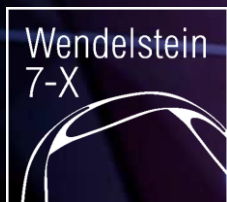
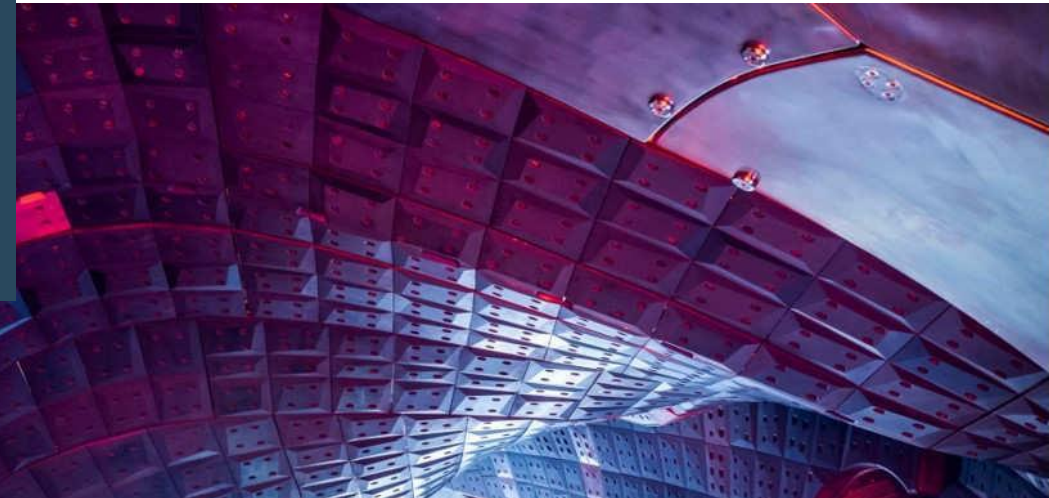


# Complete H fuel cycle with the island divertor in Wendelstein 7-X



EUROfusion

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# Outline



- **Why do we need a divertor?**
- **Wendelstein 7-X – Magnetic field and island divertor**
- **H fuel cycle**
- **Detachment**
- **Conclusion on particle exhaust at W7-X**
- **Extrapolate design criteria**

Disclaimer: All experiments shown with

- Standard configuration
- Pure ECRH heating
- Pure gas fueling
- Boronized wall

# Why do we need a divertor? Particle control!

## Reactor perspective – He concentration shrinks operational space

- He produced in a reactor, has to be removed
- Depending on assumed concentration of additional impurities  $\rho$  must be less than 10-15, the lower the better

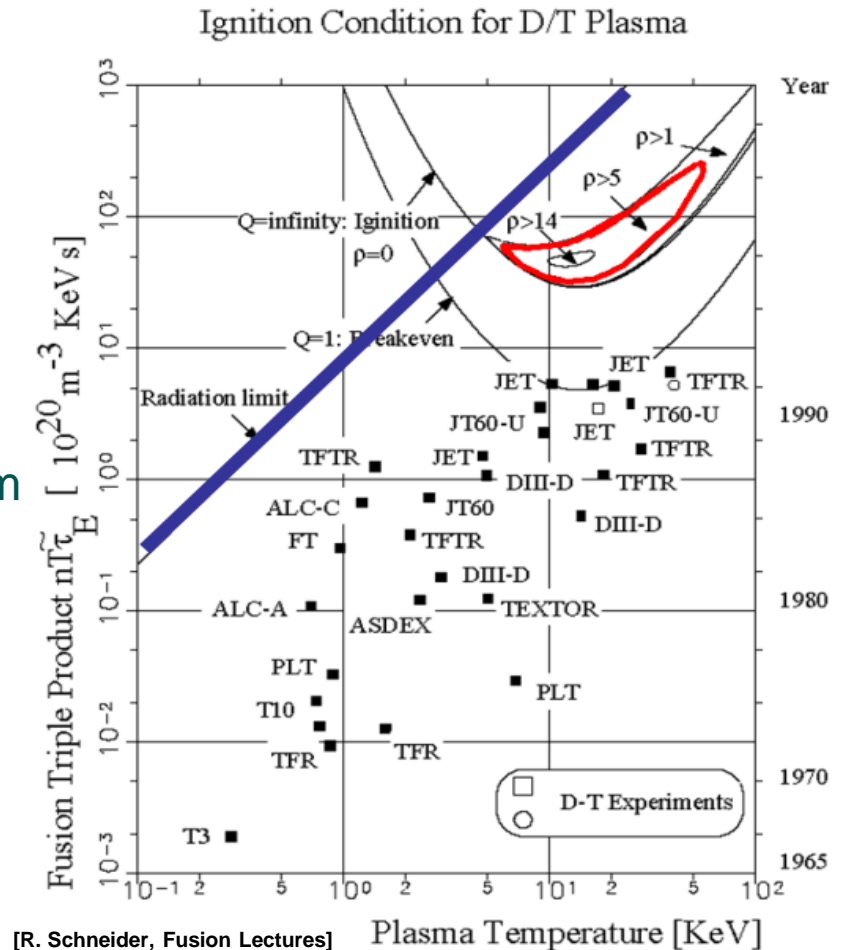
$$\rho = \frac{\tau_{\alpha}^*}{\tau_E}$$

## Operational perspective – Density control

- Particle exhaust > wall source ➡ wall independent density
- Particle exhaust = Particle source ➡ stable density in equilibrium
- Flat profiles ➡ Particle exhaust = Wall source
- Peaked profiles ➡ Particle exhaust = Core + Wall source

## Only neutral particles can be removed

- Target to intercept, neutralize and exhaust particle flux ➡ Divertor



# Divertor requirements and metrics



Reactor requirements: Exhaust enough particles to keep  $\rho < 10\text{-}15$

$$\Gamma_{\text{He-Exhaust}} = \Gamma_{\text{He-Fusion}}$$

Particle exhaust	- $\Gamma_{\text{Exhaust}} / \Gamma_{\text{Ion Divertor}} = \eta_{\text{exhaust}}$
Particle collection	- $\Gamma_{\text{Pumpgap}} / \Gamma_{\text{Ion Divertor}} = \eta_{\text{collection}}$
Particle removal	- $\Gamma_{\text{Exhaust}} / \Gamma_{\text{Pumpgap}} = \eta_{\text{removal}}$
Particle plugging	- $\Gamma_{\text{Divertor Recycling}} / \Gamma_{\text{Recycling}} = \eta_{\text{plugging}}$

Covered in this Talk

## Impurity control

- Keep confined plasma clean

Minimize erosion

-  $T_e < 5 \text{ eV}$

Erosion away from LCFS

- Divertor > Limiter

## Subsequent requirements:

### Heat load control/exhaust

< 10 MW/m<sup>2</sup>

- Detachment?

