# Verification and Validation of Extended-Magnetohydrodynamic Modeling of Disruption Mitigation

#### by

#### Brendan C. Lyons<sup>1</sup>

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\*See the author list of <u>E. Joffrin et al.</u> 2019 Nucl. Fusion 59 112021

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#### Many Grants Provide Opportunities of Synergistic Research

- US DOE grants used for code validation & close collaboration with experiment
  - GA Theory (DE-FG02-95ER54309) and DIII-D (DE-FC02-04ER54698)
  - CTTS SciDAC for MHD modeling (DE-SC0018109)
  - JET/KSTAR Disruption Mitigation Solution (DE-SC0020299)
- EUROfusion Enabling Research project for JOREK code development and validation
- National Energy Research Scientific Computing Center for high-performance computing

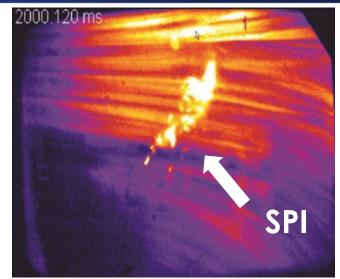


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### Studying of Disruption Dynamics and Mitigation Requires Multiphysics Models

- Simulations validated against experiments are required to project mitigation techniques to future devices
- Integrated model is required to capture all relevant physics
  - Magnetohydrodynamics (MHD) for macroscopic evolution
     of disruption dynamics
  - Atomic physics for impurity ionization/radiation
  - Drift-kinetics for runaway-electron (RE) evolution
- Disparate spatial and temporal scales make numerical modeling particularly challenging
- M3D-C1<sup>1</sup>, NIMROD<sup>2,3</sup>, and JOREK<sup>4,5</sup> are rising to this challenge
  - Different physics and numerical model provide robust verification opportunities
  - Multiple code permit parallel research efforts





DIII-D shattered pellet injection (SPI) D. Shiraki, IAEA presentation 2016

<sup>1</sup>S. C. Jardin, et al., Comput. Sci. Discovery 5, 01400<sup>7</sup> (2012)
<sup>2</sup>C. R. Sovinec et al., J. Comput. Phys. 195, 355 (2
<sup>3</sup>C. Sovinec & J. King, J. Comput. Phys. 229, 5803 (2
<sup>4</sup>G.T.A. Huysmans & O. Czarny, Nucl. Fusion 47, 659 (2007)
<sup>5</sup>O. Czarny & G. Huysmans, J. Comput. Phys. 227, 7423 (2008)

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#### **Outline and Major Results**

Overview of code models

#### Verification studies

- M3D-C1 & NIMROD show quantitative agreement in 2D, nonlinear benchmark, JOREK differences likely due to its impurity model
- M3D-C1 & NIMROD 3D nonlinear benchmarks
  - Axisymmetric, core deposition shows stable thermal quench, instability-induced current quench with large current spike
  - Injected, ablating pellet benchmark is underway
- NIMROD viscosity & deposition scans show expected thermal-quench dependence

#### Validation studies

- Initial M3D-C1 pellet-composition study shows qualitative agreement with DIII-D data, NIMROD shows quantitative agreement with experiment
- M3D-C1 and NIMROD have begun modeling of recent JET & KSTAR experiments
- JOREK shattered-pellet-injection modeling shows MHD-driven thermal quench



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#### M3D-C1 and NIMROD Extended-MHD Solvers are Coupled to Impurity Ionization/Radiation Models

- Both codes solve full, nonlinear, 3D extended MHD equations
  - M3D-C1 uses a complete C<sup>1</sup> finite-element representation
  - NIMROD uses finite elements in poloidal plane and Fourier modes toroidally
- Both have been coupled to the KPRAD<sup>1</sup> impurity model
  - Low-density, coronal non-equilibrium model based on ADPAK rate coefficients
  - Impurity & electron densities evolve according to ionization and recombination  $\frac{\partial n_z}{\partial t} + \nabla \cdot (n_z \mathbf{v}) = \nabla \cdot (D \nabla n_z) + \mathcal{I}_{z-1} n_{z-1} - (\mathcal{I}_z + \mathcal{R}_z) n_z + \mathcal{R}_{z+1} n_{z+1} + \mathcal{S}_z$
  - Thermal energy lost from plasma due to ionization and radiation
  - NIMROD uses single-temperature, M3D-C1 uses single or two-temperature

$$n_{e} \left[ \frac{\partial T_{e}}{\partial t} + \mathbf{v} \cdot \nabla T_{e} + \Gamma T_{e} \nabla \cdot \mathbf{v} \right] = (\Gamma - 1) \left( \eta J^{2} - \nabla \cdot \mathbf{q}_{e} + Q_{ei} - \mathcal{P}_{rad} \right) - T_{e} \left( \frac{\partial n_{e}}{\partial t} + \mathbf{v} \cdot \nabla n_{e} \right)$$
$$n_{ti} \left[ \frac{\partial T_{i}}{\partial t} + \mathbf{v} \cdot \nabla T_{i} + \Gamma T_{i} \nabla \cdot \mathbf{v} \right] = (\Gamma - 1) \left( -\nabla \cdot \mathbf{q}_{i} - Q_{ei} - \mathbf{\Pi} : \mathbf{v} \right) - T_{i} \left( \frac{\partial n_{ti}}{\partial t} + \mathbf{v} \cdot \nabla n_{ti} \right)$$

<sup>1</sup>D.G. Whyte, et al., Proc. of the 24th Euro. Conf. on Controlled F Plasma Physics, Berchtesgaden, Germany, 1997, Vol. 21A, p. 1137.



