

# Ammonia production, isotopic exchange and sticking on materials relevant to Fusion reactors: tungsten and 316L stainless steel

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## Abstract

- To maintain power fluxes to plasma facing components within tolerable limits, nitrogen-seeding in the edge plasma is considered
- Ammonia production has been observed in thermonuclear fusion reactors such as JET and ASDEX-Upgrade
- ITER will use a D/T mix → radioactive NT<sub>3</sub> expected → nuclear safety regulation imposes a stringent control of NT<sub>3</sub> within the reactor.
- It is necessary to understand the mechanism of ammonia production and where tritiated ammonia will stick on the reactor vessel

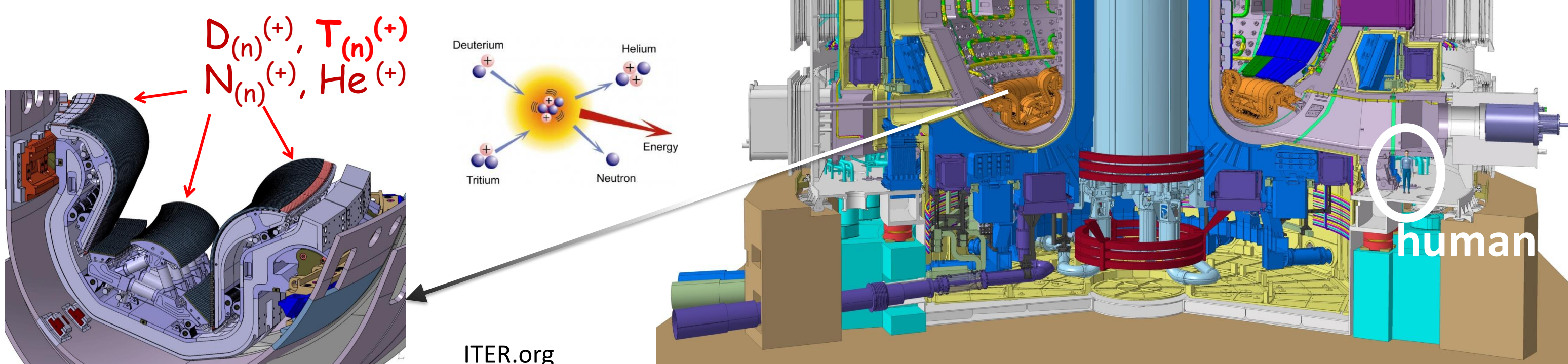
## ITER wall conditions

### SS316L vacuum vessel (60 m<sup>2</sup>)

background gases (H<sub>2</sub>, NH<sub>3</sub>...)  
+ E<sub>k</sub> > 50 eV (charge exchange neutral)

