

ORIENT-NM - Organisation of the European Research Community on Nuclear Materials

CROSS-CUTTING ISSUES IN FUSION AND FISSION MATERIALS DEVELOPMENT

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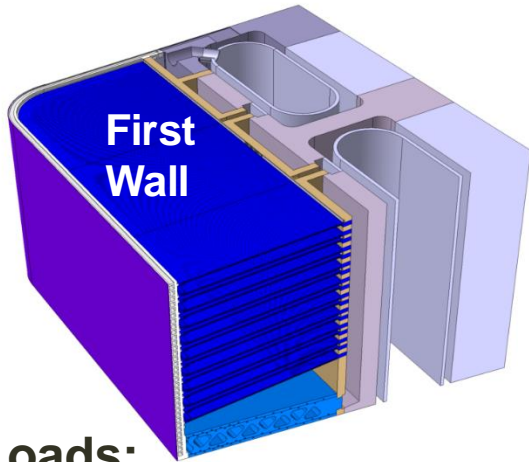
This project has received funding from the Euratom research and training programme 2019/2020 under grant agreement No. 899997

Outline:

- **Harsh conditions in fusion, fission and other energy technologies**
- **F/M steels as intersection materials**
 - **Cyclic softening/hardening**
 - **Plastic flow localisation**
 - **Improvement of creep strength**
 - **Ion irradiation as screening technique**
 - **Materials acceleration platforms**

Materials for plasma-near DEMO components will need to withstand unprecedented conditions

Blanket



Loads:

$\leq 2.5 \text{ MW/m}^2$

$\leq 25 \text{ dpa/fpy}$

$\leq 250 \text{ appm He/fpy}$

Materials

EUROFER

(9Cr RAF/M steel)

350–550°C,

400 appm He*

EUROFER-ODS

400–650°C

Tungsten alloys

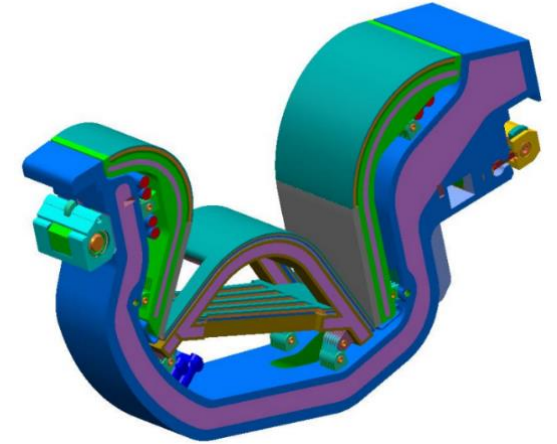
800–1100°C

Cu-1%Cr-0.1%Zr

(heat sink, high conductivity: 350
W/m/K)

fpy \equiv full power year

Divertor



Loads:

$\leq 10 \text{ (20) MW/m}^2$

$\leq 10 \text{ dpa/fpy}$

$\leq 100 \text{ appm He/fpy}$

Coolants: water, helium, (heavy) liquid metals (PbLi), in some designs simultaneously used

These are extremely high thermo-mechanical, neutron irradiation and environmental loads:
difficult to find equivalent conditions in other technologies

Nuclear fission GenIV systems also envisage largely unprecedented conditions for materials

~~framatome~~ ~~cea~~ ~~EDF~~

~~ASTRID~~

$T_{in}/T_{out} = 350/550^{\circ}\text{C}$
 Max. dpa 150
 60 yrs lifetime

~~Liquid Sodium Cooled Fast Reactor (SFR)~~

ALFRED **FALCON**

Lead-Cooled Fast Reactor

$T_{in}/T_{out} = 400/520^{\circ}\text{C}$
 Max. dpa 100
 LM corrosion

Liquid Lead Cooled Fast Reactor (LFR)

ALLEGRO **V4G4**

$T_{in}/T_{out} = 490/850^{\circ}\text{C}$
 Max. dpa 80

Gas Cooled Fast Reactor (GFR)

Control Rods
 Graphite Reflector Core
 Pump
 Blower
 Helium Coolant
 Heat Exchanger

VHTR
 Very-High-Temperature Reactor

$T_{in}/T_{out} = 650/1000^{\circ}\text{C}$
 Max. dpa 10

NC2I
 Nuclear Cogenation Industrial Initiative

(Very) High Temperature Reactor (HTR)

Control Rods
 Supercritical Water

$T_{in}/T_{out} = 280/625^{\circ}\text{C}$
 HT SCwater corrosion

NUGENIA
 Nuclear Generation II&III Alliance

SuperCritical Water Cooled Reactor (SCWR)

$T_{in}/T_{out} = 200/340^{\circ}\text{C}$
 LM corrosion

MYRRHA
sck cen
 Belgian Nuclear Research Centre

Accelerator Driven System (ADS)

MSR

Currently emerging, several startups

$T_{in}/T_{out} = 620/<750^{\circ}\text{C}$
 Max. dpa 80
 MS corrosion

Molten Salt Reactor (MSR)

GenIV systems according to GenIV Intl. Forum (2001) + ADS



Beyond nuclear energy, also solar, bio and fossil thermal energy expose materials to extreme conditions

P. Heller, DLR



Point Focus Systems

- Steam: 560°C
- Molten Salt: 560°C
- Air/Helium: 700-1000°C
- Liquid Metals: 560°C
- Heat flux: up to 6 MW/m²



Line Focus Systems

- Synthetic Oil: 390°C
- Steam: 560°C
- Molten Salt: 560°C

	Fossil-fuel (Coal)	Biomass (Wood)	Biomass (Agriculture)	Waste
pO_2	~3%	~5%	~5%	6-11%
pH_2O	~10%	20-25%	20-25%	20-25%
Reactive alkali	Low	Medium	High	High
pSO_2	High	Low	Low	Low
$pHCl$	High	Low	Medium	High
Steam temperature (state-of-the-art)	630°C	570°C	450°C	420°C