# JOREK Extended-MHD Solver Coupled to Coronal-Equilibrium Impurity Model

- JOREK solves 3D nonlinear extended MHD equations
   [Huysmans and Czarny, NF 2007; Overview article: Hoelzl et al., in preparation; <u>https://www.jorek.eu/]</u>
  - 2D C<sup>1</sup> finite elements poloidally & Fourier modes toroidally
  - Fully implicit [Czarny and Huysmans, JCP 2008]
  - Free-boundary simulations with JOREK-STARWALL [Hoelzl et al., JPCS 2012]
  - Typically run in reduced MHD (including all simulations here)
- Various extensions permit disruption mitigation modeling
  - Neutrals [Fil et al., PoP 2015]
  - Shattered-pellet injection [Hu et al., NF 2018]
  - Impurities under coronal equilibrium [Hu et al., in preparation]
  - Impurities beyond coronal equilibrium is under development [Wieschollek et al.]
  - Runaway Electrons
    - Fluid model [Bandaru et al., Phys. Rev. E 2019]
    - Test particles [Sommariva et al., NF 2017 & 2018]



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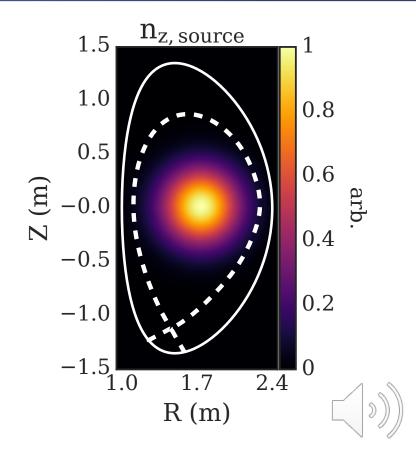




- 2D, nonlinear modeling of argon injection in DIII-D core (See pub. for details<sup>+</sup>)
- Excellent agreement found between M3D-C1 and NIMROD
  - Thermal quench agreed quantitatively
  - Current quench caused by contact with boundary shows qualitative agreement
  - Quantitative differences likely caused by disparate boundary conditions
- On-axis impurities induce inside-out thermal quench & hollowing of current
- After thermal quench, plasma forms expanding shell with core turbulence

<sup>+</sup>B.C. Lyons et al., PPCF **61**, 6 (2019). <u>doi.org/10.1088/1361-6587/ab0e42</u>

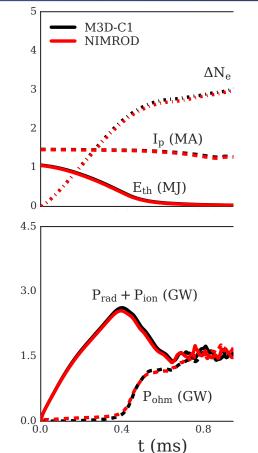




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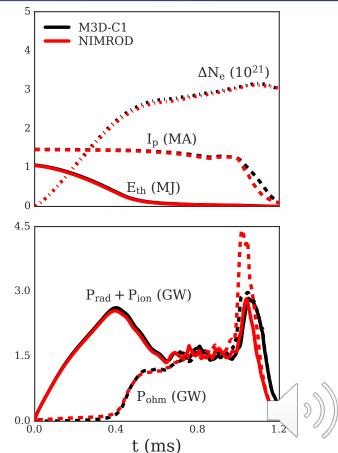




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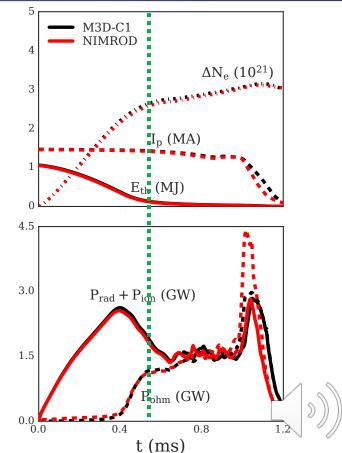




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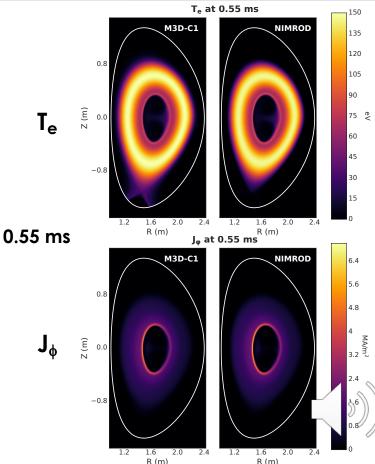




