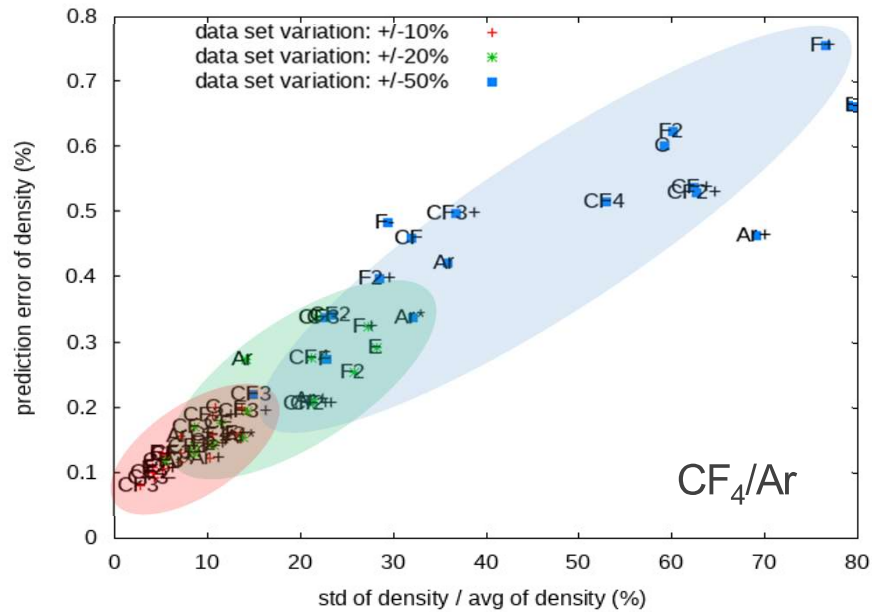
- Inversely, training operation conditions on plasma parameters
- Prediction of operation conditions for a target plasma



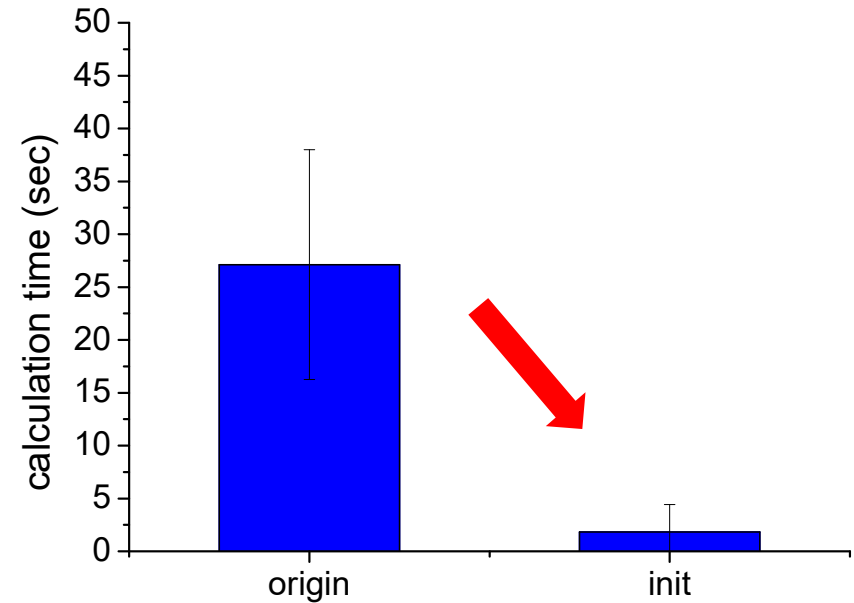
# 3. ML-aided Modeling

## Global model + Machine learning

- Global model → training → prediction
  - Prediction errors  $\propto$  data set variation
  - Sensitive species on input conditions → error ↑



- ML prediction → global model
  - Predicted values → set to be initial values
  - Improved computational efficiency

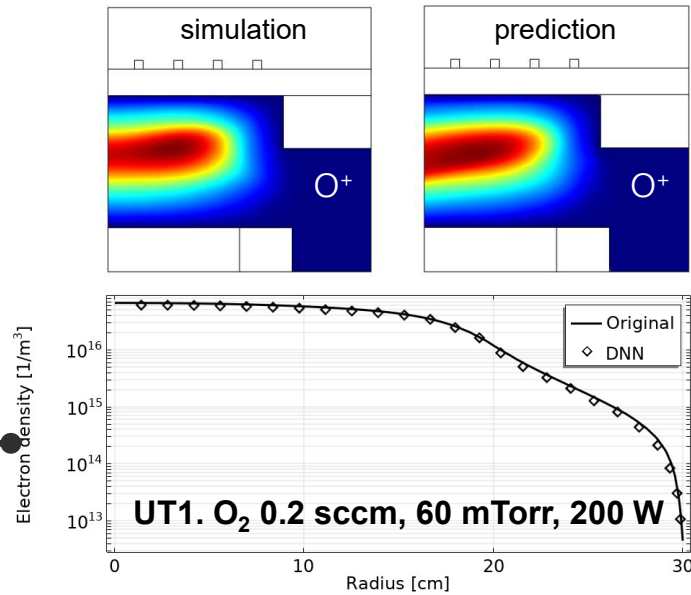


# 3. ML-aided Modeling

## Neural network for ICP sources

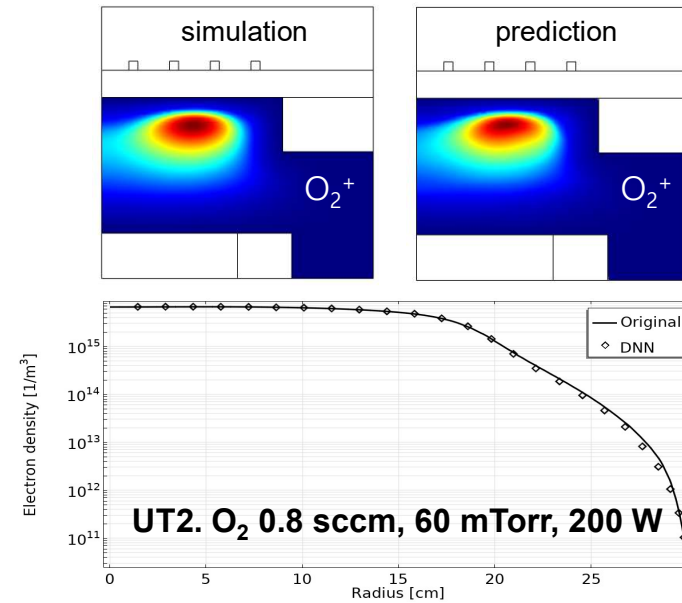
- Z-score normalization for input data
- Log normalization for output data
- Train type : Bayesian regulation (Trainbr)
- Train network : feedforward net
- Activate function type : rectified linear unit (ReLU)
- Hidden layer :  $n^{[1]} = 20, n^{[2]} = 20, n^{[3]} = 20$

DNN model optimization @ out of training range



Conditions :

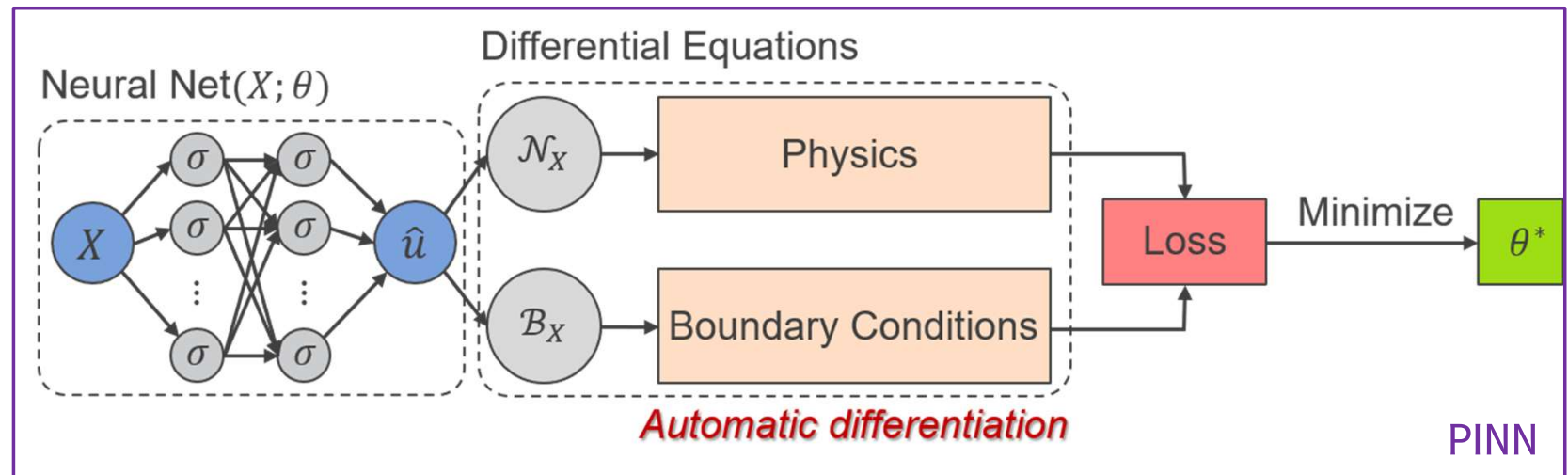
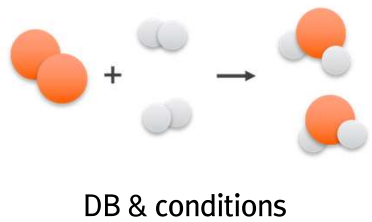
- Ar/O<sub>2</sub> total 250 sccm
- O<sub>2</sub> flow rate = 0.3, 0.4, 0.5, 0.6, 0.7 sccm
- Power = 100, 120, 140, 160, 180 W
- Pressure = 10, 20, 30, 40, 50 mTorr



# 3. ML-aided Modeling

## Physics-informed neural networks (PINNs)

- Intersection of the traditional physics model and the purely data-driven neural network approach.
- Physical parameters can be obtained without solving governing equations directly.
- DB (required), discretization (partially unnecessary) → lower barriers to entry into simulations