Corrosion – environment + material + temperature



Mechanical properties – material + temperature

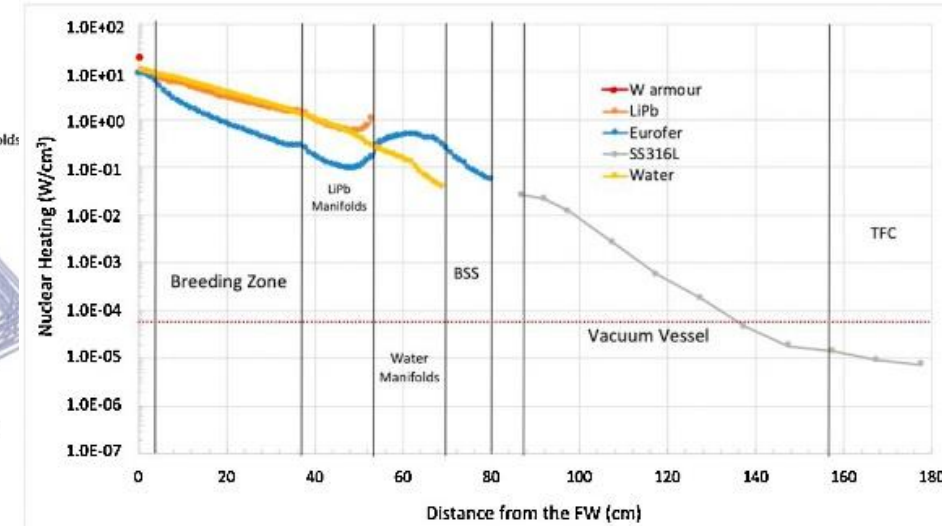
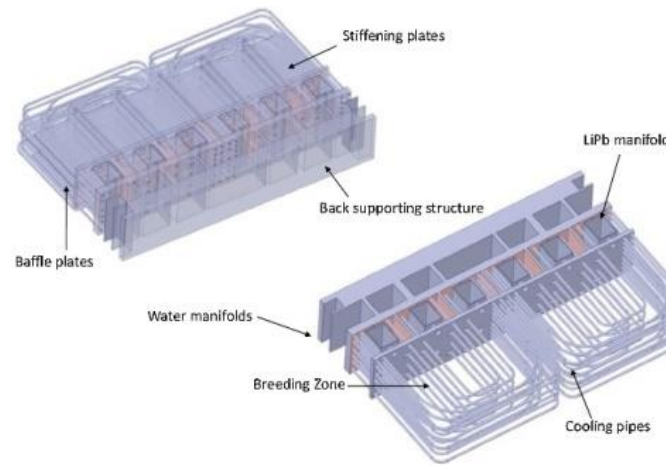
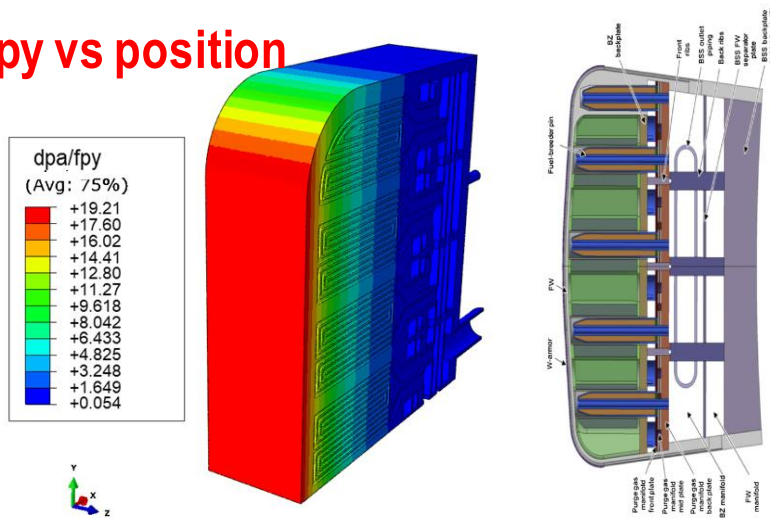


Four specificities of fusion: high helium production, high thermal shocks, activation of large quantities of structural materials, tritium

HCPB DEMO breeding blanket

WCLL DEMO breeding blanket

dpa/fpy vs position



Fusion Engineering and Design 169 (2021) 112428

Fusion Engineering and Design 168 (2021) 112514

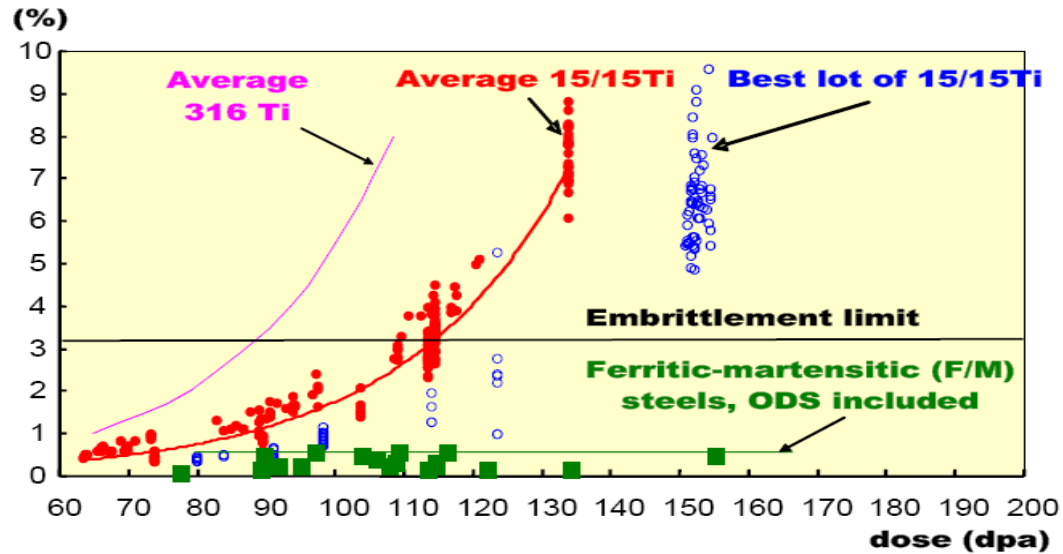
- ❑ A few centimeters make a big difference as they suffer from:
 - ❖ High He/dpa ratio: ~ 10 He appm/dpa in the steel (fusion) $\gg 0.1$ He appm/dpa (GenIV)
 - \Rightarrow Fission reactor irradiation is relevant for most structures except for these “few cm”
 - ❖ High heat flux: ~ 1 MW/m² – no equivalent in fission, comparable with solar applications
 - ❖ High heat load: $\sim 1-10$ W/cm³ in the steel and even more in tungsten
 - Special heat flux protection solutions are needed

- ❑ In addition,
 - ❖ Large quantities of material will become activated - no equivalent quantities in fission
 - \Rightarrow Reduced activation materials to facilitate decommissioning
 - ❖ Tritium production and extraction
 - \Rightarrow Tritium permeation barriers

Common structural materials for fission and fusion applications

Fission Materials	System	Fusion Materials	Component
Low alloy steels (e.g. SA-508)	(V)HTR, SCWR, current LWR	Tungsten alloys	Plasma facing components, divertor
Zr-alloys (cladding)	LWR	Cu alloys (CuCrZr)	Divertor, heat transfer components
Ni-based alloys (Hastelloy X, Inconel 617, Haynes 230, ...)	(V)HTR, SCWR, MSR, GFR, (SFR)	Reduced activation F/M steels (grade 91,92 (Eurofer, F82H, CLAM, ...))	All structural components in first wall, blanket, divertor
F/M steels (grade 91,92 (T91, EM10, ...), grade 122 (HT9), grade 22, (future) FeCrAl)	(V)HTR, SFR, future ADS, future LFR, SCWR, LWR (ATF)	RAF/M ODS steels (9%Cr)	Plasma facing components or right below plasma facing components
F/M ODS steels (9 or 14 or even 20 %Cr)	future (V)HTR, SFR, ADS, LFR, SCWR, GFR	Austenitic steels (AISI 316L(N), Mn Auss, ...)	Vacuum vessel and other parts
Austenitic steels (AISI 316L(N), 15-15Ti, 800H, advanced versions (AIM1, AIM2, AFA, ...))	(V)HTR, SFR, ADS, LFR, SCWR, GFR	SiC/SiC composites, (SiC in other forms)	Perspective material for first wall and blanket
SiC/SiC composites, (SiC in other forms)	(V)HTR, GFR, LWR(ATF)?, (SFR, LFR)	C/C composites, Beryllium and other PFC possibilities	PFC for ITER or previous tokamaks
C/C composites and graphite	(V)HTR, (<i>old GenI/GenII reactors</i>)	Other and perspective materials (V alloys, refractory High Entropy Alloys)	Perspective materials for first wall, blanket and also divertor
Other and perspective materials (V, Mo alloys, Mo-ODS, High Entropy Alloys, Max phases)	(V)HTR, GFR, LFR, ADS, MSR		

Main intersection between fission and fusion materials are F/M steels. Why?



