







Model advancements in mean-field plasma edge codes to enable computationally achievable simulations of the ITER and DEMO reactors

M. Baelmans¹, W. Dekeyser¹, N. Horsten¹, R. Coosemans¹, W. Van Uytven¹, M. Blommaert¹, S. Carli¹, V. Maes², B. Mortier², G. Samaey²

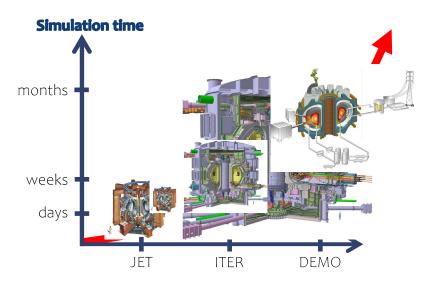
¹KU Leuven, Department of Mechanical Engineering, Leuven, Belgium ²KU Leuven, Department of Computer Science, Leuven, Belgium

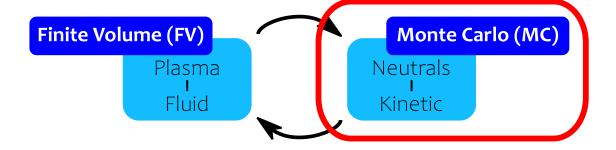




Important issues with mean-field plasma edge simulations

1. Simulation time with kinetic neutral model strongly increases for reactor-scale devices



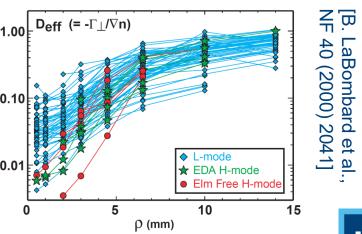


Intense plasma-neutral interactions for detached divertor conditions

2. Ad-hoc model for anomalous turbulent transport

Simple anomalous transport assumptions (constant coefficients; radial profile; ...) vs. complex poloidal transport behavior

Dependence on plasma regime/conditions?

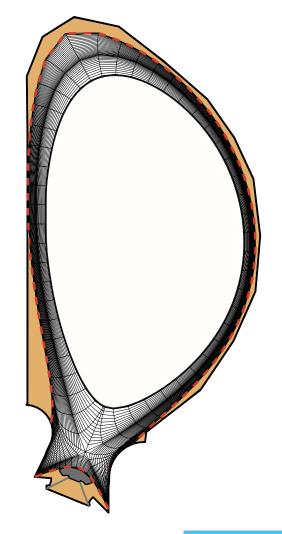


Important issues with mean-field plasma edge simulations (2)

3. Plasma mesh typically does not extend to the vessel wall

Ad-hoc boundary conditions at limiting flux surface

No realistic (far-SOL) background for neutrals, and erosion, migration and redeposition studies





- Introduction
- Speed-up of simulations with fluid and hybrid neutral models
- Self-consistent anomalous transport models
- Extending grids to the vessel wall
- Conclusions & perspectives for DEMO



- Introduction
- Speed-up of simulations with fluid and hybrid neutral models
- Self-consistent anomalous transport models
- Extending grids to the vessel wall
- Conclusions & perspectives for DEMO



Hierarchy of neutral models

Performance

Purely fluid

Improvement of existing fluid neutral models

Advanced Fluid Neutral (AFN) models

Purely fluid

Combination of fluid and kinetic descriptions

More accurate than fluid faster than kinetic

Faster than kinetic

Fully kinetic

Most complete description; 'reference'



- Introduction
- Speed-up of simulations with fluid and hybrid neutral models
 - Advanced Fluid Neutral (AFN) models
 - Hybrid neutral models
- Self-consistent anomalous transport models
- Extending grids to the vessel wall
- Conclusions & perspectives for DEMO



AFN models more consistent with kinetic counterpart [N. Horsten et al., NF 57 (2017) 116043]

Equilibration by dominant CX process – no tuning parameters!