Shallow incidence angles; Avoid leading edges

### Material science

Low activation

Tolerance to high displacements per atom



# Wendelstein 7-X – Magnetic field and divertor

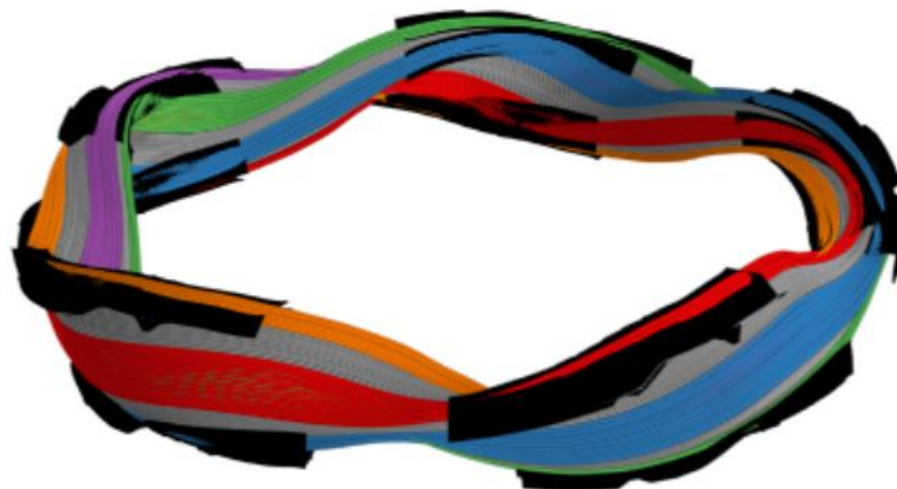
# Magnetic islands form interface for the divertor

Magnetic islands twist around the central plasma and connect the different divertor modules

[V. Perseo]

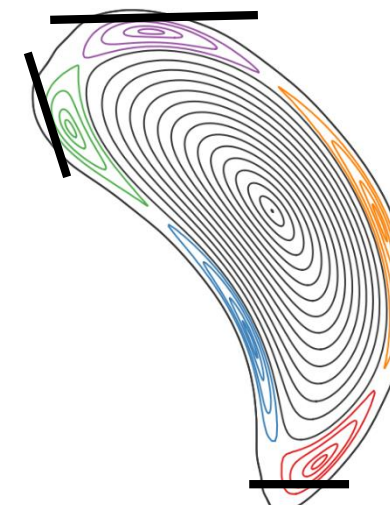
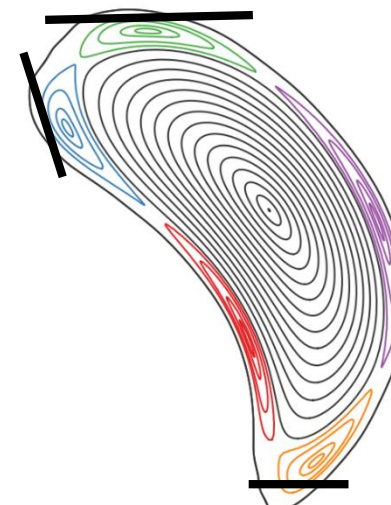
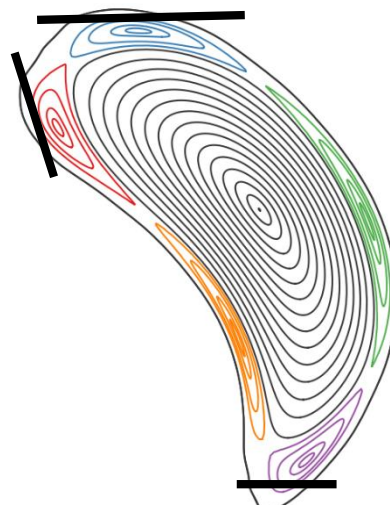
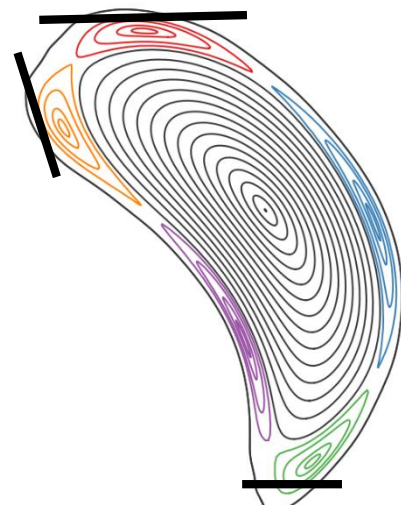
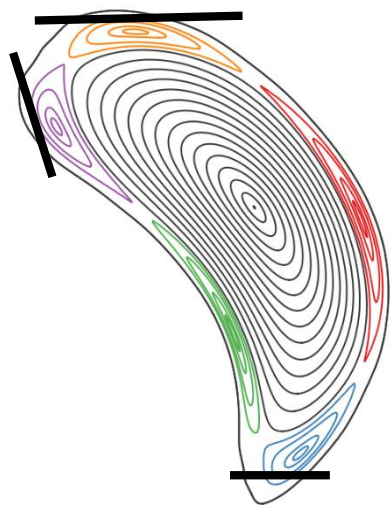
Example of  
*standard* configuration