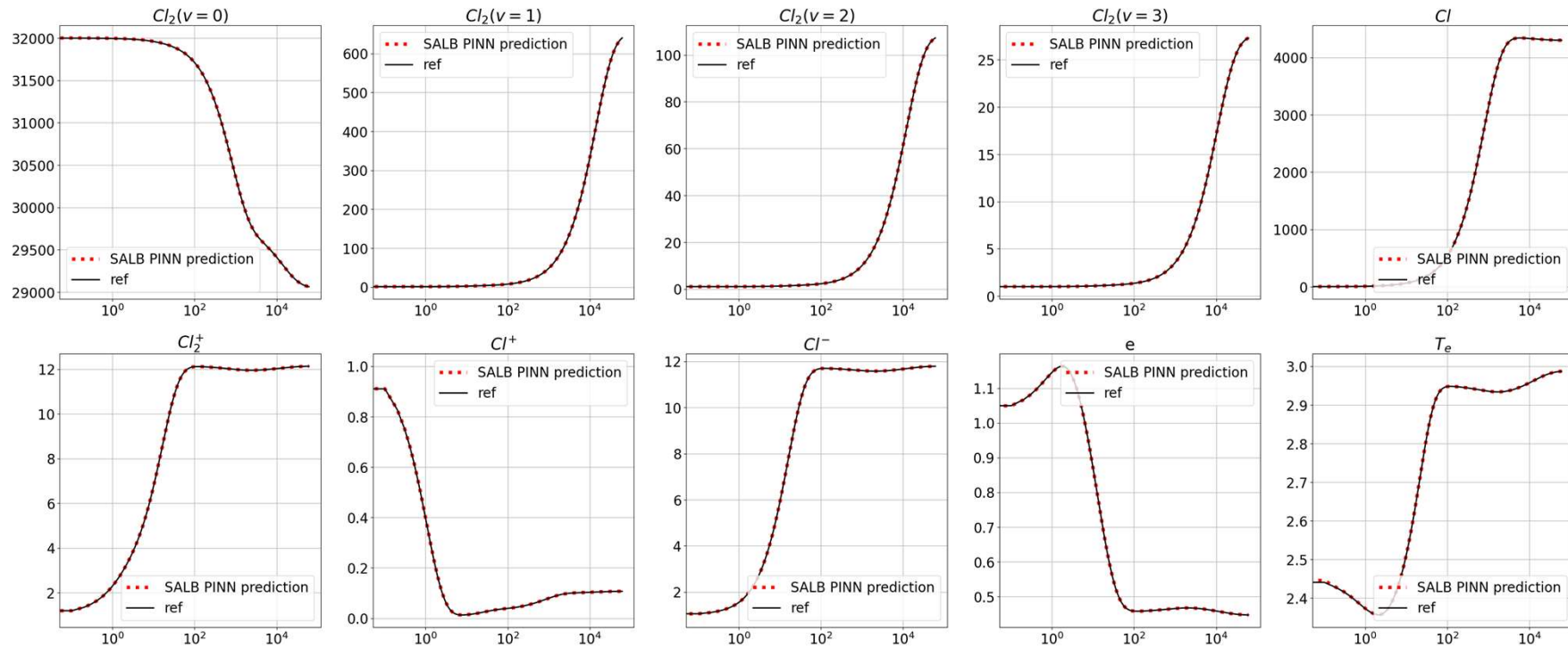


# 3. ML-aided Modeling

## Physics-informed neural networks (PINNs)



- Forward problem, Normalization
- Naive PINNs → Learn only some variable → SALB (self adaptive loss balance) loss function





# 3. ML-aided Modeling

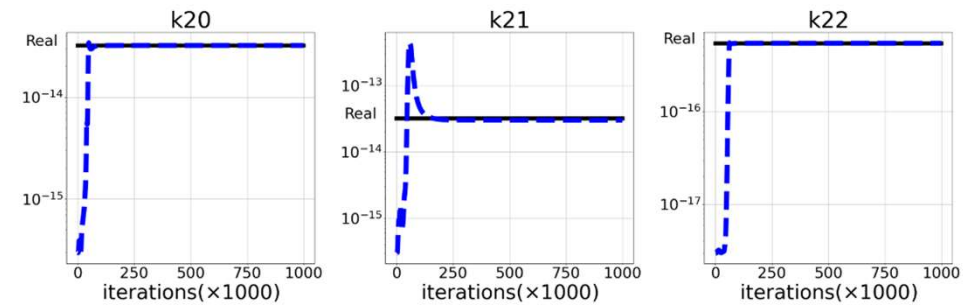
## Physics-informed neural networks (PINNs)



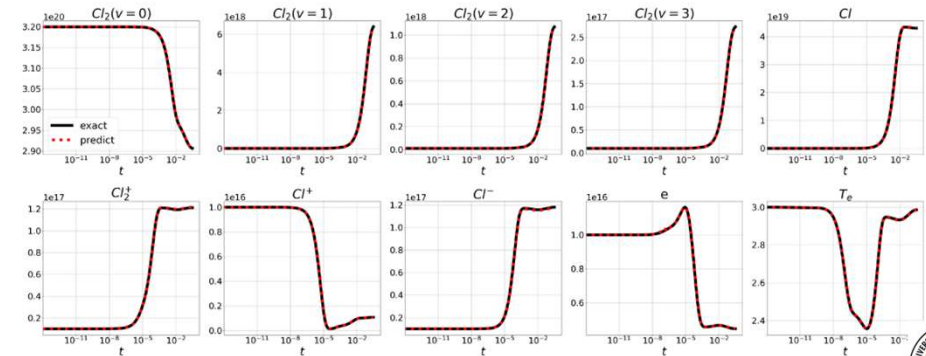
- Inverse problem to find rate coefficients

Reaction	Rate coefficient ( $\text{m}^3 \text{s}^{-1}$ or $\text{m}^6 \text{s}^{-1}$ )
(R1) $e + \text{Cl}_2(v=0) \rightarrow \text{Cl} + \text{Cl} + e$	$6.67 \times 10^{-14} T_e^{-0.10} e^{-8.67/T_e}$
(R2) $e + \text{Cl}_2(v=0) \rightarrow \text{Cl}_2^+ + e + e$	$4.87 \times 10^{-14} T_e^{0.50} e^{-12.17/T_e}$
(R3) $e + \text{Cl}_2(v=0) \rightarrow \text{Cl} + \text{Cl}^+ + 2e$	$1.79 \times 10^{-13} e^{-24.88/T_e}$
(R4) $e + \text{Cl}_2(v=0) \rightarrow \text{Cl}^+ + \text{Cl}^+ + 3e$	$1.46 \times 10^{-16} T_e^{2.16} e^{-21.42/T_e}$
(R5) $e + \text{Cl}_2(v=0) \rightarrow \text{Cl} + \text{Cl}^-$	$(22.5 T_e^{-0.46} e^{-2.82/T_e} - 12.1 e^{-0.99/T_e} + 6.54) \times 10^{-16}$
(R6) $e + \text{Cl}_2(v=1) \rightarrow \text{Cl} + \text{Cl}^-$	$(9.29 T_e^{-0.47} e^{-2.83/T_e} - 4.96 e^{-0.99/T_e} + 2.70) \times 10^{-15}$
(R7) $e + \text{Cl}_2(v=2) \rightarrow \text{Cl} + \text{Cl}^-$	$(20.1 T_e^{-0.47} e^{-2.83/T_e} - 10.8 e^{-0.97/T_e} + 5.92) \times 10^{-15}$
(R8) $e + \text{Cl}_2(v=3) \rightarrow \text{Cl} + \text{Cl}^-$	$(30.5 T_e^{-0.46} e^{-2.82/T_e} - 16.3 e^{-0.99/T_e} + 8.81) \times 10^{-15}$
(R9) $e + \text{Cl}_2(v=0) \rightarrow \text{Cl}^+ + \text{Cl}^- + e$	$3.45 \times 10^{-16} T_e^{0.13} e^{-19.70/T_e}$
(R10) $e + \text{Cl}_2(v=0) \rightarrow \text{Cl}_2(v=1) + e$	$4.35 \times 10^{-16} T_e^{-1.48} e^{-0.76/T_e}$
(R11) $e + \text{Cl}_2(v=0) \rightarrow \text{Cl}_2(v=2) + e$	$8.10 \times 10^{-17} T_e^{-1.48} e^{-0.68/T_e}$
(R12) $e + \text{Cl}_2(v=0) \rightarrow \text{Cl}_2(v=3) + e$	$2.39 \times 10^{-17} T_e^{-1.49} e^{-0.64/T_e}$
(R13) $e + \text{Cl}_2(v=1) \rightarrow \text{Cl}_2(v=2) + e$	$1.04 \times 10^{-15} T_e^{-1.48} e^{-0.73/T_e}$
(R14) $e + \text{Cl}_2(v=1) \rightarrow \text{Cl}_2(v=3) + e$	$2.98 \times 10^{-16} T_e^{-1.48} e^{-0.67/T_e}$
(R15) $e + \text{Cl}_2(v=2) \rightarrow \text{Cl}_2(v=3) + e$	$1.04 \times 10^{-15} T_e^{-1.48} e^{-0.73/T_e}$
(R16) $e + \text{Cl} \rightarrow \text{Cl}^+ + e + e$	$2.48 \times 10^{-14} T_e^{0.62} e^{-12.76/T_e}$
(R17) $e + \text{Cl}^- \rightarrow \text{Cl} + e + e$	$2.33 \times 10^{-15} T_e^{1.45} e^{-2.48/T_e}$
(R18) $e + \text{Cl}^- \rightarrow \text{Cl}^+ + 3e$	$3.38 \times 10^{-15} T_e^{0.75} e^{-25.28/T_e}$
(R19) $e + \text{Cl}^+ \rightarrow \text{Cl} + \text{Cl}$	$9.00 \times 10^{-14} T_e^{-0.50}$
(R20) $\text{Cl}_2^+ + \text{Cl}^- \rightarrow \text{Cl} + \text{Cl} + \text{Cl}$	$5.00 \times 10^{-14} (300/T_e)^{0.50}$
(R21) $\text{Cl}^+ + \text{Cl}^- \rightarrow \text{Cl} + \text{Cl}$	$5.00 \times 10^{-14} (300/T_e)^{0.50}$
(R22) $\text{Cl}_2 + \text{Cl}^+ \rightarrow \text{Cl}_2^+ + \text{Cl}$	$5.40 \times 10^{-16}$
(R23) $2\text{Cl} + \text{Cl}_2 \rightarrow \text{Cl}_2(v=0) + \text{Cl}_2$	$3.50 \times 10^{-45} e^{810/T_e}$
(R24) $2\text{Cl} + \text{Cl} \rightarrow \text{Cl}_2(v=0) + \text{Cl}$	$8.75 \times 10^{-46} e^{810/T_e}$

