



Italian National Agency for New Technologies,  
Energy and Sustainable Economic Development

# Fusion Fission Hybrid Reactor based on High field tokamak neutron source

**Francesco Paolo Orsitto<sup>1</sup> , N Burgio<sup>2</sup>, M Ciotti<sup>1</sup>, F Panza<sup>2</sup>.**

<sup>1</sup>ENEA Department Fusion and Technologies for Nuclear Safety C R Frascati ,via E Fermi 45 , 00044Frascati , Italy

<sup>2</sup>ENEA Department Fusion and Technologies for Nuclear Safety C R Casaccia ,via Anguillarese 301,, 00123 S Maria di Galeria(Roma) , Italy

*IAEA Technical Meeting on synergies between Nuclear Fusion  
Technology Developments and Advanced Fission Technologies  
6-10 June 22 IAEA Headquarters Vienna, Austria*



# The following Questions on the tokamak neutron source of a FFH ( Fusion-Fission Hybrid) Reactor are basic for this talk

A neutron source with fusion gain factor in the range  $Q=1-3$  is needed for FFH

1. Can we define the parameters of a **compact (high magnetic field based on High temperature superconductors) source of the order of 1m major radius**, producing 20MW fusion power, so that the FFH reactor has a power of the order of 200MW ?

2.1. Which are the plasma parameters of a neutron source based on tokamak Standard aspect ratio  $A=R/a=3$  and Spherical Tokamak with  $A=1.8$  using **Thermal Fusion** ?

3.1. At low values of gain factors, the **non-thermal tokamak fusion plasmas** is a reasonable alternative route to the FFH neutron Source: can we define plasma parameters for a device working in NON-thermal scheme?

3.3. **Thermal Fusion** : plasma  $T_e = T_i$  (  $T_e=8-10\text{keV}$  )

**Non-thermal Fusion** : plasma with  $T_i \gg T_e$  obtained

With direct interactions of Tritium ions with fast Deuterium

# Outline : **NEW SCALING LAWS** for Tokamak plasmas with aspect ratio $A=R/a=3$ and 1.8

1. Plasma parameters of FFH neutron sources based on tokamaks obtained from **new** scaling laws for fusion reactors.
2. Parameters of plasmas working at standard aspect ratio  $A=2.5$  and high field(  $B=8T$ ) are derived based on FTU/ALC CMOD confinement data.and extrapolated to thermal fusion.
  - 2.1. Parameters Spherical plasmas with aspect ratio  $A=1.8-2$  and high field(  $B=3-4T$ ) are derived based on NSTX /MAST confinement data and extrapolated to thermal fusion.
  - 2.2. Parameters Spherical **NON THERMAL** plasmas with aspect ratio  $A=2$  and high field (  $B=3-4T$ ) are derived based on TFTR supershots
3. The study of the FFH reactor based on the tokamak neutron sources are derived from point 1. A FFH model composed by a Tokamak source surrounded by a subcritical fission blanket and by a lithium blanket, is carried out showing one of the main property: tritium production

# MOTIVATION

**1. Tokamaks plasma confinement properties are depending on the aspect ratio  $A = \text{major radius}/\text{minor radius} = R_0/a$  . Standard tokamaks  $A \geq 2.5$ ; Spherical tokamaks  $A \leq 2$  ( $A = 1.8$ ).**