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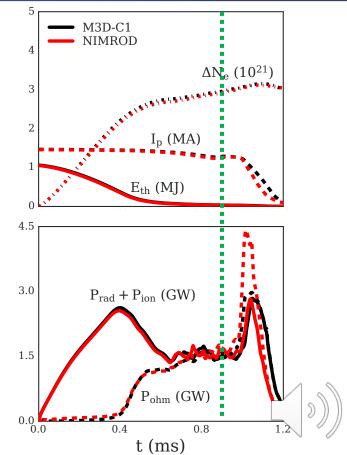


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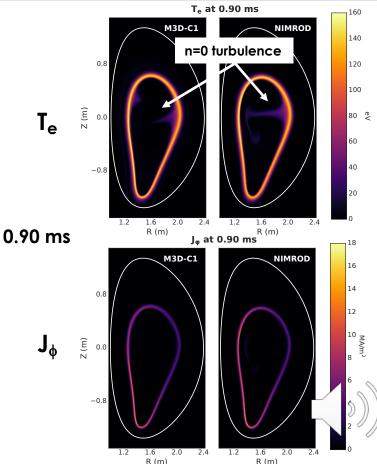




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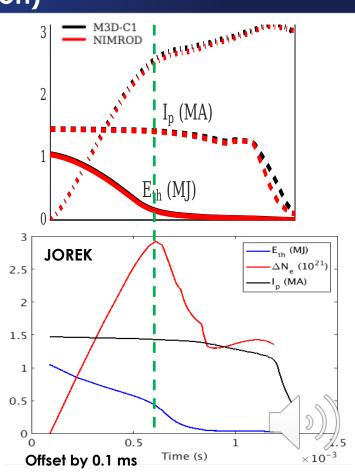




#### JOREK Modeling Shows Quantitative Differences Likely Due to Coronal-Equilibrium Impurity Model (Nardon)

- JOREK reduced-MHD simulation shows similar thermal quench timescale, though a bit slower
- Similar initial rate of density increase, but decreases in JOREK after thermal collapse
- Loss power rises more slowly in JOREK initially
- Likely due to crucial difference in impurity models
  - JOREK assume impurity charge states remain in coronal equilibrium
  - M3D-C1 & NIMROD use a coronal model, but allow each charge state to evolve in time
  - Motivates ongoing upgrade of JOREK impurity, and future work to move to collisional-radiative model in M3D-C1



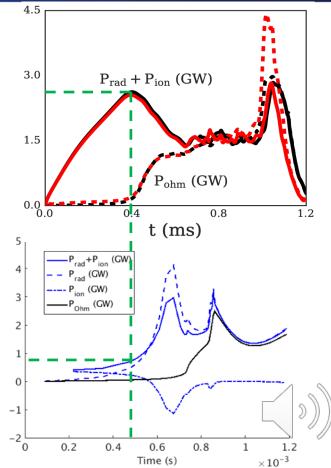


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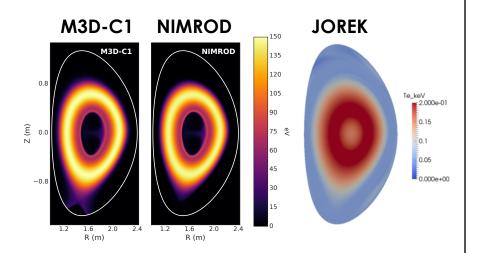
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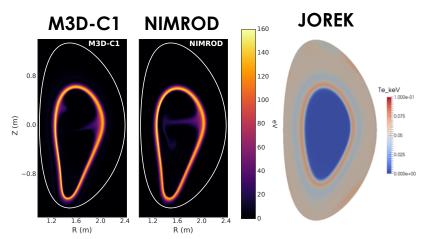




### JOREK Also Shows Inside-Out Thermal Quench and Evolving Plasma Sheet, but Differs Qualitatively (Nardon)



- Te at ~0.55 ms after injection starts
- JOREK shows hollow profile, but less so



- Te at ~1.0 ms after injection starts
- Sheet has formed in JOREK, but less shaping and no core turbuelnce





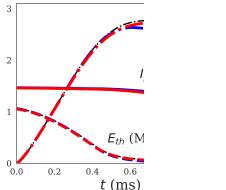
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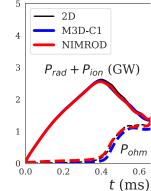
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- Plasma stays axisymmetric through 0.65 ms, identical to 2D benchmark
- Good qualitative agreement between codes during current quench
  - Rapid current quench
  - Plasma sheet goes unstable after thermal quench
  - Mixing increases radiation & ohmic heating
- Prominent current spike\*
  - 120-150 kA among largest seen in 3D, nonlinear MHD simulations
  - NIMROD spike slightly delayed and current quench is faster
  - Sensitivity to resistivity and boundary temperature under investigation