Main reason for using F/M steels in components exposed to high neutron-flux:
low swelling
(one or two orders of magnitude less than in austenitic steels ... with the caveat of He effects ...)

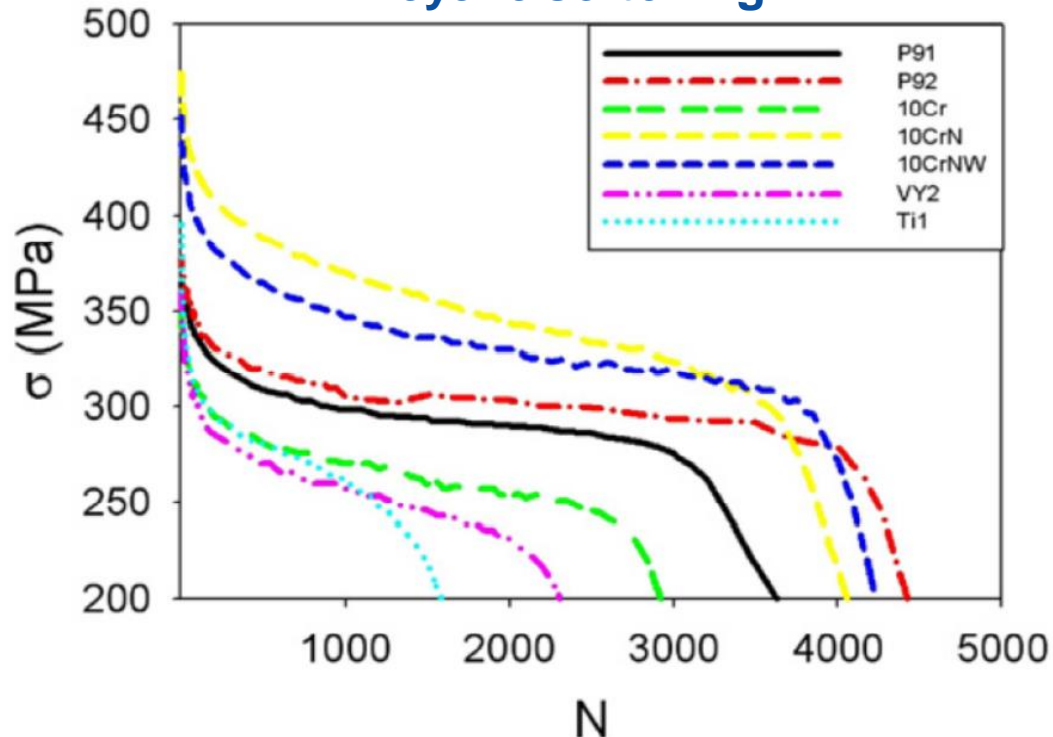
In addition ...	F/M steel	Austenitic steel
Thermal conductivity (W/mK)	26-30 >>	16-21
Thermal expansion ($10^{-6}/K$)	10-12 <	15-20
He production by transmutation	About the same or lower in F/M (with less swelling to start with)	
Price	About the same or lower in F/M (until 2010 Ni was >> expensive than Fe)	
Years for hands-on handling after irradiation	About 100	A few thousands

There are several examples of materials (F/M steel) issues that can be/ are being addressed jointly by fission and fusion

- ❑ Compatibility of structural materials with heavy liquid metals in terms of corrosion and also liquid metal embrittlement (applies to solar thermal energy, too);
- ❑ Barriers protecting structural materials from liquid metal corrosion, also investigated as hydrogen isotope barriers in fusion, to avoid tritium permeation;
- ❑ Design code rules whenever F/M steels behave differently from e.g. austenitic steels
- ❑ ...

Cyclic softening (F/M) vs cyclic hardening (AuSS)

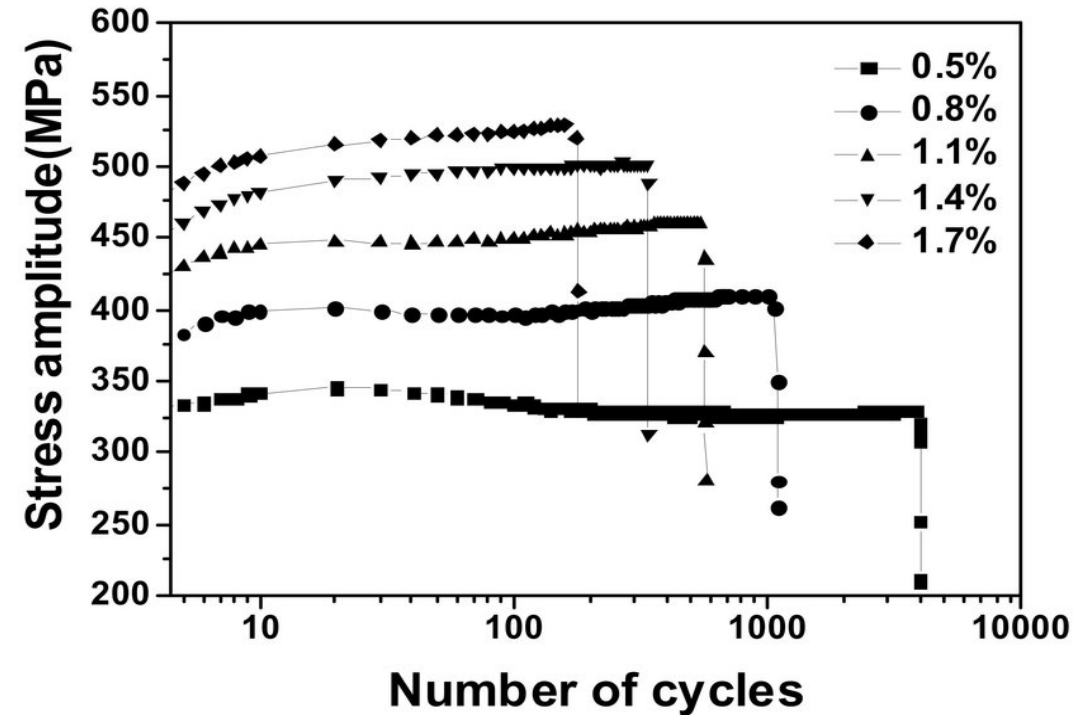
F/M steels, $\Delta\varepsilon_f=0.7\%$, $T=550^\circ\text{C}$ –
cyclic softening



Cabet et al. JNM (2019)

<https://doi.org/10.1016/j.jnucmat.2019.05.058>

316L stainless steel – cyclic hardening



Chungseok, Metals (2017) 8. 14.