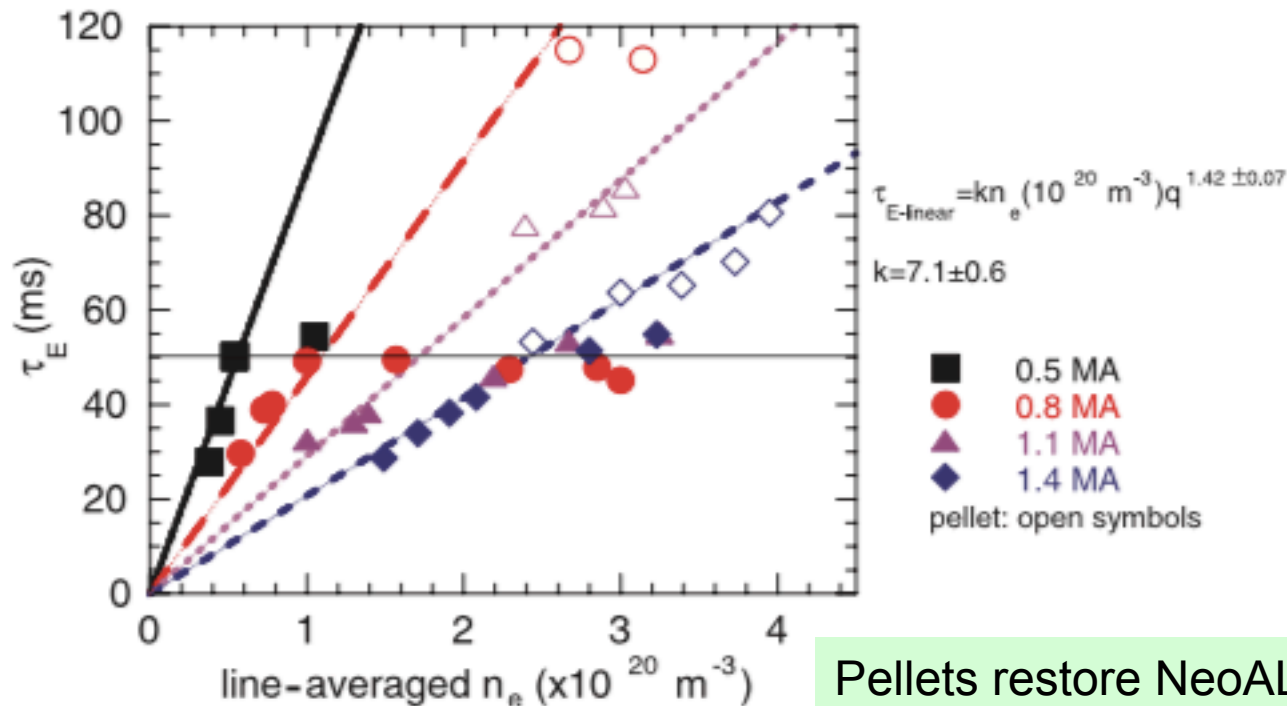
- 2. Data base for high field standard tokamak needs to be built as there is very less data available at high field  $B > 6\text{T}$  than at  $B < 6\text{T}$  for designing devices. In practice only four devices ( FT , FTU , ALCATOR-C and C-MOD).
- **2.1. The advantage of high field is well known as the device size can be made more compact reducing the costs and maximizing the performance( at the fixed cost) .** The high field tokamak plasmas can be operated at higher density and with reasonably good confinement properties in L-mode . The advantage of using L-mode is that the damage on first wall due to the ELMs can be avoided : **this is the reason why the H-mode producing type I ELMs is being under discussion for DEMO.** The High field route is now closer with the High Temperature Superconductors
- 3. High Field Spherical tokmaks (  $B = 3\text{-}4\text{T}$ ) are the parallel route explored for FFH neutron sources : For spherical tokamak we have a limited database in practice including NSTX and START and MAST . Scaling laws on spherical tokamaks are introduced and dimensions for spherical tokamak based neutron sources are given .

# Main message

- Experiments on FTU , ALCATOR-C and C-MOD support the idea that Improved L-mode( Low confinement mode) with pellets can be a candidate mode for operation at high field (  $B \geq 8T$ )
- **Tokamaks plasma confinement properties are depending on the aspect ratio  $A = \text{major radius}/\text{minor radius} = R_0/a$**
- Tokamaks ( Aspect ratio  $A \geq 2.5$ ): a low power fusion device (  $Q_{\text{Fusion}} = 1-2$ ) can be a tokamak with major radius  $R_0 = 1m$  and magnetic field on axis  $B = 8T$ , aspect ratio  $A = 2.5$
- Spherical Tokamaks (  $A < 2$ ) :Scaling laws on spherical tokamaks are introduced based on NSTX, START and MAST data. A spherical tokamak at  $Q = 3$ , Aspect ratio  $A = 1.8$  corresponds to  $R = 0.75m$  at  $B = 3T$  Along the lines of ST40 of Tokamak Energy
- NON-THERMAL fusion plasmas based on TFTR supershots/JET-Hot ion mode can be analyzed using **a novel scaling law for Supershot**.: the parameter of a spherical tokamak working in this regime are obtained and discussed .

main results from FTU  
supporting the high field route  
in L-mode with pellets

# NeoAlc and SOC on Ohmic FTU



Pellets restore NeoALC scaling

**Figure 11.** Effect of pellets (open symbols) on energy confinement time (ohmic discharges density scan at  $B_t = 7.2$ ): the linear scaling with density is recovered in multiple pellet-fuelled discharges (pellet  $\tau_E$  data are averaged over 50 ms). The horizontal line represents the saturation ohmic confinement time in FTU.

