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# Time-dependent SOLPS-ITER simulation for actuator design and system identification

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# Time-dependent SOLPS-ITER simulations were performed to address dynamic problems

- ✓ Most SOLPS-ITER simulations focus on steady-state B2.5 plasma solutions
- B2.5 plasma state converges with global particle balance achieved
- Quasi steady-state (QSS) EIRENE schemes are used
- This approach cannot deal with dynamic problems (both plasma and neutral dynamics)

#### Examples of dynamic problems in the boundary of tokamaks

- 1) Abrupt target flux drop (cliff type [1-2]) induced by strong X-point radiation with time scale of few tens of ms, observed in KSTAR experiment
- 2) System identification with time-varying gas injection signal
- 3) Design of actuators for real-time control
  - e.g., Louvre (neutral conductance regulator)  $\rightarrow$  requires time-dep. neutral solver

#### □ Two types of time-dependent SOLPS-ITER simulations to address above problems

- 1) Full time-dependent simulation (both B2.5 & EIRENE)
- 2) QSS time-dependent simulation (only B2.5, QSS EIRENE scheme)
  - → Both requires time-dependent settings in B2.5 side (w/o numerical acceleration or relaxation, etc.)

[1] Eldon, D., *et al.* 2017 Nucl. Fusion **57** 066039
[2] McLean, A. G., *et al.* 2015 J. Nucl. Mater. **463** 533 536



### Summary

□ Time-dependent SOLPS-ITER simulations were performed to address dynamic problems:

#### 1) Bifurcation-like KSTAR target flux drop

- Unstable branch solutions can be obtained which qualitatively reproduced measured target flux, radiation and density trends
- Simultaneous penetration of carbon radiation and ionization front towards the core region across X-point by excessive cooling of the fluxtube with D2 gas injection
- Both the ionization front and radiation front are strongly coupled to the  $T_{\rm e}$  (5eV front)
- $T_{\rm et}$  characterizes  $T_{\rm e}(s_{\parallel})$  for both inner/outer divertor SOL

#### 2) System identification with time-varying gas puff

- Phase space  $(n_{e,sep} vs. T_{et})$  represent system characteristic: by time-dep. throughput scan
  - a) Clearly demonstrates hysteresis and directional properties on the phase space
  - b)  $T_{\rm et}$  determines threshold of KSTAR bifurcation-like transition
- Low density branch of SPARC shows hysteresis due to thermo-electric current

#### 3) Design of Louvre actuator that controls divertor neutral pressure

- Time-dependent SOLPS-ITER can be used to actuator design (response time)
- Simulated neutral relaxation time scale agrees with analytic model
- The effects of Louvre transparency and gas throughput can be equivalent in plasma away from the pump.



# Bifurcation-like target flux drop coupled with X-point radiation observed in **KSTAR density ramp experiment**



### SOLPS-ITER SS (before drop) + time-dep. (during drop) solutions reproduced experimental target trend

#### □ Simulation setup

- $P_{SOL} = 0.8 MW$
- Species: D, C
- Core boundary particle flux (D+) = 8e19/s(neutral beam)
- Steady-state (SS) fueling throughput scans: 5e20-3e21 atom/s
- Time-dependent simulation for 4 throughputs: 3e21, 4e21, 5e21, 8e21 /s
- **QSS time-dependent simulations** were performed because plasma dynamics is more important for this problem



- Steady state behavior: OT rollover at lower  $n_{e,sep}$  than IT (reproduced [JSPark 2018 NF 58])
- Time-dependent simulation shows that collapse of the target flux profile is continuous in time within 100 ms **CAK RIDGE** (collapse time scale depends on the gas throughput)

## Simulated core density trend matches with measured $ar{n}_{ m e}$

□ Steady-state (SS) solution + time-dependent solution: GP = 3e21, 5-100 ms (20 snapshots)



•  $n_{e,core}$  ( $n_e$  at OMP core bdy.) and  $N_{e,core}$  (total # of core ptl.) increases

→ In SOLPS-ITER, 'core region' only covers core periphery so lack of core coverage gives  $\bar{n}_{e}$  trend discrepancy with experimental observation

(dominant contribution of core density to  $\bar{n}_{e}$  considering monotonic profile and width)

 $\rightarrow$  However, SOLPS-ITER core density trend agrees with experimental observation