Results of  $k$ 's values over iterations



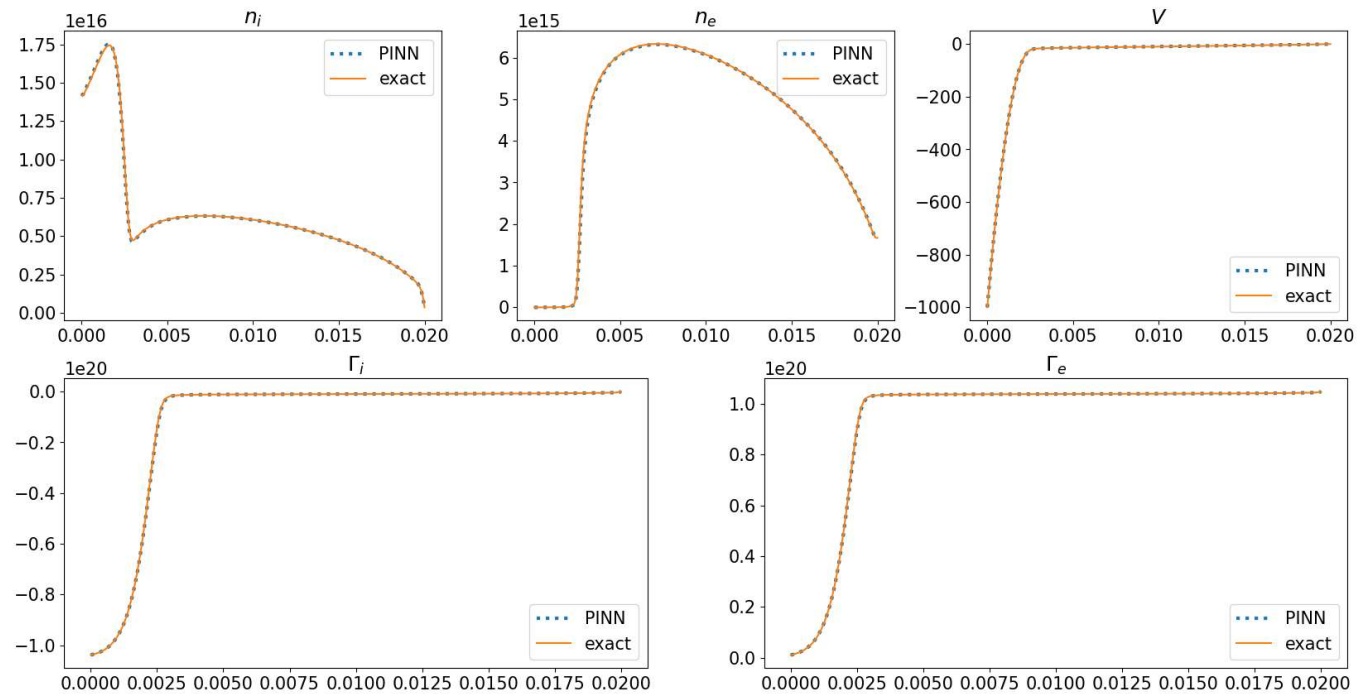
Predict results about each species



# 3. ML-aided Modeling

## Physics-informed neural networks (PINNs)

- Normalization, SALB + PINNs
- 1D DC discharge problem

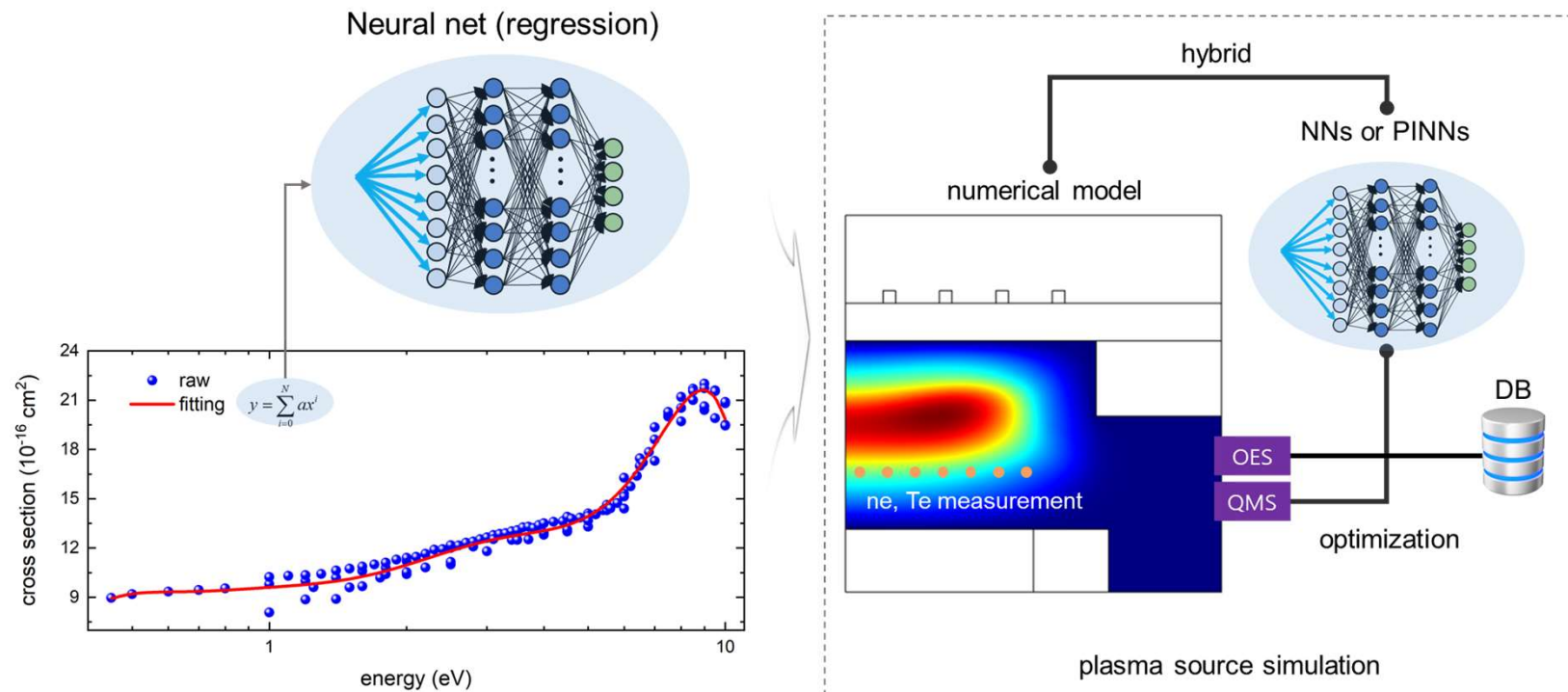


# 4

## Summary & Future works

## 4. Summary & Future works

- This talk introduces our group's simulator and database development status and the results of applying machine learning technology to plasma source monitoring and simulations
- Get helps from NNs when prediction and optimization are needed
- Fill in the blank with NNs

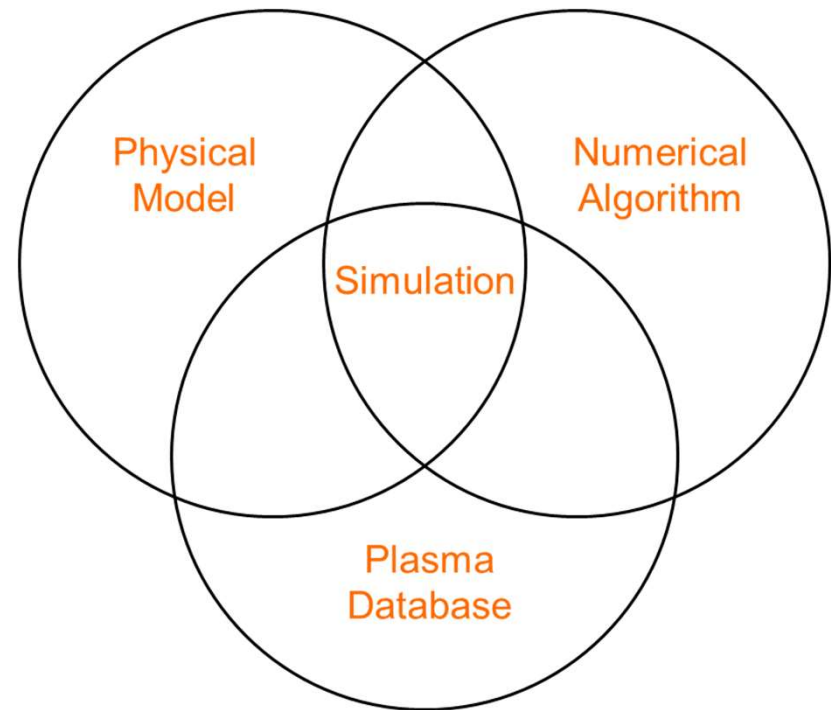
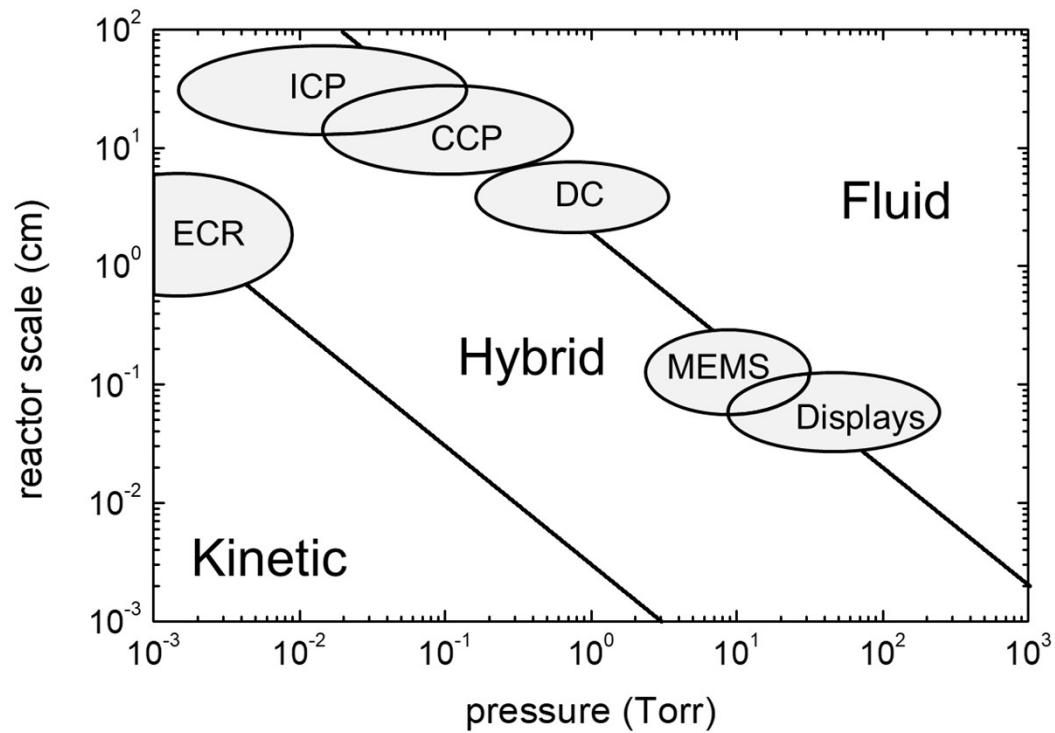


