

# The Concept of Plasma Focus driven Fusion-Fission Hybrid Reactors

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The present work was initially supported by the bilateral Chilean-Argentine project CONICYT-ACE01 ANPCyT-PICT2697 and thus by Chilean ANID PIA ACT 172101 and the Argentine programs PIDSAT and PIPAD.

# Outline

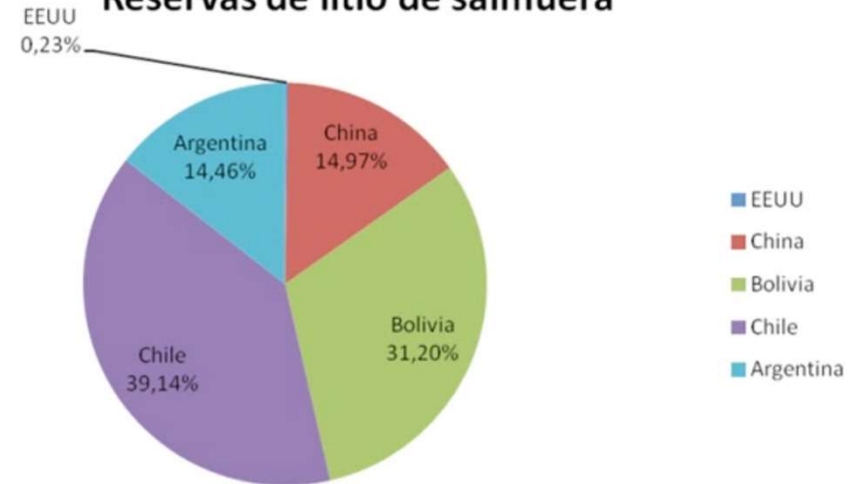
- Brief introduction about Chile, lithium and Chilean Nuclear Energy Commission.
- What is a Plasma Focus device.
- Fu-Fi hybrid nuclear reactors. Background facts.
- The concept of Plasma Focus driven fusion-fission hybrid reactors.
- Remarks and conclusions.

# South America Chile



Lithium brines in Chile, Bolivia and Argentina

Reservas de litio de salmuera



World lithium brines reserves

85% in South America  
39% in Chile

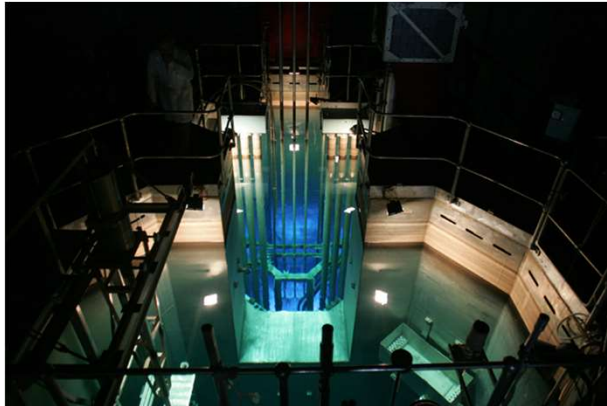
# Atacama, Chile

P<sup>2</sup>mc



lithium carbonate

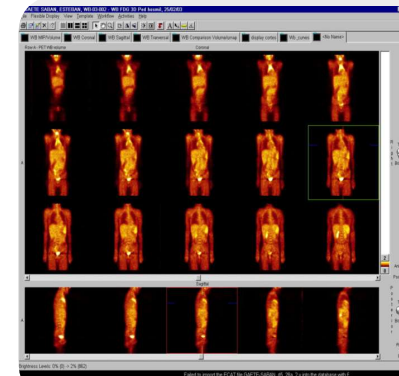
# Main facilities at the Chilean Nuclear Energy Commission $P^2mc$



**6 MW FISSION REACTOR**  
- Radioisotopes for medicine



**CICLOTRÓN**  
-Flúor 18-FDG  
-Flúor 18-NaF



**FUEL ASSEMBLY PLANT**



- **Plasma physics related with thermonuclear fusion in Z-pinches:**
  - Stability in gas embedded Z-pinch at MA currents
  - Plasma foci: increasing the plasma energy density in order to increase the thermonuclear neutron yield.
- **Miniaturization of Plasma Focus devices:**
  - Nanoflashes of radiation from miniaturized devices.
  - Scaling studies
- **Other pinch configuration:**
  - Wires arrays
- **Effects of pulsed radiation on materials**
  - First wall materials for fusion reactors
- **Effects of pulsed radiation on biological objects**
  - Cancer treatment
- **Low temperature plasmas (RF and continuous discharges)**
  - Plasma Torch for materials environment applications
  - Plasma needles for biomedicine applications
  - Scaling studies
- **Theoretical studies**
  - Statistical mechanics in non canonical systems
- **Main diagnostics:**
  - Electrical signals
  - Visible plasma images, ICCD, 4ns to 100ns gated frame
  - Optical Refractive diagnostics, Nd-YAG laser: 8ns, 1J; 170ps, 100mJ
  - Neutrons detecton (in particular low yield pulses)
  - X-rays detection (with spatial en temporal resolution)
  - Ions detection
  - Espectroscopy (visible, VUV and soft X- rays)
  - UHV radiation detection and analysis
  - Material characterization

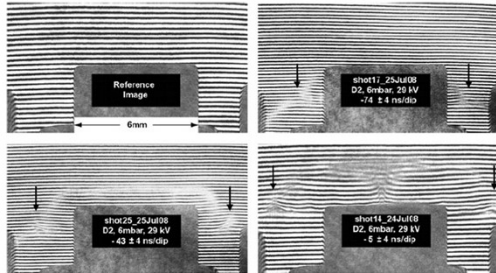
## Researchers:

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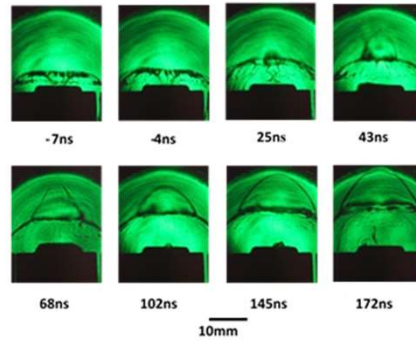
## Technicians:

Marcelo Vásquez

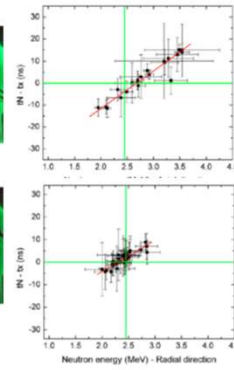
## Basic Physics



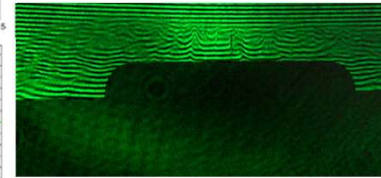
Toroidal singularity Applications



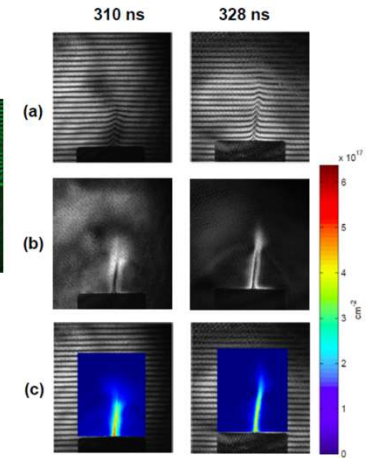
shocks



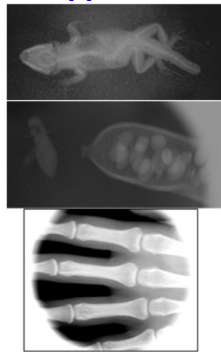
neutron energy distribution



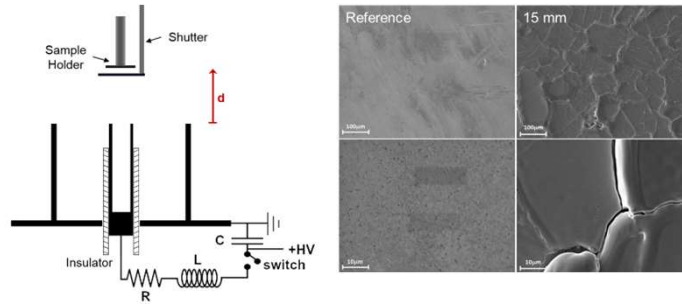
filaments



jets



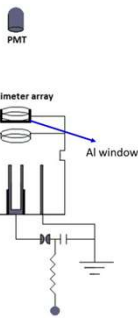
Pulsed x-ray and neutron sources



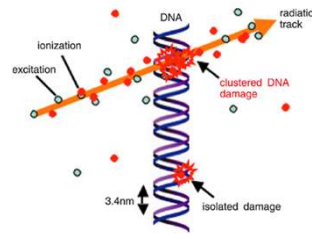
Effects on materials for 1<sup>st</sup> wall of nuclear fusion reactors



Plasma torch 20kW and microtorch 2 milliwats for materials and matter processing



Effects of pulsed radiation in life matter



Pulsed plasma thruster for nanosatellites

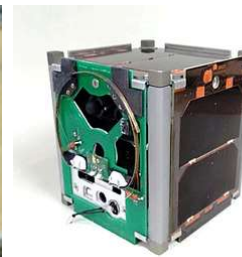
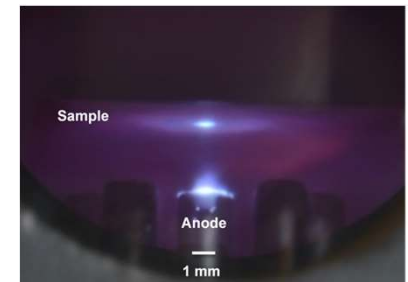


Table top plasma focus with tuneable damage factor F



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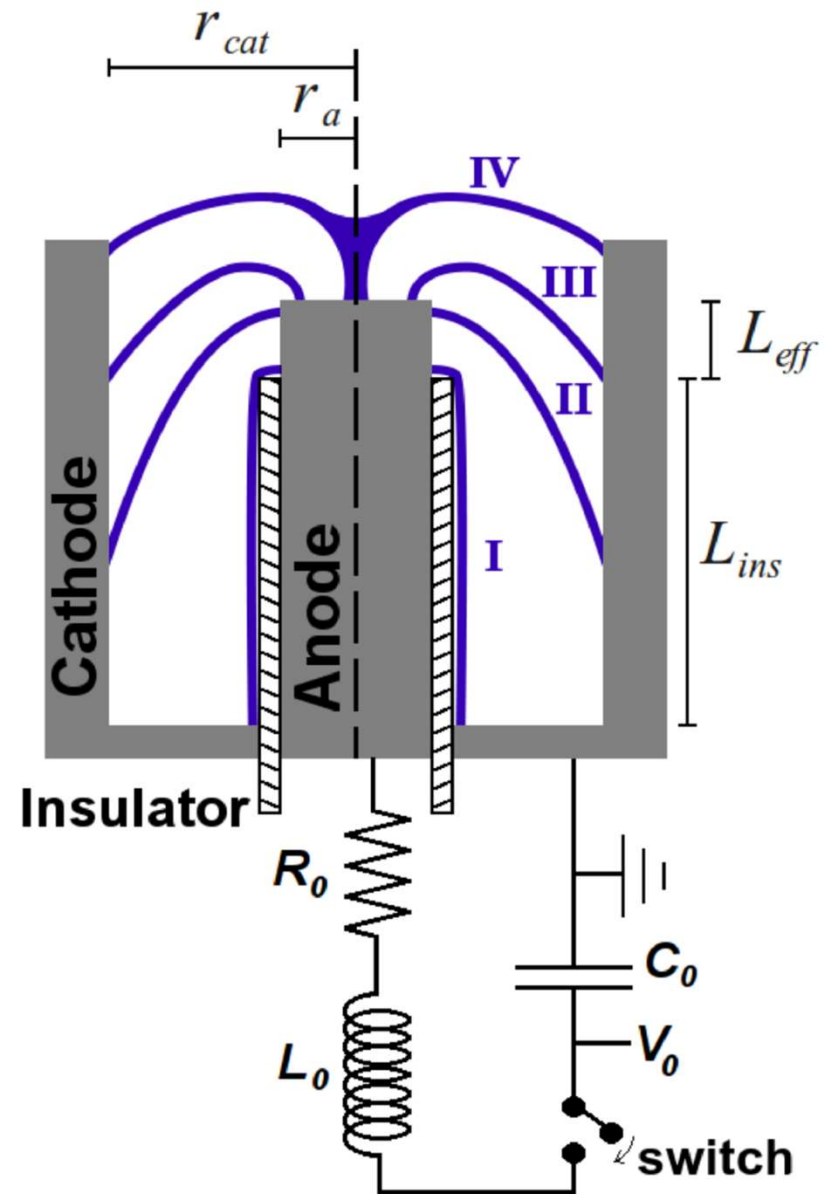


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# The plasma focus discharge

The Mather Plasma Focus (PF) is a transient electrical discharge produced in arranged coaxial electrodes, separated by an insulator, and driven typically by a capacitive pulsed power generator, which is controlled by a spark-gap switch.

