

IAEA Technical Meeting on Plasma Physics and Technology Aspects of the Tritium Fuel Cycle for Fusion Energy

# Neutral beams and the requirements they place on the fuel cycle

P. Veltri, NB Section ITER Organization

Special Thanks to: U. Fantz, B. Heinemann (IPP), D. Boilson, S. Willms, (IO), E. Sartori (RFX), R. Hemsworth, for fruitful discussions. A. Litvinov, K. Roux (IO) for CAD support

The views and opinions expressed herein do not necessarily reflect those of the ITER Organization

### Introduction

- Neutral are the beams main plasma heating method for present fusion device (They also provide current drive)
- Atom beam production based on the conversion of ions in a gas cell ("Neutralizer")
- For large fusion device like ITER, 1 MeV necessary to access the core of the plasma
- Requirements for ITER NBI extremely demanding





Abs. Valve &

Shutter

25.4 m

Calorimeter

Neutralizer RID

**Beam Source** 

Duct

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### Introduction

- Fuel Cycle consists of vacuum, tritium processing and fueling technologies
- Deuterium-Tritium is circulated through the reactor
- Deuterium is circulated through heating beams
- Tritium is recovered from water and gases



### Fluxes of Gas in the beamline

- D<sub>2</sub> gas in injected in the ion Source to ignite a RF plasma
- D<sub>2</sub> gas in injected in the Neutralizer to convert the ions into neutrals (gas cell)
- D<sub>2</sub> / T<sub>2</sub> gas recycling from tokamak was estimated to be up to 4e20 atoms/second/m2, corresponding to a throughput of 0.88 Pa m3/s (50% T , 50% D) at duct entrance
- Main Concern: the Purity of Gas in the Source, depending on all the above
- Present Requirement: 200 ppm (0.02%) T<sub>2</sub> in D<sub>2</sub>



#### 2.2.2 Gas quality and quantity requirements

[5301s610-R] The gas requirements that shall be considered for one NB Heating and CD System injector for the two phases of operation.

[5301s611] Table 2.2: Gas requirements for one NB Heating and CD System injector for the two phases of operation <sup>(1)</sup>

#### [5301s718]

(1) Refer to interface sheet for exact data. Gas purity requirement to be confirmed by NBTF operation.

	Parameter	Unit	H/He Phase	DD/DT Phase
Ion Source	Gas type		H <sub>2</sub>	D <sub>2</sub>
	Gas flow	Pam <sup>3</sup> /s	5.1	3.6
	Gas purity	Atom %	>99.999% of H2	>99.7% of D.
			<1 PPB of <sup>3</sup> H	<200 PPM of <sup>3</sup> H
			<1 PPM of O <sub>2</sub>	<1 PPM of O <sub>2</sub>
			<10 PPM of N <sub>2</sub>	<10 PPM of N <sub>2</sub>
			<1 PPM of H <sub>2</sub> O	<1 PPM of H <sub>2</sub> O
			<0.001% of other gases	<0.001% of other gases
	Supply pressure (absolute)	MPa	>0.5	>0.5
Neutraliser				
	Gas flow	Pam <sup>3</sup> /s	43	19
	Gas purity	Atom %	>99.9% of H2	>99% of D2
			<1 PPB of <sup>3</sup> H	<1% of <sup>3</sup> H
			<5 PPM of O <sub>2</sub>	<5 PPM of O <sub>2</sub>
			<10 PPM of N <sub>2</sub>	<10 PPM of N <sub>2</sub>
			<5 PPM of H <sub>2</sub> O	<5 PPM of H <sub>2</sub> O
			<0.1% of other gases	<0.1% of other gases
	Supply pressure (absolute)	MPa	0.09 - 0.5	0.09 - 0.5

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- Main Concern: the Purity of Gas in the Source, depending on all the above
- Can be Calculated by Montecarlo Codes (molecular regime)

	D <sub>2</sub>	T <sub>2</sub>	
Pump Capture Coefficient	0.3	0.25	
Qsource (Pa·m3 / s)	3.6	0.00072	
Qneutralizer (Pa·m3 / s)	19	0.19	
QTokamak	0.44	0.44	





Horizontal section - rear view of the simulated cryomodule, colours by flux of impinging particles at pumping surfaces and pressure at solid surfaces.