1. Boundary conditions: impose macroscopic neutral moment fluxes (moments $\mu(\mathbf{v}) \rightarrow$ particle, momentum and energy)

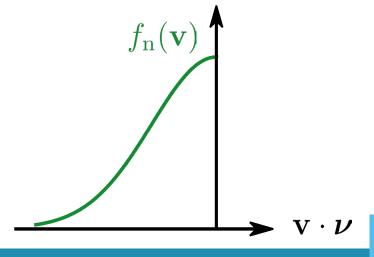
$$\Gamma_{\mathbf{n}} = \int_{\mathbf{v} \cdot \boldsymbol{\nu} < 0} \boldsymbol{\mu}(\mathbf{v}) f_{\mathbf{n}}(\mathbf{v}) (\mathbf{v} \cdot \boldsymbol{\nu}) d\mathbf{v} \qquad \longrightarrow \text{Incident part}$$

$$- \int_{\mathbf{v} \cdot \boldsymbol{\nu} > 0} \boldsymbol{\mu}(\mathbf{v}) \int_{\mathbf{v}' \cdot \boldsymbol{\nu} < 0} R(\mathbf{v}' \to \mathbf{v}) f_{\mathbf{i}}(\mathbf{v}') + f_{\mathbf{n}}(\mathbf{v}')) (\mathbf{v}' \cdot \boldsymbol{\nu}) d\mathbf{v}' \longrightarrow \underset{\text{reflected part}}{\mathsf{Recycled}}$$

- V Particle velocity vector
- ν Surface normal (pointing inward the plasma domain)

reflection database

- $f_i(\mathbf{v})$ Ion distribution \rightarrow Maxwellian (possibly accelerated by sheath)
- $f_{\rm n}({\bf v})$ Neutral distribution \rightarrow assumed to be a Maxwellian for incident neutrals



AFN models more consistent with kinetic counterpart (2)

[N. Horsten et al., NF 57 (2017) 116043]

2. Transport coefficients: derived from AMJUEL/HYDHEL databases

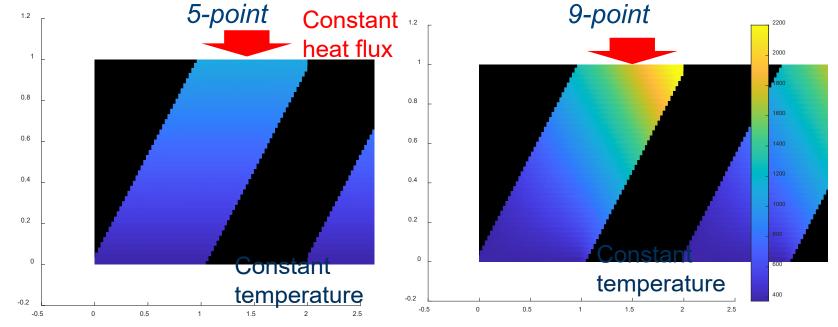
3. 9-point stencil: improved numerical solution

[W. Dekeyser et al., NME 18 (2019) 125-1307

E.g. effect for simple heat conduction equation



Required by isotropic character of neutrals!





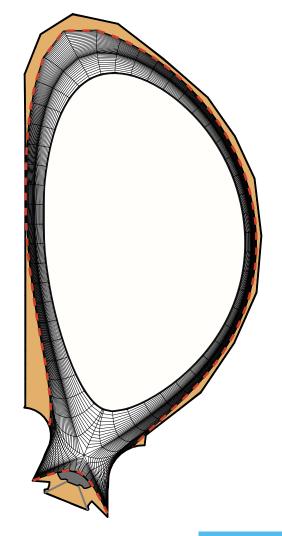
Remaining shortfalls of AFN models

1. No transport in void regions

2. Only hydrogenic atoms: molecules and impurities do typically not reach the fluid limit

Fluid – kinetic comparison in next slides: **ITER case** with only D atoms without voids and no drifts

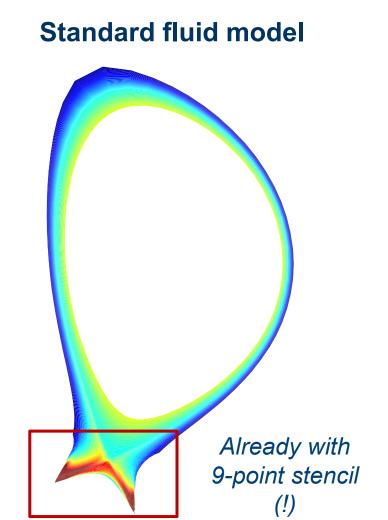
Molecules are assumed to dissociate at the surface → Resulting atoms get energy of 2 eV (Franck-Condon dissociation)