- (I) The discharge starts over the insulator.
- (II) The Lorentz force pushes the plasma sheet to move axially.
- (III) and then to move radially.
- (IV) Finally the sheet collapses to form a dense column of plasma (pinch). During these stage, when operating with deuterium, hard X-rays and neutron are generated.



# The plasma focus discharge

$$E \sim 0.1\text{J} - \text{MJ}$$

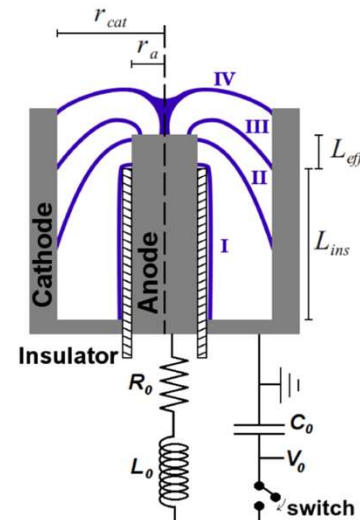
$$I \sim 100\text{kA} - 1\text{MA}$$

$$t_p \sim 1\text{ns} - 100\text{ns}$$

$$Y_n \propto E^2$$

$$Y_n \propto I^{3.3-4.7}$$

$$n \sim 10^{25} \text{ m}^{-3}$$



- The plasma focus has the special feature that is a self-scale kind of z-pinch. For devices in the energy range 1MJ to 0.1J of stored energy optimized for neutron emission:
  - axial rundown velocity and radial compression velocity has practically the same value, being  $4 \times 10^4$  m/s to  $1 \times 10^5$  m/s and  $1 \times 10^5$  m/s to  $2 \times 10^5$  m/s respectively
  - same ion plasma density in the pinch in the order of  $10^{24} \text{ m}^{-3}$  to  $10^{25} \text{ m}^{-3}$
  - same magnetic field in the pinch edge of order of 10 to 20 T
  - same Alfvén estimated to be above  $1 \times 10^5$  m/s
  - same temperature  $\sim 0.5$  to 1keV.

L. Soto et al., Plasma Sources Sci. Technol. 19,055017 (2010).

- Axial plasma shocks from table top plasma focus produce the same damage factor in materials than the expected in ITER and IFE.

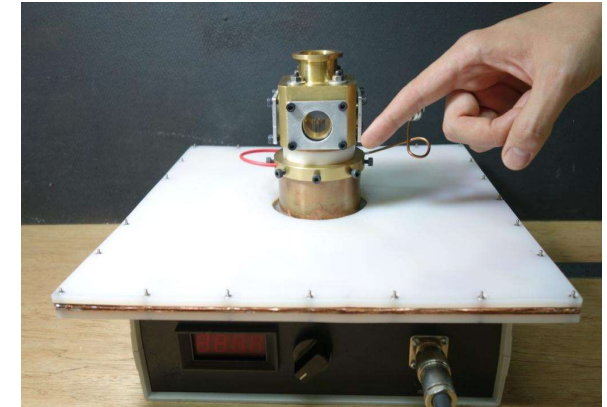
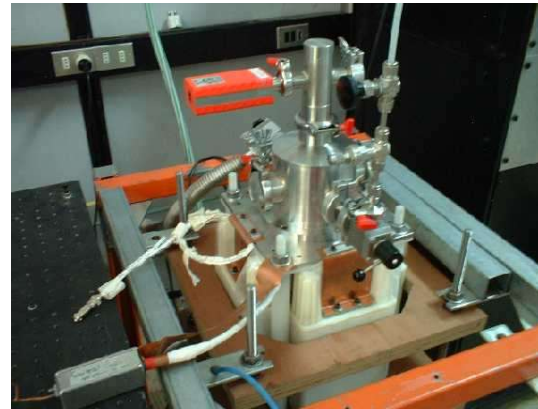
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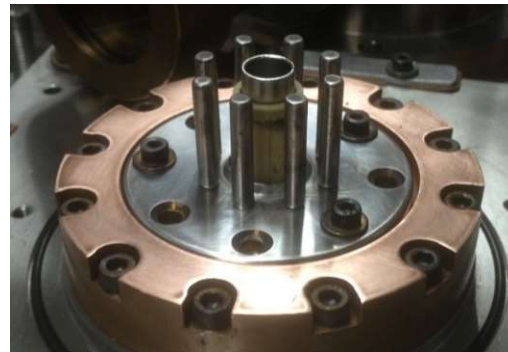
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# PF devices at CCHEN

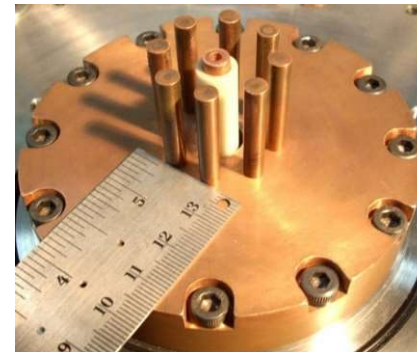
## kJ and under kJ



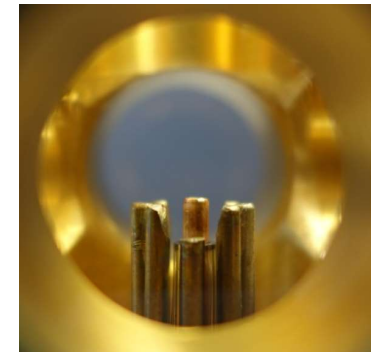
**PF-2kJ, 180kA**



**PF-400J, 130kA**



**PF-50J, 60kA**



**PF-2J, 15kA**



## PF- SPEED 2 187kJ, 4MA

# The Concept of Plasma Focus driven Fusion-Fission Hybrid Reactors

## Fu-Fi hybrid nuclear reactors. Background facts

- The concept of Fusion-Fission Hybrid Reactor involves a subcritical fission reactor driven by the neutrons generated in a nuclear-fusion device
- It was proposed already in the 1950s. Thus, the concept taken up in the 1970s (Hans Bethe 1979).
- Then interest declined, due to lack of economic incentive rather than technical difficulties.
- But it has increased over the last two decades because of its possible use in energy production, whether with uranium 235 or "breeding" uranium 233 from thorium, and also for the destruction of radioactive waste.