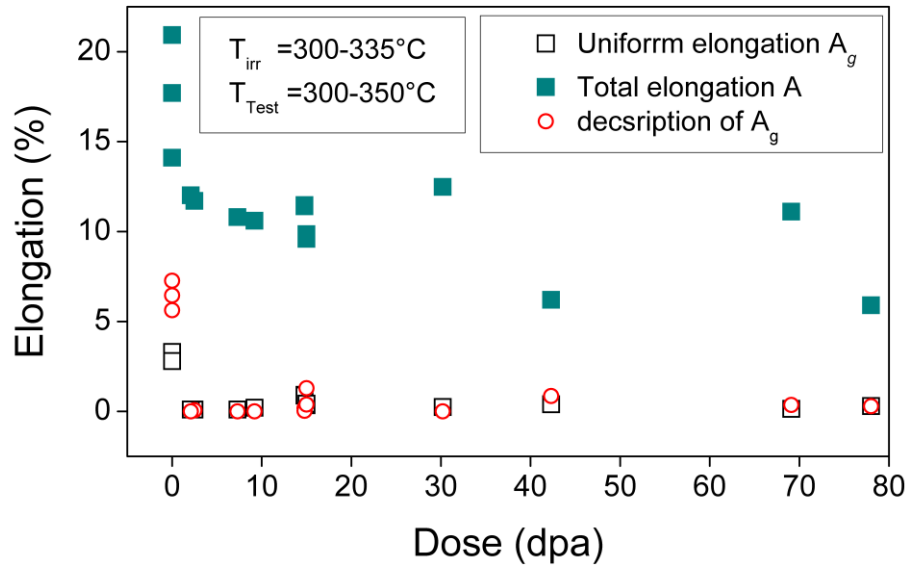
[10.3390/met8010014](https://doi.org/10.3390/met8010014)

The behaviour under fatigue conditions is qualitatively different between F/M and austenitic steels.

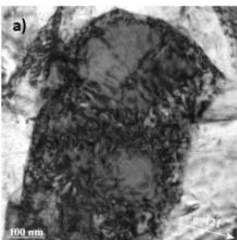
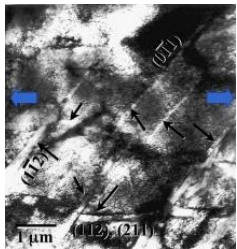
Design rules for austenitic steels are *not* extendable to F/M steels: need to understand, collect data and elaborate different criteria and rules

Localisation of deformation: problem and results

E. Gaganidze, J. Aktaa, Fusion Eng. Des. 88 (2013)



S. Zinkle, B.N. Singh, J. Nucl. Mater. 351 (2006)



Traditionally loss of elongation is attributed to creation of clear bands free of defects, removed by moving dislocations, observed in Fe

Electron microscopy on Eurofer97 in M4F suggests that in some grains loops are absorbed with dislocation wall formation → preferential channels for plastic deformation causing softening

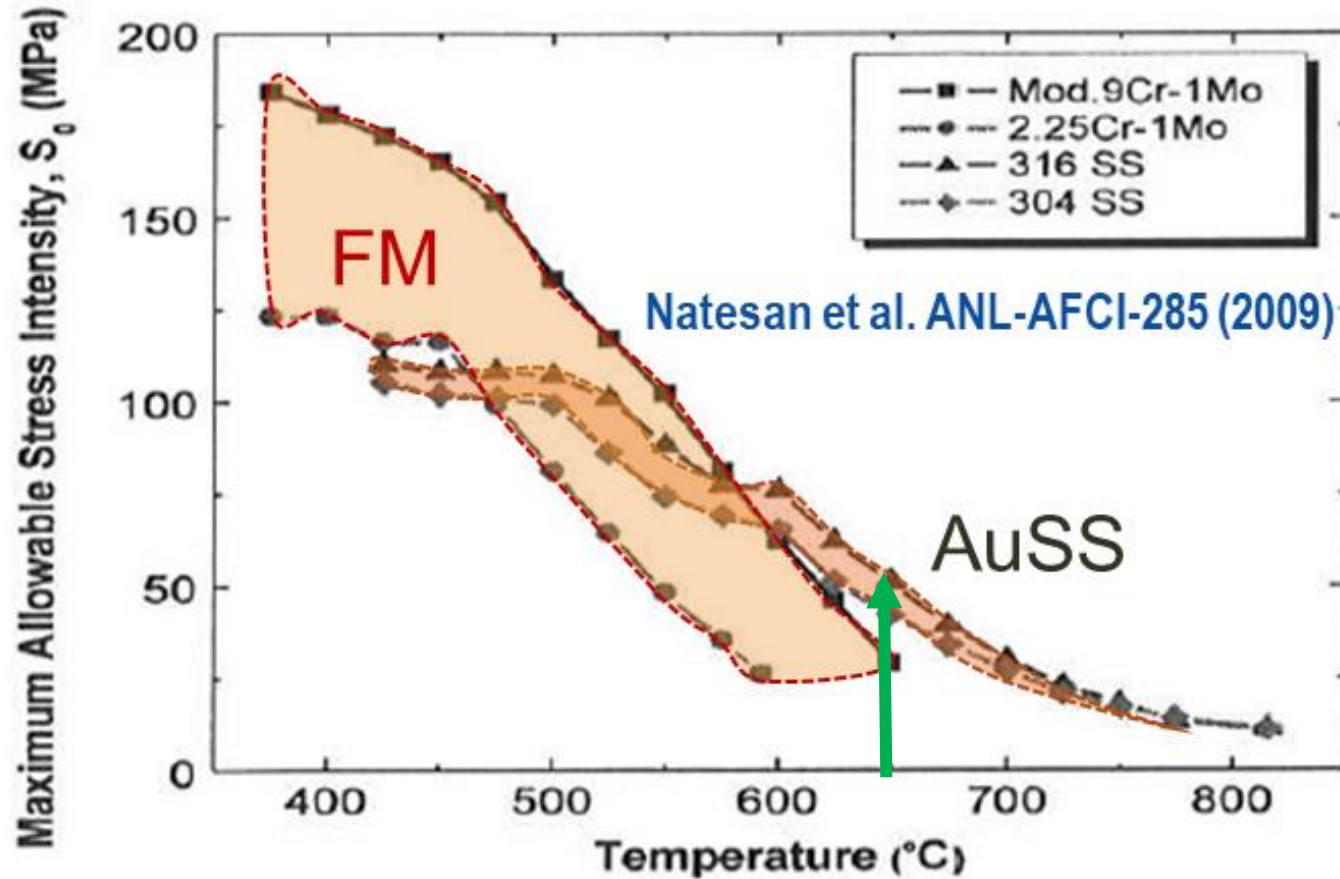
Problem:

Current design rules consider the elongation as only indicator of ductility → F/M steels are unusable according to this criterion!