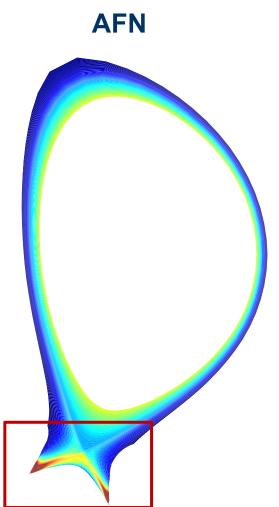


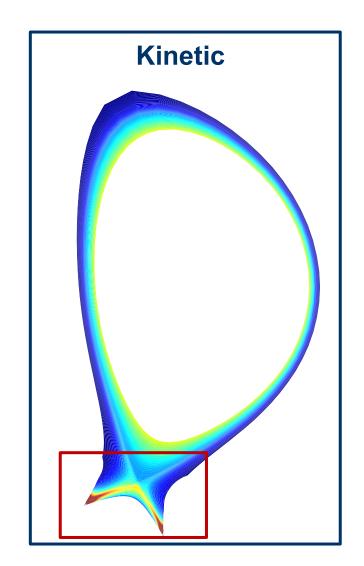


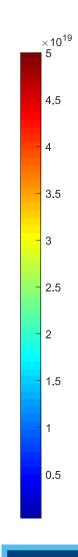
AFN model significantly reduces fluid-kinetic discrepancies

[W. Van Uytven et al., NF 62 (2022) 086023]







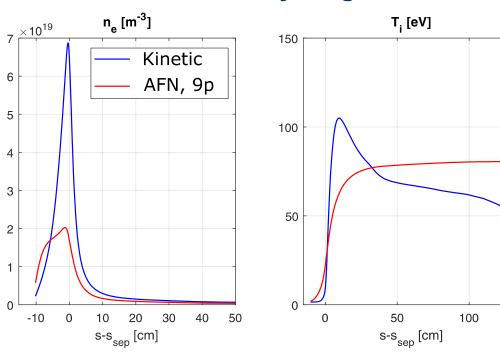




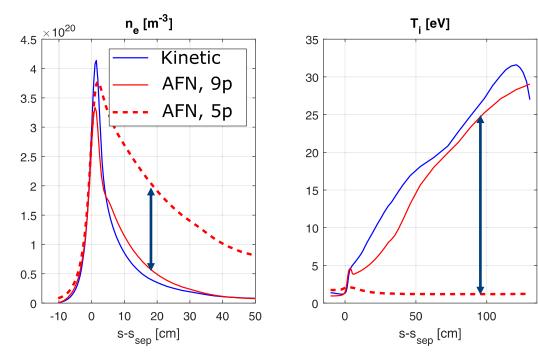
Fluid approximation becomes valid for high-recycling conditions

[W. Van Uytven et al., NF 62 (2022) 086023]

Low recycling



High recycling



Effect of 9-point stencil!



Further improvements with hybrid approach



- Introduction
- Speed-up of simulations with fluid and hybrid neutral models
 - Advanced Fluid Neutral (AFN) models
 - Hybrid neutral models
- Self-consistent anomalous transport models
- Extending grids to the vessel wall
- Conclusions & perspectives for DEMO



Methods in plasma edge neutral community

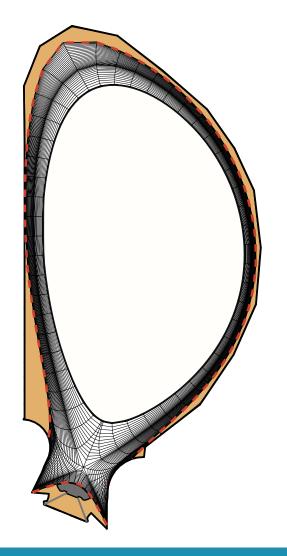
- Spatially hybrid [M. Blommaert et al., NME 19 (2019) 28-33]
- Evaporation/condensation [M. Valentinuzzi et al., NME 18 (2019) 41-45]
- Micro-macro decomposition [N. Horsten et al., JCP 409 (2020) 109308]
- Kinetic-diffusion Monte Carlo schemes [B. Mortier et al., CPP 60 (2020) e201900134]

Combined in [W. Van Uytven et al., CPP (2022) e202100191]

This presentation



Hybrid approach includes void regions and a fully kinetic treatment for the molecules