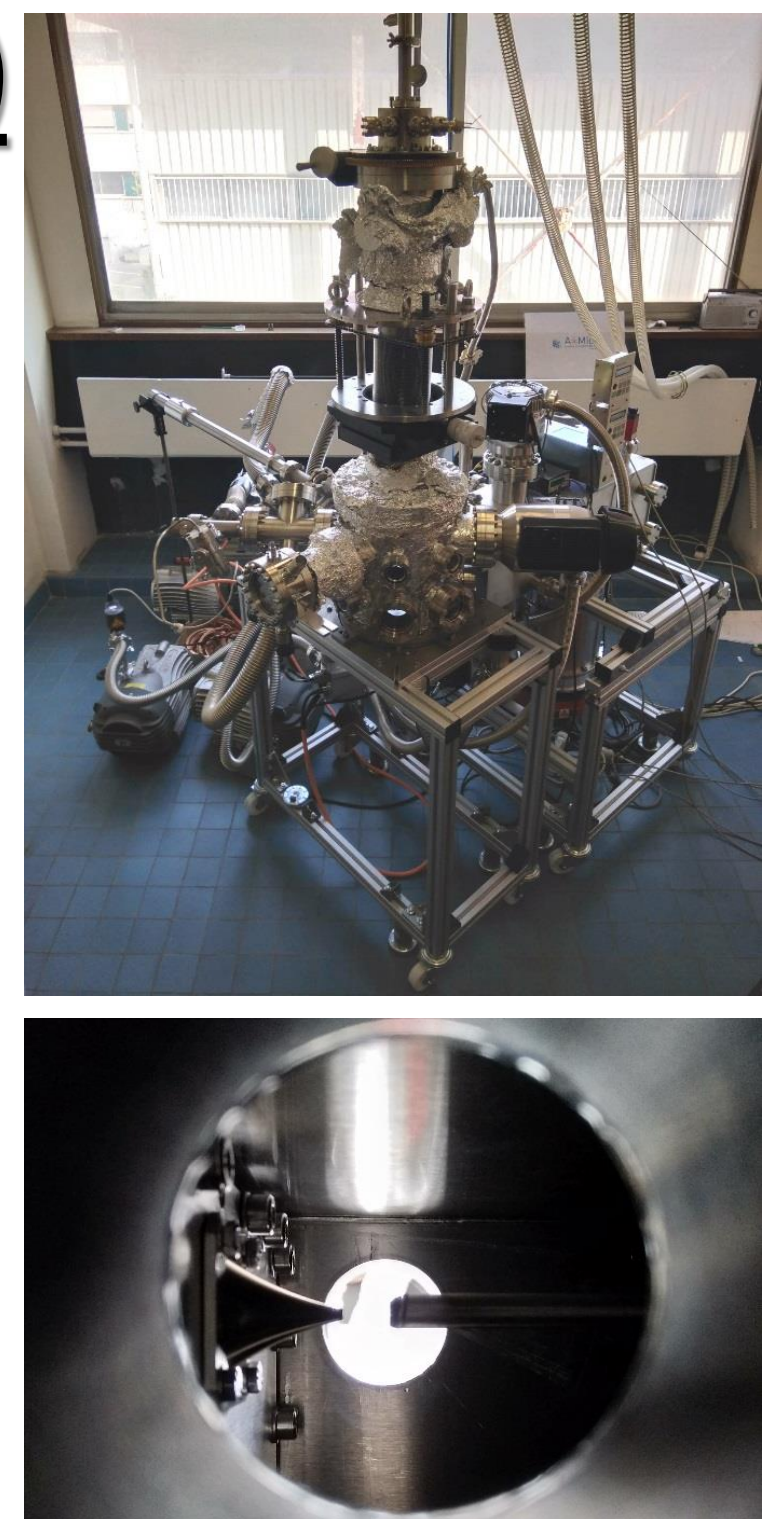
### Tungsten divertor (200 m<sup>2</sup>)

+ E<sub>k</sub> < 50 eV (ion and neutral)