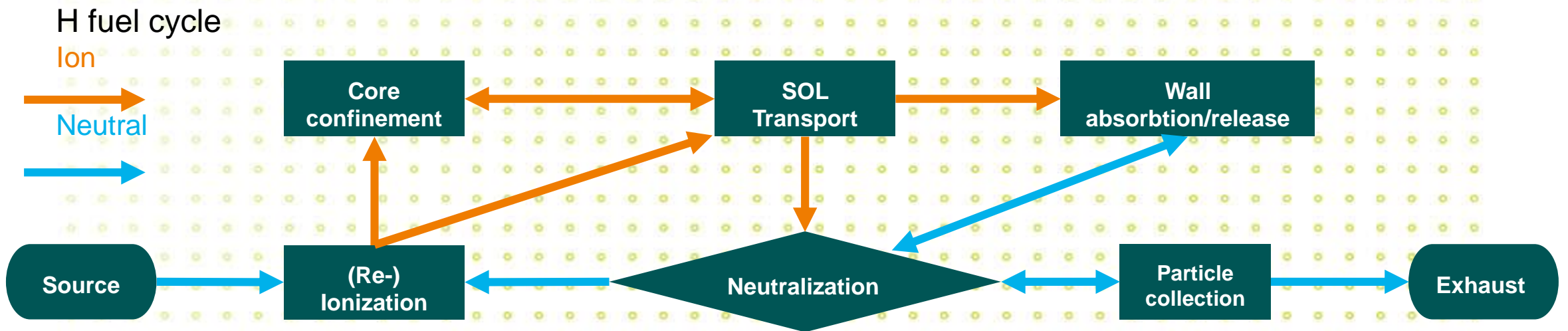
W7-X divertor:  
*island divertor*



SOL with 5  
independent islands

10 units  
made of fine graphite



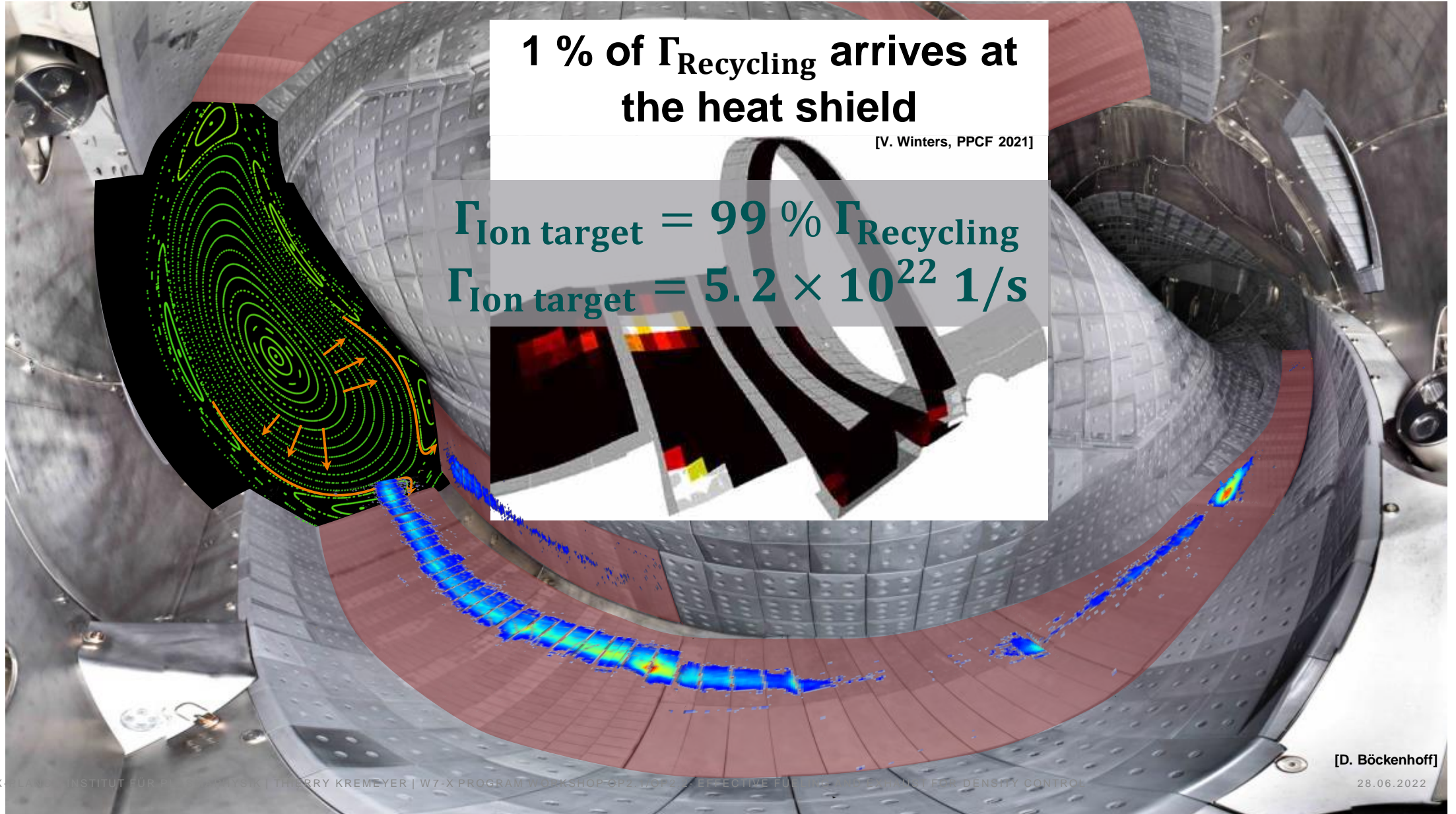


# ~99% of particles neutralize on divertor target

1 % of  $\Gamma_{\text{Recycling}}$  arrives at  
the heat shield

[V. Winters, PPCF 2021]

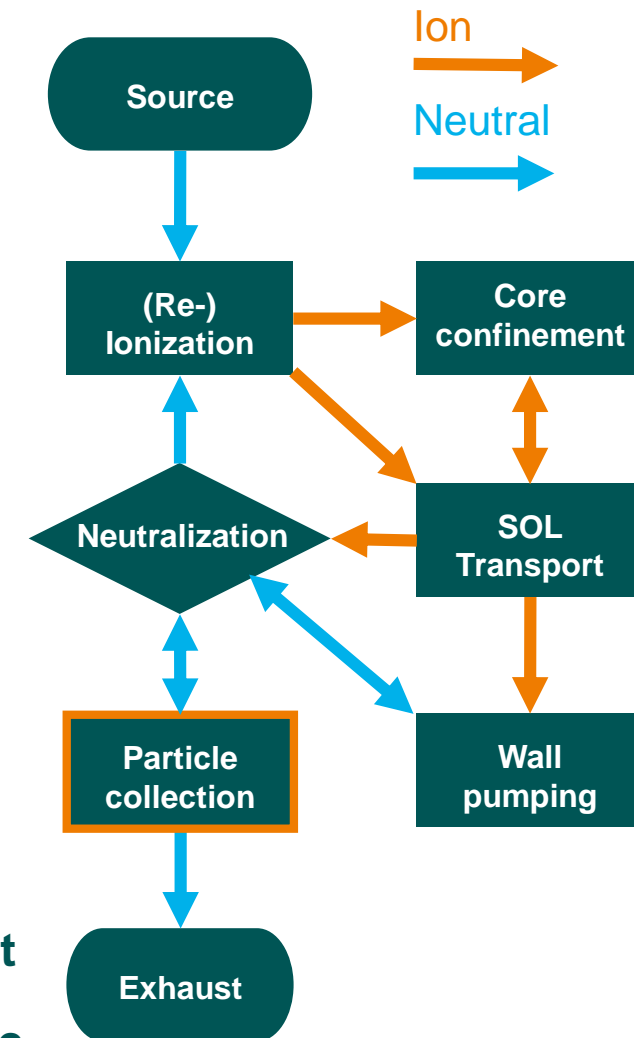
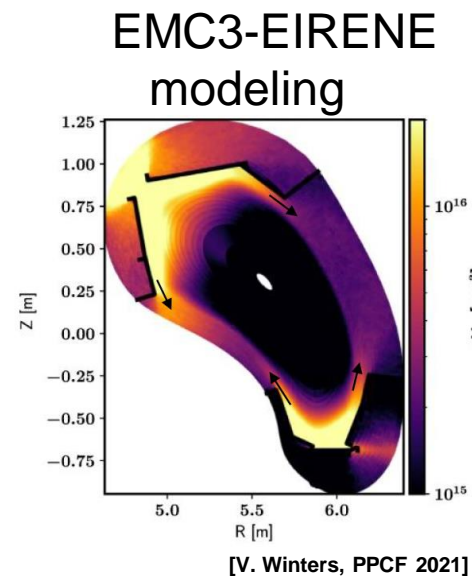
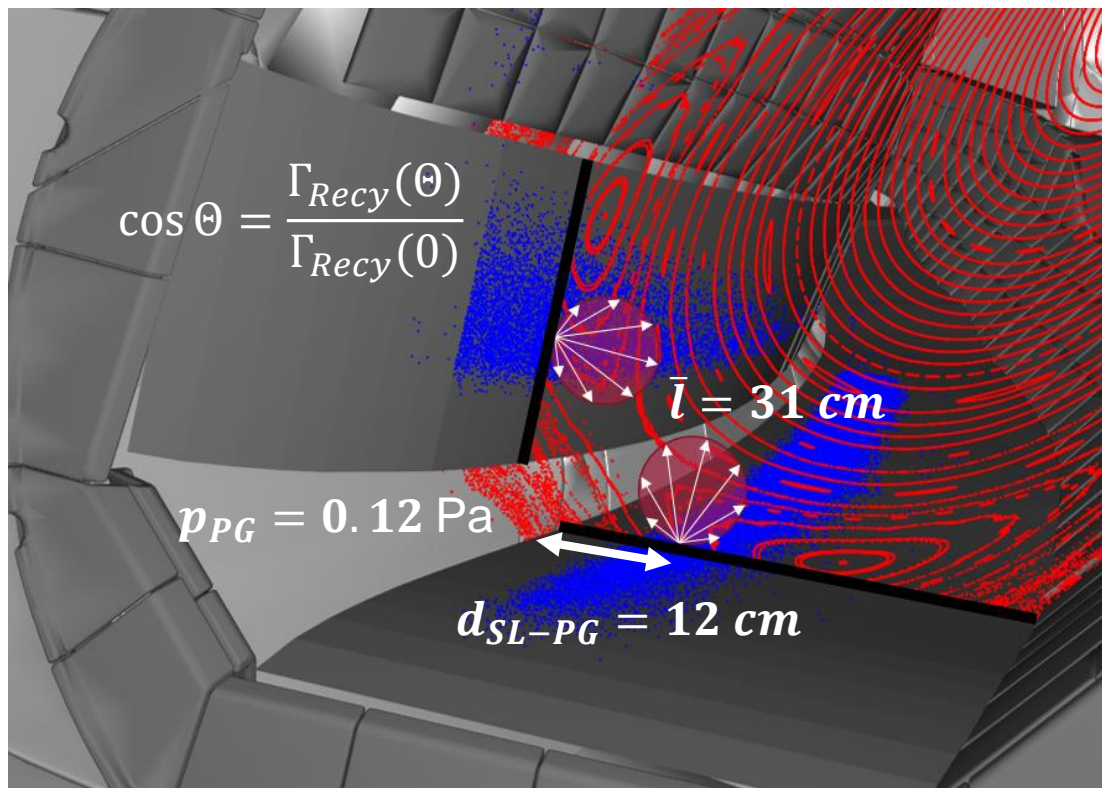
$$\Gamma_{\text{Ion target}} = 99 \% \Gamma_{\text{Recycling}}$$
$$\Gamma_{\text{Ion target}} = 5.2 \times 10^{22} \text{ 1/s}$$