Thank you for your attention



## 5. Supplementary

### Kinetic, Hybrid, and Fluid models

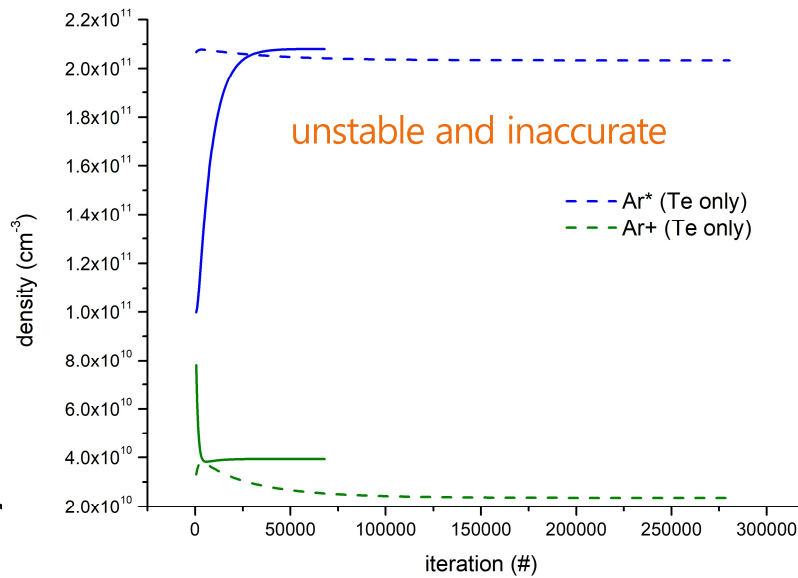
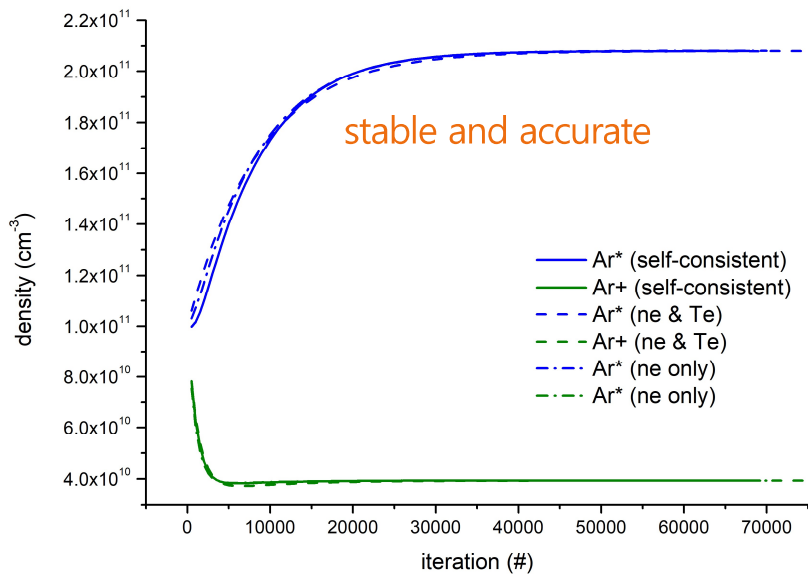


# 5. Supplementary

## CHEM-global (chemical reaction analyzer using a global model)

### Quasi-neutrality

In some cases, the quasi-neutrality condition was not satisfied → after solving the continuity equation, densities are normalized



### normalization

$$\sum_i n_i^+ = \sum_j n_j^- + n_e$$

$$\rightarrow \sum_i n_i^+ - \sum_j n_j^- = n_e$$

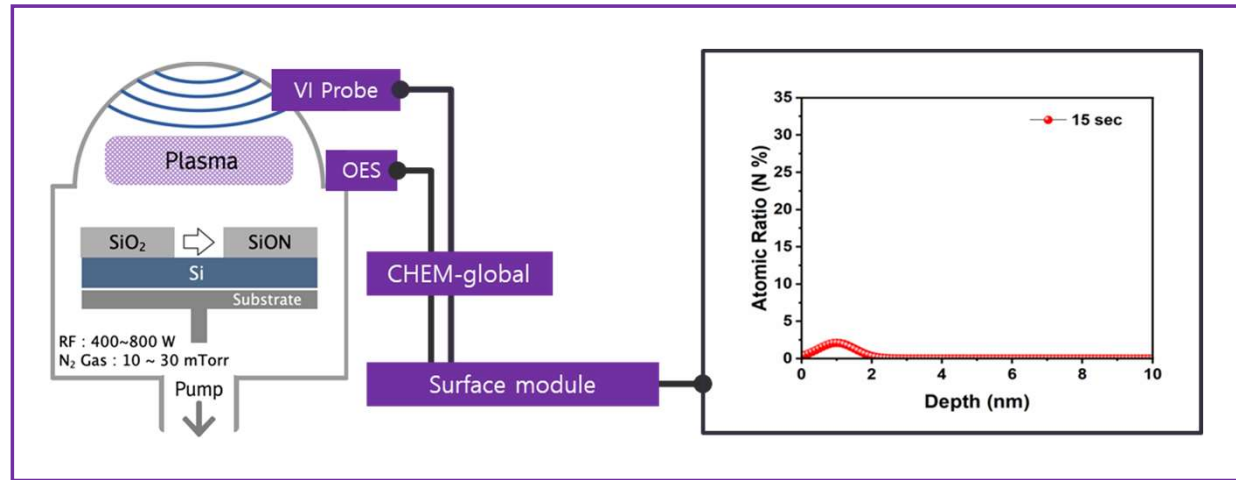
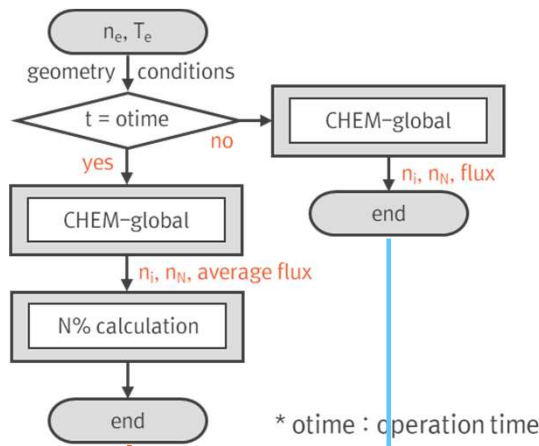
$$\text{Step 1. } \hat{n} = \sum_i n_i^+ - \sum_i n_i^-$$

$$\text{Step 2. } \kappa = \frac{n_e}{\hat{n}}$$

$$\text{Step 3. } n_i = \kappa n_i$$

# 5. Supplementary

## Sensor-bulk-surface coupling model



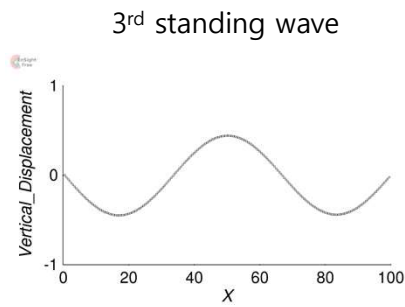
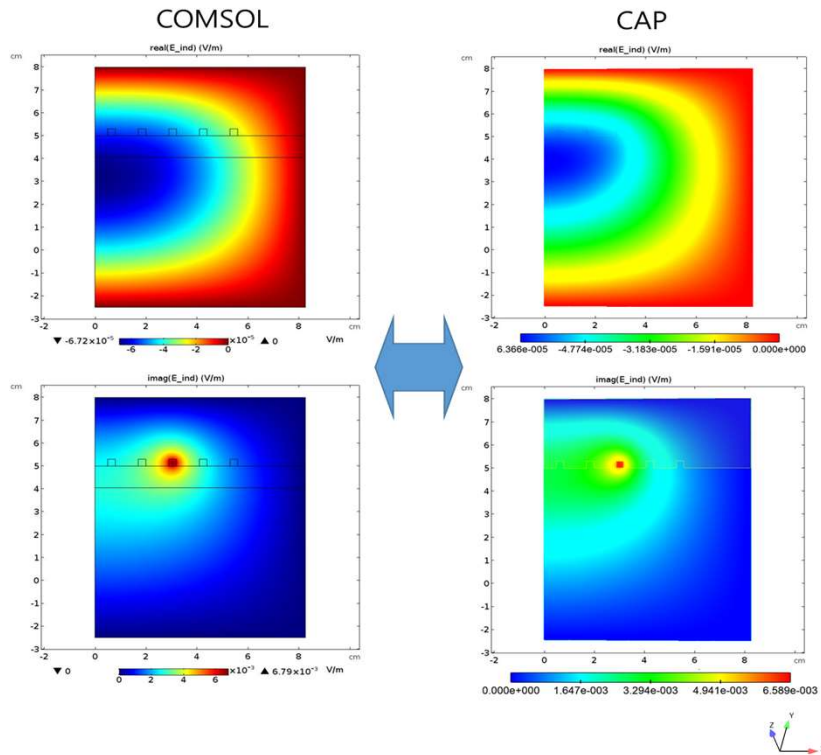
```

~/Code/NT_8.6.8 > ./CHEM-global -n 6.31e10 -t 2.96 -s 600. -d 20. -v 2.0 -c 60. -f 5.e16 -x 1
N2+:6.065187e+10 N+:2.448126e+09 N:1.533671e+13 N2*:7.423527e+12 N2:4.641126e+14 N(2P):7.076060e+11 N(2D):1.330500e+12
3.805098e+16

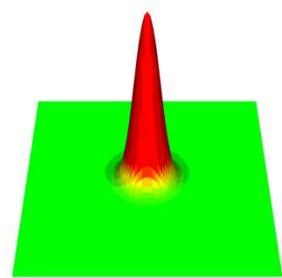
~/Code/NT_8.6.8 > ./CHEM-global -n 6.31e10 -t 2.96 -s 600. -d 20. -v 2.0 -c 600. -f 5.e16 -x 1
N2+:6.065187e+10 N+:2.448126e+09 N:1.533671e+13 N2*:7.423527e+12 N2:4.641126e+14 N(2P):7.076060e+11 N(2D):1.330500e+12
3.805098e+16
2.000000e+00 4.529994e+01
4.000000e+00 6.137989e+00
6.000000e+00 1.510557e-01
8.000000e+00 9.260711e-04
1.000000e+01 1.406361e-06
1.200000e+01 5.106815e-10
1.400000e+01 4.336434e-14
1.600000e+01 8.488942e-19
1.800000e+01 3.794496e-24
2.000000e+01 3.847017e-30
  
