

Federal Environmental, Industrial and Nuclear Supervision Service

SEC NRS

Scientific and Engineering Centre for Nuclear and Radiation Safety

# MODELING OF SEVERE ACCIDENTS FOR SODIUM AND LEAD COOLED REACTORS

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Technical Meeting on the Safety Approach for Liquid Metal Cooled Fast Reactors and the Analysis and Modelling of Severe Accidents 13–17 Mar 2023 IAEA

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## > Application of the calculation results to

assess the safety review of fast neutron reactors with sodium and lead coolant.

# **Objectives of the work**

- Creation of computational models of reactors with sodium and lead coolant;
- Evaluation of the veracity of the results obtained using the developed computational models;







# **Reactor BN-800 with sodium coolant model**

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## Models of fuel elements for fuel assemblies of the core of BN-800



- FA with enriched uranium dioxide pellets and depleted uranium dioxide pellets in the upper and lower breeding zones (FA UTT);
- FA with vibrocompacted MOX fuel and depleted uranium dioxide pellets in the upper and lower breeding zones (FA SVUT);
  - FA with pellet MOX fuel and pellets of depleted uranium dioxide in the lower breeding zone (FA STT);
  - The height of the layers was chosen in accordance with the axial profile of the energy release in the reactor.





The nodalization scheme includes :

- Pressure chamber
- Upper drain cavity
- High and low pressure collectors
- Channels of fuel assemblies of the core and fuel assemblies of the side breeding zone
- CPS and trigger neutron source cooling channels
- Leaks channels in the space between
   cassettes and steel and boron protection
   assemblies

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## **Thermal-hydraulic model of BN-800**



- Three circulation loops with

   a common tract in the section
   between the pressure
   chamber of the core and the
   reactor tank;
- The regions of the reactor in which the pressure vessel and internal protection are cooling;
- Second and third circuits of the reactor were prepared.



# Relative deviations of the results of the thermal-hydraulic characteristics calculating between SOCRAT-BN and design data



■ 1 -Total sodium flow through the core

- **2** -The average sodium temperature at the outlet of the fuel assembly
- 3-Average sodium temperature at the inlet to the intermediate heat exchanger
- 4 -Average sodium temperature at the outlet of the intermediate heat exchanger



Thermal-hydraulic characteristics of the second circuits

- 1 -The total flow of sodium through the sections of the steam generator
- 2 -Average sodium temperature at the outlet of the intermediate heat exchanger
- 3 -Average temperature of sodium at the outlet of the steam generator sections

# Relative deviations of the results of the thermal-hydraulic characteristics calculating between SOCRAT-BN and design data



Maximum relative deviations of sodium and feed water temperature calculation:

- ✓ the first circuit 1.4%
- ✓ second circuit 3.7%
- ✓ third circuit 0.5%

Maximum relative deviations of sodium and feed water flow calculation:

- ✓ the first circuit 0.7%
- ✓ second circuit 4.5%
- ✓ third circuit 5.1%



1 - The flow of feed water in the steam generator

- 2 -Average temperature of the feed water at the inlet to the steam generator
- 3 -Average steam temperature at the outlet of the steam generator
- 4 -Feed water pressure at the inlet to the steam generator



# Calculation of a severe accident with core elements melting in a sodium cooled reactor

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## The accident modeling



- The design basis accident calculation with blocking of the flow pass section of one FA when the reactor is operating at the nominal power level was performed;
- Blocking of the flow pass section at the inlet part of one FA with MOX pellet fuel was modeled;
- It is postulated that the blocking of the flow pass section of the FA starts from 118 sec from the start of the calculation;
- ≻ Complete blocking of the flow pass section of the FA happens for 120 sec.



#### The accident with blocking of the flow pass section



Coolant flow rate at the outlet of the emergency fuel assembly Coolant temperature at the outlet of the emergency fuel assembly

# The accident with blocking of the flow pass section



Mass of molten fuel and molten steel

- Boiling of sodium in the inter fuel rod space of the FA as a result of blocking the flow pass section happens at 1.78 seconds after the complete blocking of the flow pass section;
- Fuel cladding melting begins at the 4 second after the complete blocking of the flow pass section of the FA;
- Fuel melting begins at the 7 second after the complete blocking of the flow pass section of the FA.

## The accident with blocking of the flow pass section



Distribution of materials in the fuel rods of emergency fuel assembly with MOX pellet fuel

- The change in the mass of the molten fuel and steel of the fuel element cladding during the accident occurs due to the transfer of part of the melt by the sodium flow to the sections of the fuel element with a lower temperature;
- The collapse of the upper layer of the fuel part due to the moving down of fuel and fuel cladding steel occurs at 143 seconds.