[D. Böckenhoff]



# Particle collection with an open carbon divertor



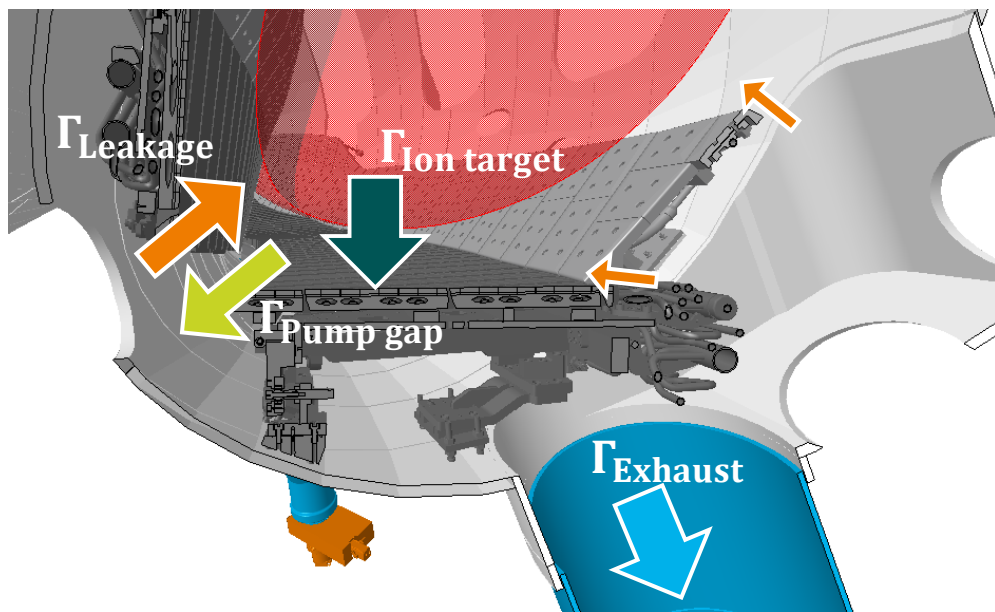
Particle collection:

Pumpgap opening ~ 68°- 90°      ~7.3 % of  $\Gamma_{Target}$

EMC3-EIRENE      4.0 % of  $\Gamma_{Target}$

Only particles that don't ionize on the way, make it to pump gap

# Particle removal and sub-divertor leakage



$$\Gamma_{\text{Ion target}} = 5.2 \times 10^{22} \text{ 1/s}$$

$$\Gamma_{\text{Pump gap}} = 4 \% \Gamma_{\text{Ion target}}$$

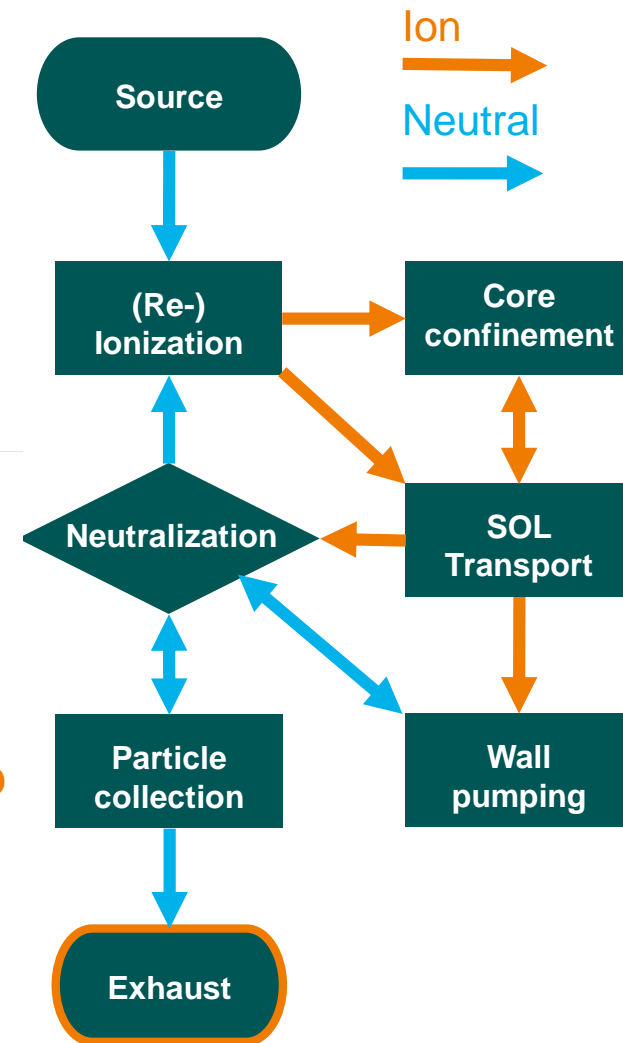
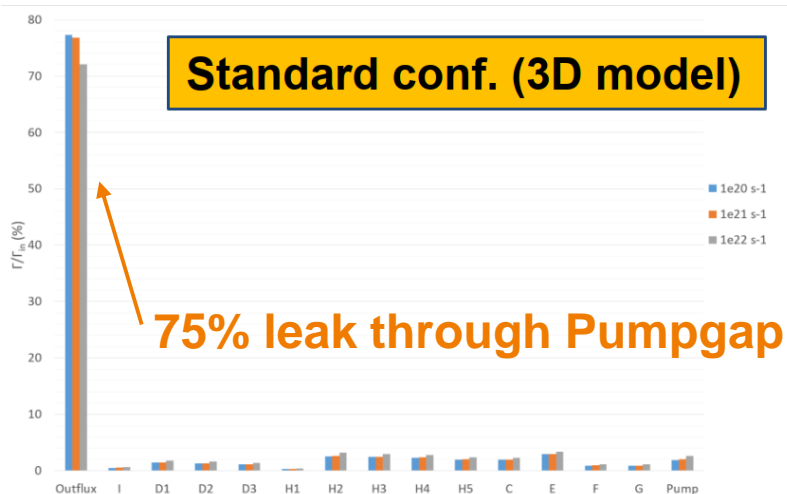
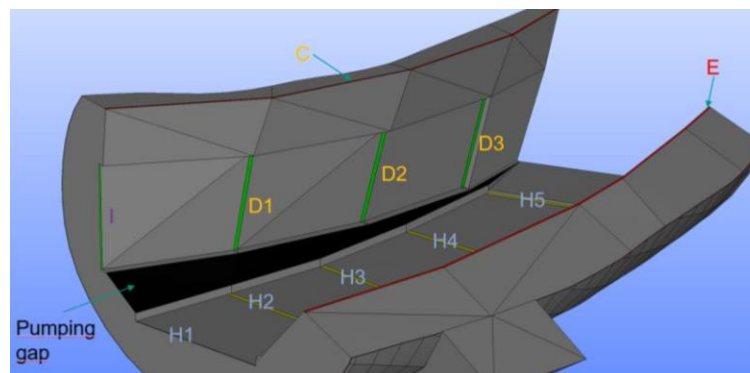
$$\Gamma_{\text{Exhaust}} = p_n \times S_{\text{eff}}$$

$$\Gamma_{\text{Exhaust}} = 6 \% \Gamma_{\text{Pump gap}}$$

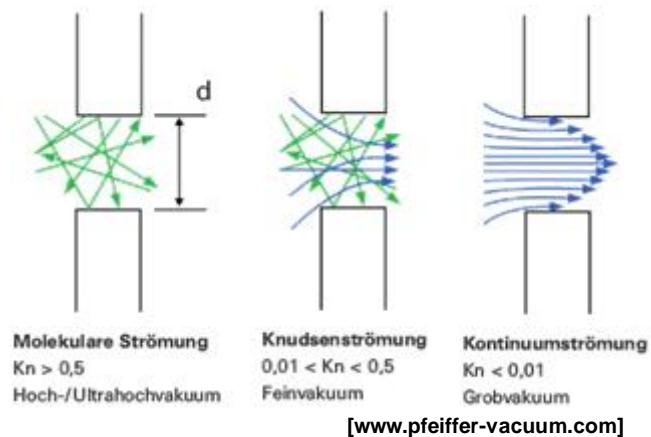
$$\Gamma_{\text{Leakage}} = \Gamma_{\text{Pump gap}} - \Gamma_{\text{Exhaust}}$$

$$\Gamma_{\text{Leakage}} = 94 \% \Gamma_{\text{Pump gap}}$$

## DIVGAS modeling



# Continuous flow minimizes leakage



$$Kn = \frac{\bar{l}}{d} \quad d_{PG} = 90 \text{ mm}$$

How to access continuous flow regime?

- Increase pump gap opening
- Increase pump gap pressure
  - Shifting strike line closer to pump gap
- Increasing density
- Change the target geometry

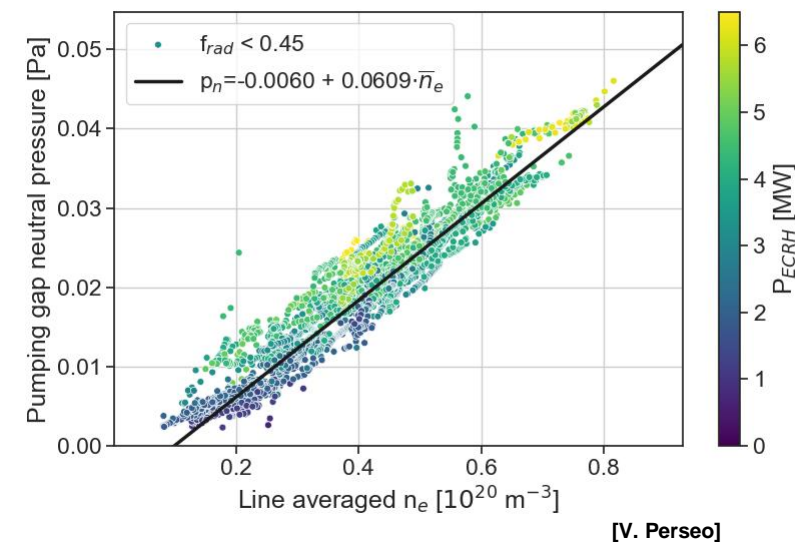
$$I_{cc} = 0 \text{ kA} \quad d_{SL-PG} = 12.1 \text{ cm}$$

$$I_{cc} = 2 \text{ kA} \quad d_{SL-PG} = 6.2 \text{ cm}$$

Increase of  $p_{PG}$  by 25%

Shifting SL as close as possible to PG  
Increase of  $p_{PG}$  ~50%?