B Esposito PPCF 2004

Design criteria for a MCF neutron source :  
scaling laws plasma



# Scaling laws for reactor plasmas in Hmode

If we define the set of the following conditions :

1.  $Q=Q_0$  fixed
2.  $\tau_{SD} = \Lambda_{SD} \tau_E$  ( $\Lambda_{SD} \ll 1$ ) ( slowing down time of alpha particles  $\ll$  energy confinement time) ,
3.  $P_\alpha = \Lambda_{LH} P_{LH}$  ( $\Lambda_{LH} > 1.5$ ) the alpha heating is sufficient to keep the plasma in H-mode

We find that **the scaling parameter linking equivalent fusion plasmas** is :

$$S_{FR} = R B^{4/3} A^{-1} * Q_0^{1/3}$$

M Romanelli, F Romanelli, F Zonca – 28th EPS Funchal 2001, ECA vol 25 A(2001)697

F P Orsitto and T N Todd , Proceedings Conference FUNFI3 Hefei 2018

<https://www.enea.it/it/seguici/pubblicazioni/edizioni-enea/2019/funfi3-international-conference-on-fusion-fission>

M Romanelli and F P Orsitto , PPCF 63 (2021) 125004

# H mode $Q_{fus}=1-2$

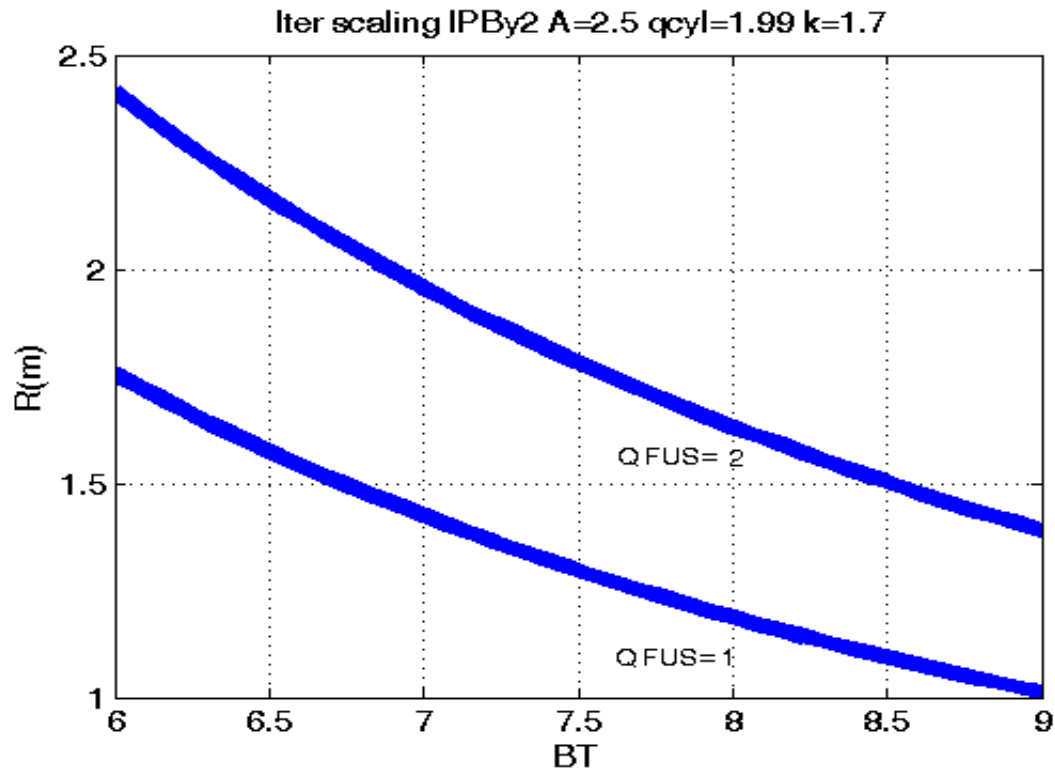


Fig.1. Major radius vs magnetic field of devices at  $Q_{fus}=1$  and  $2$ , aspect ratio  $A=2.5$ ,  $q_{cyl}=1.99$ , elongation  $k=1.7$