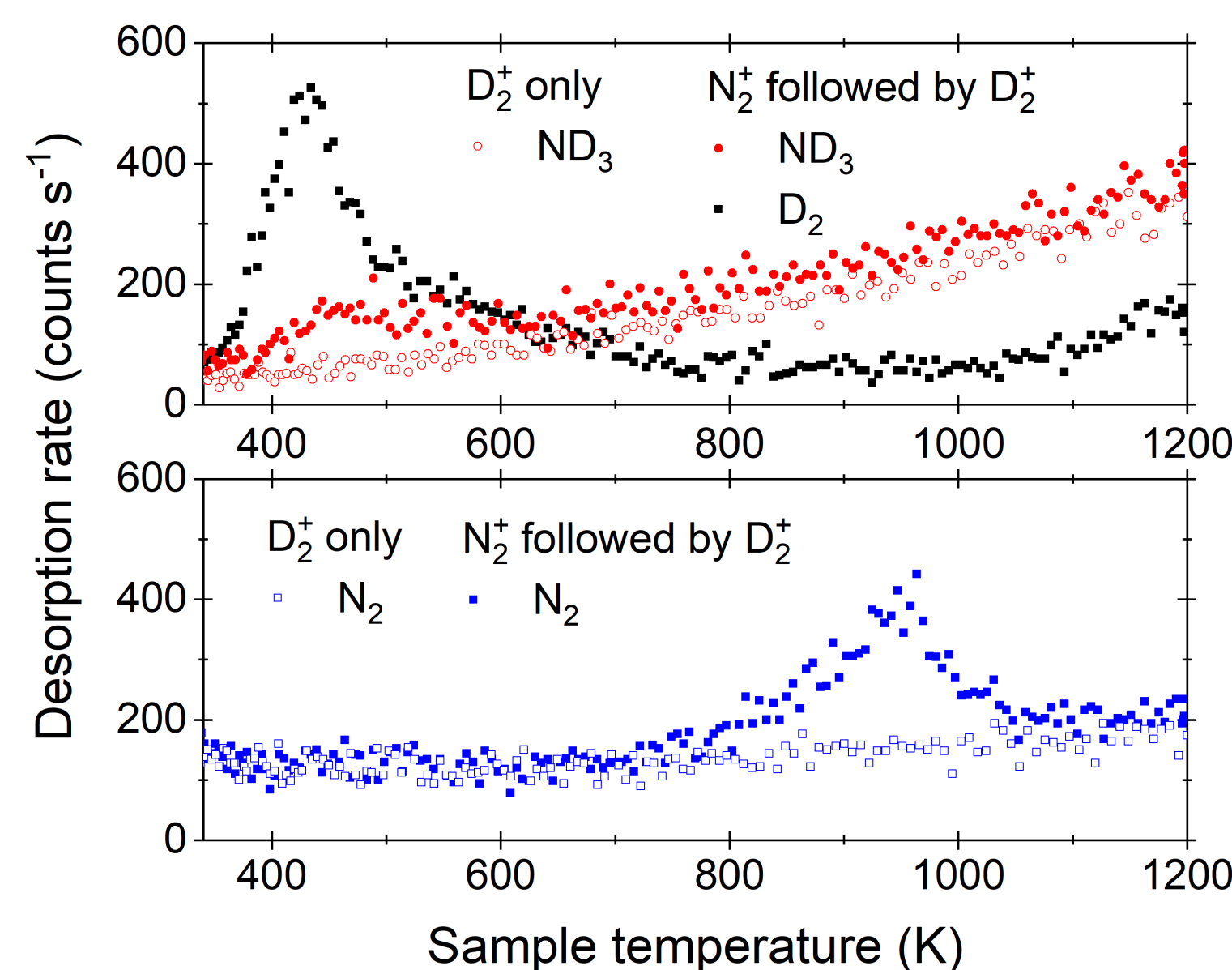
## Experimental methods (UHV)

- Poly-W: ALMT, 99,99%, native oxide
- 316L steel: Goodfellow, Fe > 60%, Cr 18%, Ni 10%, Mo 3%, Mn <2%, Si <1%, N <0.1%, P <0.045%, C <0.03%, S <0.03%
- W: 1000 K anneal (native oxide is left)
- SS316L: 800 K anneal (avoid sublimation)
- Ammonia production: co-implantation with 250eV/N (D) ion sources
- Ammonia sticking: supersonic molecular beam



## NH<sub>3</sub> production measurements on W

- Ammonia (ND<sub>3</sub>) production has been detected with a Quadrupole Mass Spectrometer (QMS) at m/z=20 only when N and D co-implantation are performed (excludes D<sub>2</sub>O)
- ND<sub>3</sub> desorption occurs in the same temperature window than D<sub>2</sub> desorption (350 – 650 K)
- N<sub>2</sub> desorption occurs well after ND<sub>3</sub> and D<sub>2</sub> desorption