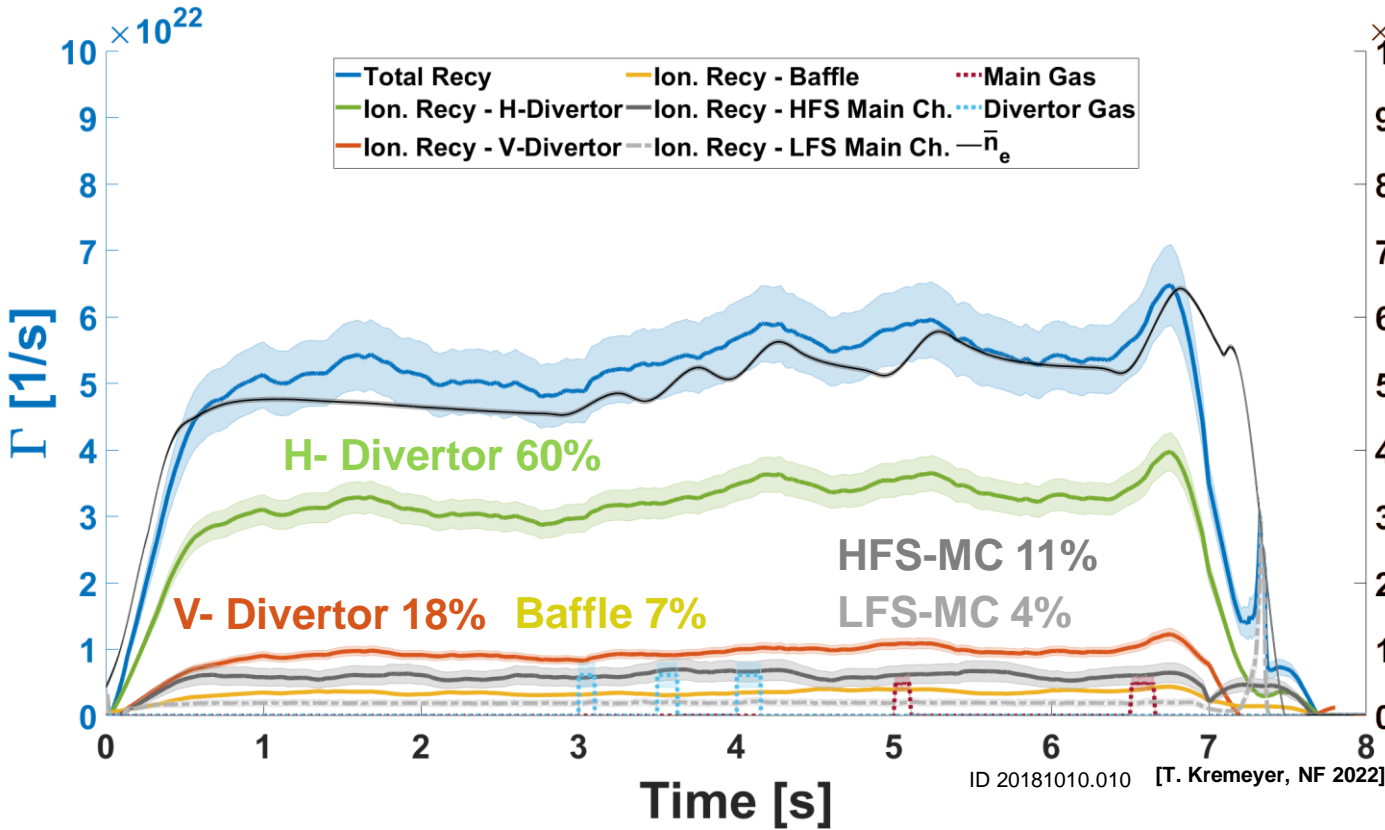
	Best OP1.2	Knudsen	Continuos
$Kn$	3.4	< 0.5	< 0.01
$\bar{l}$ [m]	0.31	0.045	0.0009
$p_{pg}$ [Pa]	0.12	0.82	40



# Re-ionisation shows good plugging

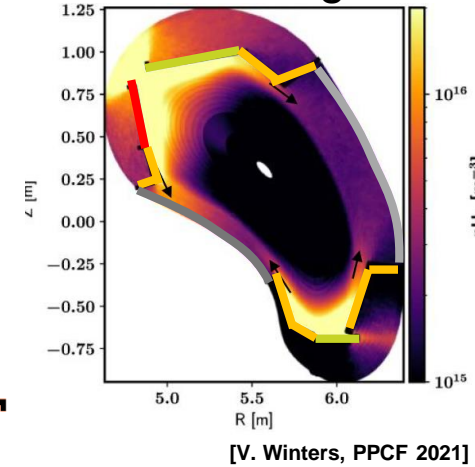
$$\Gamma_H^{\text{tot}} = \Phi_{H\alpha} * S/XB_{\text{eff}}$$