# H mode $Q_{fus}=1-2$ plasma parameters

Table II Parameters of  $Q=2$  Tokamaks  $A=2.5$

	Q=2	Q=2
<b>R(m)</b>	1,5	2,4
<b>A</b>	2,5	2,5
<b>B(T)</b>	8,5	6
<b>I<sub>p</sub>(MA)</b>	10	9,84
<b>n<sub>G</sub>(10<sup>20</sup> m<sup>-3</sup>)</b>	6,28	3,4
<b>n (10<sup>20</sup> m<sup>-3</sup>)(0.8*n<sub>G</sub>)</b>	5	2,7
<b>Beta(%)</b>	3,7	5,3
<b>beta<sub>N</sub>(%)</b>	2,1	3,1
<b>P<sub>fus</sub> (MW)</b>	44	51,4
<b>P<sub>input</sub>(MW)</b>	22	25,7
<b>T<sub>0</sub>(keV)</b>	7,3	9,8
<b>f<sub>i</sub>(dilution)</b>	0,8	0,8
<b>Neutron flux (10<sup>20</sup> n/s)</b>	0,158	0,183

# Scaling parameter for L-mode confinement

$$S_{FRL} = R B^{1.5} A^{-0.74} Q_0^{-0.7}$$

R = major radius

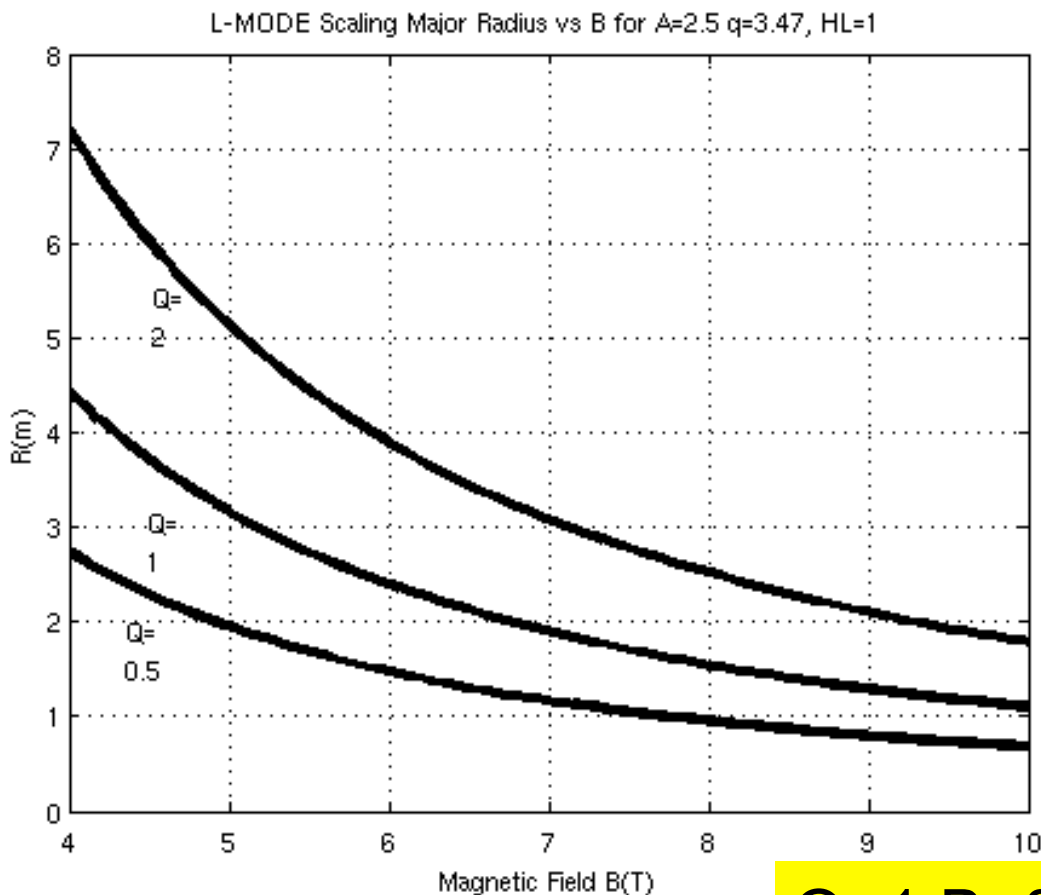
A=aspect ratio

B=magnetic field

Q0=fusion gain factor

All the other parameters are fixed equal to the reference device  
Taken as reference for the scaling : in particular Mass, safety factor and dilution