# Central Idea and Feasibility

- **Concept: surrounding a source of neutrons produced by fusion, with fissile material, so that it would function as a sub-critical reactor.**
- Synthesis of the fission reactor. For safety and control it is usual to limit the effective multiplication factor at most to about 0.95 in thermal reactors, which greatly limits the amplification factor. This limit was overcome with the concept of **a cascade reactor** introduced at the beginning of the fifties, being still sub-critical the reaction.
- **There is still no general consensus on which would be the optimum fusion device that can be used as neutron source to feed the subcritical cascades.** There are energetic, economic, and geometrical constraints which should be considered and balanced; but recent theoretical studies suggest that simplicity and volume would be the key concepts. Among the possible candidates to comply with these requirements, Plasma Focus (PF) devices have emerged as a very interesting alternative, bringing about the concept of Plasma-Focus driven Fusion-Fission Hybrid Reactors (PF-FFHR).

## Central Idea and Feasibility

- There are a **few studies** that entertained the idea of **using a PF device as the seed of neutrons for a hybrid fusion–fission system** (Gribkov and Tyagunov, 1983; Zoita and Lungu, 2001). Those **studies analyzed the simplest array of a single subcritical region hosting a PF device, concluding that, achieving break-even conditions would require energies as high as 10 MJ capable of deliver currents of 20 MA in 1 μs to produce pulses of 10<sup>18</sup> neutrons. Alas, that sort of figure is out of the range of the current technology.** In effect, although since their invention 50 years ago several projects were carried out to push higher the upper energy limit of PF facilities, the neutron production ceases to increase beyond 1 MJ (Nukulin and Polukhin, 2007; Lee, 2009).



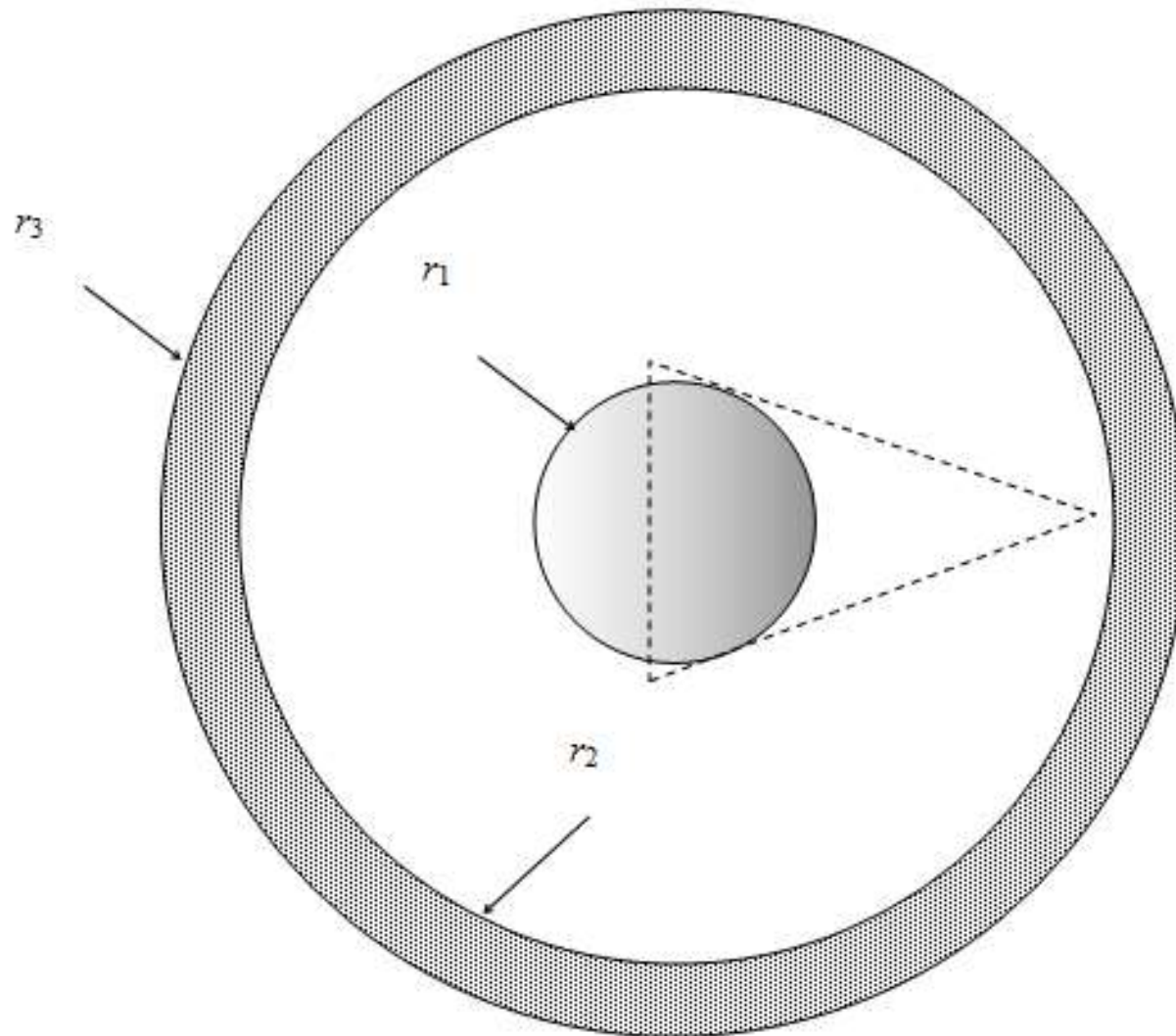
# Our approach

Details in A. Clause, L. Soto, C. Friedli and L. Altamirano “Feasibility study of a hybrid subcritical fission system driven by Plasma-Focus fusion neutrons”, *Annals of Nuclear Energy* 78, 10-14 (2015)

- In this work our approach consists in a “**Cascade Fission Nuclear Reactor Maintained by Fusion Neutrons from a Central Plasma Focus (PF)**”
- The analysis starts from the model of a two-stage cascade presented by [Barzilov et al. \(1996\)](#), which is here specified for a spherical geometry, deriving a set of equations to assess the neutronic amplification in terms of the geometric parameters.
- **The occurrence of optimum configurations is determined here for two spherical fission blankets, varying the size of each region while keeping constant the total volume of the system.**

# Cascade Fission Nuclear Reactor Maintained by Fusion Neutrons from a Central Plasma Focus (PF)

- It consists of two multiplicative sections whose coupling is not symmetrical, so that neutrons produced in the first section easily penetrate the second while those produced in the second have little effect on the first (see Figures 1 and 2)
- Selective absorption and geometric arrangement are used to approach the ideal cascade (in which the feedback from the region 2 is null). And the design of section 1 generates faster neutrons, that can reach the 2, where they are multiplied and, being greater its moderation there, they become more thermal. But these hardly reach the region 1 through an absorbent of the thermal. On the other hand, figure 1 shows how the geometry also collaborates in this.
- A sustained oscillatory regime is produced by a periodic train of neutron pulses from the central PF, amplified in the two fission sections, each treated, as already said, analytically and numerically with diffusion equations of a single neutron-group, and corroborated the results with Monte Carlo calculations.



