

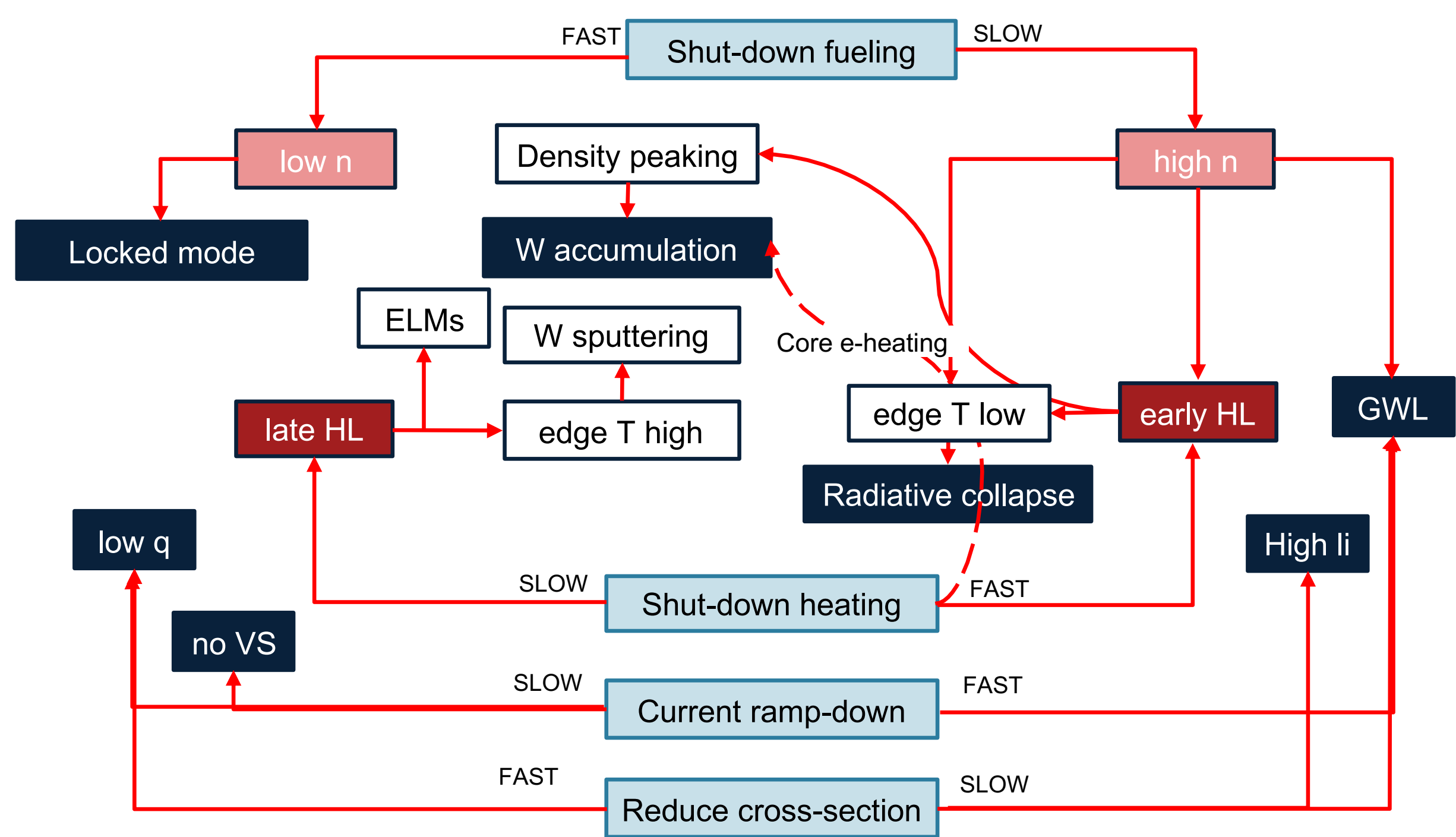
The ITER plasma termination phase: physics constraints on control