# Parameters for Devices operating in L-mode Aspect ratio $A = 2.5$ Major radius $R_0$ vs magnetic field $B$



**Q=1 B=8T R=1.5m**

**Q=2 B=8T R=2.5m**

# Scaling laws for spherical tokamaks(\*)

$$R_{ST} = C_{ST} Q_0^{0.61} B^{-1.13} A^{1.59} M^{0.22} q^{0.4}$$

$$C_{ST} = \left( \frac{\Lambda_{SD}}{A_{SD}} \right)^{-0.036} \left( \frac{\Lambda_{th} A_{lh}}{f_\alpha} \right)^{0.24}$$

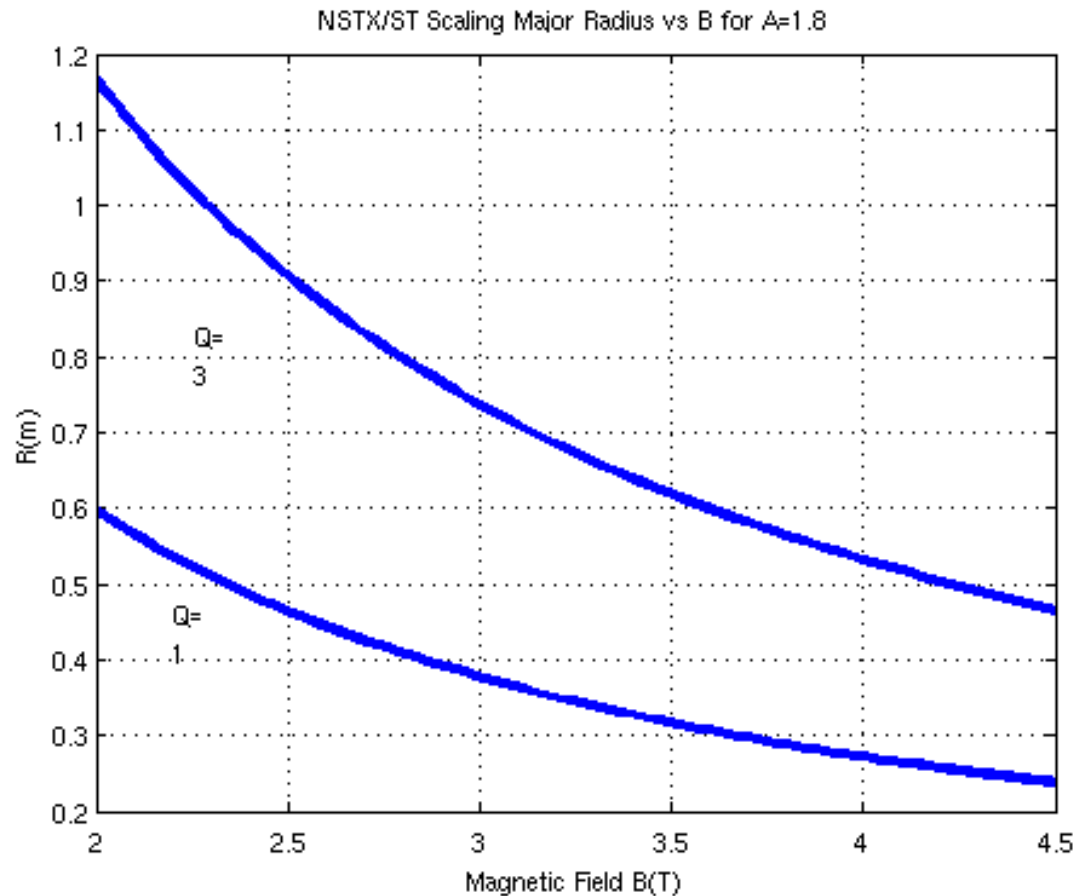
This scaling law has been obtained using the same Hypothesis as the other scaling laws

Incorporating also the ST confinement time scaling law ( see P F Buxton PPCF 61(2019)035006)

(\*) M Romanelli and F P Orsitto PPCF 63 (2021) 125004

# Parameters for Spherical Tokamak Devices

## R0 vs Magnetic field B



A=1.8 B=2T Q=1 R=0.8m

A=1.8 B=3T Q=3 R=0.75m

NON-thermal fusion scheme :  
ST Tokamaks design parameters using the  
TFTR Supershots confinement scaling