*Figure 1.* Spherical cascade diagram consisting of a central multiplicative core surrounded by a multiplicative spherical shell.

## Neutron-monogroup equations, both prompt and delayed, governing the density $C(x, t)$ of the precursor atoms and that of neutrons $n(x, t)$

$$\frac{\partial n}{\partial t} - Dv \nabla^2 n = -\Sigma_a v n + (1 - \beta) \bar{v} \Sigma_f v n + \lambda C + S$$

$$\frac{\partial C}{\partial t} = -\lambda C + \beta \bar{v} \Sigma_f v n$$

The spatial distribution of neutrons is described with the Helmholtz equation:

$$\nabla^2 n + B^2 n = 0$$

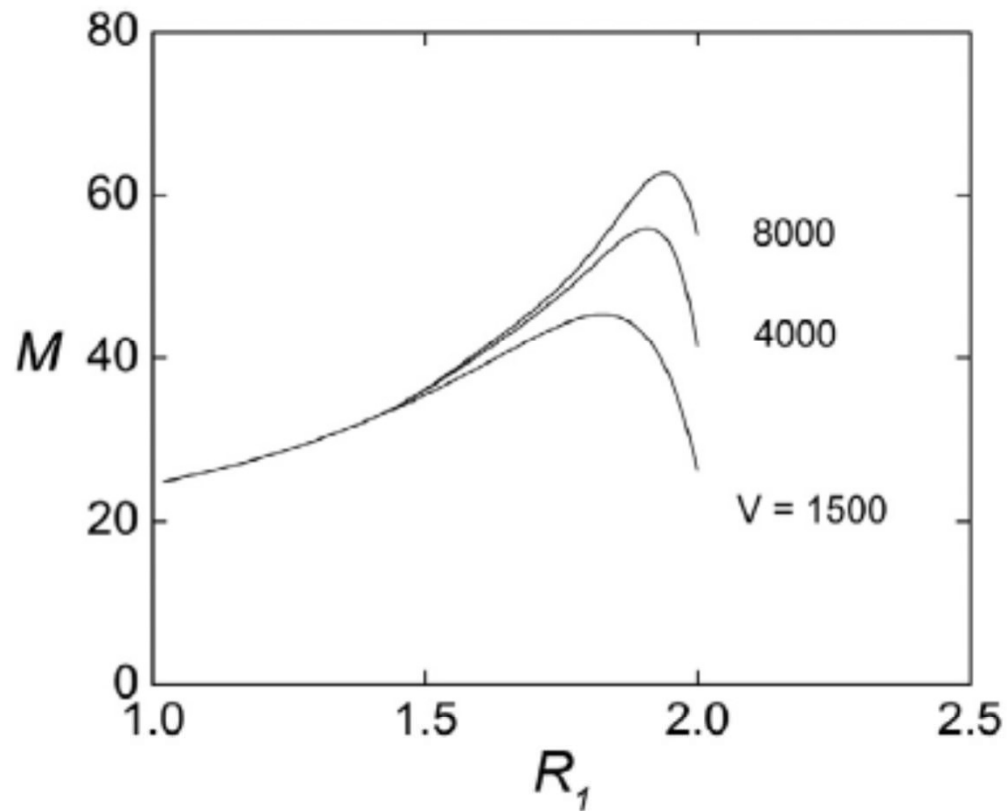
# Analytical results for the cascade, from the neutron-monogroup model and the geometric configuration of the hybrid system

Analytical expressions are obtained for the amplification factor  $M$ , the asymmetry  $\varepsilon$  and the coupling  $c$ , which have been defined, respectively, by:

$$M = \frac{F_1 + F_2}{S_1 + S_2} \quad \varepsilon = \frac{S_1}{S_1 + S_2} \quad c = \frac{\left(\frac{1}{p_1} - \frac{k_{\infty 1}}{k}\right) \left(\frac{1}{p_2} - \frac{k_{\infty 2}}{k}\right)}{\left(\frac{1}{p_1} - 1\right) \left(\frac{1}{p_2} - 1\right)}$$

In these relationships:

- $M$  is the total number of fission neutrons per neutron inserted by the sources.
- $F_1$  and  $F_2$  are the number of fission neutrons produced in regions 1 and 2, respectively.
- $S_1$  and  $S_2$  are the densities of the neutrons that enter per second in 1 and 2, respectively.
- $p_1$  and  $p_2$  are the probabilities that neutrons *will NOT come out* from 1 and 2, respectively.
- $k$ ,  $k_{\infty 1}$ , and  $k_{\infty 2}$  are the total effective, and the infinite multiplication factors of regions 1 and 2, respectively.



**Fig. 2.** Amplification factor of the spherical cascade for different volumes of 8%-enriched Uranium ( $k_\infty = 1.18$ ) calculated with the analytical approximation given by Eqs. (12)–(14). All dimensions are given in units of the diffusion length times  $\pi$ . The effective multiplication factor of the whole system is in all cases  $k = 0.95$ .

## Corroboration using the code Monte Carlo MNCP5

- The analytical results were corroborated with the Monte Carlo code MCNP5.
- Effective multiplication factors  $k = 0.95$  and  $k_{\infty} = 1.18$  (also  $k_{\infty} = 2$ ), and spherical symmetry.
- Metallic uranium with enrichment of 8%.
- 14.1 MeV neutron point source, which simulates D-T PF.
- Figures 3, 4 and 5 show some of the results.
- A conservative PF energy value for "break-even", was obtained, namely,  $E_{PF} \sim 4000 \text{ kJ} / M$ .