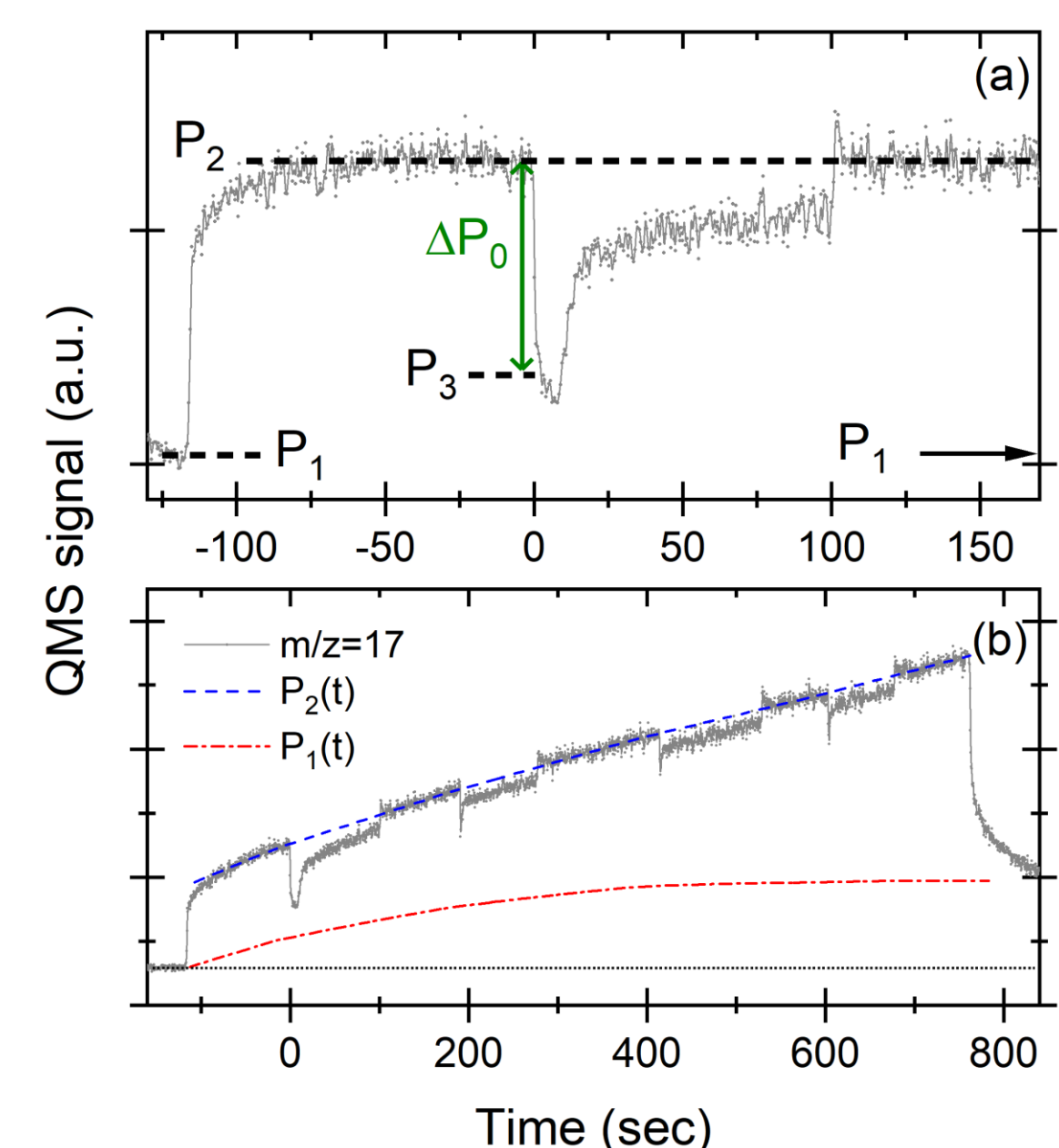


## NH<sub>3</sub> sticking measurements

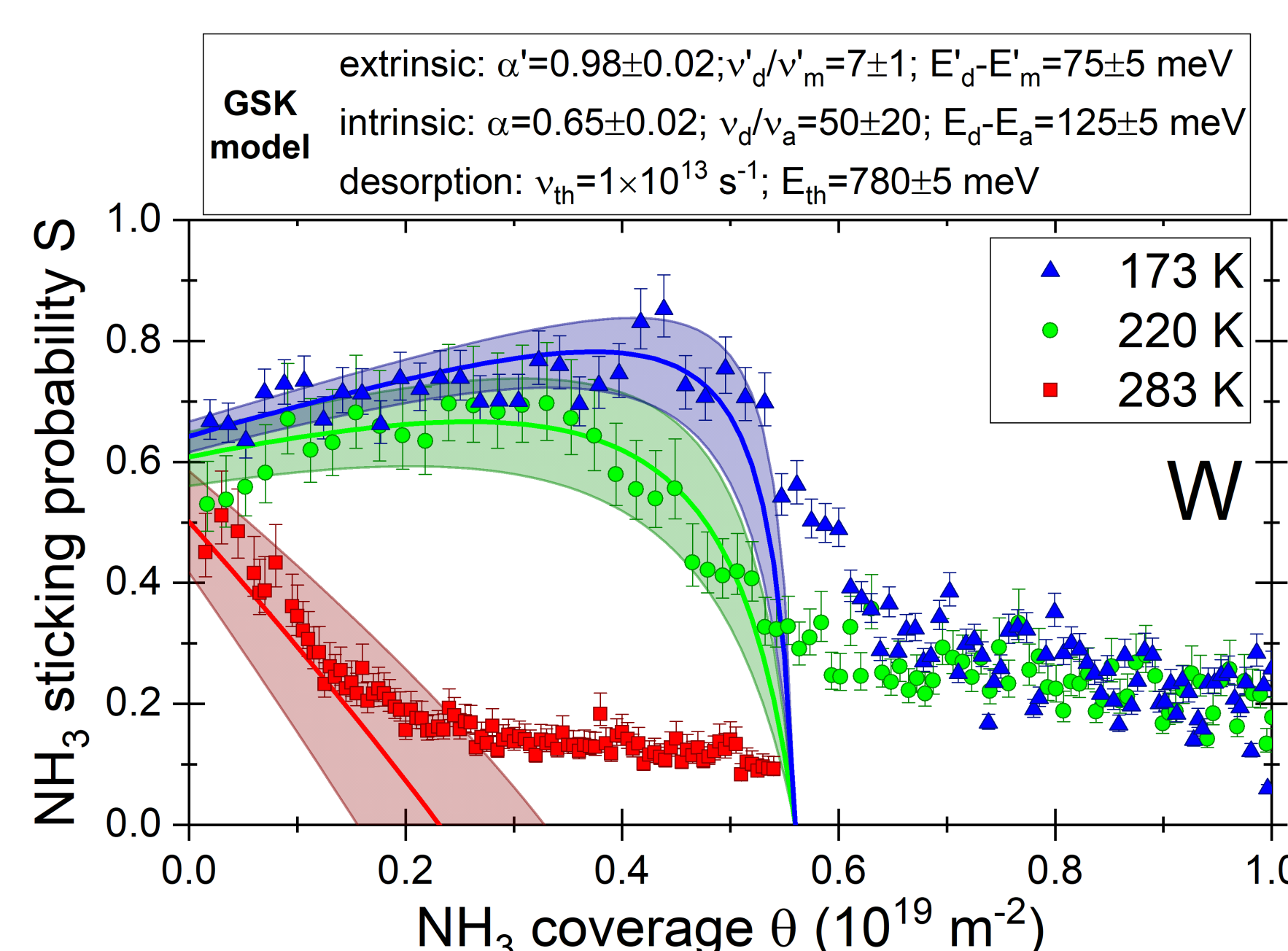
- Difficult for NH<sub>3</sub> because it is a sticky molecule on the vacuum chamber walls (316L)

$$S_0 \approx \frac{|\Delta P_0|}{P_2(t) - P_1(t)} \quad S(t) \approx \frac{P_2(t) - P(t)}{P_2(t) - P_1(t)}$$