```

# 5. Supplementary

## K-PLASMA unit test 1

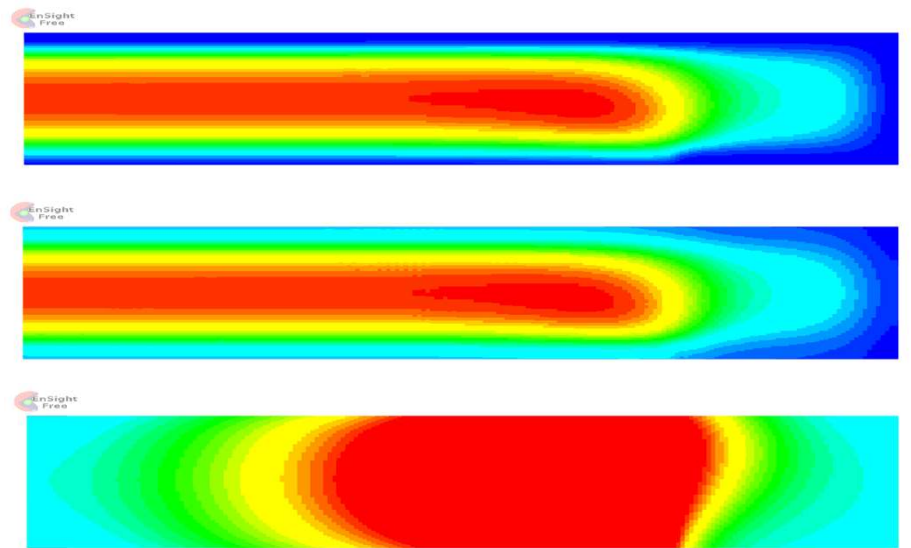


Gaussian function wave source



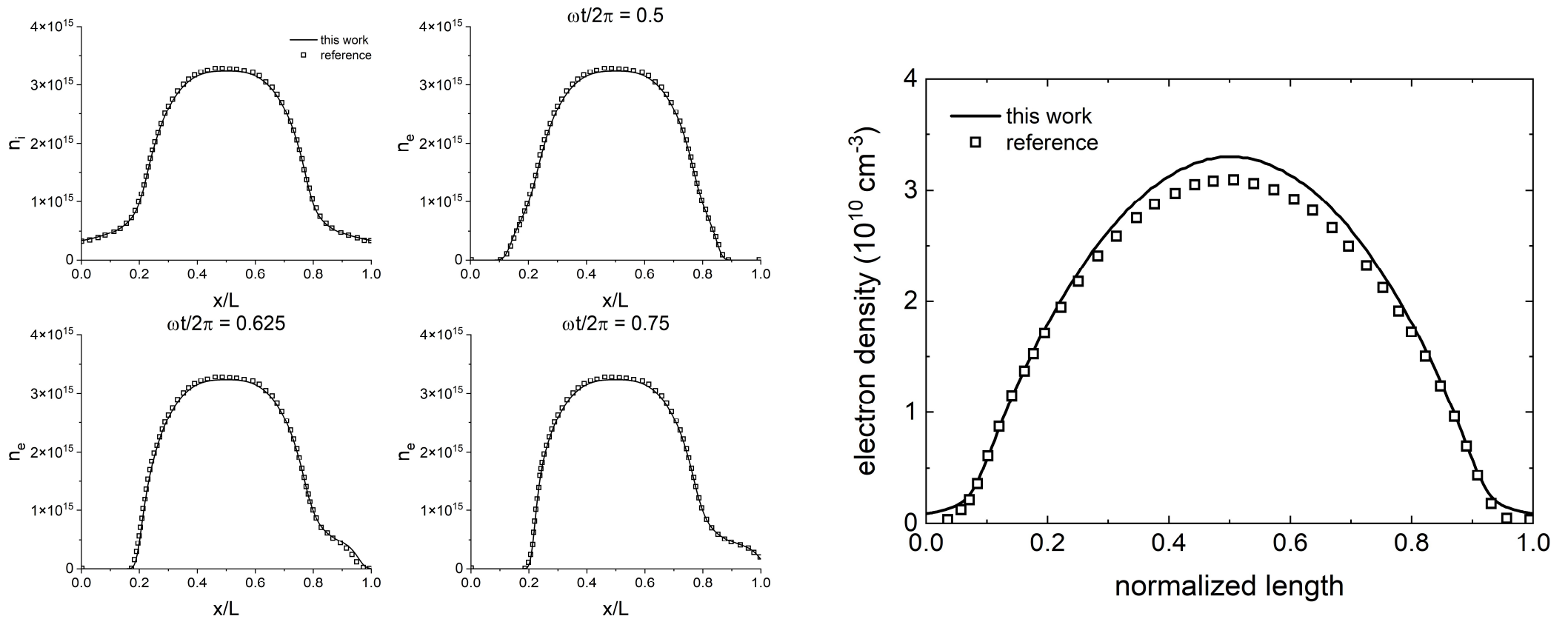
vortex extric field  $\mathbf{E}_t = -\frac{\partial \mathbf{A}}{\partial t}$

$$-\nabla^2 \left( -\frac{\partial \mathbf{A}}{\partial t} \right) = -\mu_0 \epsilon_0 \frac{\partial^2}{\partial t^2} \left( -\frac{\partial \mathbf{A}}{\partial t} \right) - \frac{\partial}{\partial t} \left\{ \mu_0 \left[ \mathbf{J} + \epsilon_0 \frac{\partial}{\partial t} (-\nabla \phi) \right] \right\}$$



# 5. Supplementary

## K-PLASMA unit test 2



## 5. Supplementary

### K-PLASMA – algorithm

$$\frac{\partial n_e}{\partial t} + \nabla \cdot \mathbf{\Gamma}_e = R_e$$

$$\frac{\partial}{\partial t} \left( \frac{3}{2} n_e k_B T_e \right) + \nabla \cdot \mathbf{Q}_e = P_{ind} - e \mathbf{E} \cdot \mathbf{\Gamma}_e + E_e$$

$$N_e = \ln n_e$$

$$n_\varepsilon = \frac{3}{2} n_e k_B T_e$$

$$E_\varepsilon = \ln n_\varepsilon$$

$$\frac{\partial n_e}{\partial t} = \frac{n_e}{n_e} \frac{\partial n_e}{\partial t} = n_e \frac{\partial (\ln n_e)}{\partial t} = n_e \frac{\partial N_e}{\partial t}$$

$$\frac{\partial}{\partial t} \left( \frac{3}{2} n_e k_B T_e \right) = \frac{\partial n_\varepsilon}{\partial t} = \frac{n_\varepsilon}{n_\varepsilon} \frac{\partial n_\varepsilon}{\partial t} = n_\varepsilon \frac{\partial (\ln n_\varepsilon)}{\partial t} = n_\varepsilon \frac{\partial E_\varepsilon}{\partial t}$$

$$\mathbf{\Gamma}_e = -\frac{qn_e}{m_e \nu_{eN}} \mathbf{E} - \frac{n_e}{m_e \nu_{eN}} \nabla T_e - \frac{T_e}{m_e \nu_{eN}} \nabla n_e$$

$$= -\mu_e n_e \mathbf{E} - n_e \nabla D_e - D_e \nabla n_e$$

$$\rightarrow \mathbf{\Gamma}_e = -\mu_e n_e \mathbf{E} - n_e \nabla D_e - n_e D_e \nabla N_e$$

$$\Rightarrow n_e \frac{\partial N_e}{\partial t} + \nabla \cdot [-\mu_e n_e \mathbf{E} - n_e \nabla D_e - n_e D_e \nabla N_e] = R_e$$

$$\mathbf{Q}_e = \frac{5}{2} \mathbf{\Gamma}_e k_B T_e - \frac{5 n_e k_B T_e}{2 m_e \nu_{eN}} \nabla (k_B T_e)$$

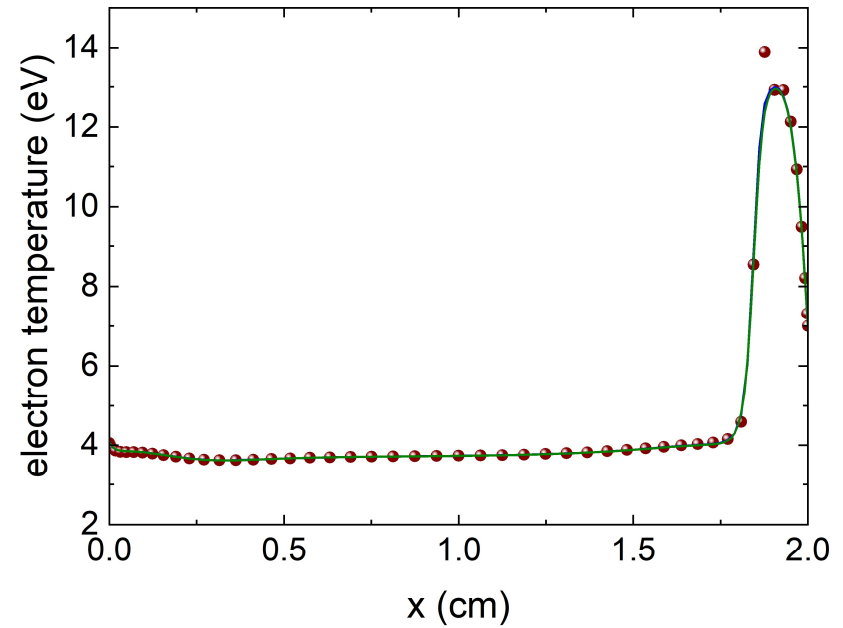
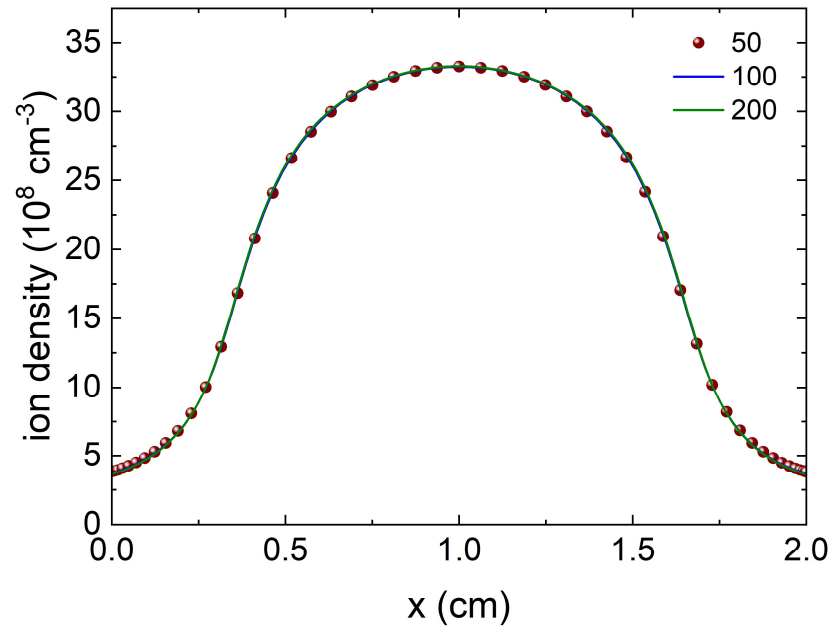
$$\rightarrow \mathbf{Q}_e = -\mu_\varepsilon \mathbf{E} n_\varepsilon - D_\varepsilon n_\varepsilon \nabla E_\varepsilon - n_\varepsilon \nabla D_\varepsilon$$

$$\Rightarrow n_\varepsilon \frac{\partial E_\varepsilon}{\partial t} + \nabla \cdot [-\mu_\varepsilon n_\varepsilon \mathbf{E} - n_\varepsilon D_\varepsilon \nabla E_\varepsilon - n_\varepsilon \nabla D_\varepsilon] = P_{ind} - e \mathbf{E} \cdot \mathbf{\Gamma}_e + E_e$$