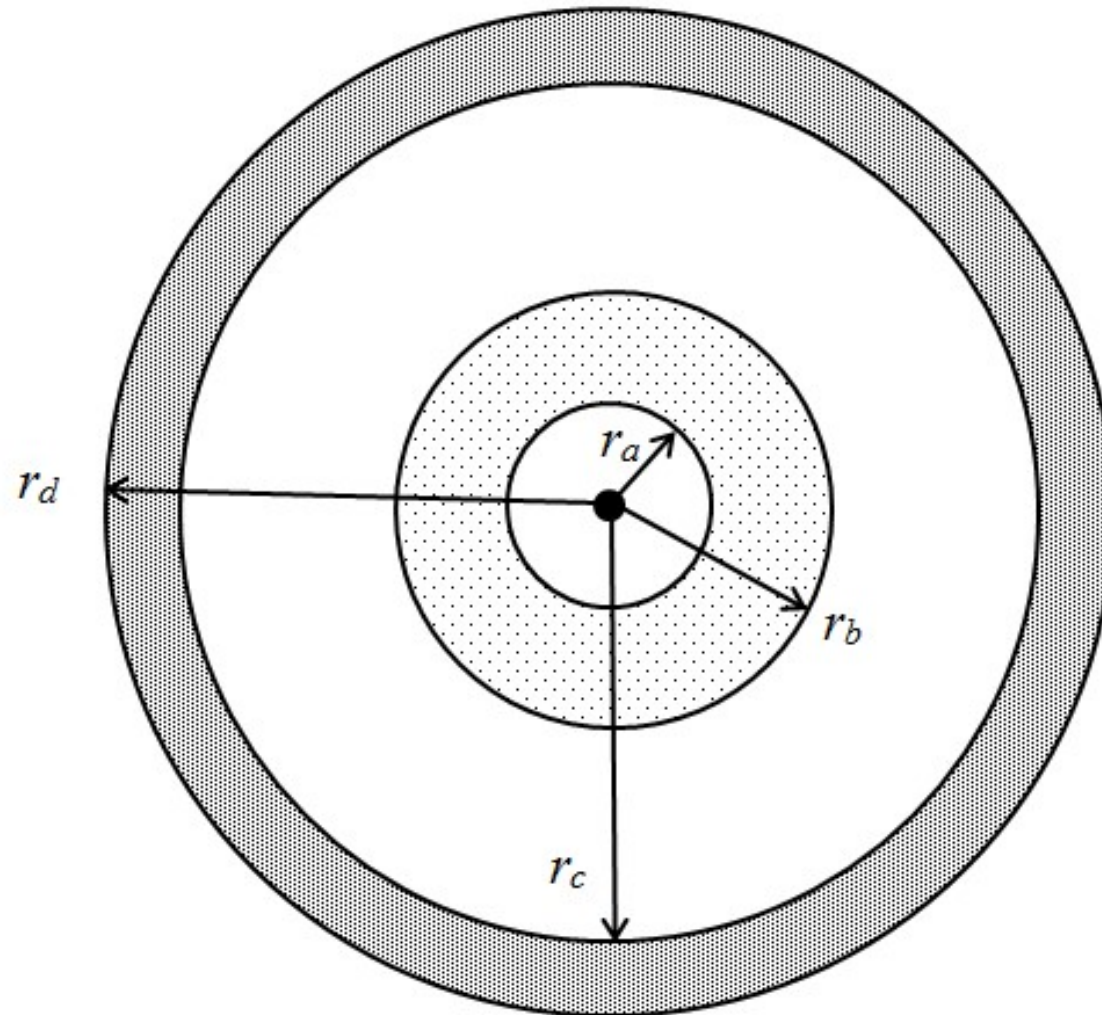
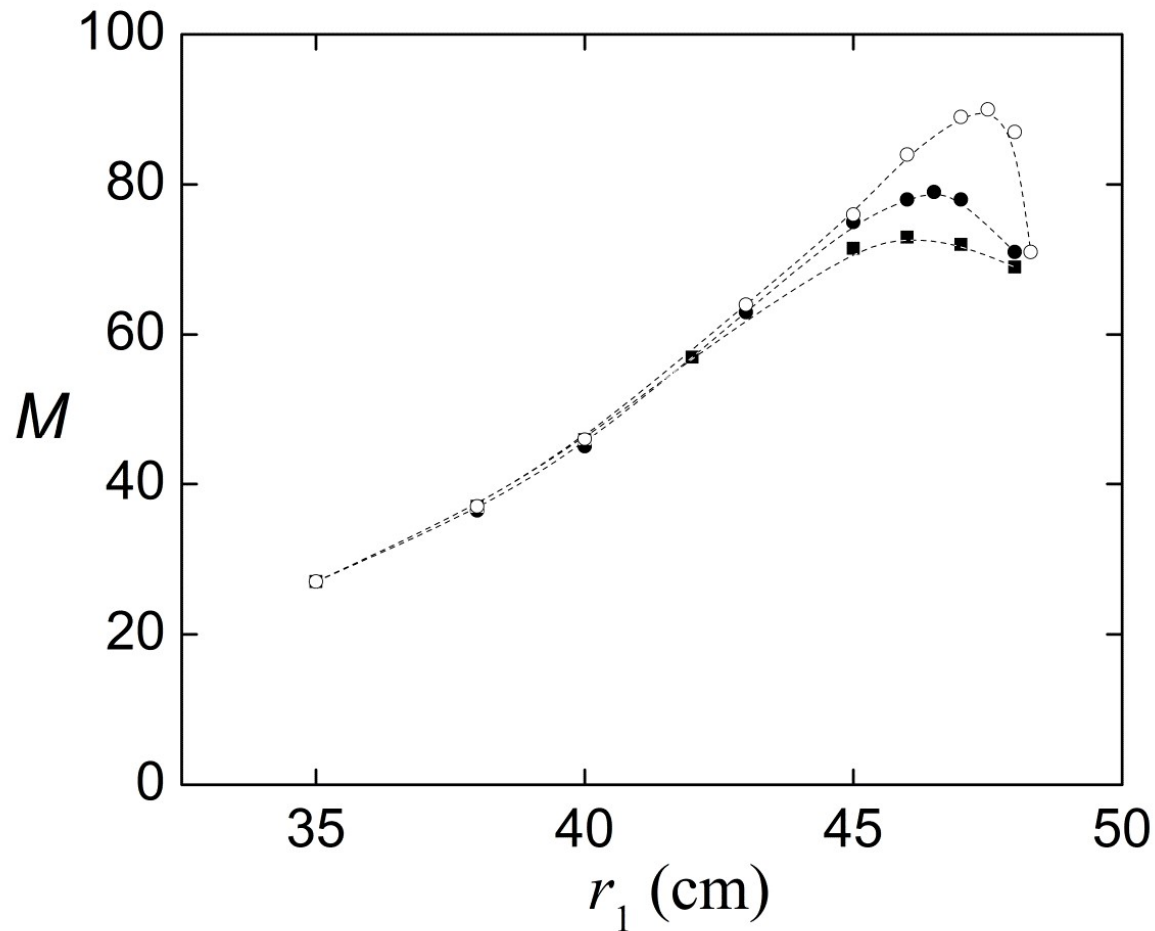