$$S/XB_{\text{eff,Div}} = 34 \pm 2.3 \quad S/XB_{\text{eff,MC}} = 19 \pm 4.8$$

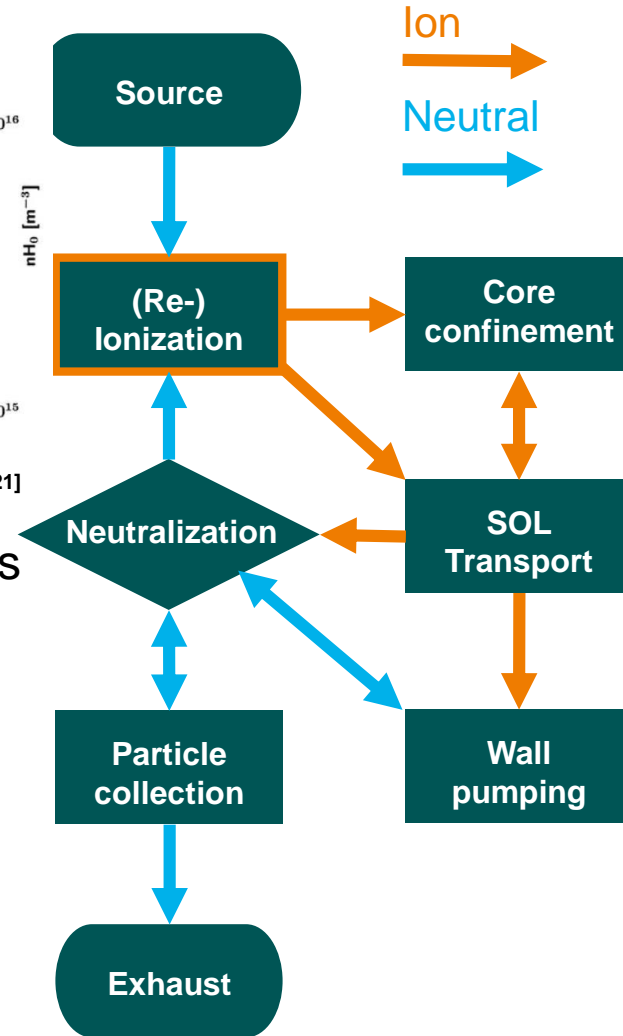


$$\Gamma_{\text{Plugged}} = 85 \% \Gamma_{\text{Ion target}}$$

## EMC3-EIRENE modeling



- Neutral particles escape poloidally and toroidally from divertor





## Detachment at W7-X

# Detachment definition and power balance



## Observations of detachment in Tokamak are:

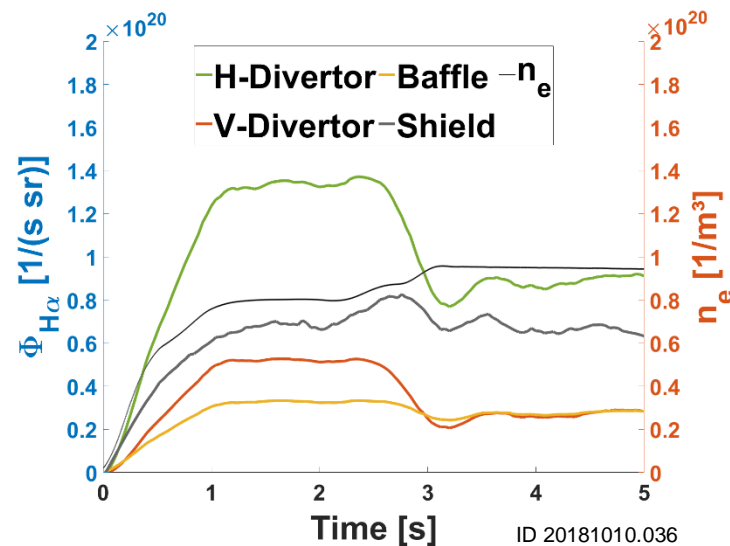
- ‘roll-over’ and decrease of the ion saturation current,  $j_{+sat}$ , of Langmuir probes built into the divertor targets
- $H_\alpha$  radiation from the target regions does not roll over/decrease, but continues to increase with  $n_e$
- A further feature of detachment is that it occurs when the target Langmuir probes indicate low temperatures,  $T_e \approx$  a few eV or less “

- Stangeby, Plasma Boundary Book IoP 2001

Detachment easily accessible with stable radiation front

But  $H_\alpha$  decreases

Particle and Power detachment achieved by radiating power in the SOL through seeded and/or intrinsic impurities



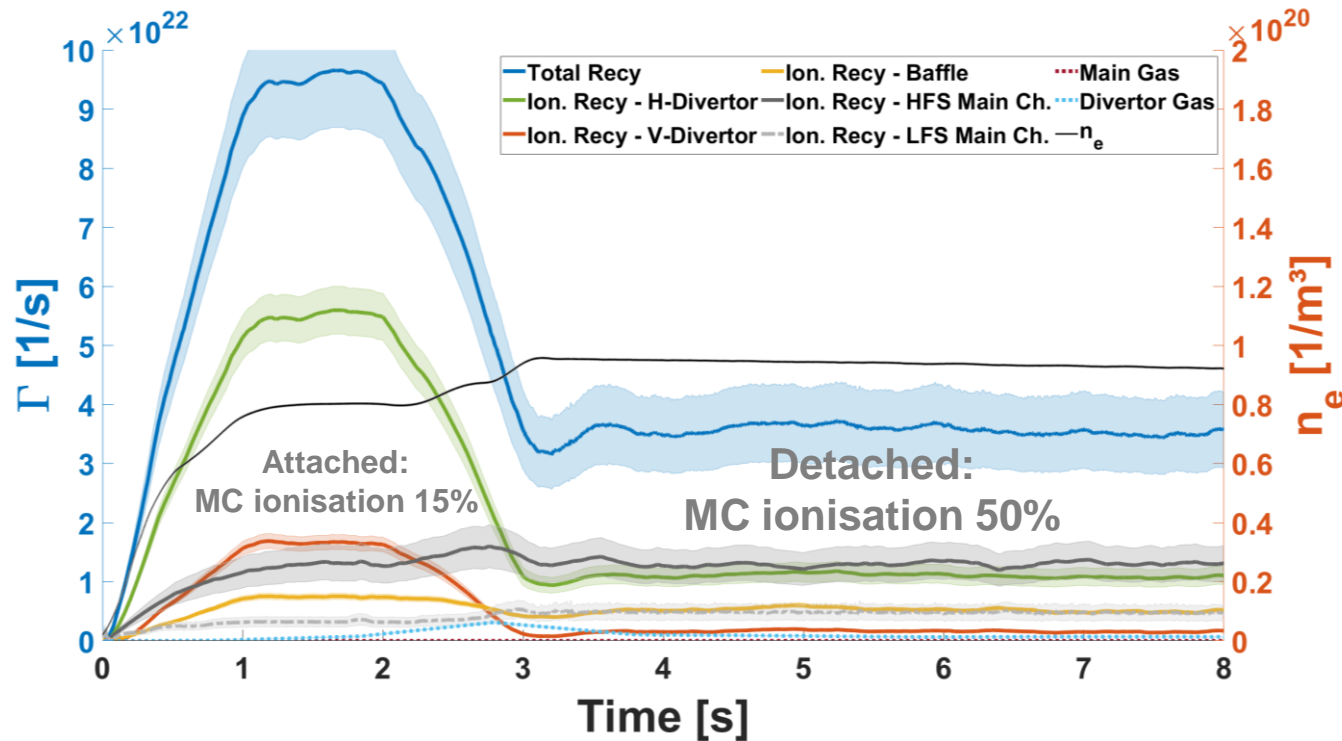
## Power balance

$$P_{in} = \Gamma_{rec}(\gamma T_t + \epsilon_i) + f_{rad} P_{in}$$

Recycling flux reduced at high  $f_{rad}$

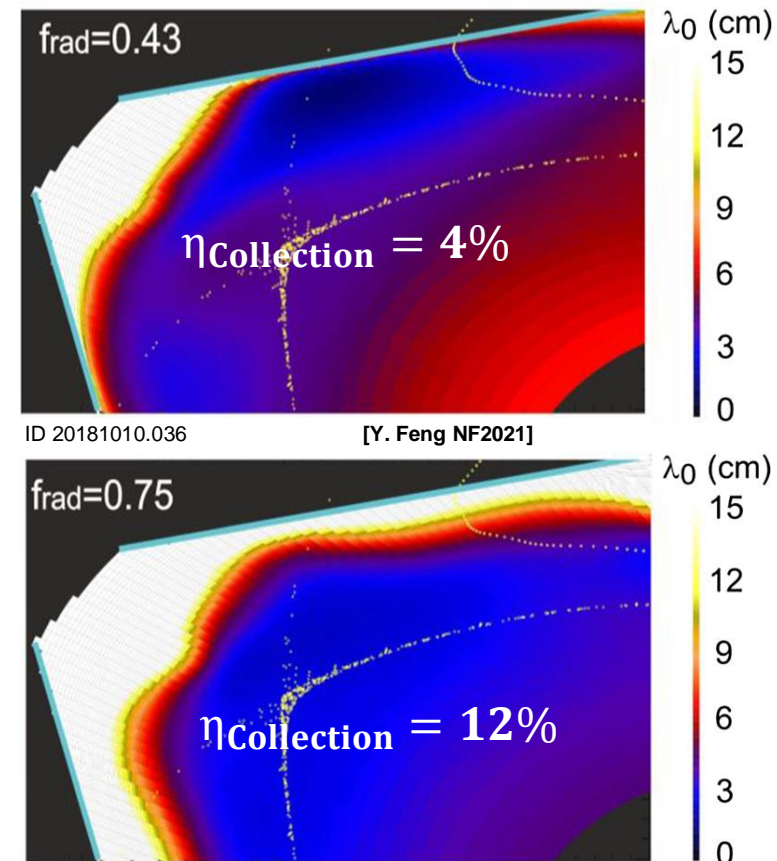
[M. Jakubowski, NF2021] [Y. Feng, NF2021]