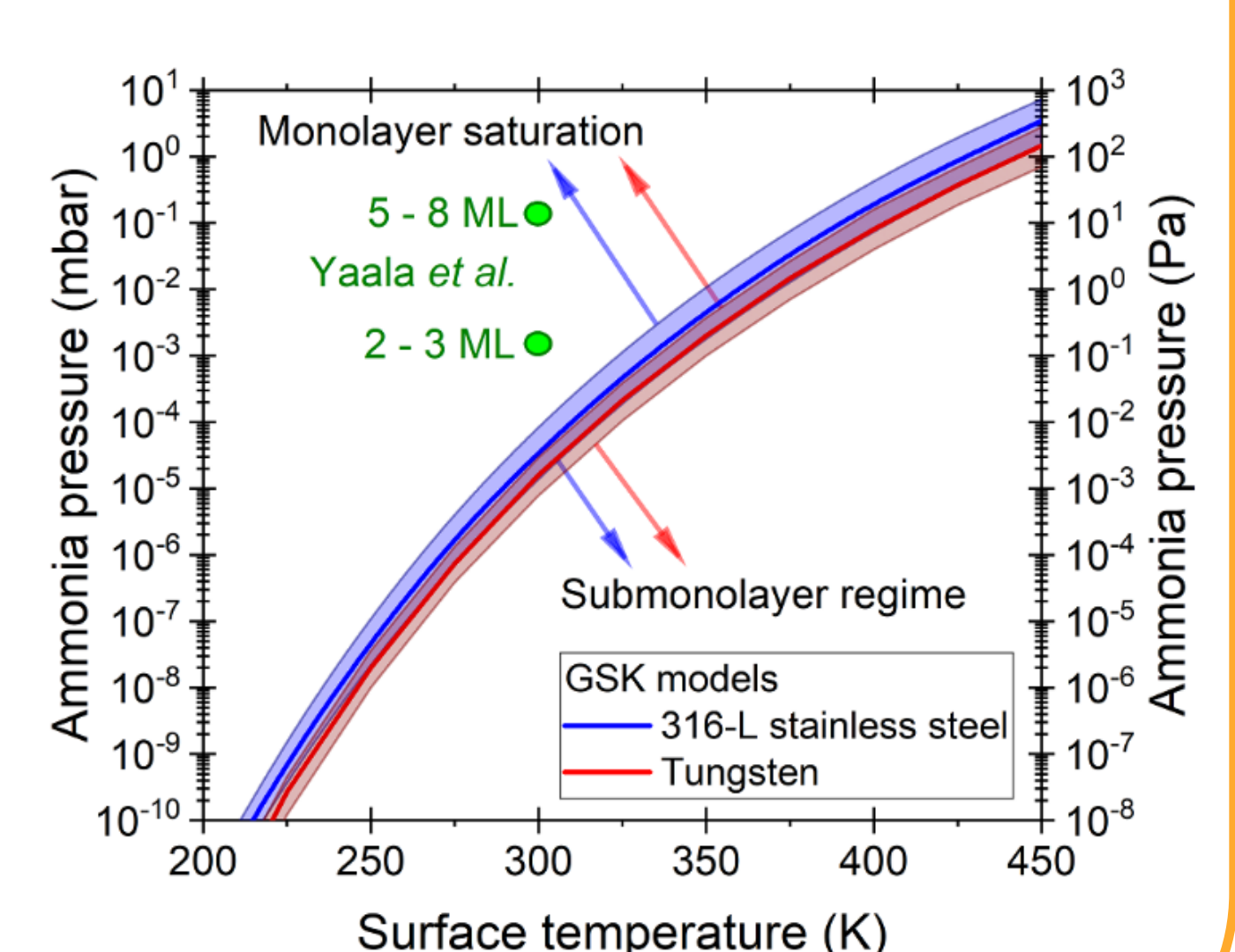
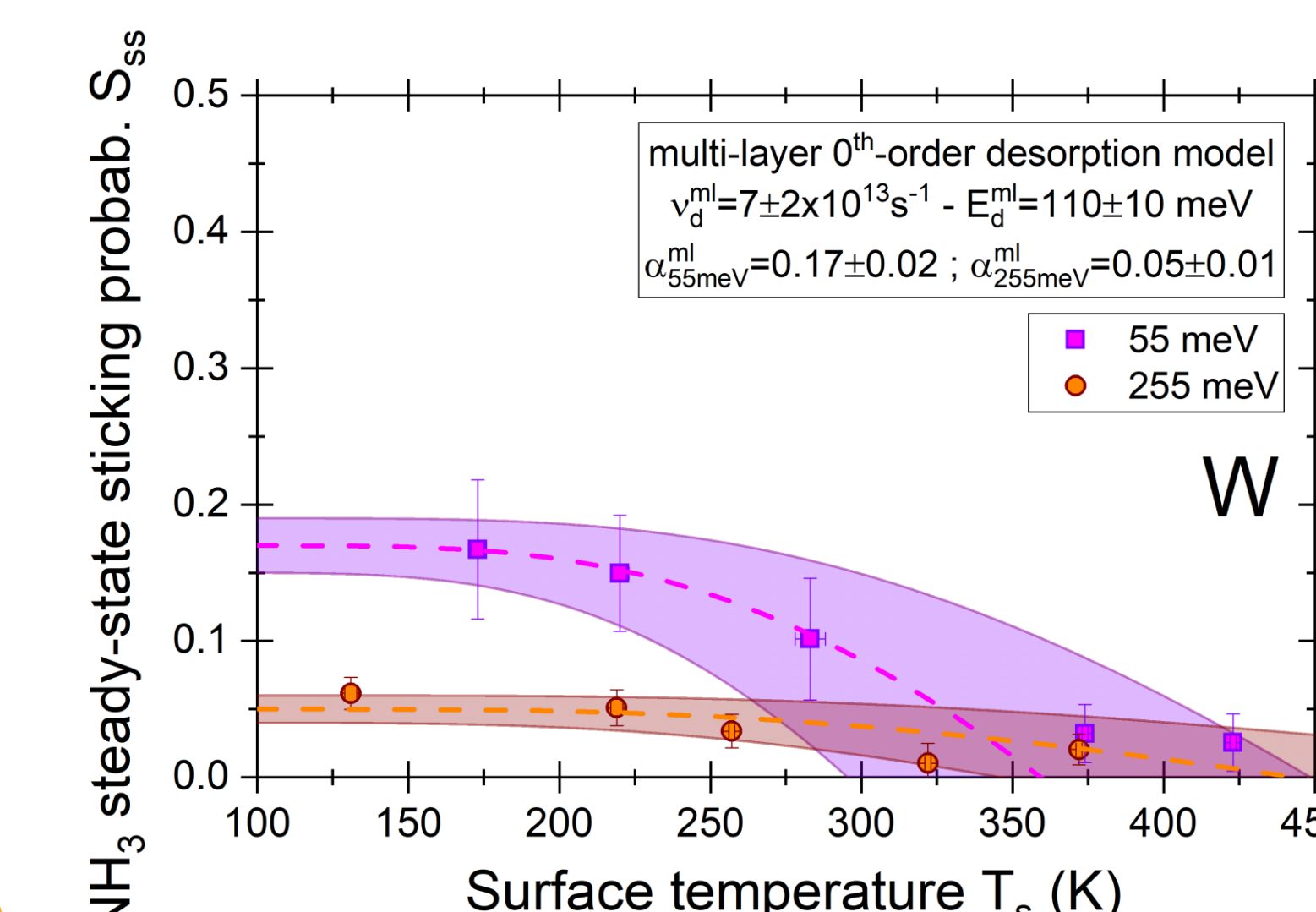
$$S(\theta) = F \int_{t_0}^t S(t) dt \quad F: \text{flux}$$