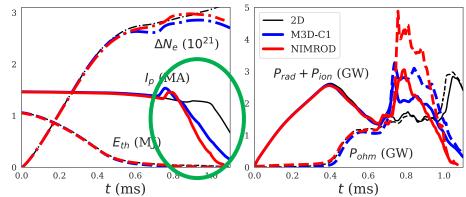








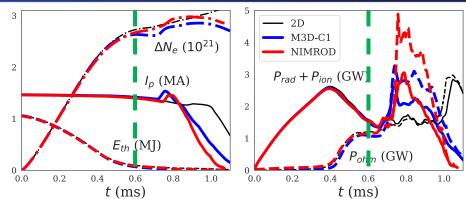
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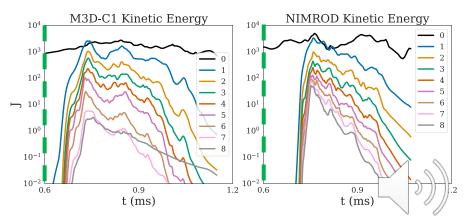






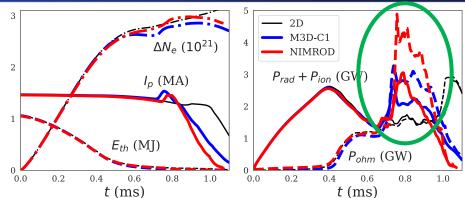
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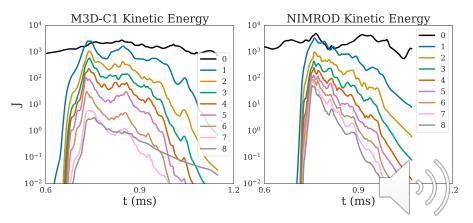






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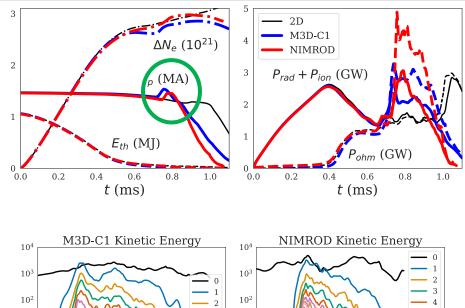
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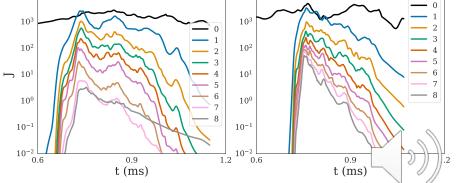
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\*Letter on M3D-C1 current spike in preparation







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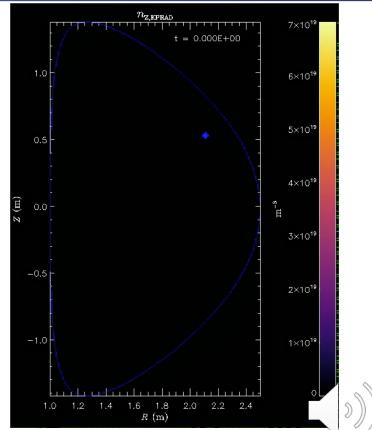
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- DIII-D 160606 @ 2990 ms: 0.7 MJ, 1.28 MA
- 3D nonlinear MHD with fixed boundary and single-temperature equation
- Pellet parameters
  - 3 mm radius, pure neon
  - 5 cm poloidal and 2.4 m toroidal deposition half-width
  - 200 m/s with realistic trajectory
- First results have obvious discrepancies
  - Early, quantitative agreement in number of electrons (i.e., ablation and ionization)
  - Both show strong MHD at ~1.8 ms, but n=3 in M3D-C1 and n=5 in NIMROD
  - Induces rapid thermal quench in M3D-C1, but not in NIMROD
- Work to improve match will continue in earnest in near future



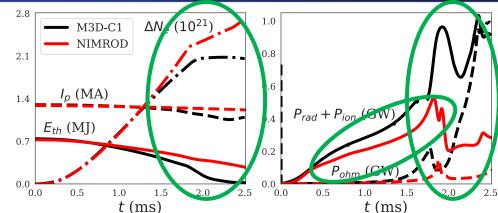


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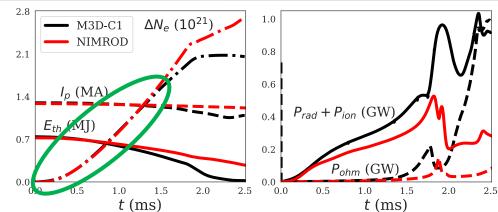