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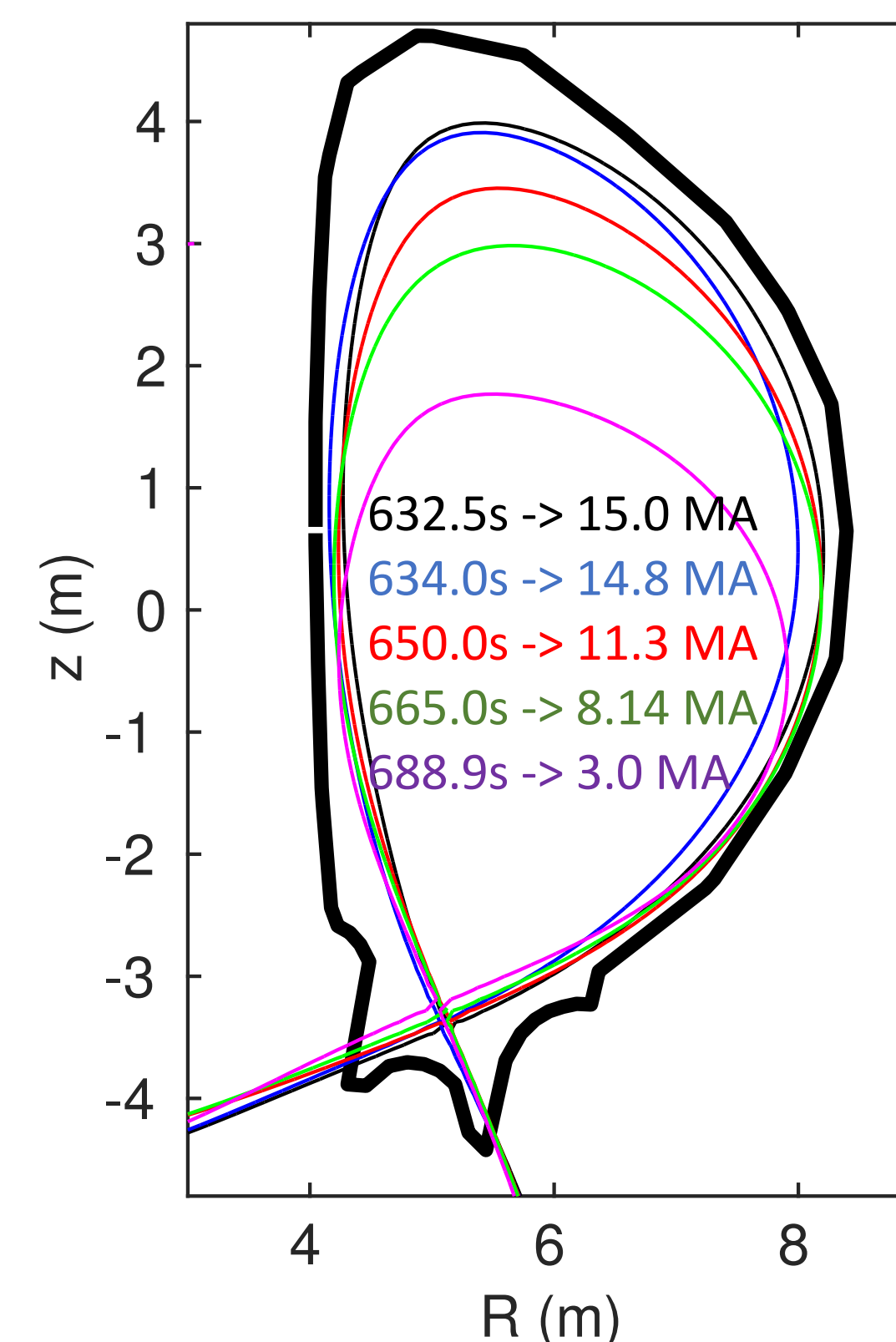
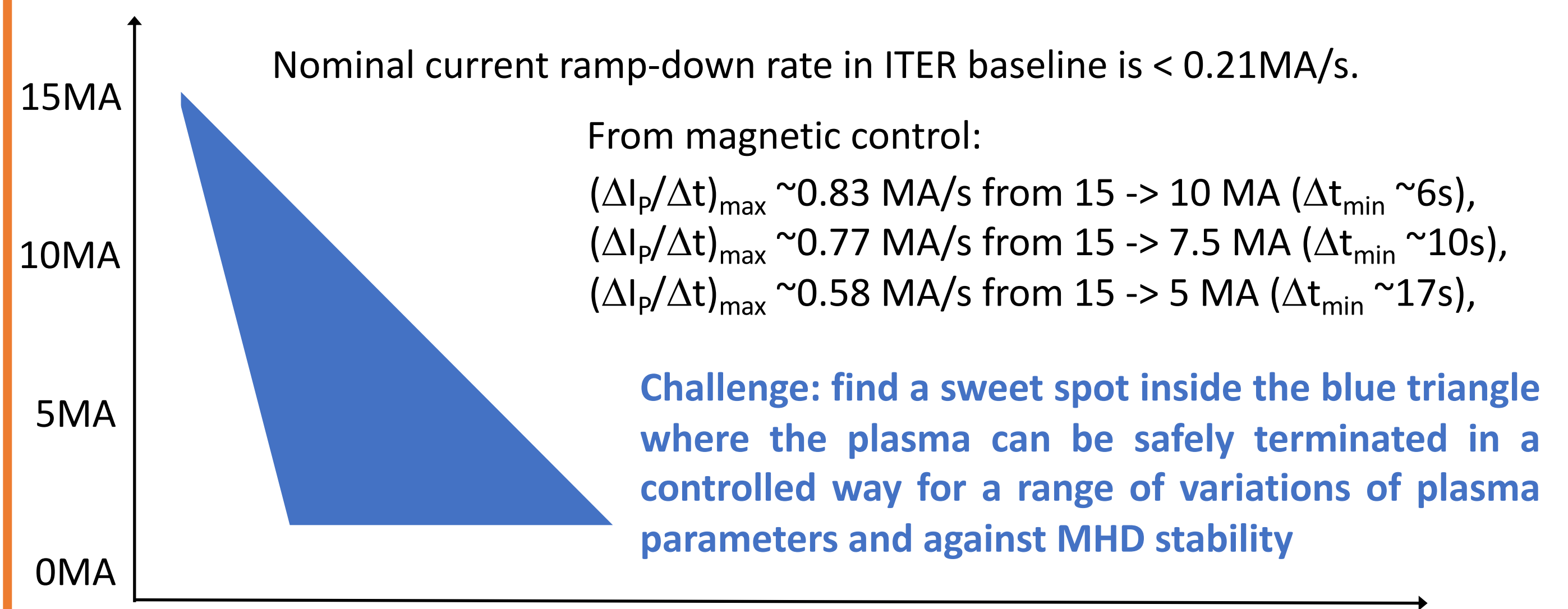
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A controlled ramp-down should balance all responses