- Three models were developed in M4F to address the problem of the effect of dislocation channel formation on mechanical behaviour in 9%Cr Fe alloys :
 - Mean field continuum model at aggregate level
 - Full field continuum model, also at aggregate level
 - Constitutive equations enabling FEM at component level
- Dose dependent formation of shear bands was correctly predicted

Tools to assess the effect of plastic flow localisation at the component level were produced, which are of use to produce design rules for both fission and fusion

Creep strength of F/M steels is somewhat worse than austenitic steels: improvement is needed

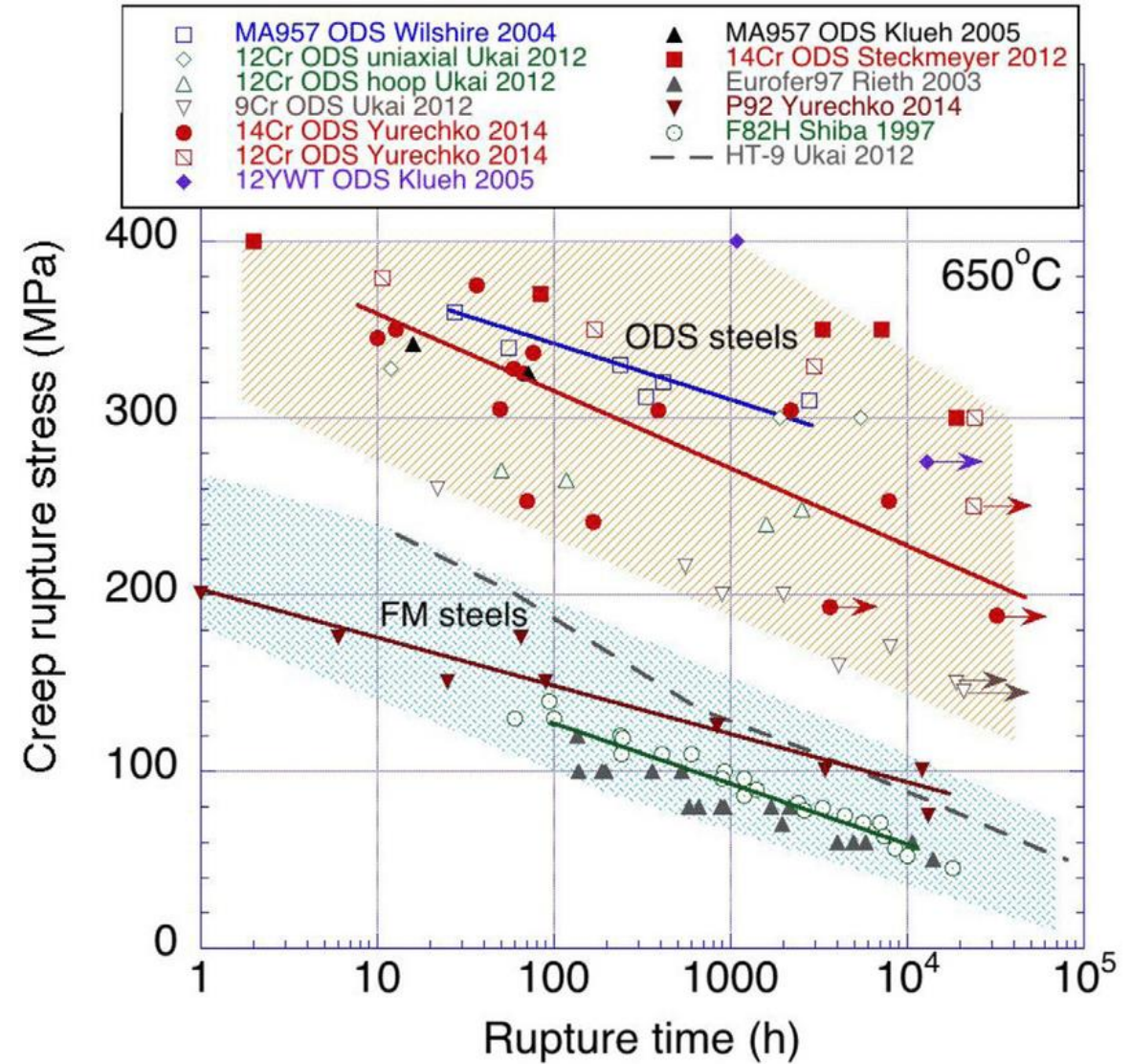
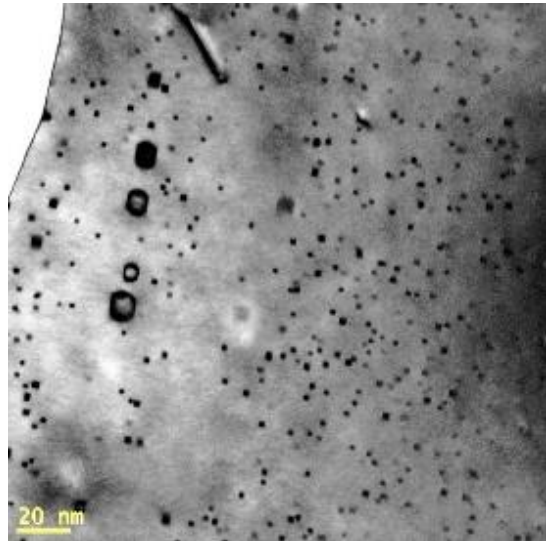
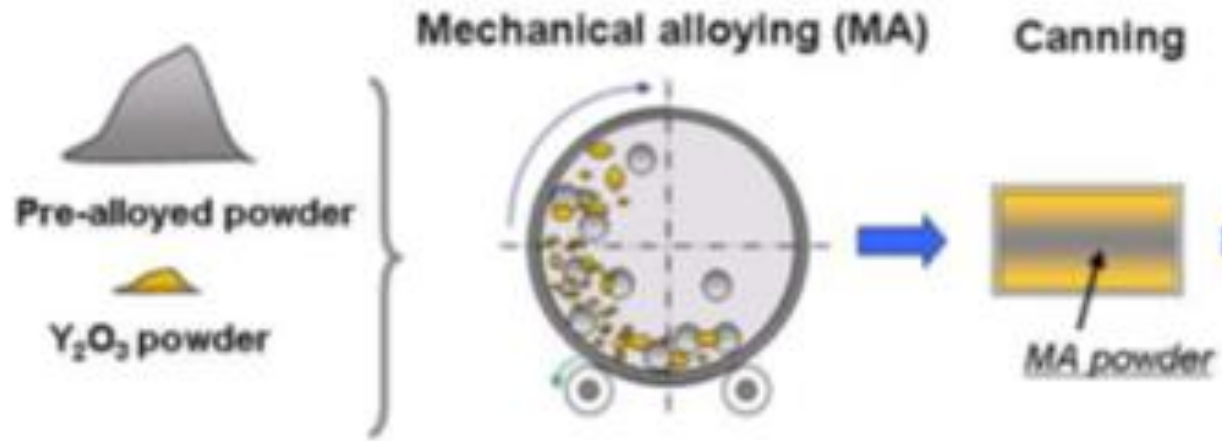


Increase of creep strength is beneficial for ANY high temperature application

Two routes:

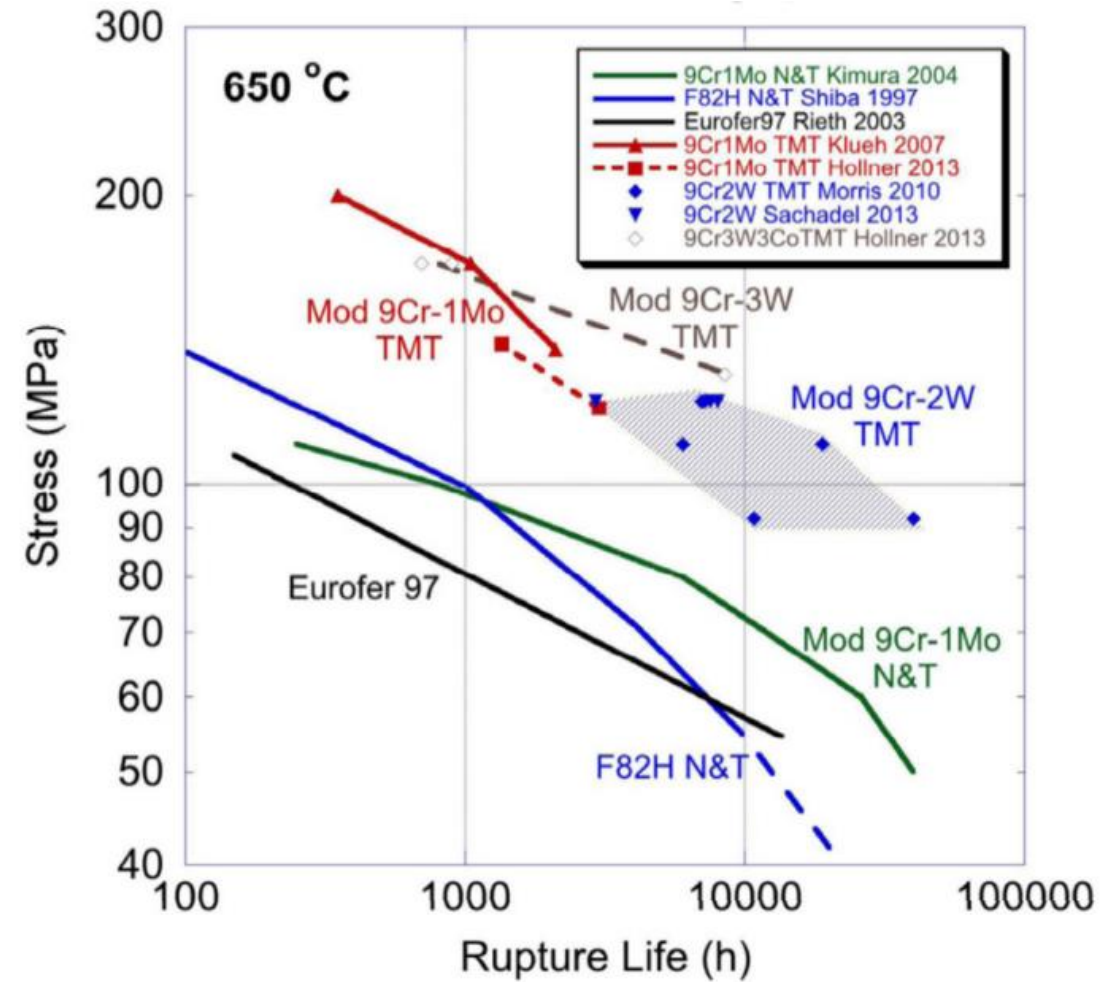
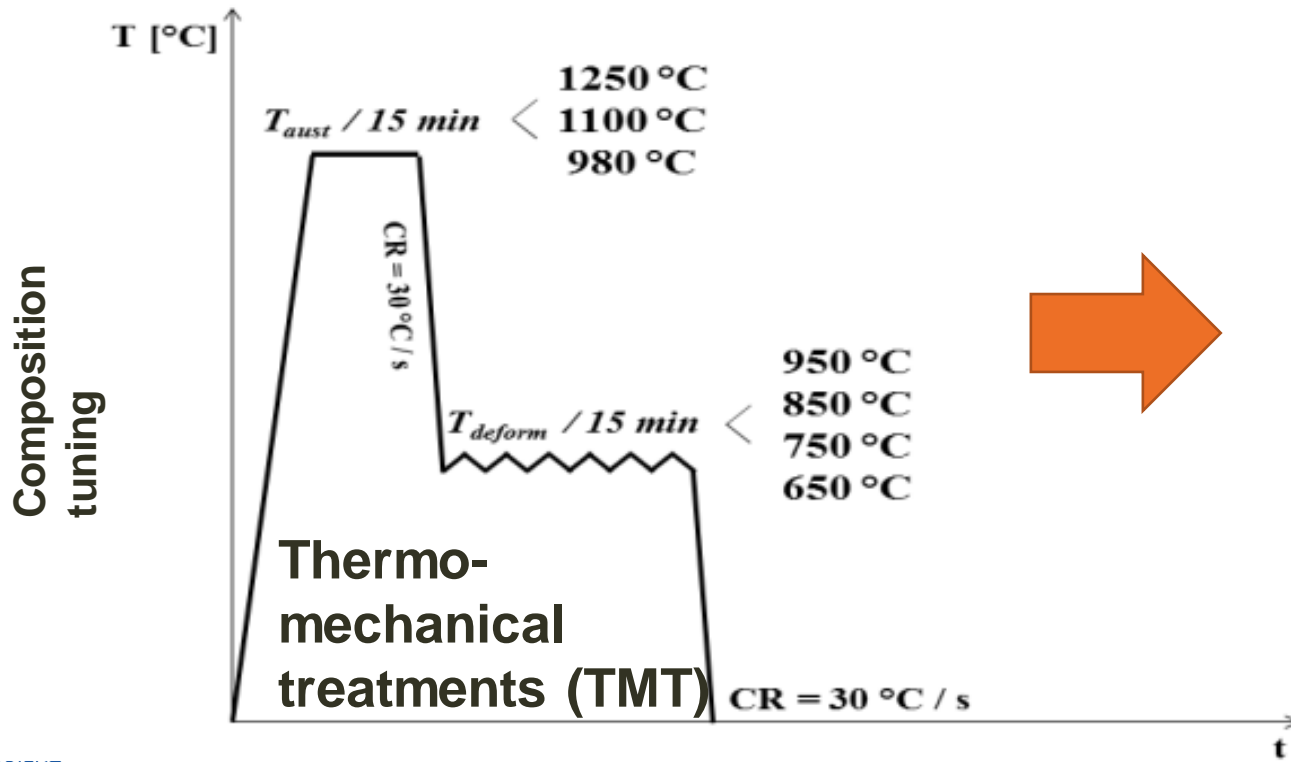
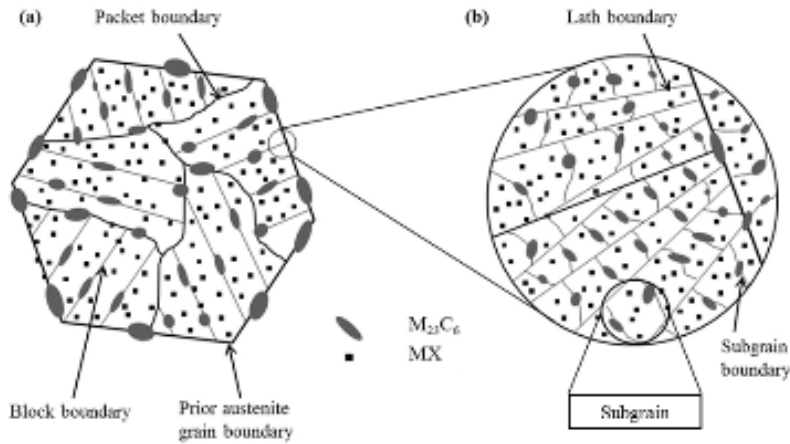
- Oxide dispersion strengthened steels**
- Creep-strength enhanced steels**