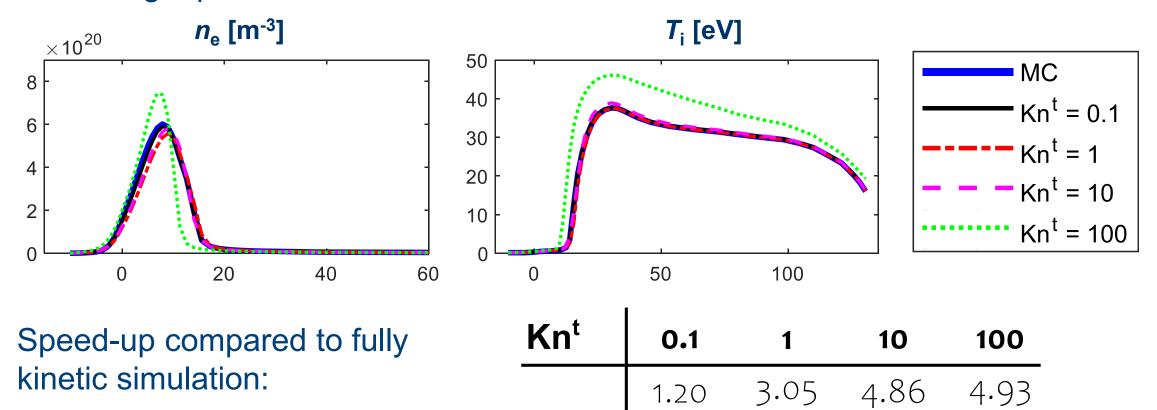
- Void regions: fully kinetic treatment of neutrals by sampling at the plasma-void interfaces
- Plasma fluid grid: atoms are transferred from the kinetic to fluid population when

$$Kn^{
m p} < Kn^{
m t}$$
Local particle
User-defined
Knudsen number
User-defined

Fully kinetic treatment of molecules in the whole domain

Hybrid model with $Kn^t = 10$ gives accurate results with factor 5 speed-up

Outer target profiles:



Speed-up still limited due to fully kinetic treatment of molecules!



- Introduction
- Speed-up of simulations with fluid and hybrid neutral models
- Self-consistent anomalous transport models
- Extending grids to the vessel wall
- Conclusions & perspectives for DEMO



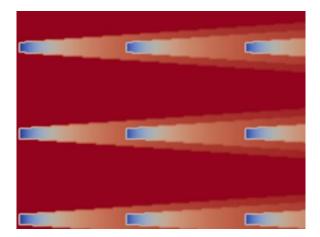
Hydrodynamic turbulence

Wide range of simulation strategies...

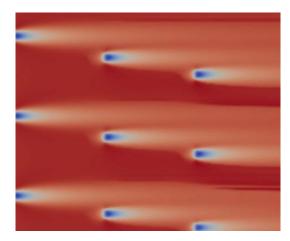
Model accuracy

Computational efficiency

Analytical models

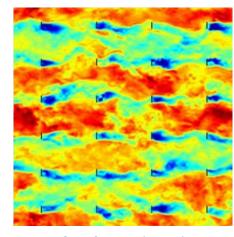


Reynolds-Averaged Navier-Stokes (RANS)



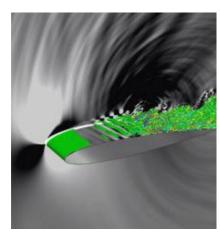
[Schmidt (2014)]

Large-Eddy Simulation (LES)



[Calaf et al. (2010)]

Direct Numerical Simulation (DNS)

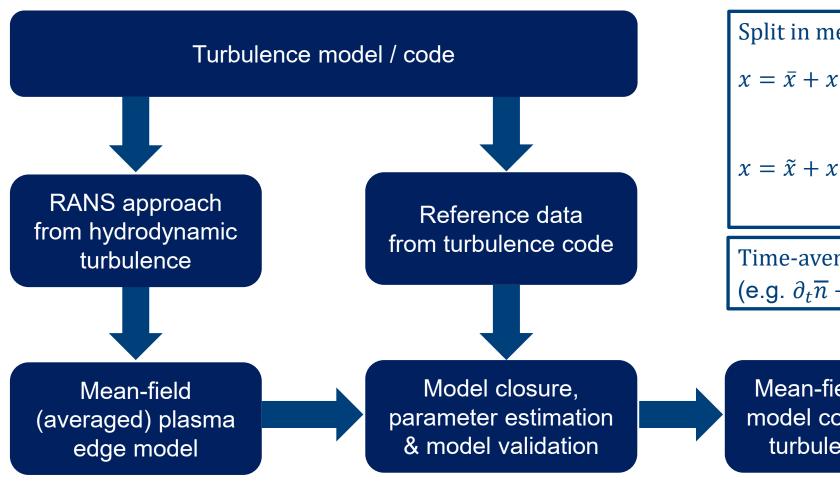


[Sandberg & Jones (2011)]