# Supershot /Hot ion scaling

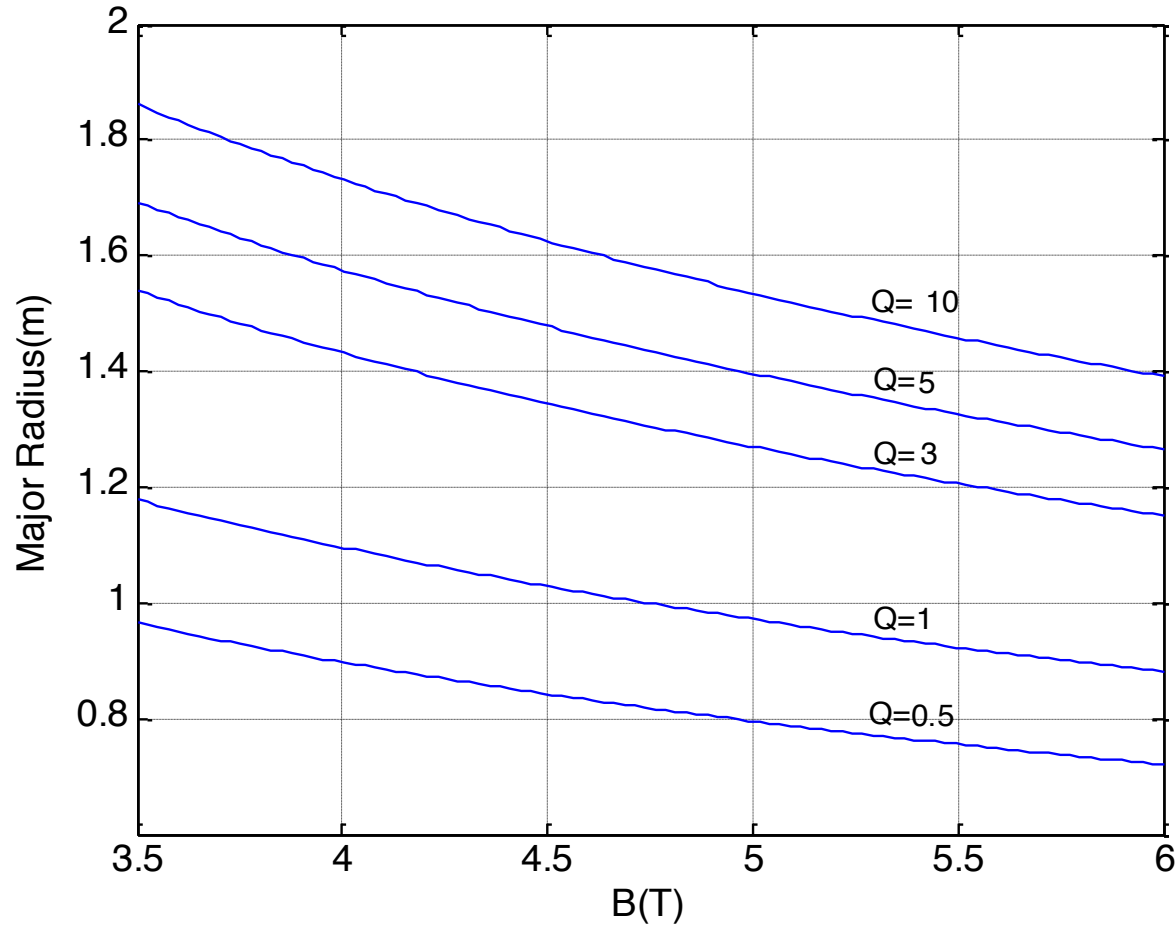
- The scaling law of confinement in TFTR supershots was given by J Strachan in a Nuclear Fusion paper vol.33 , 1993.
- An extension of this scaling laws to arbitrary geometry was proposed in the following form

$$\tau_{\text{TFTR}} = I_p^{0.22} B t W_{\text{beam}}^{-0.56}$$

$$\tau = I_p^{0.22} B t W_{\text{beam}}^{-0.56} R^{1.83} A^{0.06} k^{0.64} \left( \frac{n}{\langle n \rangle} \right)^{1.5} n^{0.4}$$

# Q=0.5-10 scan major radius vs B

ST REACTPR : AST=2, KST=2.8, I<sub>p</sub>(MA)=7, n=10, WB(keV)=80, nPek=3.5



# Summary plasma parameters for tokamak neutron sources

Q	R	B	A	Plasma Scenario
1	1,5	7	2,5	Hmode
2	2	7	2,5	Hmode
2	1,5	8,5	2,5	Hmode
1	1,5	8	2,5	L-mode w pellets
2	2,5	8	2,5	L-Mode w pellets
1	0,8	2	1,8	NSTX scaling
3	0,75	3	1,8	NSTX scaling
1	1,2	3,5	2	TFTR supershots
3	1,4	4	2	TFTR supershot