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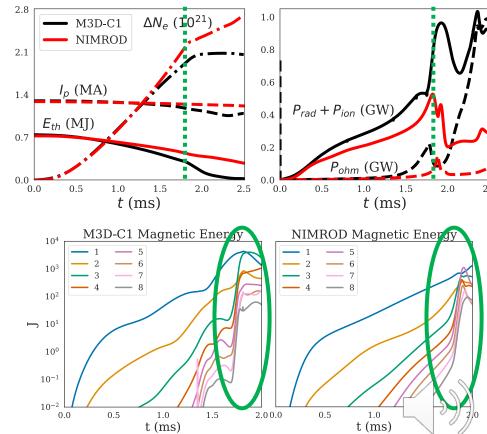


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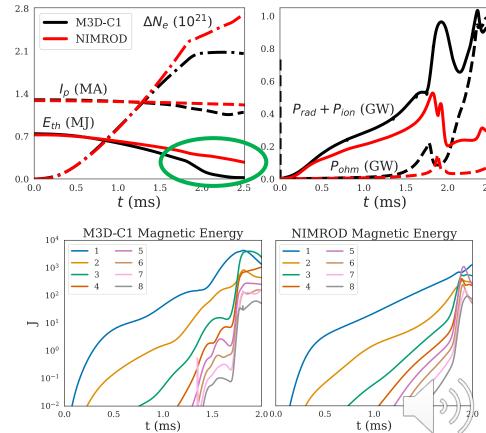


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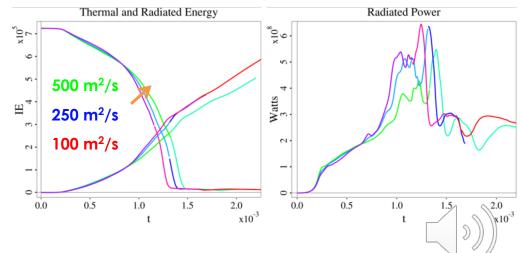




# NIMROD Modeling Shows Lower Viscosity Leads to Shorter Thermal Quench due to Stronger Linear MHD Response (Kim)

viscosity	$d\phi/2\pi$	$ au_{TQ} \ (\mathrm{ms})$	$P_{rad}^{peak}$ (GW)	$E_{rad}/E_{th}$	assim.
$500 \text{ m}^2/\text{s}$	0.05	1.451	0.55	45%	34%
$250 \text{ m}^2/\text{s}$	0.05	1.379	0.64	47%	38%
$100 \text{ m}^2/\text{s}$	0.05	1.316	0.64	44%	41%

- Decreasing viscosity accelerates dynamics
  - Stronger linear response
     [(2,1),(3,2)] driven by ablating fragments
  - Earlier nonlinear saturation but not necessarily larger amplitude
- Higher viscosity suppresses MHD activity, decreasing radiation

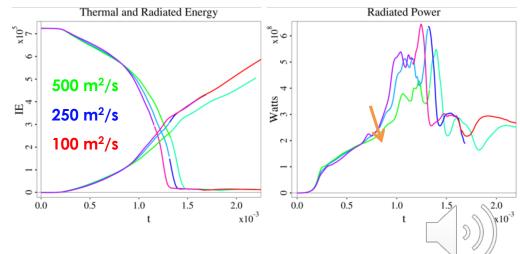




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# NIMROD Modeling Shows Broader Toroidal Deposition Causes Shallower Penetration but Higher Assimilation (Kim)

viscosity	$d\phi/2\pi$	$ au_{TQ} \ (\mathrm{ms})$	$P_{rad}^{peak}$ (GW)	$E_{rad}/E_{th}$	assim.
$500 \text{ m}^2/\text{s}$	0.05	1.451	0.55	45%	34%
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$100 \text{ m}^2/\text{s}$	0.05	1.316	0.64	44%	41%
$500 \text{ m}^2/\text{s}$	0.10	1.478	0.50	40%	42%
$250 \text{ m}^2/\text{s}$	0.10	1.268	1.46	58%	66%
$100 \text{ m}^2/\text{s}$	0.10	1.227	0.93	45%	61%

#### Overall, broader deposition causes

- Shorter thermal quench
- Larger fraction of pellet ablated
- Trends within broader deposition cases are less consistent, possibly due to nonlinear mixing from crossing of more flux tubes



#### **Outline and Major Results**

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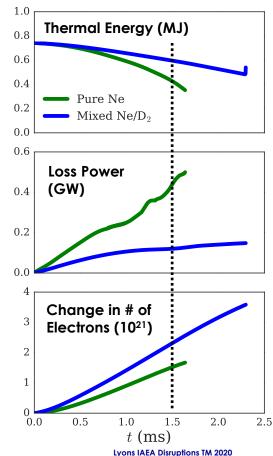




# M3D-C1 Validation with DIII-D Pellet Composition Shows Thermal Quench for Pure Neon Pellet Faster than Mixed Ne-D2 (Lyons)

- Simulations
  - DIII-D 160606
  - Single, monolithic pellet
  - Realistic velocity
  - Half-widths: 10 cm pol.
     3 m tor.
- Radiative losses several times higher with pure neon than 10:1 D2:Ne
- Trends are consistent with NIMROD modeling and experiment
  - NIMROD agrees well with experiment
  - Increased resolution improved results from publication\*