Both the separatrix and core carbon concentration increases, and core radiation
 CAK RIDGE become dominant as abrupt target flux drop proceeds

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# El front and Prad front coincides with 4-5 eV fronts

□ 20 snapshots of time-dep solution and SS solution



- $T_{\rm et} \sim s_{\parallel}(5 \text{ eV})$  relation can be changed by geometry or IT/OT
- However, El front and Prad front (mainly carbon) always coincides with 5eV front
- $\mathbf{\mathcal{A}}_{\text{National Laboratory}}$  Regardless of the flux tubes, front location is tightly coupled with  $T_{\text{et}}$

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## Radial distribution of $n_e$ , $T_e$ , $P_{rad}$ , $S_{na}$ just above X-pt (core – SOL)



- Radiation and ionization source both peaks at the X-pt then penetrates core
- Density and ionization source peaks near the X-pt & core temperature cooled with radiation
- Strong localized radiative cooling makes  $T_{\rm e}$  profile partially non-monotonic at the X-point

### System identification of KSTAR with time-varying gas puff



bifurcation is not likely to be occurred (lack of  $T_{et}$  and density limit)



• Hysteresis observed on the phase space

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### Directional property test on the attached branch



Control of plasma state on the phase space is bi-directional in the same branch
 Crossing the branch is unidirectional: makes bifurcation (gap) on the phase space master to edit

## Fully automated algorithm for system identification with bifurcation



- Coupled system identification performed best with correlated variables  $\Phi_{e,OT}$  and  $n_{e,sep}$
- $T_{e,OT}$ : serves as a threshold for bifurcation /  $n_{e,sep}$ : feature identified most strongly
- Phase diagram shows model turnover (--) near inflection points in slope between observed variables
- A prediction horizon of at least 500 ms is used, where e models are truncated to within 5% error threshold before retraining over a new scrolling interval. First order linear models are identified in each interval to avoid overfitting bifurcation discontinuities



### SPARC v2y operation space (time-dep Ne seeding)

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current and is presumably due to the narrow PFR geometry (future work).

# SPARC "Louvre" actuator design using full time-dependent SOLPS-ITER simulation (time-dependent EIRENE)



- Louvre controls neutral conductance
- 29MW pure D scenario with a toy model geometry (chamber, duct and Louvre)
- Full time-dependent SOLPS-ITER simulation with dt (B2.5) = dt (EIRENE) scans over 1e-6 to 1e-3 s
- Fixed background plasmas to check neutral relaxation time
- Saturated number of particle (IPRNL) in the census array scales with dt (EIRENE) that limits taking too small dt







### Time-scale of neutral pressure evolution is consistent with analytic model [1] and is dominated by pumping speed



0.1

time (s)

0.15

0.2

 $\tau = 5.7 \,(ms)$ 

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Analvtic model [

0.16

0.14

Duct width x1/2

the set of the set of

0.05

Duct length x4

0.06

0.08

0.1

time (s)

0.12

0.04

= 4.3 (ms

(Pa) م<sup>2</sup> 0.02

Pplenum (Pa) mol (Pa) 20.0

0.01



t=0: open Louvre, no neutral t=0.1 s: 90% closed Louvre

$$V\frac{dP}{dt} = -C\Delta P + SP$$

- Only extreme changes in duct geometry (e.g., duct length 0.1 m  $\rightarrow$  5 m) affects relaxation time scale otherwise pumping speed S dominates neutral pressure evolution time
- Time scale with decreased pumping speed agrees with experimental neutral relaxation time scale (e.g., C-Mod  $\sim$  100 ms [2])



FIG. 5. Results during a discharge in Alcator C-Mod. G plasma main chambe X-poin divertor plenum bypass intrinsic leakage 0.1 m duct (G)



[2] C. S. Pitcher RSI 2000

# Full-time dependent simulation coupled with plasma on a realistic geometry (open to 90% opaque louvre at t=0)



□ Simulation setup

- Lower single null
- D only, D2 puff scan
- Input power: 10 MW (low power scenario)
- $T_{\rm e,div} \sim 50 \text{ eV}$

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- 'v2y' geometry
- Full time-dependent



Neutral pressure

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## Actuator equivalence: GP throughput vs. Louvre transparency