Approach



Split in mean + fluctuating components

$$x = \bar{x} + x', \qquad \bar{x} = \lim_{T \to \infty} \frac{1}{T} \int_0^T x dt$$

$$x = \tilde{x} + x'', \qquad \tilde{x} = \frac{\overline{nx}}{\overline{n}}$$

Time-average governing equations (e.g. $\partial_t \overline{n} + \nabla \cdot \overline{\Gamma} = \overline{S}$)

Mean-field transport model consistent with turbulence model



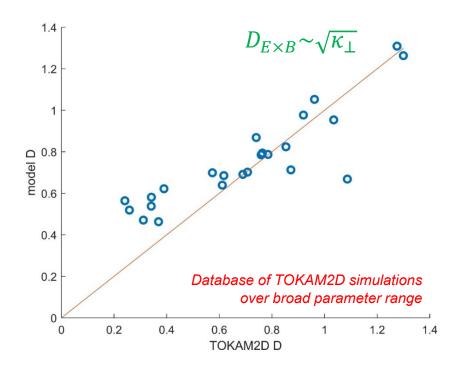
RANS approach for electrostatic interchange turbulence

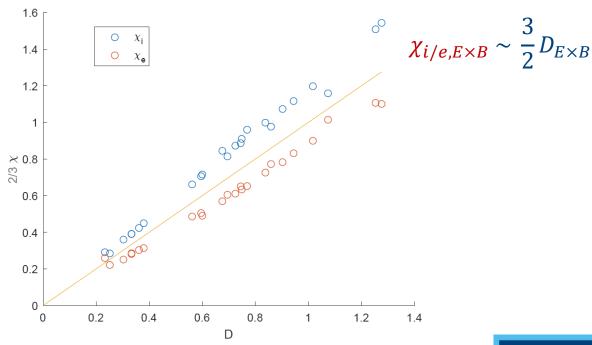
• Average fluxes, electrostatic turbulence: fluctuating $E \times B$ -terms need closure

$$\circ \quad \overline{\Gamma}_{i/e,E\times B} = \overline{n_i' u_{E\times B}'} \quad \sim -D_{E\times B} \nabla_{\perp} \overline{n}_i$$

- Proposal: relate to turbulent kinetic energy κ_{\perp} as measure of local intensity of the turbulence/transport
- Diffusive transport model based on 2D interchange simulations [Coosemans et al., CPP 2022, e202100193.]

$$D_{E\times B}=C_D\rho_L\sqrt{\frac{\kappa_\perp}{m_i}}$$







Sources and transport of κ_{\perp} for interchange turbulence

[R. Coosemans, PhD thesis, 2022]

[1e5 Wm⁻³]

• Transport equation for κ_{\perp} for 2D electrostatic interchange turbulence

$$\frac{\partial}{\partial t} \bar{n} \kappa_{\perp} + \nabla \cdot \left(\overline{\Gamma}_{i} \kappa_{\perp} + \overline{\phi' J'_{||}} \right) = \overline{S}_{IC} + \overline{S}_{||} + \overline{S}_{RS}$$

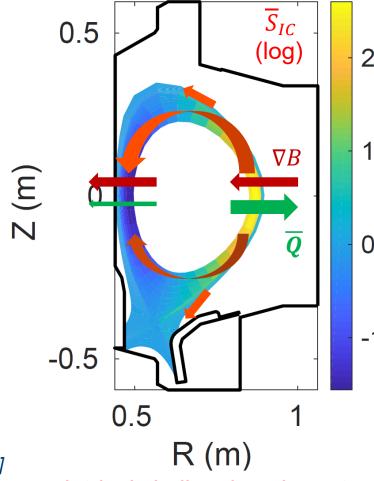
Total heat flux due to $E \times B$ fluctuations drives production of κ_{\perp} [Coosemans et al., CPP 2022, e202100193.]

$$\overline{S}_{IC} = -\frac{2}{3}\overline{\boldsymbol{Q}}_{i+e,E\times B} \cdot \nabla \ln B^2$$
 (exact)

- Source in 'bad-curvature' regions, sink in 'good-curvature' regions
- \circ Parallel transport of κ_{\perp} governed by plasma conductivity
 - Strongly exceeds parallel convection with $\tilde{u}_{||}!$
- Turbulence suppression due to flow shear: negative viscosity model

...coupled to 'regular' mean field equations [Dekeyser et al., CPP 2022, e202100190.]