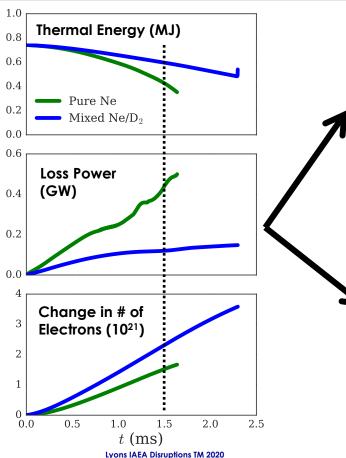


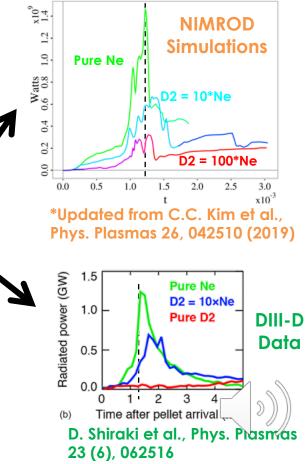


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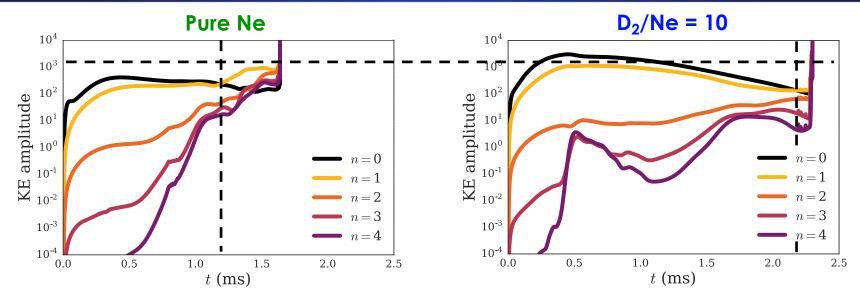
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# Pure Neon Pellet Induces Dominant n=1 Mode, Mixed Pellet Remains More Quiescent (Lyons)



- Preliminary results: to be rerun with
  - Higher toroidal resolution
  - Newer, more stable code version
- Pure neon pellet drives linear instability
- Both go numerically unstable when plasma highly non-axisymmetric



## **Outline and Major Results**

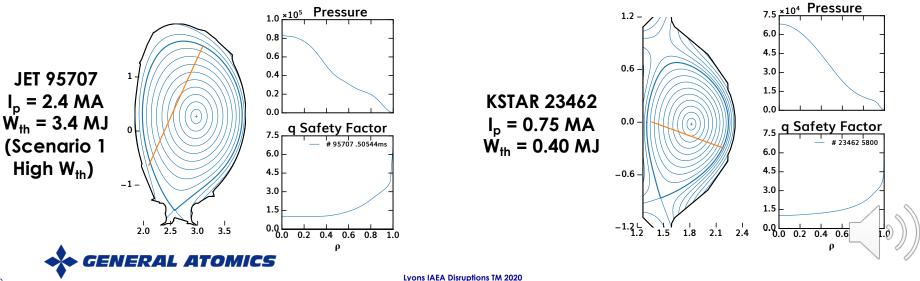
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# New International Collaboration will Validate M3D-C1 and NIMROD against Recent JET and KSTAR SPI Experiments

- Modeling component of grant has several objectives
  - Interpret recent mitigation experiments
    - JET, particular high thermal energy and radiation fraction/asymmetry
    - KSTAR, particularly dual, symmetric shattered-pellet injection
  - Develop cross-machine database to inform ITER disruption-mitigation system
  - Make predictions for additional experiments
- Equilibria reconstructed with kinetic profiles acquired for recent experiments

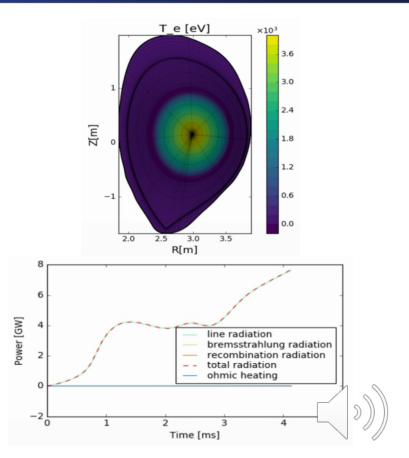


# Initial Modeling of JET & KSTAR is Underway (McClenaghan, Lyons)

#### JET modeling of 95707

- Initial 2D NIMROD modeling shows outside-in thermal quench driven by line radiation
- 3D M3D-C1 nonlinear modeling shows quiescent, radiation-driven thermal quench
  - Two different toroidal depositions, but varied diffusivity parameters
  - No significant MHD activity (beyond sawteeth) before numerical instability
- M3D-C1 2D KSTAR modeling underway, 3D & NIMROD to follow
  - Dual injector simulations planned
  - Multi-injector simulations demonstrated w/ NIMROD in DIII-D