# Detachment reduces particle flux, brings higher collection, but weaker plugging



$\Gamma_{\text{Ion divertor}} \searrow 60\%$

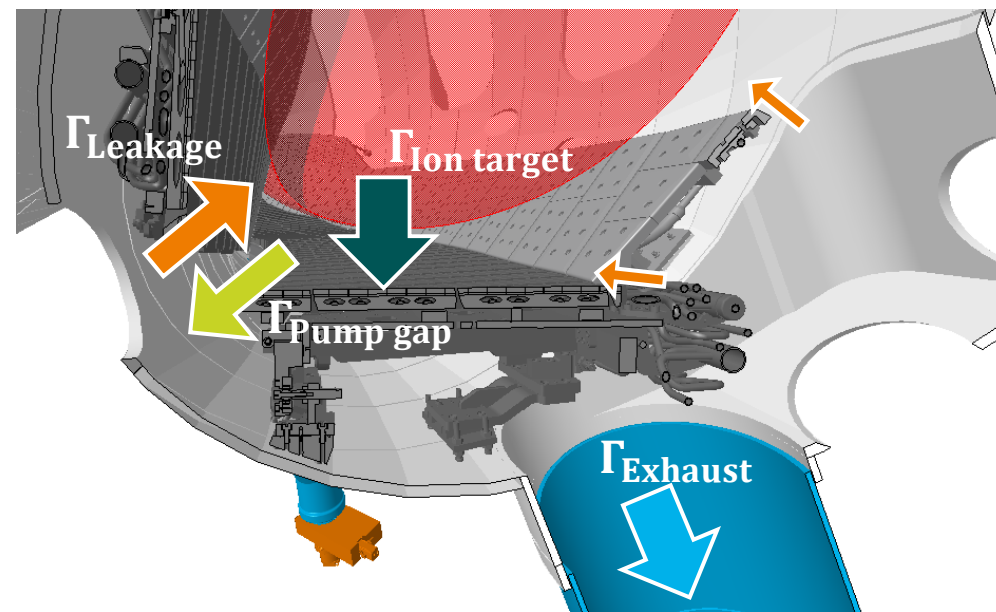
$\searrow \eta_{\text{Plugged}} \approx 50\%$



	Pump gap [mbar]	Midplane [mbar]
Attached	$6.2 \text{ E-4} \pm 6.0 \text{ E-5}$	$3.0 \text{ E-6} \pm 6.7 \text{ E-7}$
Detached	$7.0 \text{ E-4} \pm 5.2 \text{ E-5}$	<b><math>1.2 \text{ E-5} \pm 1.6 \text{ E-6}</math></b>

# Full magnetic flexibility at effective, but in-efficient exhaust

- Particle collection dominated by pump gap opening angle to strike line
- Sub-divertor leakage dominated by pump gap
- Exhaust and Wall source at same order
- Reasonable plugging, despite toroidally open divertor
- Stable detachment opens up neutral channels
- W7-X detachment decreases particle flux towards divertor



Attached

$$\Gamma_{\text{Ion target}} = 99 \% \Gamma_{\text{Recycling}}$$

$$\eta_{\text{Collection}} = 4 \% \Gamma_{\text{Ion target}}$$

$$\eta_{\text{Removal}} = 6 \% \Gamma_{\text{Pump gap}}$$

$$\eta_{\text{Exhaust}} = < 1 \% \Gamma_{\text{Ion target}}$$

$$\eta_{\text{Plugged}} = 85 \% \Gamma_{\text{Ion target}}$$

Attached

Detached

Detached

$$\Gamma_{\text{Ion divertor}} \text{ decreases } 60 \%$$

$$\eta_{\text{Collection}} = 12 \% \Gamma_{\text{Ion target}}$$

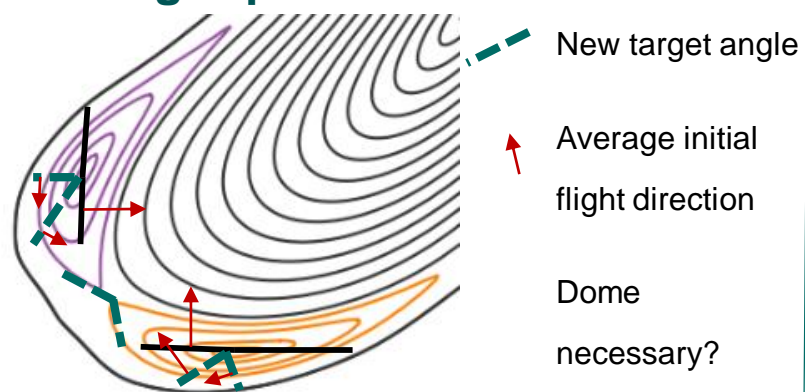
$$\eta_{\text{Plugged}} = 50 \% \Gamma_{\text{Ion target}}$$



# Design criteria for a reactor divertor

## Particle collection

- Maximize pump gap opening angle – Cosine law initial flight path

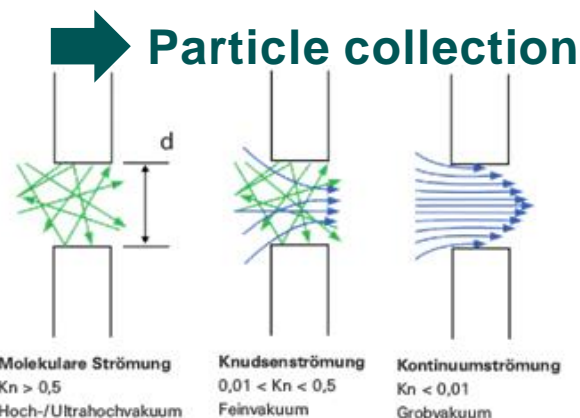


- How does initial flight path of neutrals change with  $W$ ?

How much exhaust do we need?  
 $\rho < 10 \Rightarrow \text{SOL} \Rightarrow ? \Rightarrow \eta_{\text{exhaust}}$   
 Target geometry should provide more, throttle pumps

## Particle removal

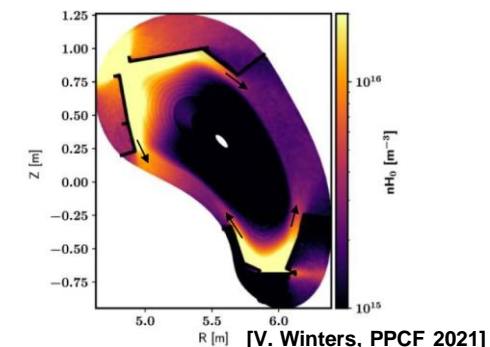
- Minimize Knudsen number
- Increase pressure



$$Kn = \frac{\bar{l}}{d}$$

## Particle plugging

- Close poloidal and toroidal neutral channels
- Block neutrals by baffles where thermal loads allow
- Ionize neutrals



- Weakend by detachment
- BUT less relevant as  $\eta_{\text{exhaust}}$  increases