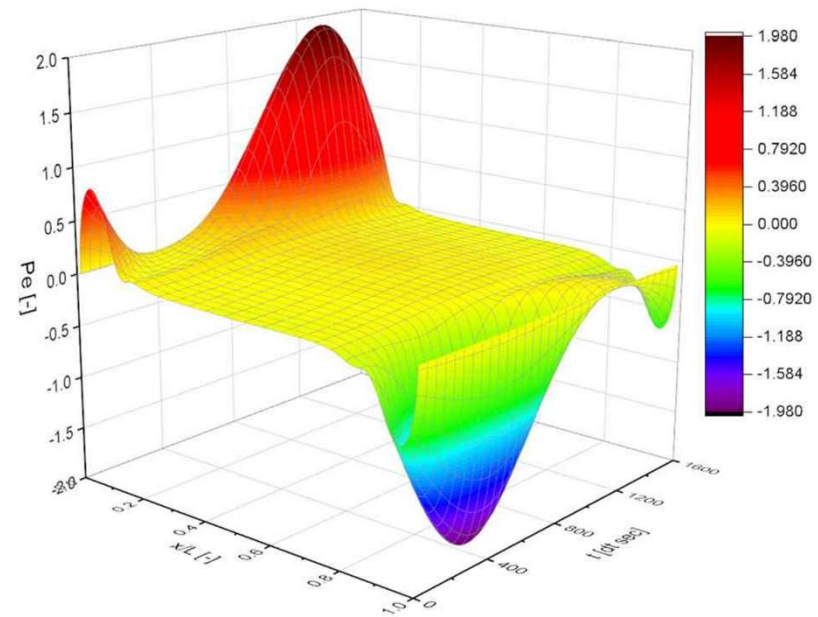
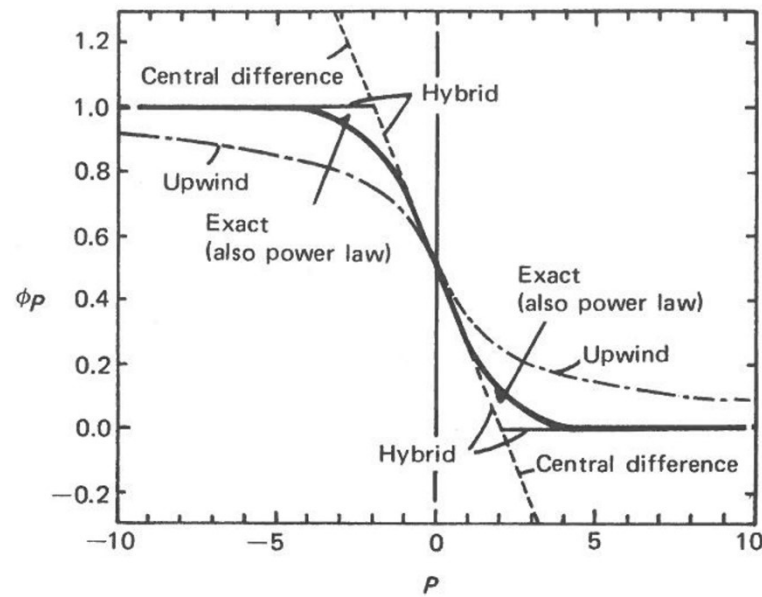
## 5. Supplementary

### K-PLASMA – algorithm



# 5. Supplementary

## K-PLASMA – algorithm



# 5. Supplementary

## K-PLASMA – algorithm

$$\begin{cases} \frac{\partial \Gamma_i}{\partial t} + \nabla \cdot (\Gamma_i \mathbf{u}_i) = \frac{en_i}{m_i} \mathbf{E} - \frac{1}{m_i} \nabla (n_i k_B T_i) - \nu_{iN} \Gamma_i \\ \Gamma_i = \frac{en_i}{\nu_{iN} m_i} \mathbf{E}_{eff} - \frac{1}{\nu_{iN} m_i} \nabla (n_i k_B T_i) \end{cases}$$

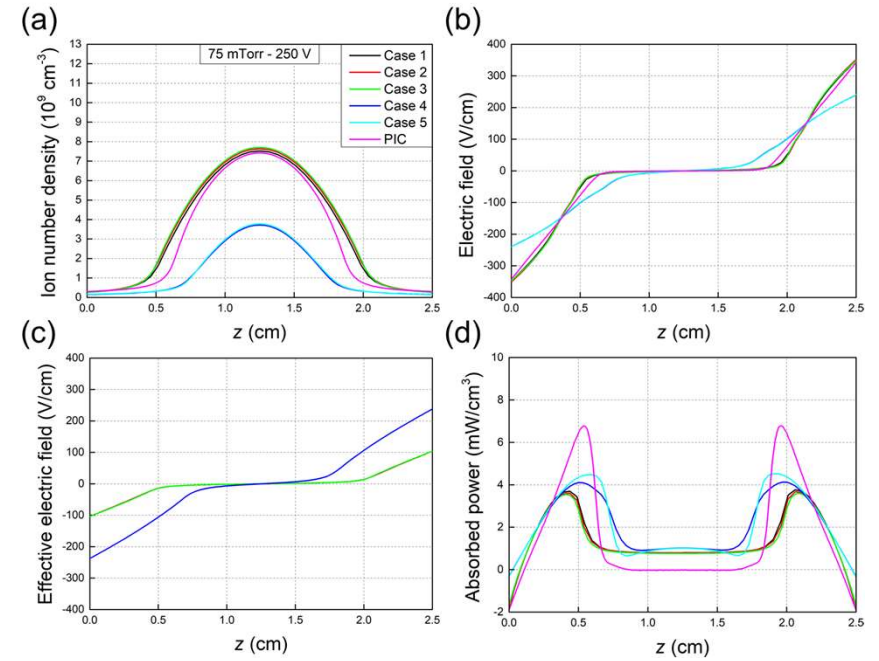
assuming  $\frac{\partial}{\partial t} \left[ \frac{1}{\nu_{iN} m_i} \nabla (n_i k_B T_i) \right] \approx 0$ ,  $\nu_{iN} = const$

$$\frac{\partial}{\partial t} \left( \frac{en_i}{\nu_{iN} m_i} \mathbf{E}_{eff} \right) = \frac{e}{\nu_{iN} m_i} \left( n_i \frac{\partial \mathbf{E}_{eff}}{\partial t} + \mathbf{E}_{eff} \frac{\partial n_i}{\partial t} \right) = \frac{e}{\nu_{iN} m_i} \left[ n_i \frac{\partial \mathbf{E}_{eff}}{\partial t} + \mathbf{E}_{eff} (R_i - \nabla \cdot \Gamma_i) \right]$$

$$\begin{aligned} \rightarrow \frac{en_i}{\nu_{iN} m_i} \frac{\partial \mathbf{E}_{eff}}{\partial t} &= -\nabla \cdot (\Gamma_i \mathbf{u}_i) + \frac{en_i}{m_i} \mathbf{E} - \frac{1}{m_i} \nabla (n_i k_B T_i) - \nu_{iN} \left[ \frac{en_i}{\nu_{iN} m_i} \mathbf{E}_{eff} - \frac{1}{\nu_{iN} m_i} \nabla (n_i k_B T_i) \right] - \frac{e}{\nu_{iN} m_i} \mathbf{E}_{eff} (R_i - \nabla \cdot \Gamma_i) \\ &= -\nabla \cdot (\Gamma_i \mathbf{u}_i) + \frac{en_i}{m_i} \mathbf{E} - \frac{1}{m_i} \nabla (n_i k_B T_i) - \frac{en_i}{m_i} \mathbf{E}_{eff} + \frac{1}{m_i} \nabla (n_i k_B T_i) - \frac{e}{\nu_{iN} m_i} \mathbf{E}_{eff} (R_i - \nabla \cdot \Gamma_i) \end{aligned}$$

$$\rightarrow \frac{\partial \mathbf{E}_{eff}}{\partial t} = -\frac{\nu_{iN} m_i}{en_i} \nabla \cdot (\Gamma_i \mathbf{u}_i) + \nu_{iN} \mathbf{E} - \nu_{iN} \mathbf{E}_{eff} - \frac{1}{n_i} \mathbf{E}_{eff} (R_i - \nabla \cdot \Gamma_i)$$

$$\Rightarrow \frac{\partial \mathbf{E}_{eff}}{\partial t} = \nu_{iN} (\mathbf{E} - \mathbf{E}_{eff}) - \frac{\nu_{iN} m_i}{en_i} \nabla \cdot (\Gamma_i \mathbf{u}_i) - \frac{1}{n_i} \mathbf{E}_{eff} (R_i - \nabla \cdot \Gamma_i)$$



- Case 1; full momentum equation
- Case 2; full effective electric field
- Case 3; Ignoring the third term on RHS
- Case 4; Ignoring the second and third terms on RHS
- Case 5; without the effective electric field

## 5. Supplementary

### Equivalent circuit of dielectric wall ICP sources

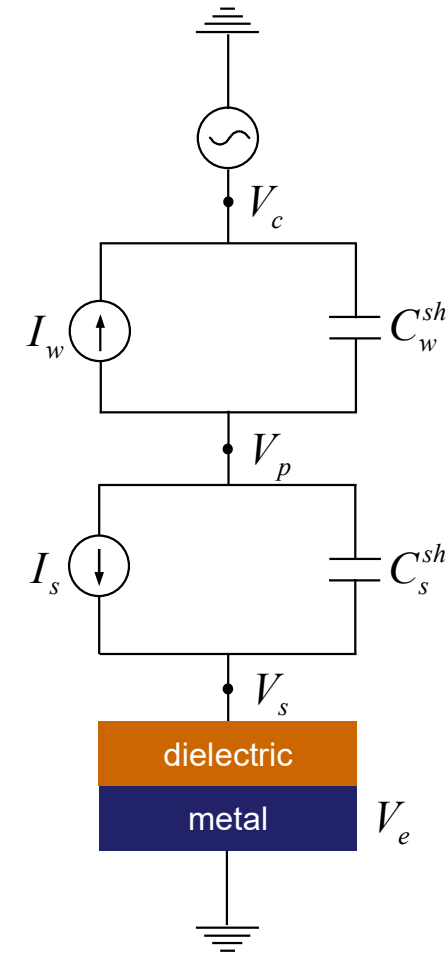
$$\begin{cases} C_w^{sh} \frac{\partial}{\partial t} (V_p - V_c) + I_w + C_s^{sh} \frac{\partial}{\partial t} (V_p - V_s) + I_s = 0 \\ \frac{\partial V_s}{\partial t} = \frac{1}{C_{eff}} (I_i - I_e + I_d) = \frac{1}{C_{eff}} I_s + \frac{1}{C_{eff}} C_s^{sh} \frac{\partial}{\partial t} (V_p - V_s) \end{cases}$$

$$I_s = I_i - I_e \quad I_d = C_s^{sh} \frac{\partial}{\partial t} (V_p - V_s)$$

$$\Rightarrow \begin{cases} C_w^{sh} \frac{\partial}{\partial t} (V_p - V_c) + I_w + C_s^{sh} \frac{\partial}{\partial t} (V_p - V_s) + I_s = 0 \\ \frac{\partial V_s}{\partial t} = \frac{1}{C_{eff}} I_s + \frac{C_s^{sh}}{C_{eff}} \frac{\partial}{\partial t} (V_p - V_s) \end{cases}$$

where  $C_{eff} = \frac{\epsilon_r \epsilon_0 A_w}{d_f}$ ,  $A_w$  is the surface area of the dielectric wall,

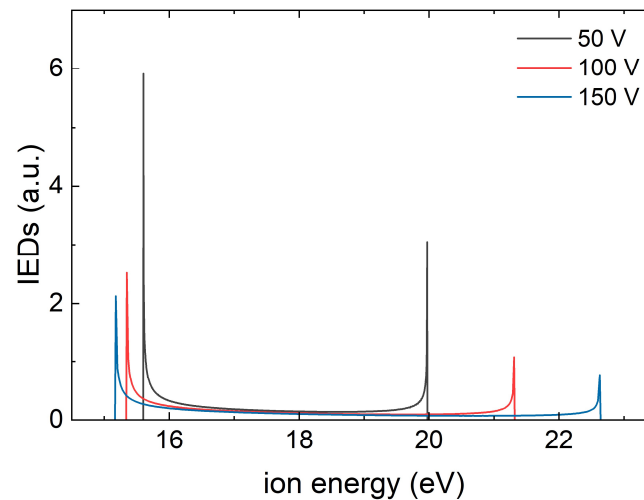
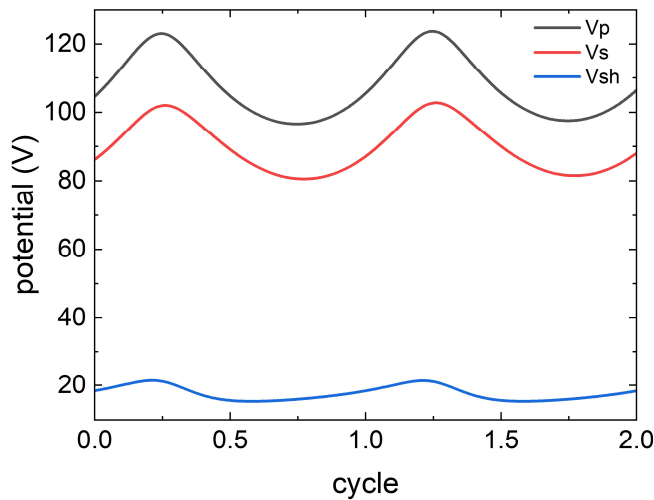
$\epsilon_r$  and  $d_f$  are the dielectric constant and thickness of the dielectric material.