Oxide dispersion strengthened steels



Zinkle et al. Nucl. Fusion 57
(2017) 092005

Creep-strength enhanced steels



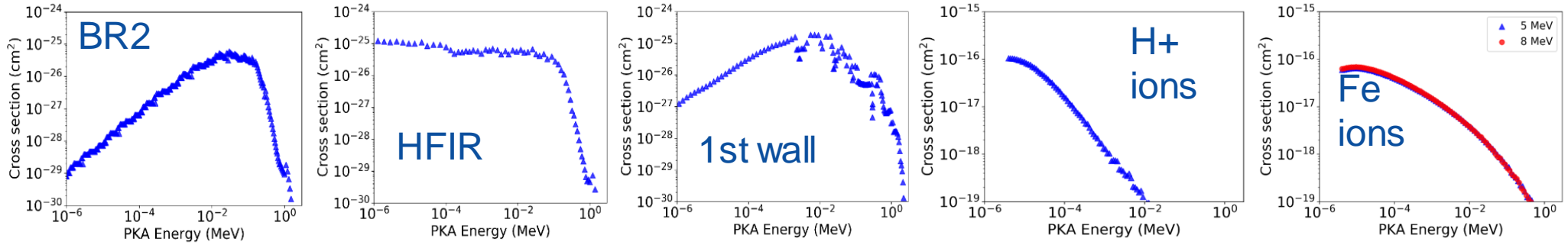
These developments can be accelerated using modern, digital tool-based, techniques

Zinkle et al. Nucl. Fusion 57 (2017) 092005

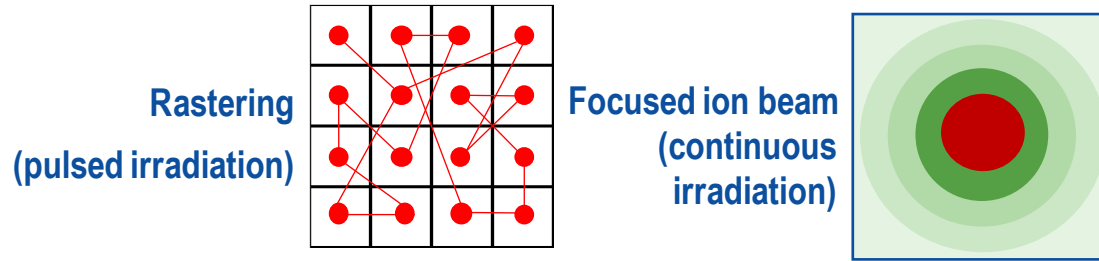
Ions as nuclear materials screening tools: transferability issues

Different PKA spectrum and thus different damage

Different dpa rate

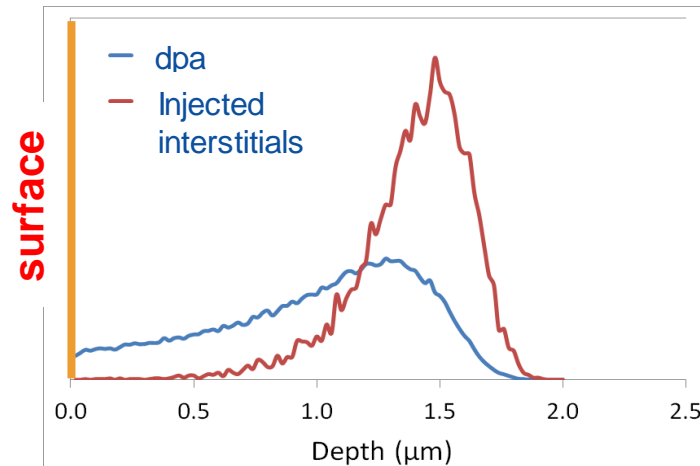


Rastering versus defocusing



Is it possible to minimise these effects?

Limited penetration, closeness of surface
Damage profile, damage gradient
Injected interstitials



1) Microstructure evolution models for “transfer function”

2) Explore conditions through characterization

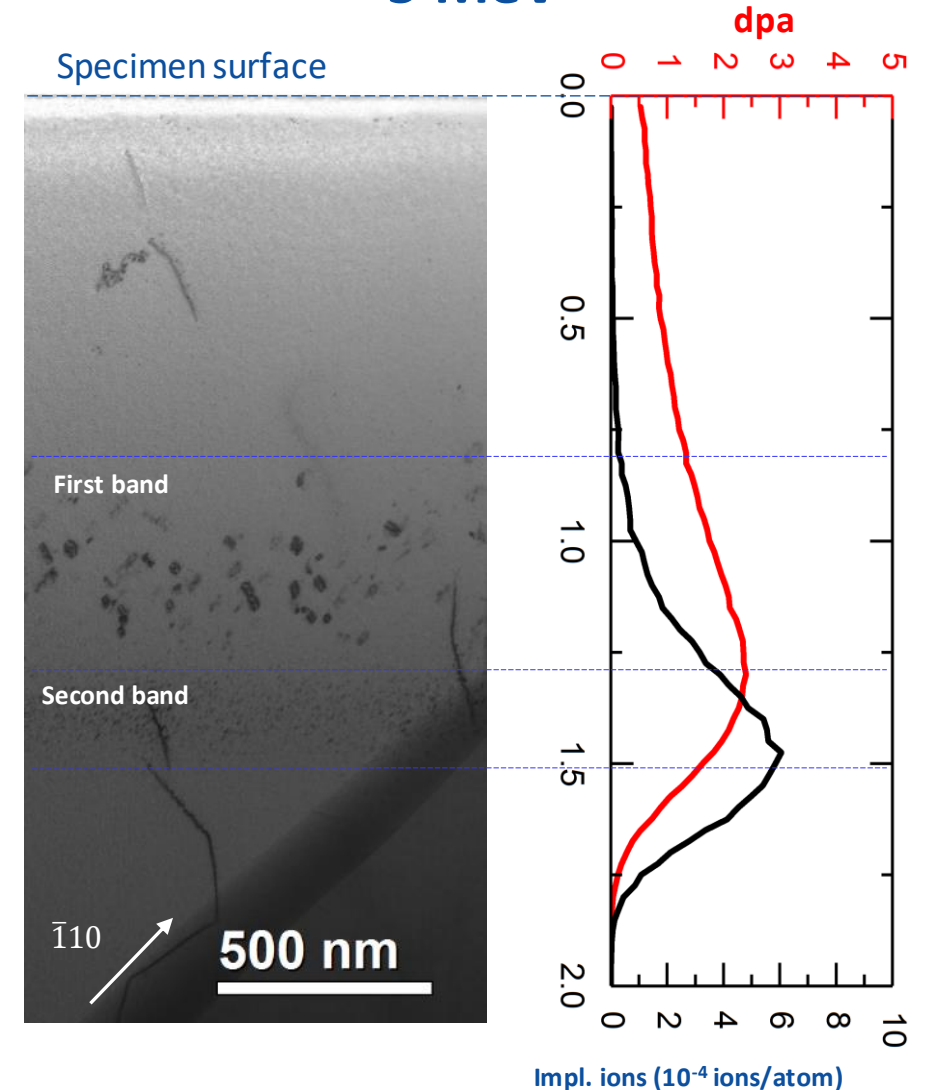


- **Ion irradiations were performed applying different parameters**
 - Different ion energy, focused beam versus rastering, different doses and temperatures, but same materials
 - Most difficult variable to control: C contamination