# Modeling of severe accidents for lead cooled reactor (BREST)

### Lead cooled reactor core model (BREST)



BALOVNEV, A., DAVYDOV, V., ZHIRNOV, A., KALUGINA, K., MOISEEV, A., UMANSKY, A., SMIRNOV, V., Analysis of reactivity effects in emergency situations with steam entering the core of a lead-cooled fast reactor, Conference of young professionals. Innovations in nuclear energy, JSC "NIKIET", Moscow, 2019.

#### The core of the BREST consists of:

 $\succ$  FA of the central zone (FA CZ) ≻FA of the peripheral zone (FA PZ)  $\succ$  the rods of the control and protection system (CPS) ➤ reflector channels (RC) ≻reflector channels with a passive feedback system (RC with PFS)  $\blacktriangleright$  steel channels of radiation protection (PC)



#### **Neutron-physical model of the core**

#### 1. "Cold" state

- The temperature of the fuel, lead coolant and all constructional elements are set the identical;
- The coolant level in reflector channels with a passive feedback system is set minimum (the space is filled with argon);
- Thermal-hydraulic calculation for this state was not carried out.





#### Neutron-physical model of the core





- 2. Operating ("hot") state
- Nominal level of thermal power is 700 MW;
- The critical state provided by the position of the automatic control rods;
- The level of lead coolant in reflector channels with a passive feedback system is set maximum;
- The temperature distribution is set in accordance with the thermal-hydraulic calculation.

#### **Cross-verification of the reactor calculated values**

#### Deviations cartogram of the calculated results between SERPENT and MCU-BR

- The largest relative energy release deviations are observed in FA with CPS rod with a dysprosium titanate absorber;
- Deviations of the efficiencies of shutdown systems and spatial energy release are not more 7% and 4%, respectively;
- The results obtained demonstrate the correctness of the application of the models developed using the codes
   SERPENT/ATHLET for safety assessment of the lead cooled reactor.





# Calculation of lead cooled reactor under conditions of possible accidents

### **Choice of states for calculations**



The following states were analyzed:

- 1) Core cooling followed by coolant freezing;
- 2) Coolant level changes in the reactor and core;
- 3) Removing (floating) of fuel claddings from the core.

### 1. Cooling of the core with freezing of the coolant



#### **State characteristic**

- Cooling of the core with freezing of the coolant can also occur at the reactor commissioning stage;
- Temperature change (to final temperature 20°C) and coolant density.

#### **Calculation results**

- The introduced positive reactivity reduces the subcriticality of the shutdown reactor for 6.81% from the initial value;
- The efficiency of the CPS rods is sufficient to hold the subcriticality of the reactor.

#### 2. Coolant level change in the reactor and core



#### **Calculation results:**

- The introduced reactivity has a variable character;
- Maximum introduced negative reactivity is -9,17 % δK/K;
- The efficiency of CPS rods is sufficient to maintain the reactor subcriticality in all states with the loss of coolant without changing the configuration of the core.

#### 3. Floating of fuel claddings from the core



#### **State characteristic**

- Lead boiling temperature (1745°C) exceeds the melting temperature of fuel claddings (1400–1500°C) for reactors with a lead coolant;
- Were carried two calculations:
- for seven central FAs (fuel rods number is 2,26% of all fuel rods in the core);
- 2) for all FAs in the central zone (fuel rods number is 61,97% of all fuel rods in the core).

#### **Calculation results**

- When fuel claddings floating up, a positive effect of reactivity is appears;
- The introduced positive reactivity during the melting and floating of the claddings of all fuel rods in the central zone is 2.3% δK/K.

#### Finding:

- 1) More than 2% subcriticality is provided;
- 2) The introduced reactivity can have a significant impact during accidents such as ULOF and UTOP.

1) https://proryv2020.ru/smi/bn-800-sdan-v-promyshlennuyu-ehkspluataciyu

2) The ninth national report of the Russian Federation on the fulfillment of commitments resulting from the convention on nuclear safety. To the Joint Eighth/Ninth Review Meeting of the Contracting Parties under the Convention on Nuclear Safety

# Conclusion

- Calculation models of reactors with sodium and lead coolant have been created
- Cross-verification was carried out to evaluate the calculations of the stationary characteristics of the core
- The results of the calculations confirm the correctness of the developed calculation models for the stationary states and accidents in BN-800 and BREST reactors







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# Thank you for your attention!

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