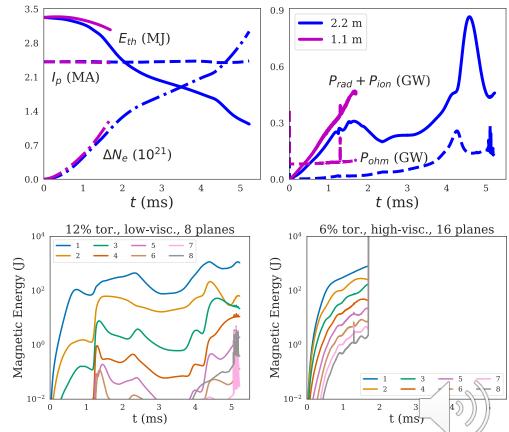


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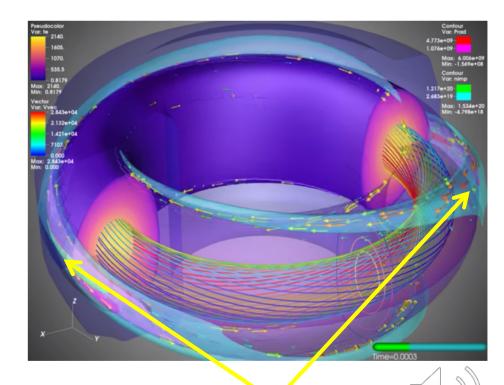


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NIMROD Dual Injection in DIII-D

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# JOREK Modeling of JET Reference Scenario 1 Discharge Show MHD Driven Thermal Quench (Bonfiglio)

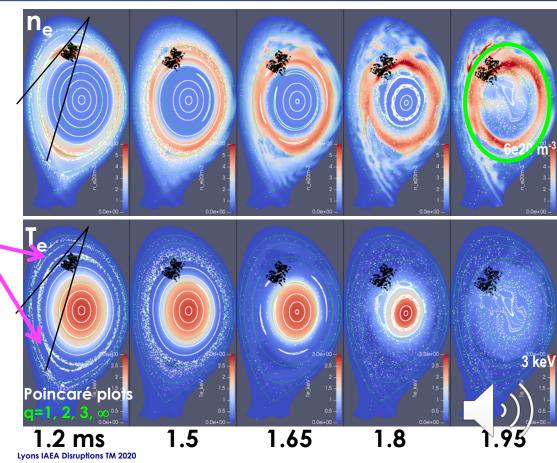
#### • Shot 89800

- From earlier MGI experiment
- Used for current Scenario 1
- Pellet size and composition under active investigation
  - 4.5 mm vs 8 mm
  - Pure Ne vs mixed Ne/D2

#### • Example of 4.5 mm pure Ne

- MHD activity induced by n=0 current contraction and helical cooling on rational surfaces
- Stochasticazation causes thermal quench, but core remains at low density (potentially bad for runaway suppression)
- Synthetic diagnostics are being implemented for experimental validation





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## Verification, Validation, and Predictive Modeling Will Continue

#### M3D-C1 and NIMROD

- Complete 3D benchmark this year
- Extensive validation with experiment
  - DIII-D: dual SPI, thermal & magnetic energy
  - JET: high thermal energy and radiation fraction/asymmetry
  - KSTAR: dual, symmetric SPI
- Model upgrades
  - Collisional-radiative impurity model
  - Coupling to detailed pellet ablation code
- JOREK

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- Use synthetic diagnostics for JET validation
- Upgrade to impurity model (ongoing) to complete 2D benchmark
- All codes will make predictions for efficacy of ITER disruption-mitigation system
  - Cross-machine, cross-code database will provide robust understanding of SPI dynamics
  - High-fidelity, 3D nonlinear modeling of relevant ITER scenarios



## **Acknowledgments and Disclaimers**

- This material is based upon work supported by the U.S. Department of Energy, Office of Science, Office of Fusion Energy Sciences, using the DIII-D National Fusion Facility, a DOE Office of Science user facility, under Awards DE-FG02-95ER54309, DE-FC02-04ER54698, DE-SC0018109, and DE-SC0020299.
- This research used resources of the National Energy Research Scientific Computing Center (NERSC), a U.S. Department of Energy Office of Science User Facility operated under Contract No. DE-AC02-05CH11231.
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- This work has been carried out within the framework of the EUROfusion Consortium and has received funding from the Euratom research and training program 2014-2018 and 2019-2020 under grant agreement No 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission.