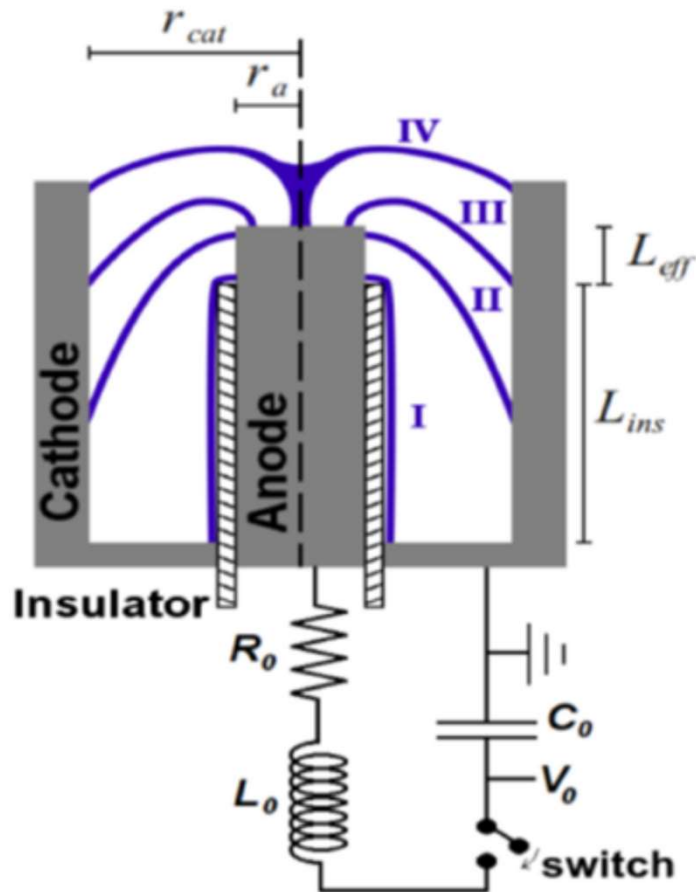
Figure 2. Configuration of the spherical cascade used in the Monte Carlo calculations.





**Figure 3:** Monte Carlo results for the amplification coefficient  $M$  in spherical cascade of volumes: 4.2 m<sup>3</sup> (■), 11.3 m<sup>3</sup> (●) and 22.6 m<sup>3</sup> (○). Effective multiplication factor  $k = 0.95$  and radius  $r_a = 20$  cm from the center of the PF to the limit of the vacuum surrounding it (see Fig. 2).

# Neutron pulses due to Fusion in Central Plasma Focus



$$\text{D-D} : Y \sim 10^7 E^2$$

$$\text{D-T} : Y \sim 10^9 E^2$$

$Y$ : neutron yield per pulse

$E$ : bank energy for the PF, in kJ

$$Y(E_{PF}) \cong 10^9 \text{ kJ}^{-2} E_{PF}^2 \quad (23)$$

The number of fissions produced by  $Y$  is then  $(M/\bar{\nu})Y(E_{PF})$ . Considering that the fissile fuel is  $U^{235}$  ( $193 \text{ MeV} \cong 3 \cdot 10^{-14} \text{ kJ}$  per fission,  $\bar{\nu} \cong 2.43$ ), the fission energy produced in each shot is:

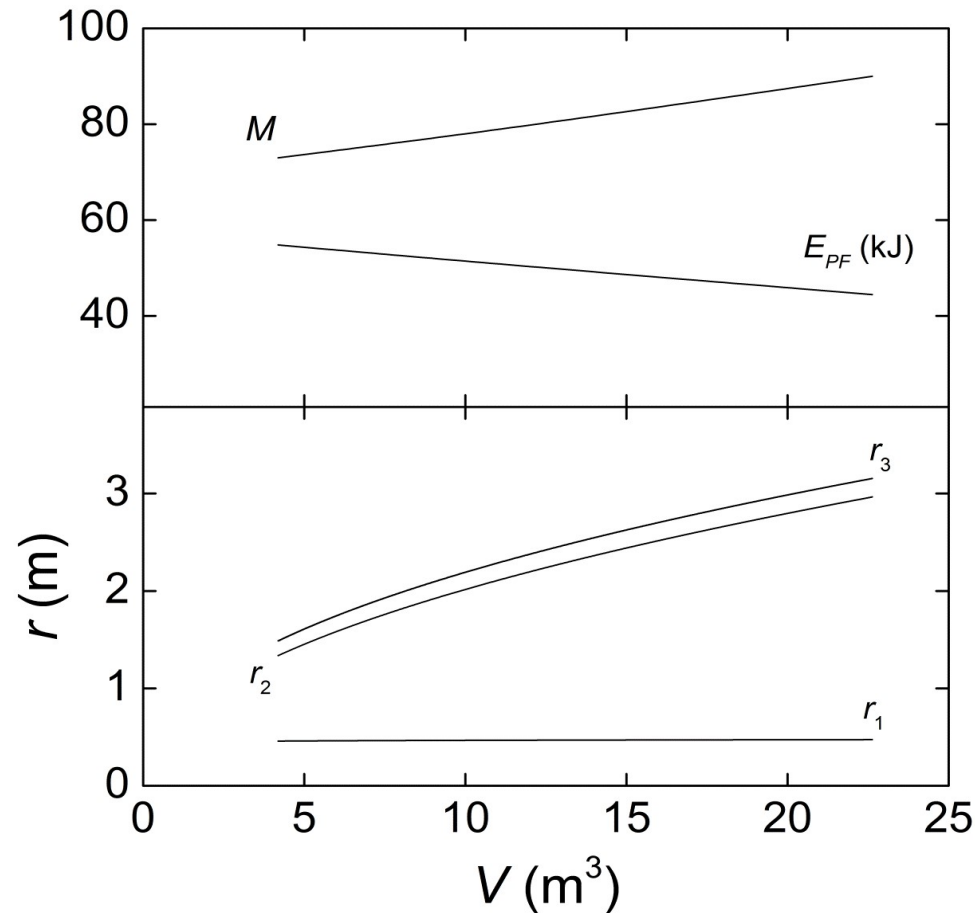
$$E_f \cong 1.23 \cdot 10^{-5} \text{ kJ}^{-1} E_{PF}^2 M \quad (24)$$