- Power step-down
 - Shut-down auxiliary power and fueling => IC coupling, EC, NBI shine-through, fast ions
 - Controlled exit from burn and H-mode => radial position control
 - Maintain control of impurities/radiation => seedling, core electron heating
- Current ramp-down
 - Avoid vertical instability due to increase of I_i (shape+heating) => reduce cross-section
 - Avoid additional flux consumption => reduce plasma current
 - Stay in X-point as long as possible to maintain particle and power handling => ~2MA

Simulations of the ITER termination phase need to satisfy all operational limits



- PF/CS coil limits
- Vertical position control
 - reduce elongation to keep I_i low
- Shape/gaps control
 - Plasma diverted down to 2MA
 - Radial mid-plane gap > 7 cm
 - Min. gap between inner/outer separatrix > 4cm

Use a parametrization for the edge as boundary condition for core transport

TRANSP calculates transport and outfluxes

edge input core output (@ $\psi=1$)
 Total input power P_{SOL}
 DT ion outflux $\Gamma_{\text{DT,sep}}$
 Helium ion outflux $\Gamma_{\text{He,sep}}$
 $\xi_{\text{ei}} = P_e / P_i$

Edge input – external control
 Pumping speed S_{ENG}
 Gas puffing rate Γ_{puff}

SOLPS parametrization gives values at separatrix

Core+pedestal input edge output (@ $\psi=1$)
 Separatrix temperature $T_{\text{i,sep}}, T_{\text{e,sep}}$
 Separatrix density $n_{\text{sep}}, n_{\text{He,sep}}$
 Neutral influxes $\Gamma_{\text{DT,n,sep}}, \Gamma_{\text{He,n,sep}}$
 Neutral temperature $T_{\text{DT,sep}}, T_{\text{He,sep}}$
 Impurity concentration