## Sticking probability as a function of materials temperature and NH<sub>3</sub> coverage



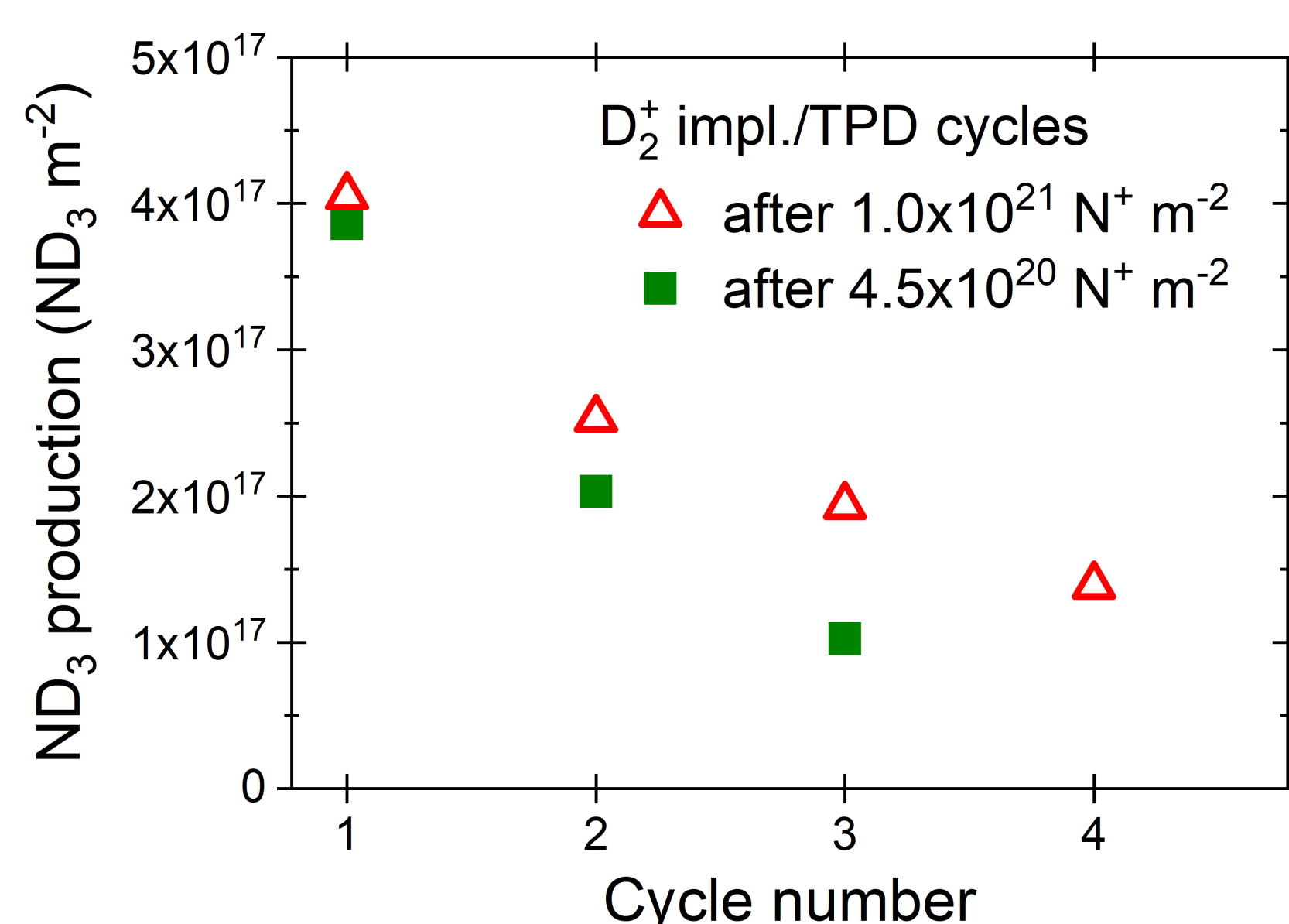
A two precursors adsorption model & an island-based multi-layers adsorption model are able to reproduce all our sticking results and are consistent with Yaala *et al.* (Nuc. Fusion **58** (2018) 106012) experiments



Published results: M. Minissale *et al.*, J. Phys. Chem. C **124**, (2020) 17566

## NH<sub>3</sub> production mechanism on W

- Cycles of ND<sub>3</sub> production from a saturated N layer in W is realized by repeating D implantation and desorption up to 750 K (i.e. keeping the N layer in W after desorption)
- A linear (exponential ?) decay of ND<sub>3</sub> production is observed
- The total quantity of ND<sub>3</sub> produced is less than 2% of available Nitrogen in the layer
- Total consumption of N is about 16% of the W surface atomic density
- N surface density consistent with SD.TRIM calculations (Meisl *et al.*, New J. Phys, **16** (2014) 093018)
- ND<sub>3</sub> production surface-limited (N diffusion negligible <750 K)



## Conclusion

Ammonia production is surface-limited on tungsten. Ammonia sticking on tungsten and 316L stainless steel is mediated by two precursors. Transient and steady-state surface coverage depend on NH<sub>3</sub> pressure and materials temperature and are described by the present models.

The views and opinions expressed herein do not commit the ITER Organization in his role of nuclear operator.