**Analyzing the various options of plasma scenarios it seems possible  
Defining the plasma parameters of a compact neutron source  
with major radius  $R_0 \approx 1.5\text{m}$  with  $Q \approx 2$ .**

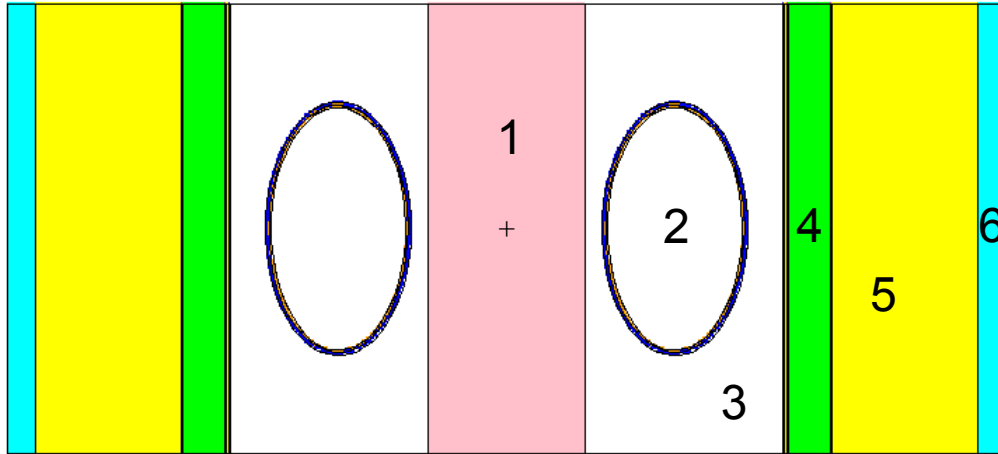
# Tokamak neutron source plasma parameters

The scaling parameter linking equivalent fusion plasmas Hmode (ITER scaling) is:

SFR =scaling parameter for fusion reactors =  $R B^{4/3} A^{-1} Q^{1/3}$

<b>Q</b>	2
<b>R</b>	1,5
<b>A=R/a</b>	2,5
<b>B</b>	8,5
<b>Y (neutr/s)</b>	1.50E+19
<b>Pfus (MW)</b>	40
<b>a</b>	0,6

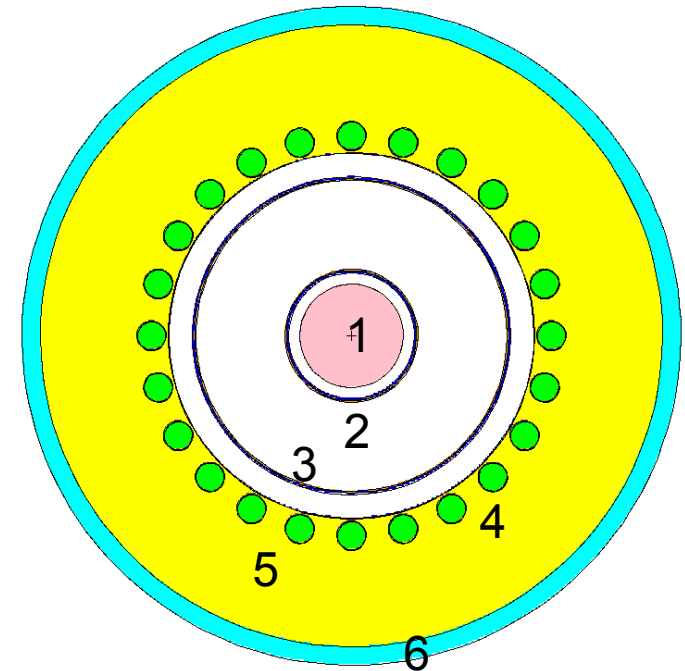
# MCNP model for FFH conceptual design: tritium production evaluation in fusion blanket