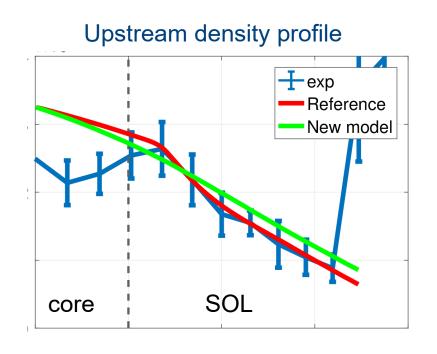
Intrinsic ballooning character and 'self-saturation'

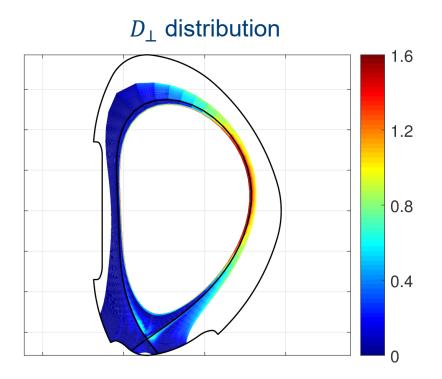


First comparison to experiments: COMPASS

[S. Carli et al., CPP 60 (2020) e201900155.]

- Promising results w.r.t. reference case and experiment, despite 'crude' dissipation model
- Ballooning nature of transport retrieved

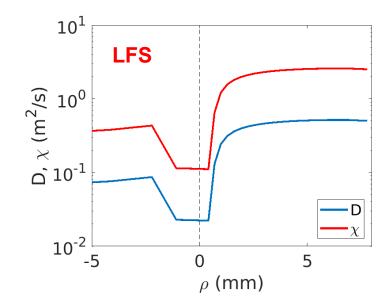


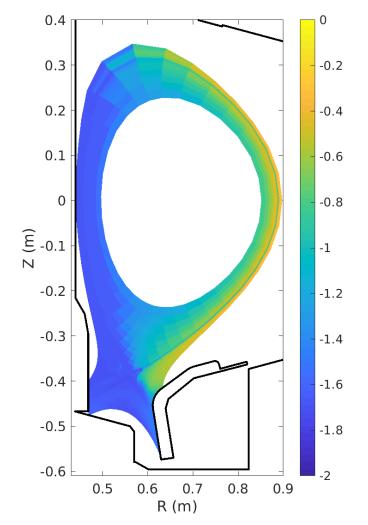




First comparison to experiments: C-Mod [W. Dekeyser, PSI-25, Jeju, Korea, 2022.]

- With few parameters, the RANS-model can reproduce radial transport coefficients at the LFS midplane similar to those found through manual tuning...
 - ...but now providing also full poloidal description, incl. suppression at HFS & separatrix!
 - ...consistent variation with regime (?)



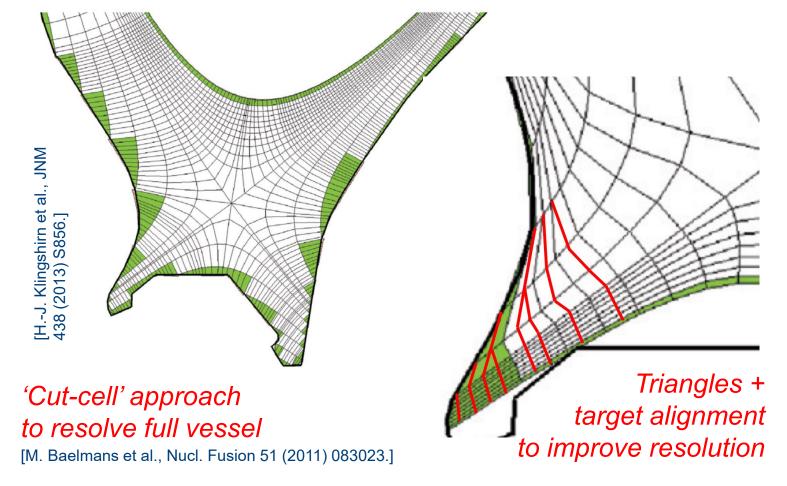


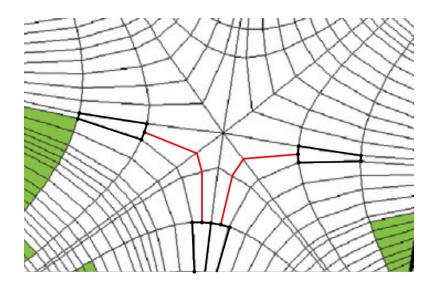


- Introduction
- Speed-up of simulations with fluid and hybrid neutral models
- Self-consistent anomalous transport models
- Extending grids to the vessel wall
- Conclusions & perspectives for DEMO