# 5. Supplementary

## Equivalent circuit of dielectric wall ICP sources

$$\left\{ \begin{aligned} \frac{\partial V_p}{\partial t} &= \frac{C_w^{sh} C_{eff} + C_w^{sh} C_s^{sh}}{C_w^{sh} C_{eff} + C_w^{sh} C_s^{sh} + C_s^{sh} C_{eff}} \frac{\partial V_c}{\partial t} - \frac{C_{eff} + C_s^{sh}}{C_w^{sh} C_{eff} + C_w^{sh} C_s^{sh} + C_s^{sh} C_{eff}} \left[ I_w + I_s - \frac{C_s^{sh}}{C_{eff} + C_s^{sh}} I_s \right] \\ \frac{\partial V_s}{\partial t} &= \frac{1}{C_{eff} + C_s^{sh}} I_s + \frac{C_s^{sh}}{C_{eff} + C_s^{sh}} \left\{ \frac{C_w^{sh} C_{eff} + C_w^{sh} C_s^{sh}}{C_w^{sh} C_{eff} + C_w^{sh} C_s^{sh} + C_s^{sh} C_{eff}} \frac{\partial V_c}{\partial t} - \frac{C_{eff} + C_s^{sh}}{C_w^{sh} C_{eff} + C_w^{sh} C_s^{sh} + C_s^{sh} C_{eff}} \left[ I_w + I_s - \frac{C_s^{sh}}{C_{eff} + C_s^{sh}} I_s \right] \right\} \end{aligned} \right.$$



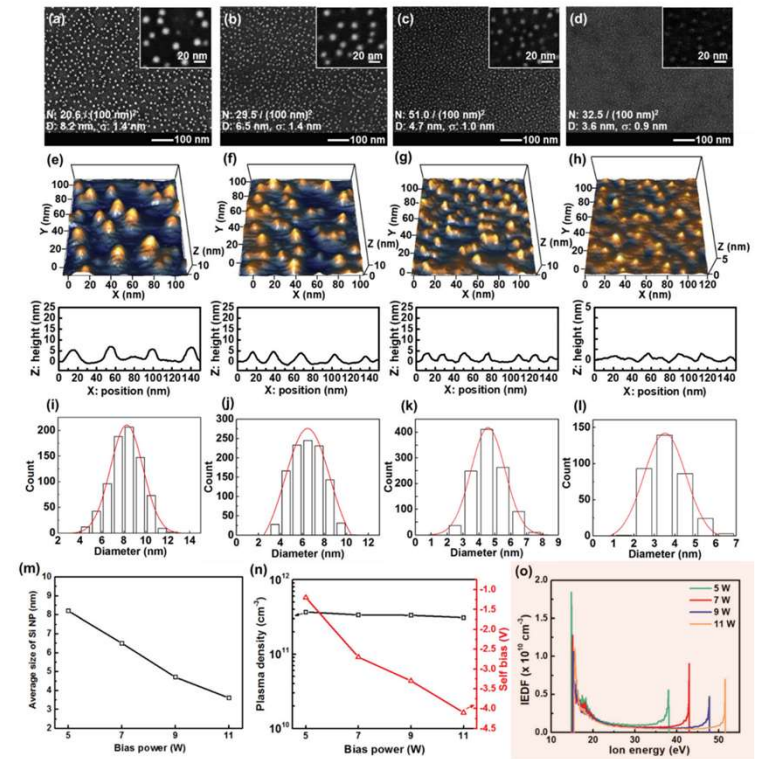
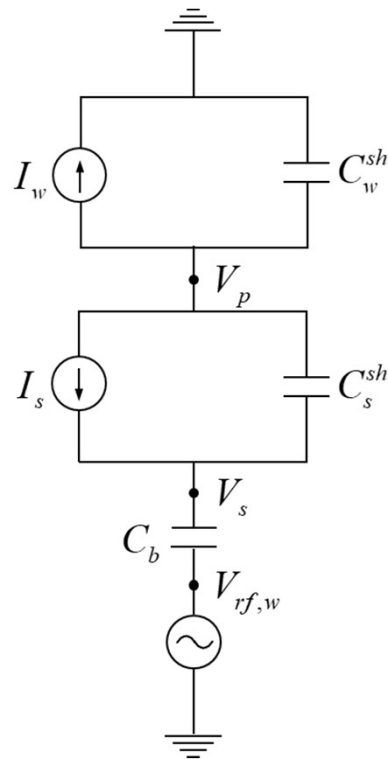
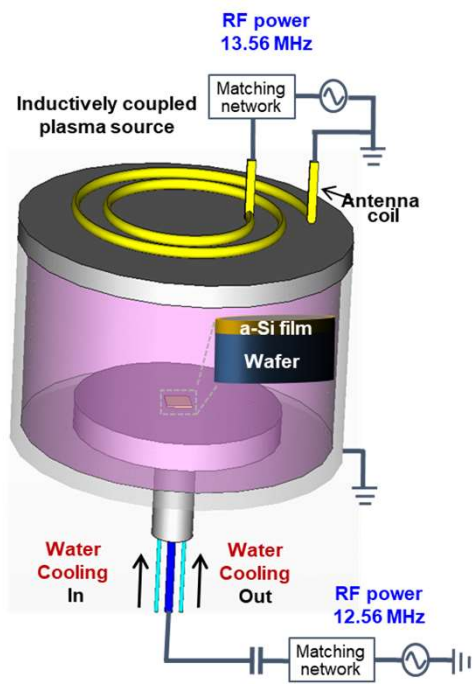
$$\frac{d\chi}{dx} \left( \frac{\partial f}{\partial \chi} + \frac{\partial f}{\partial y} \right) = -q(y) f(\chi, y) + C(\chi) \delta(y)$$

where  $\chi = \frac{-e\phi}{k_B T_i}$ ,  $x = \frac{z}{L}$ ,  $y = \frac{m_i v^2}{2k_B T_i}$ ,  $q(y) = \frac{L}{\lambda(y)}$

Riemann obtained the IEDs at the chamber wall by solving the Boltzmann equation

# 5. Supplementary

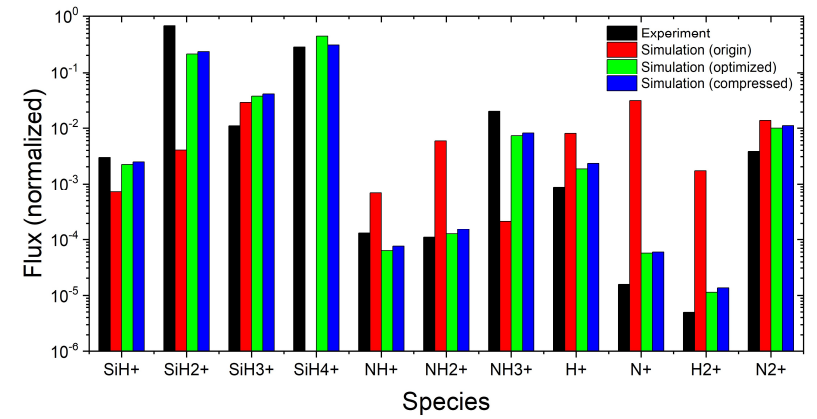
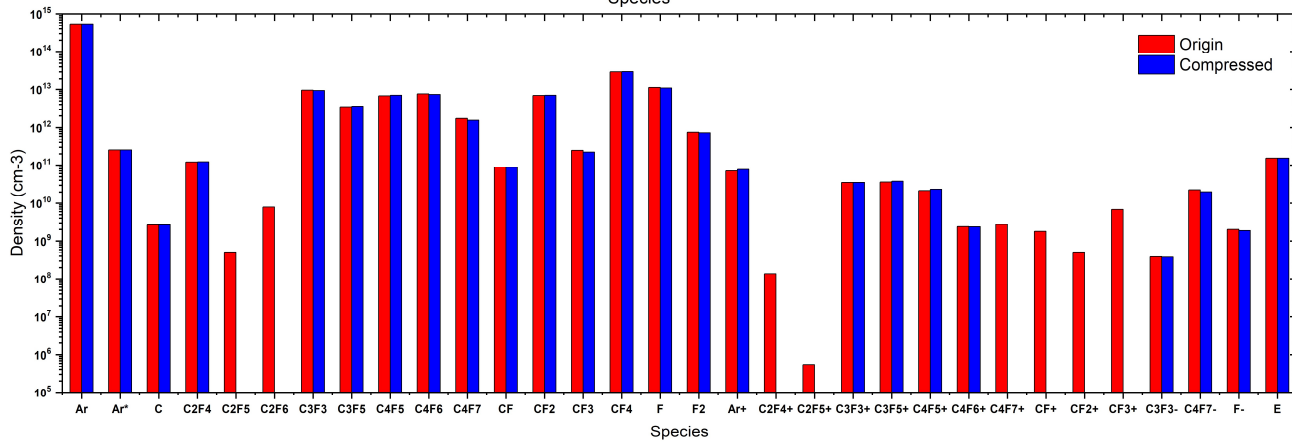
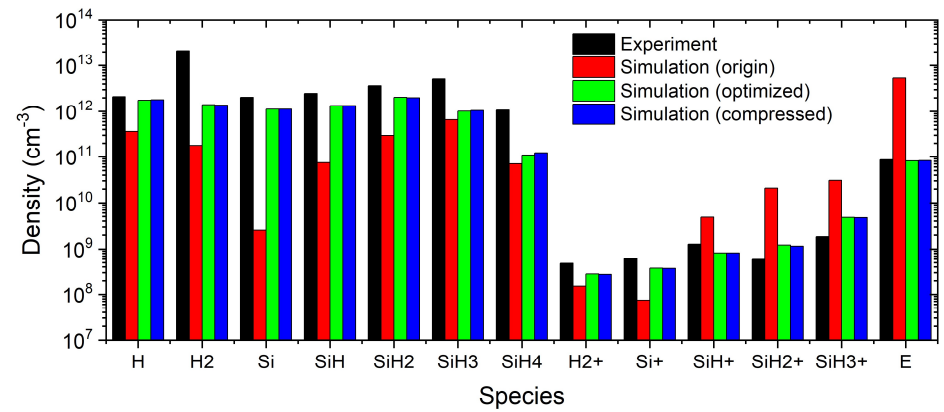
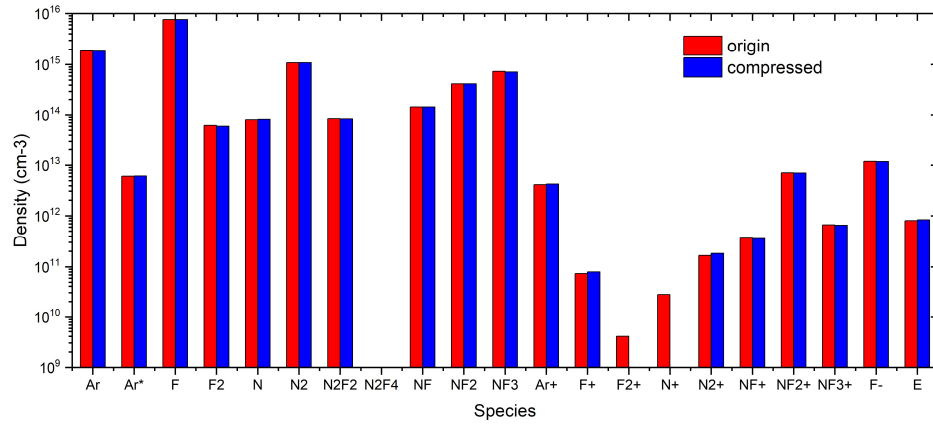
## Equivalent circuit for rf-biased sheath