(a) Pumping speed and (b) capture probability of the cryopanels calculated with Avocado model as a function of the charcoal sticking probability

- Cryopumps too complex: one can use a sub model to obtain the capture probability [1] starting from the geometry and the sticking probability of charcoal, known from experiments[2] $\rightarrow$  about 0.3, and scales with mass
- In addition to cryopumps the duct exit toward ITER VV is also pumping, with sticking=1

[1] E. Sartori et al. RFX-MITICA-TN 147 rev2 (2014)

[2] M. Dremel, C. Day, S. Hanke, X. Luo, Cryopump design development for the ITER Neutral Beam

Injectors, Fusion Engineering and Design 84 (2009) 689–693

### D<sub>2</sub> / T<sub>2</sub> Distribution Along the Beamline

- T<sub>2</sub> From Tokamak Negligible
- T<sub>2</sub> From Source filling line reflect the set purity (200 ppm)
- T<sub>2</sub> From Neutralizer contribute to 600 ppm in the ion source
- Source-Neutralizer Fluxes could be slightly different
- T<sub>2</sub> from Neutralizer 0.05-0.1% > 0.02%

	D <sub>2</sub>	T <sub>2</sub>
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### **Tritium traces in Positive ion sources**

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In principle the use of T instead of D/H affect the source performances (arc efficiency,...), but not at low fraction



Prior to D-T experiment at JET, a campaign with T traces in D2 (1% doping) were carried out at JET positive ions injectors of  $D_2$  [1] **Result:** 

"PINI operation with such a gas mixture did not require any specific commissioning, since at such a low tritium concentration the PINI operating characteristics are indistinguishable from those of pure deuterium."

T. Jones et al. JET report: JET-P(99)08

#### BUT

Of course the physics involved in positive ions sources is much simpler than for H- sources....

### **Negative ion sources: Why?**

- Large Fusion devices requires the beam to travel long distances into the plasma
- In the case of ITER, efficient beam absorption requires D<sup>0</sup> Energy in the 1 MeV range
- Negative ions are mandatory!

Main Consequences:

- H-/D- generation much more challenging than H+/D+
- H-/D- are fragile, destroyed by hot e- in the plasma
- Their extraction from the source is accompanied by Co-extracted electrons (see later)



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### **Negative ion Generation**

- Negative ions are (mainly) created by surface conversion of atoms / positive ions on plasma facing materials
- Need electrons! Electrons in a solid are confined by the ions charge and cannot escape
  - When the electron affinity  $E_a$  of the atom is  $E_a > \phi$  (work function) the probability that an electron is captured from the surface and a negative ion is formed is enhanced:







- $E_a$  of H- / D- is around 0.75 eV
- Coverage of alkali metals on source wall lowers the work function
- Cs has the lowest work function (2.2 eV) and is the best electron donor

### **Negative ion sources: Cs dynamic**

- Small quantity of Caesium vapor injected in the source by temperature controlled Cs ovens
- Caesium is transported and re-distributed by the plasma
- The work function of surfaces (PG electrode, in Moly-coated Cu) is reduced (≈pure Cs)
- Negative ion production dramatically enhanced  $\rightarrow$  "ion-ion plasma"
- <u>Co-extracted electrons reduced</u>

#### Practical Usage:

- Source Conditioning needed  $\rightarrow$  several plasma pulses to re-distribute Cs
- Plasma grid temperature @ 100°- 250° ", source body temperature at > 35° to avoid trapping of Cs on the walls
- Cs is highly reactive! Requires an impurity-free environment (O<sub>2</sub>, ...)





D. Faircloth, ISIS, CERN Acc. School on Ion Sources, 2012

### **Negative ion sources: Isotope Effect**

Operation of the sources in  $D_2$  plasma much more challenging than operation in  $H_2$  plasma:

- Co-extracted electron current increases
  - At high power (ITER source to be operated at 80-100 kW/driver)
  - in time (issue for long pulses)
- Saturation of extracted current (j<sub>EX</sub>)
- D<sub>2</sub> Operation accompanied by higher Cs densities in the plasma
- $\rightarrow$  Root cause seems to be linked with degradation of the Cs layer (enhanced Sputtering?)