New unstructured finite volume solver for SOLPS-ITER





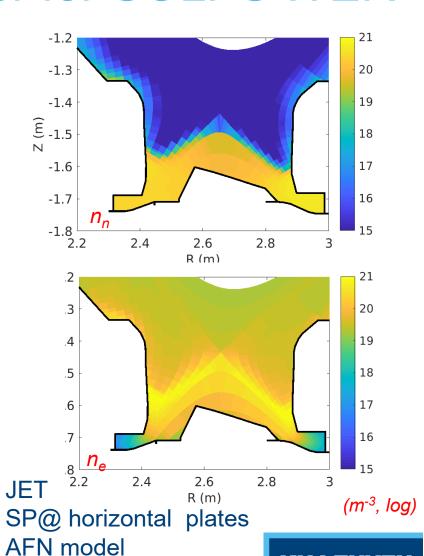
Improved resolution at X-point using pentagonal cells

Large grid flexibility needed to meet conflicting resolution requirements ⇒ choice for unstructured FV solver (*)



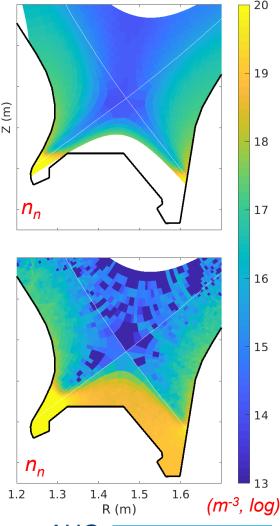
New unstructured finite volume solver for SOLPS-ITER

- Arbitrary poloidal grid and cell topologies now possible (toroidally symmetric)
 - SN, DN, limiter,....
 - Advanced Divertor Configurations (multiple X- and O-points,...)
 - New configurations, e.g. without confined plasma, enabled
- Grid generation
 - Carre2 restricted to 'standard' configurations (SN, DN)
 - Flexible TIARA grid generator under development @ ITER



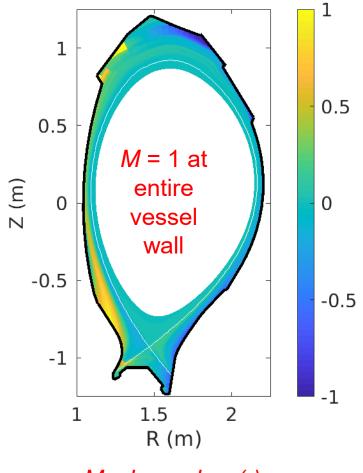
Status extended grids version of SOLPS-ITER

- Extended grids functionality implemented for default SOLPS-ITER model (model based on v3.0.6)
 - Incl. drifts and currents
 - Solver verified on various cases, incl. MMS
- Fully backwards compatible* with v3.0.6 for default model options on existing, non-extended, structured grids
 - *except for bugfixes, implicit geometry assumptions, and when not using improved stencil
- New features available
 - Improved numerical schemes (in particular, 9-point stencil)
 - Advanced fluid and hybrid neutral models
 - Anomalous transport models based on RANS approach
 - o Parameter estimation and optimization framework (see talk W. Dekeyser)

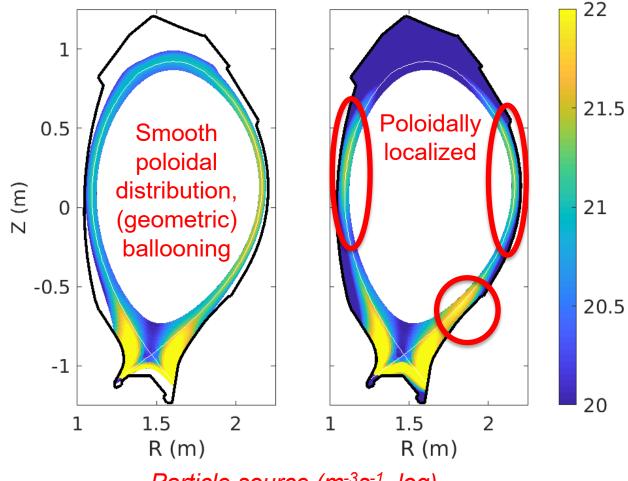




Poloidally localized MC recycling [W. Dekeyser et al., NME 27 (2021) 100999.]