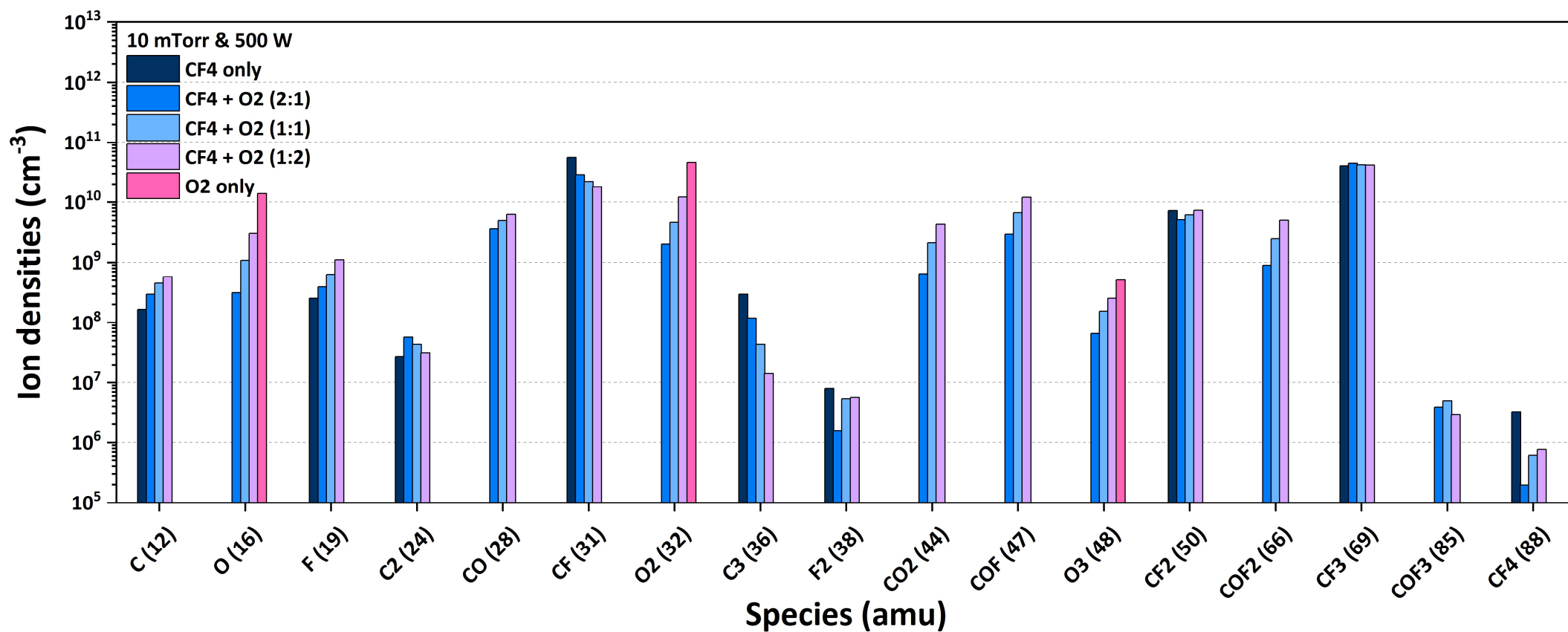
# 5. Supplementary

## Database development



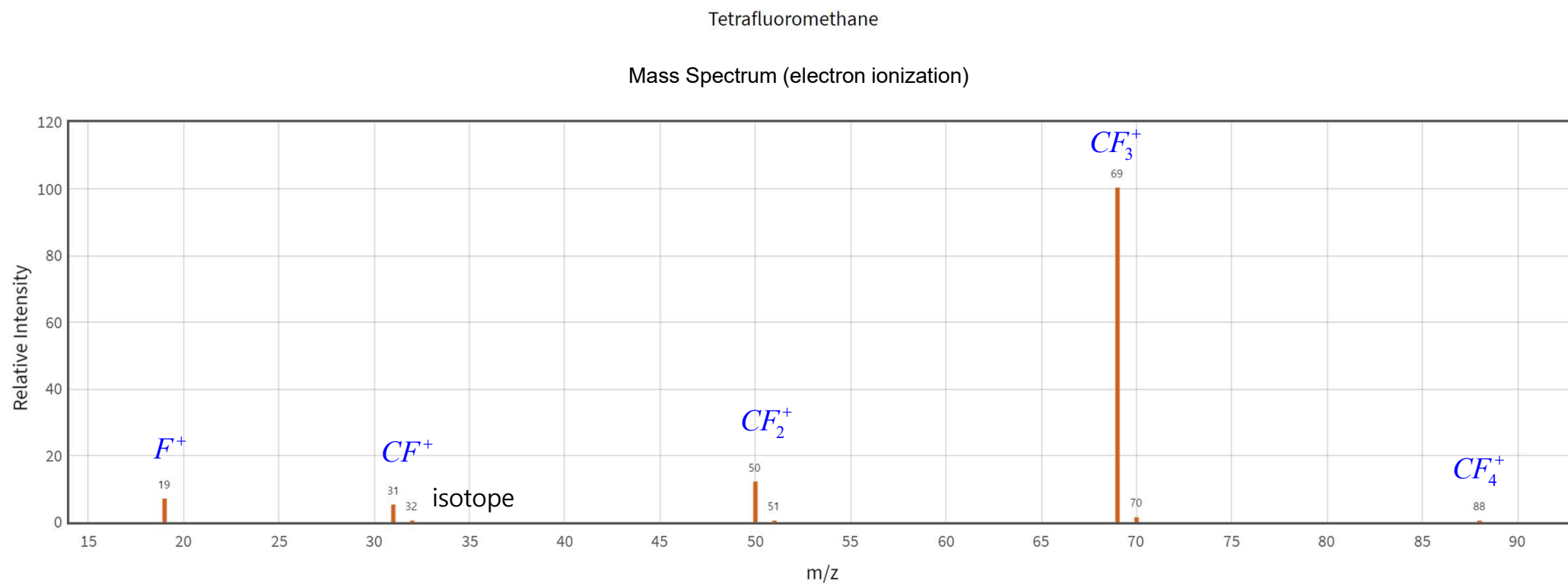
## 5. Supplementary

### Database development (CF<sub>4</sub>/O<sub>2</sub> mixture)



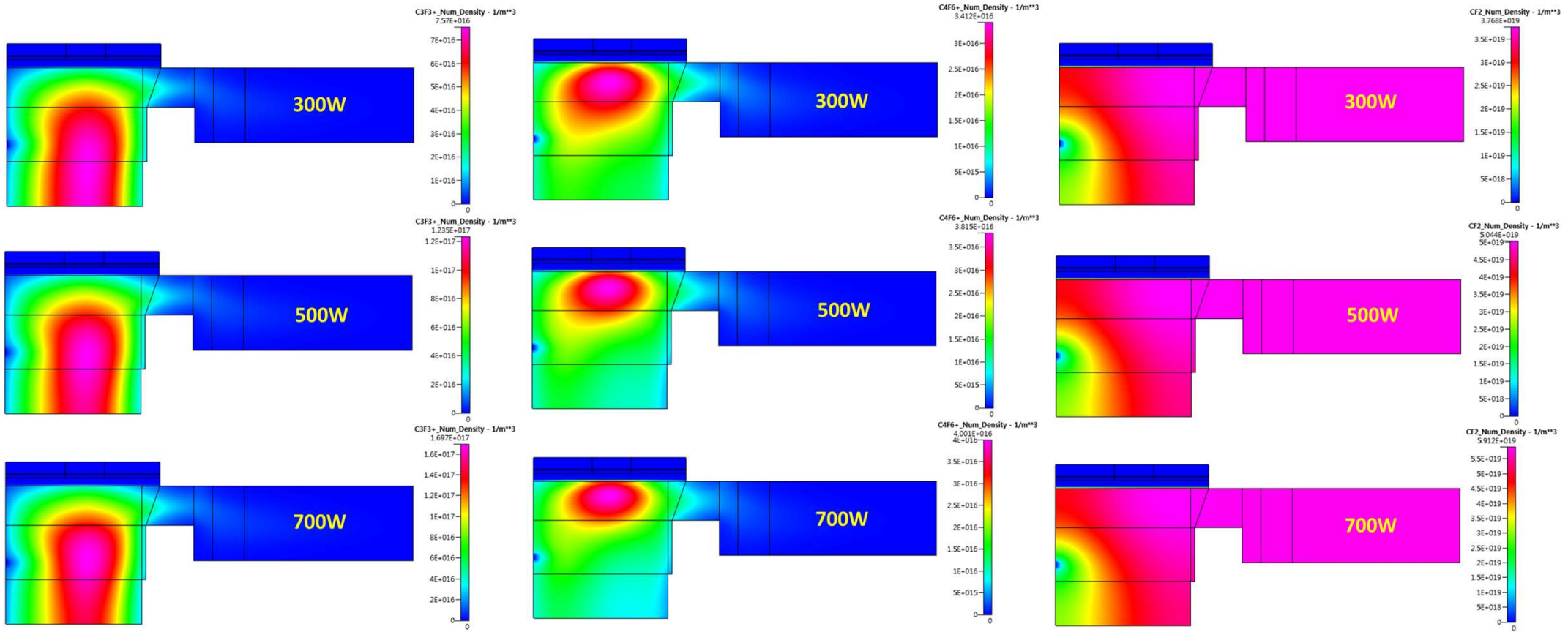
## 5. Supplementary

### Database development ( $\text{CF}_4/\text{O}_2$ mixture)



# 5. Supplementary

## 2D simulations at 20 mTorr



## 4. Summary & Future works

Neural net (regression)