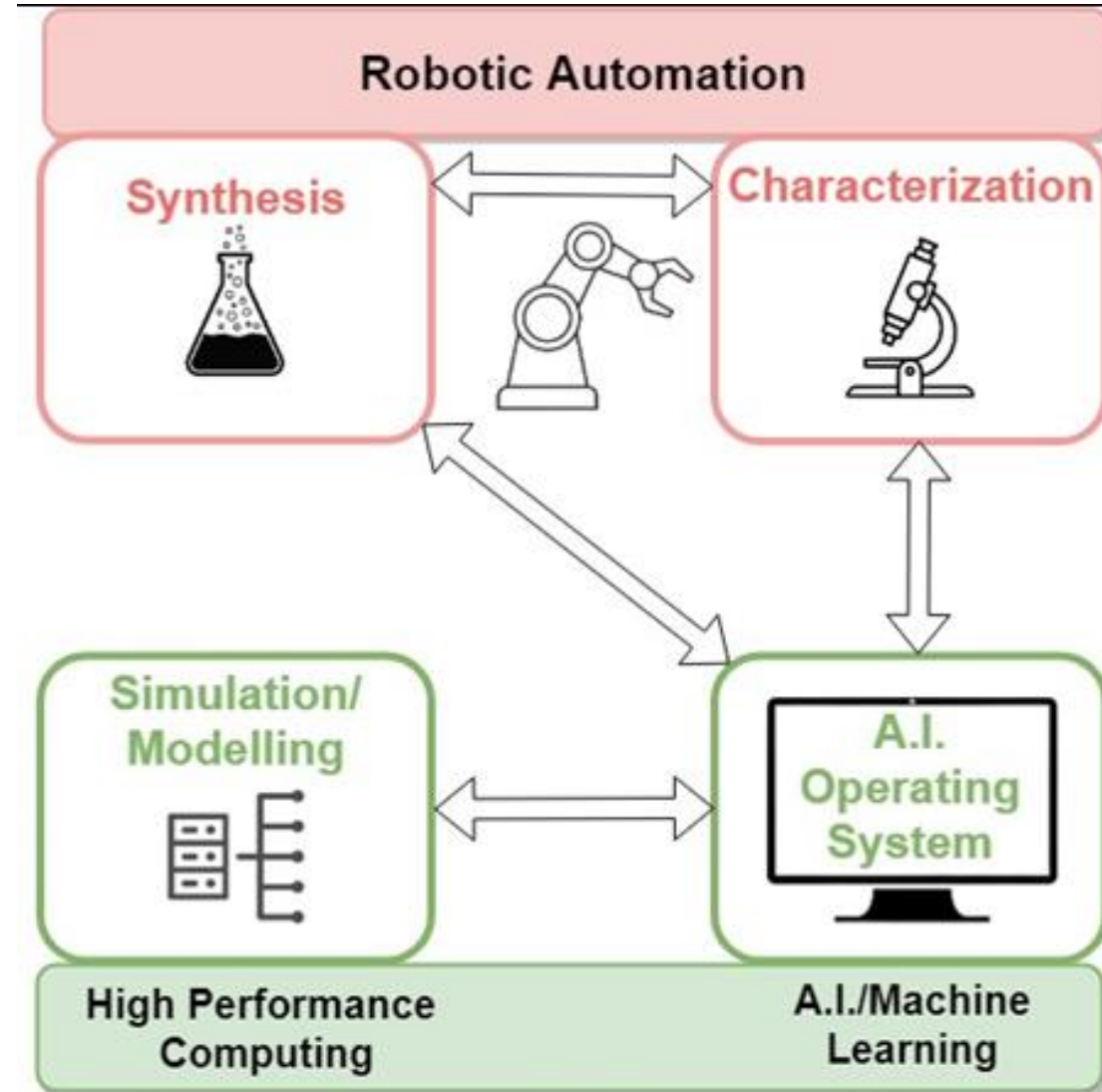
This clarified several effects and suggested good practices to mimick neutron irradiation

- **Three new different microstructure evolution models have been developed, each offering new modelling opportunities, not available before**
 - Simulation of the whole ion penetration thickness
 - Simulation of Cr concentrated alloys including precipitation
 - Simulation of the effect of minor solutes
- **Good practices to assess the mechanical properties of ion irradiated materials using nanoindentation have been drafted**
 - Standards for testing have reached the level of a **CEN workshop** and relevant publication

5 MeV



Materials acceleration platforms



- Closed-loop coupling of synthesis, characterization and computation
- Robotic automation
- Accelerated experimental planning and simulation/modeling through AI machine learning algorithms
- Develop novel materials and devices

Sample preparation

- High reproducibility
- High repeatability
- Use of novel or commercially available materials
- Variety of sample geometries

Sample analysis

- Definition of proxy parameters and development of suitable proxy tests for short cycle times
- Automated evaluation of the descriptors

ML-based DoE

- Bias-free parameter optimization
- Selection of best performers
- Improvement of data analysis during test campaigns

Corrosion MAP

Material development

- Biggest challenge for integration into a MAP due to the metallurgical processes involved
- Biggest breakthrough potential
- Bridging classical high-throughput concepts with MAP philosophy necessary

Advanced analysis

- Methods not suitable for automation due to technical or time constraints
- Applied to selected samples for obtaining mechanistical information or long term property analysis

A “corrosion MAP” is being developed at the BAM laboratories of Erlangen, Germany

Nuclear-orientated MAPs need integration of ion irradiation in the loop

Nuclear-orientated MAPs are of equal benefit for fission and fusion



Natural Resources
Canada

Ressources naturelles
Canada



Summary and Concluding Remarks

Materials will be subjected to unprecedentedly harsh conditions in both fusion and GenIV fission reactors

Some non-nuclear technologies (e.g. CSP, geothermal energy, bioenergy, ...) also expose materials to comparably harsh conditions (except irradiation)

Fusion specificities: high He production, skyrocketing thermal shocks, tritium permeation and need for low activation materials

Both GenIV and fusion require materials resistant to irradiation, temperature and fluid attack

F/M steels are the main intersection between fusion and fission materials: future for GenIV, only choice for fusion, due to low swelling, thermal stability, possibility to reduce activation, maybe price and He as well

F/M steels require:

- ❖ Bespoke design rules to be developed, to account for: cyclic softening, creep-fatigue, low T embrittlement and loss of elongation, liquid metal corrosion/embrittlement
- ❖ Improvement of creep strength and compatibility with fluids

These two points define a common research agenda, part of which has been or is being addressed in GenIV, fusion and cross-cutting projects (Matter, Eurofusion, M4F, ...)

The second point will benefit from the development of nuclear-oriented MAPs that should include ion irradiation in the loop, provided that suitable good practices are agreed upon to perform unbiased irradiation experiments



Ciemat



sck cen



Thank you!

www.eera-jpnm.eu/orient-nm



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