Mach number (-)

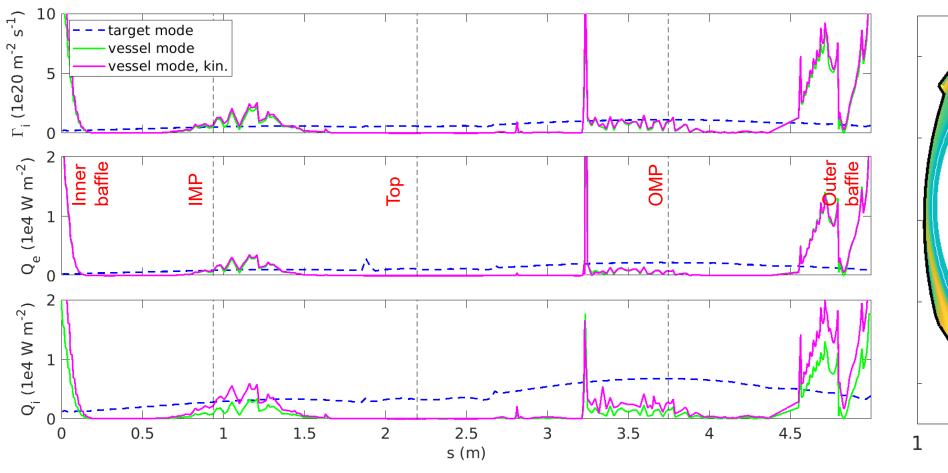


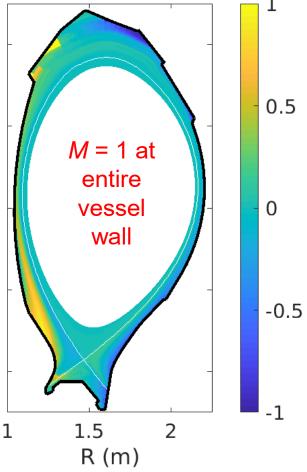
Particle source (m⁻³s⁻¹, log)



Simulation of wall fluxes

[W. Dekeyser et al., NME 27 (2021) 100999.]







- Introduction
- Speed-up of simulations with fluid and hybrid neutral models
- Self-consistent anomalous transport models
- Extending grids to the vessel wall
- Conclusions & perspectives for DEMO



Conclusions

- Advanced fluid and hybrid neutral models can provide significant speed-up compared to fully kinetic simulations of reactors
 - AFN qualitatively correct for high-density conditions
 - Hybrid approach able to correct remaining fluid-kinetic discrepancies
- Anomalous transport models based on RANS-approach may provide consistent description of mean field transport mechanisms (parallel, drifts, anomalous)
 - Some basic transport features (ballooning) reproduced inherently by the models
 - Successful first comparisons to experiment
- Simulations up to the wall enabled with SOLPS-ITER
 - o Providing consistent plasma backgrounds for erosion studies
 - Facilitating far-SOL transport studies



Challenges and perspectives for DEMO

- Advanced fluid and hybrid neutral models
 - Ready to be applied to DEMO
 - Even more accurate results expected due to increased ion-neutral collisionality
 - Speed-up limited by fully kinetic treatment of molecules → fluid/hybrid model, e.g. [A. Holm, et al., NME 19 (2019) 143-148]
- Extension of RANS models towards reactor-relevant turbulence regimes
 - o Improved description of impact fluctuations in parallel direction (in particular, *drift waves*)
 - Effect of neutrals and recycling conditions
 - Extensive model validation & calibration needed (incl. 3D turbulence simulations)
- Extended grids
 - Potential to provide consistent plasma backgrounds for various reactor studies
 - Combination with AFN models may further reduce fluid-kinetic discrepancies by removing the voids
 ⇒ extended range of applicability of AFN?



Challenges and perspectives for DEMO

- Rigorous model validation framework:
 - Combining data & errors from all available diagnostics
 - Estimating the error bars on the unknown model parameters
 - Propagating expected model errors to DEMO predictions
- Do we have sufficient experimental data to validate/extrapolate all the model aspects? E.g.
 - 2D (poloidal-radial) resolved data?
 - Turbulence characteristics for the RANS models?
 - 0 ...
- Can we fill some gaps by calibrating parameters with scaling laws?



KU LEUVEN



Thank you! Questions?