Position of caesium oven Diagnostic ports

Experimental DATA from ELISE ion source @ IPP Garching



D. Wünderlich et al 2021 Nucl. Fusion **61** 096023



D. Wünderlich et al. Rev. Sci. Instrum. 90, 113304 (2019)

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### **Negative ion sources: Isotope Effect**

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H<sub>2</sub> doping tests at BATMAN test bed in IPP [1]: H<sub>2</sub> plasma with D<sub>2</sub> doping (6%, 15%, 28%)



#### CAVEATS:

- The study was done for  $D_2$  doping in  $H_2$  (effect of  $T_2$  in  $D_2$  might be different)
- It is at relatively high pressure (test done at 0.4 and 0.7 Pa)
- These results were obtained when the Cs content in the oven was low,

#### RESULTS

- At 6% experiments were done by adding 6% D<sub>2</sub> to baseline pressure of H<sub>2</sub>. → Effects of doping might be hidden by those related to overall pressure increase (for example: electron current decrease)
- Test with constant pressure were only done of higher D fraction → "A proportion of 15% of deuterium shows a slight reduction of the extracted negative ion current and a moderate increase of the co-extracted electrons."

0.02% Seems really too stringent  $\rightarrow$  Relaxation by a factor 10-20 is acceptable (from now on I will assume 0.2%)





Figure 7: Variation of the extracted H and the  $j_e/jH$  as a function of the deuterium proportion during one day. The measured Cs evaporation rate is also plotted.

[1] IPP-FinalReportPRIMA-WP13v1

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### **Power Loading Considerations: Beam fraction evolutions**

- Assuming equal ionization/dissociation/negative ion yield as per D<sub>2</sub>, a T<sup>-</sup> beam having 0.2% of D- current (60 A) is extracted/accelerated
- Beam interact with the background gas in the beamline: losses
- With the gas profile and the cross sections we can evaluate the beam fractions at any point along the beamline



- cross section from ORNL Redbook (Barnet 1990)
- Electron capture process can be neglected (very minor effect)  $\rightarrow$  H- can only be destroyed

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	Fraction <sup>1</sup>	Lost Current/Power <sup>2</sup>
	(%)	(mA/kW)
Extracted Beam Current T-		120
Lost in The Accelerator	34%	40.8
Lost at RID (A)	29%	35.2
Lost In the Duct,	9%	11.2
Injected in ITER	27%	32.8



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### **Power Loading Considerations: Power on the Duct**

Beam interact with the background gas in the beamline: losses Stripping  $\rightarrow$  T<sup>+</sup>/T<sup>0</sup> lost in Source/Accelerator Neutralization  $\rightarrow$  T<sup>+</sup>/T<sup>-</sup> lost at RID Re-Ionization  $\rightarrow$  T<sup>+</sup> Lost along beamline, duct...

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<sup>1</sup>These are fractions of the Extracted current. Typically fractions of the accelerated current are used <sup>2</sup>for a 60A, 1 MeV D- beam

DLM RIGHT (Tot Power: 87 kW) Power density (MW/m<sup>2</sup>) 0.3 0.25 0.2 0.15 0.1 0.05 0 -0.5 z (m) -1.5 19 20 21 22 23 24 x (m)

Power Loading on NB Duct (Worst Case)

#### DLM LEFT (Tot Power: 69 kW)



Power Loading on NB Duct for three B field Scenarios



 Duct liner is already cooled almost everywhere to cope with re-ionized power at different B fields

 Power loading on Front end Components to be checked

### **Tritium Implantation and Retention: RID**

- Part of the accelerated T beam impact with surfaces with non negligible probability to be implanted.
- $T^+/T^-$  fluxes on RID,  $T^+/T_2^+T_3^+$  back-streaming towards the source
- Let's take the RID case. TRIM calculation [1] shows that the implantation fraction for D at 1 MeV on copper is >90%. Should be similar for T.
- Fraction for T+/T- on RID are similar, therefore an ionic tritium flux of about 2.5e17 s<sup>-1</sup> particles are therefore implanted in the RID. → This would correspond to 40 g over ITER lifetime.
- Similar Amount on Calorimeter, but for much shorter time (only conditioning).