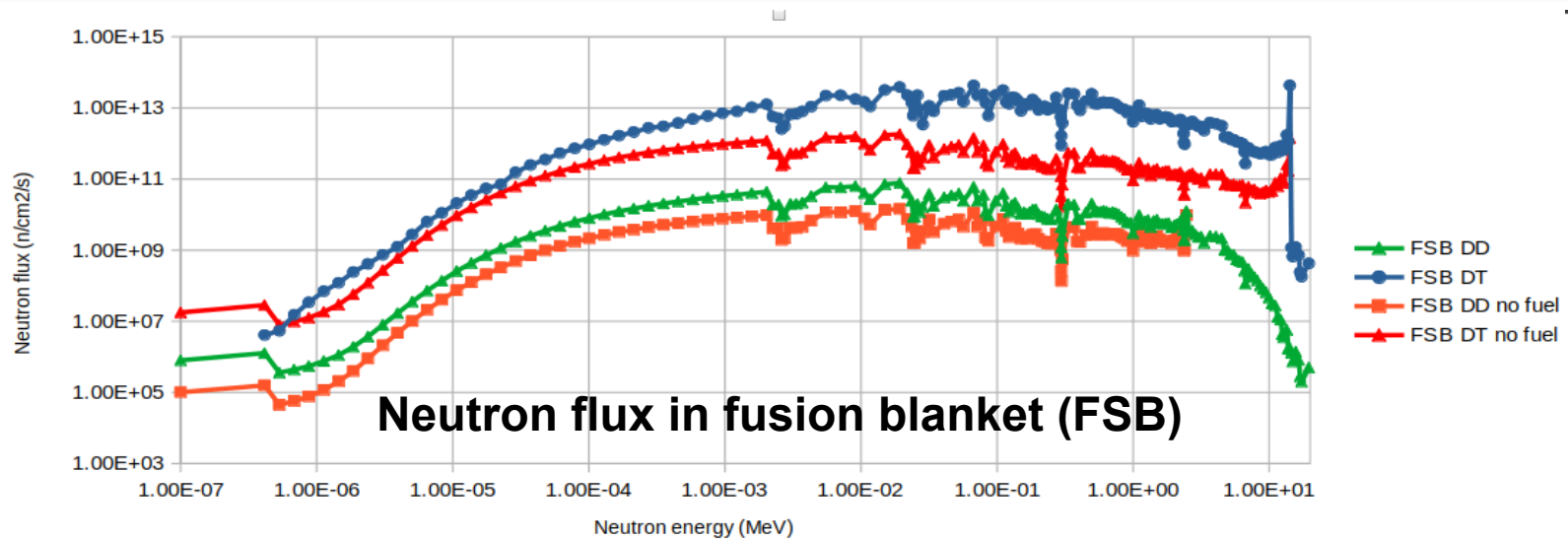
- FFH's Model layout
1. Central solenoid
  2. Plasma chamber
  3. Torus first wall
  4. Fuel
  5. Fusion blanket
  6. Reflector

## Main Design parameters

Fuel	Fresh MOX (Natural U + 5 at% $^{239}\text{Pu}$ oxides, density 7.91 g/cm <sup>3</sup> ), 24 fuel rods (Height=400 cm, Radius=19 cm)
Coolant	Helium
Fusion breeder	$\gamma$ lithium aluminate
Neutron yield (n/s)	1.50E+19 (DT) 1.50E+17 (DD)



# MCNP model for FFH conceptual design: neutronic parameters ( $k_{\text{eff}} = 0.96$ )



The tritium yielding rate estimation, calculated according to the following relation

$$dR/dt = \int \Phi(E) \sigma(E) dE,$$

$dR/dt$  = Tritium yield;  
 $\Phi(E)$  = Neutron spectrum;  
 $\sigma(E)$  =  ${}^6\text{Li}(n,\alpha)\text{T}$  cross-section;

shows a factor 4.33 and 5.66 gains for tritium production in DD and DT mode, respectively, using the fuel rods.

# Conclusions

- 1.  $Q=1-3$  plasma parameters obtained using new scaling laws for tokamak at low ( $A=1.8-2$ ) and standard ( $A=3$ ) aspect ratio obtained for thermal plasma in L-mode (low confinement mode) and H-mode (High Confinement mode)
- 1.1. NON thermal plasma are considered as well
- 2. Tokamak Major radius  $R_0 \approx 1.5-2\text{m}$  are reasonable plasma dimensions
- 3. High field  $B=8\text{T}$  for  $A=3$ , and  $B=4\text{T}$  for  $A=1.8$ .
- 4. FFHR evaluated using fusion-fission blankets :  
Tritium production is a striking characteristic of these blankets.