• Two actuator gives similar  $p_{\rm neut}^{\rm sp}$  or  $p_{\rm neut}^{\rm div}$  with different  $p_{\rm neut}^{\rm pump}$ 



- $\Phi_{pump} = \Phi_{puff}$  (pumped flux = gas throughput)
- $\Phi_{pump} = p_{pump}S_{pump}$  ( $S_{pump}$  is pumping speed)
- $p_{pump} \sim \Phi_{puff}$  (S<sub>pump</sub> is const.  $\rightarrow$  thermalized D2 dominates)
- $p_{\text{pump}} \sim p_{\text{strike pt.}}$  (relation determined by neutral conductance,
- **CAK RIDGE** e.g., Louvre condition)



# **Backup Slides**



## Introduction - SOLPS-ITER code and B2.5-EIRENE coupling

SOLPS-ITER: tokamak boundary plasma simulation code suite managed by ITER that includes fluid plasma solver B2.5 + kinetic MC neutral solver EIRENE



# Coupling schemes "usually" assumes quasi-steady-state (QSS) neutral approximation

□ Time steps

- **dt (B2.5)** = 1e-7 to 1e-4 s
- **dt (EIRENE)**: DTIMV is effectively EIRENE time step for each EIRENE calls (default = 1e-3 s)
- $\hfill\square$  Two EIRENE schemes for coupled simulations
- 1) Quasi-steady-state (QSS) scheme
  - dt (EIRENE) = 1e-3 s (default),
  - dt (EIRENE) for ITER: large (~1e9 s) for ensuring QSS, limited by max CPU time assigned
  - → Long-lived neutrals beyond dt (EIRENE) will be cut-off so neutral info can be underestimated or distorted (e.g., ionization sources distribution)
  - Long enough dt (EIRENE) gives fully relaxed ionization profile for each EIRENE call, for given plasma background, ignoring neutral propagation time
  - Still okay for QSS time-dependent simulation (only B2.5 plasma side) if the phenomenon of interest is governed by plasma dynamics rather than neutral dynamics (i.e., assuming neutral dynamics >> plasma dynamics)

#### 2) Time-dependent EIRENE (full time-dependent SOLPS-ITER simulation)

- dt (B2.5) = dt (EIRENE) = 1e-6 to 1e-4 s (practical range)
- Using the "census data" that records long-lived neutral information (position, velocity and weight) in a time-dependent stratum
- Small dt requires more census data  $\rightarrow$  limits practical range of dt

## Schematic of volumetric processes coupled with Te

 $\rightarrow$  Inspired by M. Fenstermacher PPCF 1999



# Sources from the neutrals can be underestimated with default dt (EIRENE)

/data1/f3p/SOLPS\_runs/KSTAR/KSTAR\_bifurcation/r KSTAR L-mode gas puff scan with different EIRENE scheme and time step \_steady\_state\_1e20\_QSS\_eirene\_step\_dt\_1e9\_long

		++-				
dt (EIRENE) [s]	1e-3 (default)	1.0	1.33e9 (ITER-like)	1.33e9 (ITER-like)	1e-4 = dt (B2.5)	
EIRENE scheme	QSS	QSS	QSS	QSS	Time- dependent	
NTCPU [s]	50	50	50	90	100	
D <sub>2</sub> puff rate = 1e20 atom/s	Particle balance not achieved	$n_{ m e,sep} = 1.1  imes 10^{19}  { m m}^{-3}$	$n_{ m e,sep} = 1.1 \times 10^{19}  { m m}^{-3}$	$n_{ m e,sep} = 5.1 \times 10^{18}  { m m}^{-3}$	3e18 with NPRNL = 200000	
D <sub>2</sub> puff rate = 1e22 atom/s	$n_{\rm e,sep} = 1.1 \times 10^{19} \mathrm{m}^{-3}$	$n_{\rm e,sep}$ = 2.0 × 10 <sup>20</sup> m <sup>-3</sup>	$n_{\rm e,sep} = 2.0 \times 10^{20} \mathrm{m}^{-3}$	$n_{ m e,sep} = 2.0 \times 10^{20} \ { m m}^{-3}$	Bb8 (density 급증중)	

# Update result

 Default EIRENE time step is not sufficient for KSTAR L-mode due to cut-ott of the long-lived neutrals due to long mean free path of neutrals by 1) KSTAR geometry and 2) low density, low temperature in given discharge condition