	Fraction	Particle	tot in ITER
	(%)	Flux (1/s)	Lifetime (g)
Lost in The Accelerator	34%	2.5E+17	49.0
Lost at RID (A)	29%	2.2E+17	42.2
Lost In the Duct	9%	7.0E+16	13.4
Injected in ITER	27%	2.0E+17	39.4





[1] C. Hopf, TRIM calculation of D and H beam on copper (ITER IDM ref.: 4HDWTC)

### **Tritium Implantation and Retention: The case of the RID**

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#### BUT

- a saturation in the material should be reached earlier  $\rightarrow$  T ion/atoms recombine in molecules and are released from metal
- Studied for T saturation at JET suggest 20% saturation in atomic density [2] on Copper
- Rough calculation with the figures above and assuming the impact surface on RID panels, and implantation depth of 1 micron → Saturation at 0.5-1 g of accumulated tritium
- Another Example: Back streaming ions can also be implanted in the ion source but flux is smaller: 1.2e16 s<sup>-1</sup>
- Positive T flux from beam-gas interaction in the accelerator about 1e16 s<sup>-1</sup>. Large part back-streams
- Positive T flux from beam-plasma in the Neutralizer can be calculated from Bohm velocity from plasma density and Te (1e14, 3 eV $\rightarrow$  2e15 s<sup>-1</sup>

C. Hopf, TRIM calculation of D and H beam on copper (ITER IDM ref.: 4HDWTC)
T.T.C. Jones et al. / Fusion Engineering and Design 47 (1999) 205–231



### **Tritium Implantation and Retention: "Clean-up"**

• Experimental results from JET "PTE" experiment showed that the use of D and H beams after the T-beam campaign effectively "clean-up" surfaces from T. For example in [1] it is concluded that *"The implanted tritium can be removed by operating the injector using a different isotope."* 



- Penetration depth is different, then cleanup is not 100%,
- The position of impact at RID is the same for D/T, then clean-up is effective  $\rightarrow$  retained quantity is decreased
- In the source back-streaming ions fall at slightly different location (mv/B) on the source back plate → cleanup less effective
- Also along duct and FECs the positions of implantation differ but these components will be anyway activated

[1] H-D Falter et al., Implantation and desorption of tritium and tritium recovery from the JET neutral beam injectors, J. Nucl. Mater. 196 1992

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- Present Requirement for Gas purity in the ion Source NBIs (<200 PPM of T<sub>2</sub>) of are probably too stringent
- The number was set on the basis of the concern on:
  - Degradation of source performances (co-extracted electrons)
  - Location of Power loading of re-ionized T+ atoms
- Experiment at IPP show that fraction at about 0.2-0.5% are probably acceptable.
- T ion implantation would happen in the in-vessel component of the NBIs (Ion Source, RID, Neutralizer) increasing the nuclear dose there. Qualitative consideration suggest that this would not be a serious issue, but more detailed calculation are advisable
- None of the point above justifies the present requirement on gas purity
- A relaxation by an order of magnitude is quite possible (up to 0.2%), that is <u>still challenging for the Isotope Separation</u> <u>System!</u>

## Thank you!



### **Implantation of Tritium and clean-up**

"Beam-target emission could be successfully described by a 'local mixing model' taking into account the stopping function of the incident particles.

- This model assumes that the local concentration of hydrogen isotopes cannot exceed a given saturation level (which is dependent upon temperature).
- When the saturation level is reached locally, one hydrogen atom is released for every incoming atom which stops at that particular location; the probability that the released atom is of a given isotope is assumed to reflect the local isotopic mix.
- The displaced atom is assumed to diffuse rapidly to the surface without being trapped in any adjacent non-saturated region; at the surface it is assumed eventually to re-combine to form a molecule and to leave the material.
- The local saturation density of all the hydrogen isotopes implanted in the Cu material was taken to be 20%

[...] It is therefore concluded that up to 20% of the initial tritium content of the calorimeter panels is retained at the end of the clean-up phase. In order to scavenge this residual tritium content, it would be necessary to employ deuterium beams with at least 20% HIGHER ENERGY"



Fig. 19. Tritium implantation profile at the start and end of the cleanup phase of operation, and the average range of implantation of deuterium ions as a function of incident energy.

T.T.C. Jones et al. / Fusion Engineering and Design 47 (1999) 205–231