Now, only a small part of the energy of the capacitor bank is consumed in the pinch to produce the thermal conditions for fusion reactions. A reasonable figure of this fraction is about 5% (González et al., 2009). In that case, the fusion–fission break-even condition satisfies:

$$0.05 E_{PF} \cong 1.23 \cdot 10^{-5} \text{ kJ}^{-1} E_{PF}^2 M \quad (25)$$

Therefore, the  $PF$  energy required for hybrid break-even is given by:

$$E_{PF} \cong \frac{4000 \text{ kJ}}{M} \quad (26)$$



**Figure 4.** Optimal amplification factor, PF energy for "break-even" and geometric parameters of the spherical cascade as functions of the volume of 8%-enriched Uranium, calculated with MCNP.

Considering an optimal value of the total number of fission neutrons per neutron inserted by the sources,  $M \sim 80$ ,

From the relation;

$$E_{PF} \cong \frac{4000 \text{ kJ}}{M} ,$$

the energy of the Plasma Focus required for break-even in the optimum spherical configurations for the range of volumes considered in the MCNP calculations is about 50 kJ, which is within the range provided by the current technology.

Moreover, the reactor external radius is about 2 m, which is also a feasible figure.

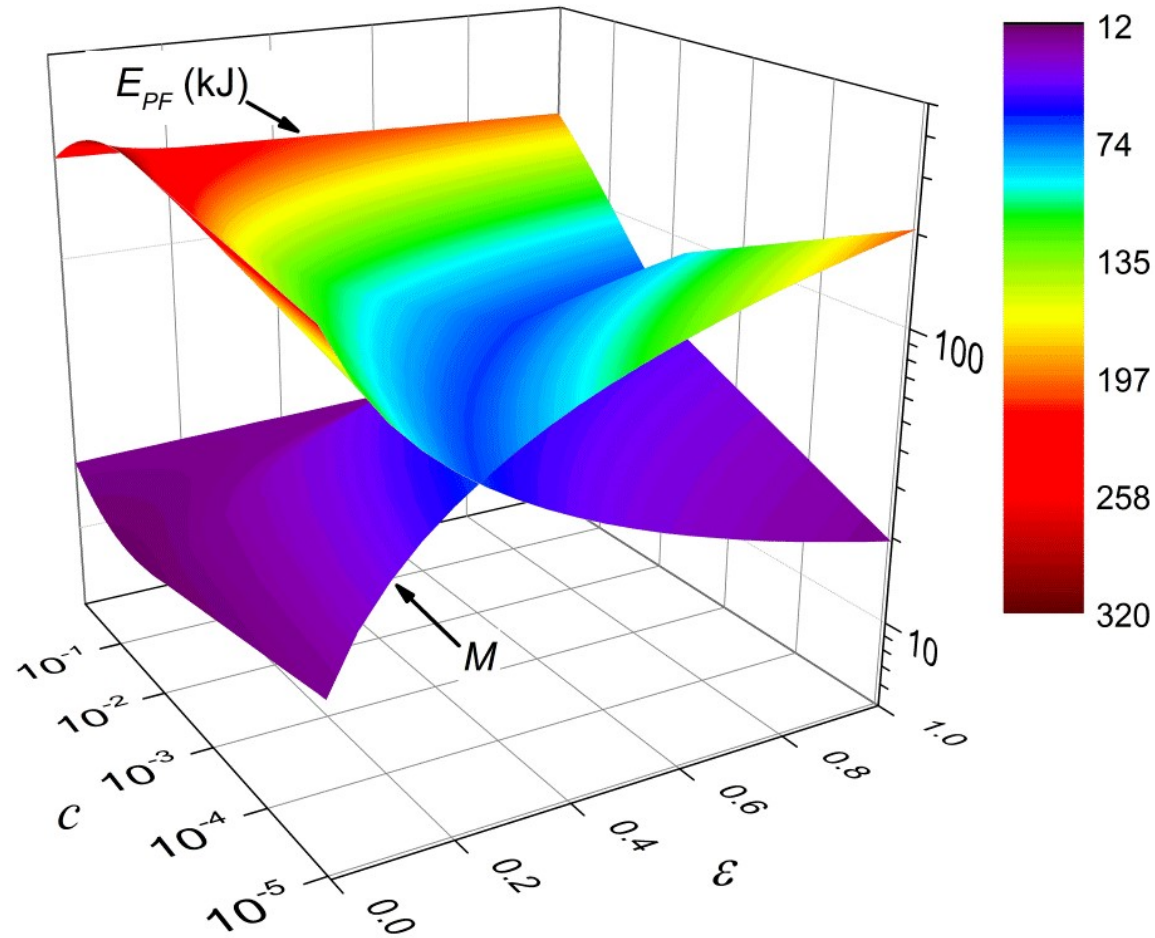


Figure 5. Amplification coefficient  $M$  and energy  $E_{PF}$  of the plasma focus at the break-even equilibrium point in the case of  $k_1 = k_2 = k$  sub-critical cascade ( $k_\infty = 2, k = 0.95$ )

- The feasibility of a hybrid fusion–fission system consisting of a two-stage spherical subcritical cascade driven by a Dense Plasma Focus was studied.
- An analytical model based on the one-group neutron diffusion equation was developed to estimate the amplification achieved per source's neutron knowing the neutronic parameters of each region. The conditions for energy break-even for this hybrid concept were assessed. It was found that in principle the concept is feasible given the current Plasma-Focus technology (PF of tens of kJ).
- The results were corroborated by means of Monte Carlo calculations and a design chart was produced for assessing the optimum configuration of the spherical cascade to achieve different levels of neutron amplification.

- The energy of the Plasma Focus required for break-even in the optimum spherical configurations for the range of volumes considered in the MCNP is about 50 kJ, which is within the range provided by the current technology. Moreover, the reactor external radius is about 2 m, which is also a feasible figure.
- The present novel analysis of PF-driven two-region reactors is valuable regarding that the technology of PF neutron sources, in spite of its limited neutron yield, is currently more advanced than their counterparts based in inertial fusion.
- The remaining challenge is to increase the discharge rate of PF devices of tens of kJ in order to achieve reasonable power outputs.



Thank you for your attention

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