• Lack of the ionization source from cut-off can be compensated by increasing puffing rate

• ITER-like dt (EIRENE) gives the same result as dt (EIRENE) = 1.0 case, limited by CPU time (50 s here) National Labo Time-dependent run gives the same steady-state solution as QSS scheme ? Open slide master to edit

## Time-scale of bifurcation depends on the throughput



## Time-scale of bifurcation depends on the throughput



## Target flux bifurcation in KSTAR L-mode experiment



#### **Discharge condition**

- $I_{\rm p} = 0.6$  MA,  $B_{\rm T} = 2.5$  T (forward field, ion B× $\nabla$ B direction downwards into the lower divertor)
- External heating power = 0.93 MW (mostly from neutral beam)
- $\bar{n}_e = 2.0 3.5 \times 10^{19} \text{ m}^{-3}$  ramped with fixed gas puff (1e21/s) without feedback control of fuel throughput



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### Majority of C radiation comes from: Te = 4-11eV (over whole region)



## $P_{\rm rad}$ /Vol: radiation spot penetrates core

(a)-(e): steady-state solutions(f)-(h): time-dependent solutions



(a)-(e): steady-state solutions (f)-(h): time-dependent solutions

## $T_{\rm e}$ : 5eV front penetrates core



(a)-(e): steady-state solutions (f)-(h): time-dependent solutions

## $S_{na}$ : ionization front penetrates core



 $n_{\rm e}$ : hd zone moves target  $\rightarrow$  Xpt  $\rightarrow$  core (Xpt)<sup>(f)-(h): time-dependent solutions</sup>



### Parallel distribution (OT~OMP) of $n_e$ , $T_e$ , $P_{rad}$ , $s_n$ (1<sup>st</sup> SOL ring)



• High density zone forms at [target  $\rightarrow$  Xpt], then peak decreases

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- $T_{\rm e}(s_{\parallel})$  is always monotonic and 5eV front moves upstream across Xpt
- Ionization front, radiation front moves upstream across Xpt, then peak value gradually decreases at further upstream



## Target flux bifurcation in KSTAR L-mode experiment



#### **Discharge condition**

- $I_{\rm p} = 0.6$  MA,  $B_{\rm T} = 2.5$  T (forward field, ion B× $\nabla$ B direction downwards into the lower divertor)
- External heating power = 0.93 MW (mostly from neutral beam)
- $\bar{n}_{\rm e} = 2.0 3.0 \times 10^{19} \, {\rm m}^{-3}$  ramped with feedback control of fuel throughput

- Transition happens in 10-30 ms
  - → intermediate state in the middle of the target flux cliff is unstable
- Time scale is similar or longer than the parallel SOL transport timescale

## Characteristic of the target flux bifurcation



Target flux rollover → stable rollover + abrupt & unstable transition



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## Characteristic of the target flux bifurcation



#### 1) Existence of the 'critical density':

Bifurcation-like transition to the detached regime happens when  $\bar{n}_{e}$  reaches at 'critical density'  $\bar{n}_{crit.}$ 

#### 2) Hysteresis of 'critical density':

[Re-attachment  $\bar{n}_{crit.}$ ] > [detachment  $\bar{n}_{crit.}$ ]

→ Representation of divertor condition with delays, implies that there can be a better classifier such as divertor (downstream) physical quantities rather than upstream quantity,  $\bar{n}_{e}$ 



# 3) Bifurcation time-scale $\tau_{bifurcation}$ : 10-40 ms

 $\tau_{\parallel} \leq \tau_{bifurcation} < \tau_{\perp}$ 

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	1st detach	2nd detach	3rd detach	4th detach	#20267 detach
$t_{\rm detach start}[ m sec]$	7.170	7.528	7.798	8.070	6.970
$t_{\rm detachend}[ m sec]$	7.200	7.548	7.814	8.109	7.000
$\Delta t  [ m sec]$	0.030	0.020	0.016	0.039	0.030

## Bifurcation is not related with carbon sputtering

- In JET (with carbon divertor), self-sustained oscillation of the A. Loarte PRL 1999 detached <-> attached states were observed
- KSTAR maximum target temperature



> At least  $Y_{\text{chem}}$  does not change!