# **Additional slides**



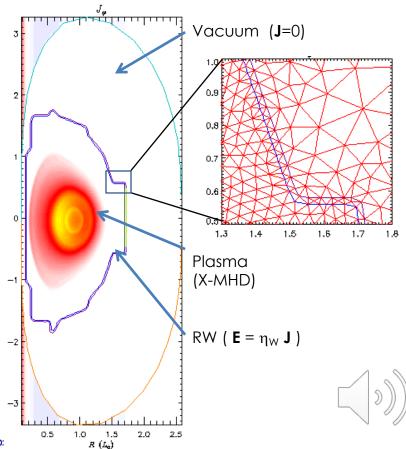


### M3D-C1\* Solves the Extended-MHD Equations

- Three-dimensional toroidal geometry
- Full (not reduced) MHD
- Solves for potential and stream-function fields for  $\vec{A} \& \vec{v} (\nabla \cdot \vec{B} = 0$  intrinsically)
- Includes resistivity, density diffusivity, viscosity, & thermal conductivity
- Two-fluid effects (optional)
- 3D high-order finite elements
  - Unstructured, triangular mesh in poloidal plane
  - Structured toroidally, but can pack planes
- Can solve with finite-thickness resistive wall in domain\*\*

\*S. C. Jardin, et al., Comput. Sci. Discovery 5, 014002 (2012). \*\*N.M. Ferraro, et al. ,Phys Plasma23 056114 (2016).





Lyons IAEA Disruptions TM 202

## M3D-C1 Solves the Extended-MHD Equations

$$\begin{aligned} \frac{\partial n}{\partial t} + \nabla \bullet (n\mathbf{V}) &= \nabla \bullet D_n \nabla n + S_n \end{aligned} \qquad \text{Blue terms are 2-fluid} \\ \frac{\partial \mathbf{A}}{\partial t} &= -\mathbf{E} - \nabla \Phi, \quad \mathbf{B} = \nabla \times \mathbf{A}, \quad \mathbf{J} = \nabla \times \mathbf{B}, \quad \nabla_{\perp} \bullet \frac{1}{R^2} \nabla \Phi = -\nabla_{\perp} \bullet \frac{1}{R^2} \mathbf{E} \\ nM_i (\frac{\partial \mathbf{V}}{\partial t} + \mathbf{V} \bullet \nabla \mathbf{V}) + \nabla p &= \mathbf{J} \times \mathbf{B} - \nabla \bullet \mathbf{\Pi}_i + \mathbf{S}_m \end{aligned} \\ \mathbf{E} + \mathbf{V} \times \mathbf{B} &= \frac{1}{ne} (\mathbf{R}_e + \mathbf{J} \times \mathbf{B} - \nabla p_e - \nabla \bullet \mathbf{\Pi}_e) - \frac{m_e}{e} \left( \frac{\partial \mathbf{V}_e}{\partial t} + \mathbf{V}_e \bullet \nabla \mathbf{V}_e \right) + \mathbf{S}_{CD} \\ \frac{3}{2} \left[ \frac{\partial p_e}{\partial t} + \nabla \bullet (p_e \mathbf{V}) \right] &= -p_e \nabla \bullet \mathbf{V} + \frac{\mathbf{J}}{ne} \bullet \left[ \frac{3}{2} \nabla p_e - \frac{5}{2} \frac{p_e}{n} \nabla n + \mathbf{R}_e \right] + \nabla \left( \frac{\mathbf{J}}{ne} \right) : \mathbf{\Pi}_e - \nabla \bullet \mathbf{q}_e + Q_\Delta + S_{eE} \\ \frac{3}{2} \left[ \frac{\partial p_i}{\partial t} + \nabla \bullet (p_i \mathbf{V}) \right] &= -p_i \nabla \bullet \mathbf{V} - \mathbf{\Pi}_i : \nabla \mathbf{V} - \nabla \bullet \mathbf{q}_i - Q_\Delta + S_{iE} \\ \mathbf{R}_e &= \eta ne \mathbf{J}, \quad \mathbf{\Pi}_i = -\mu \left[ \nabla \mathbf{V} + \nabla \mathbf{V}^\dagger \right] - 2(\mu_e - \mu) (\nabla \bullet \mathbf{V}) \mathbf{I} + \mathbf{\Pi}_i^{GV} \\ \mathbf{\Pi}_e &= (\mathbf{B} / B^2) \nabla \bullet \left[ \lambda_h \nabla (\mathbf{J} \bullet \mathbf{B} / B^2) \right], \quad Q_A = 3m_e (p_i - p_e) / (M_i \tau_e) \end{aligned}$$

×

## Ablation model for Ne-D2 pellets implemented in M3D-C1

 Practical, analytic expression fit to more complex ablation model (Parks)

$$G\left({\rm g/s}\right) = \lambda\left(X\right) \left(\frac{T_e}{2000~{\rm eV}}\right)^{5/3} \left(\frac{r_p}{0.2~{\rm cm}}\right)^{4/3} \left(\frac{n_e}{10^{14}~{\rm cm}^{-3}}\right)^{1/3}$$

 $\lambda$  is fitting function, depending on molar fraction of D2, X

- M3D-C1 implementation
  - Advance pellet location in time
  - Calculate number of particles ablated and pellet-surface recession at each time step
  - Deposit main ion and/or impurities onto arbitrary spatial distribution (e.g. 2D or 3D Gaussian)