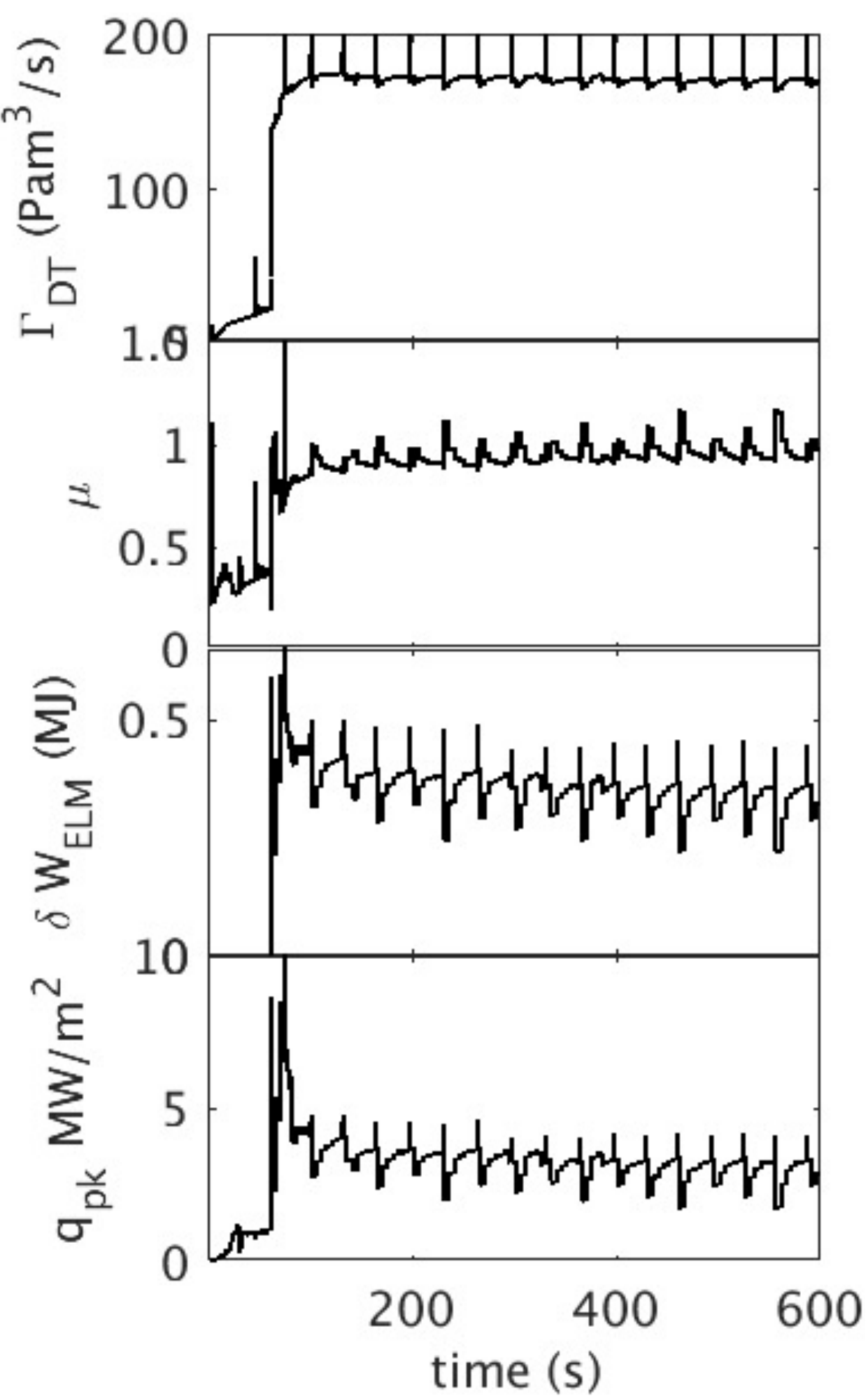
Core input – external control
 Auxiliary heating power P_{aux}
 Core DT fueling Γ_{core}

Throughput $\Gamma_{\text{DT}} = \Gamma_{\text{puff}} + \Gamma_{\text{core}} \leq 200 \text{ Pa m}^3 \text{ s}^{-1}$
 limited by cryopump and T inventory

Peak power loading $q_{\text{pk}} \leq 10 \text{ MW/m}^2$
 Limited by target design

Edge parametrization from Pacher et al, JNM 463 (2015) 591

Observables for control



$$\Gamma_{\text{DT}} = \Gamma_{\text{SOL}} + \Gamma_{\text{ELM}} + \Gamma_{\text{LFS}}$$

$$\mu = (\Gamma_{\text{DT}} / 250 S_{\text{ENG}})^{0.83} P_{\text{SOL}}^{-0.52}$$

$$\delta W_{\text{ELM}} = 0.2 P_{\text{SOL}} / f_{\text{pel}} \quad f_{\text{pel}} = 35 \text{ Hz}$$

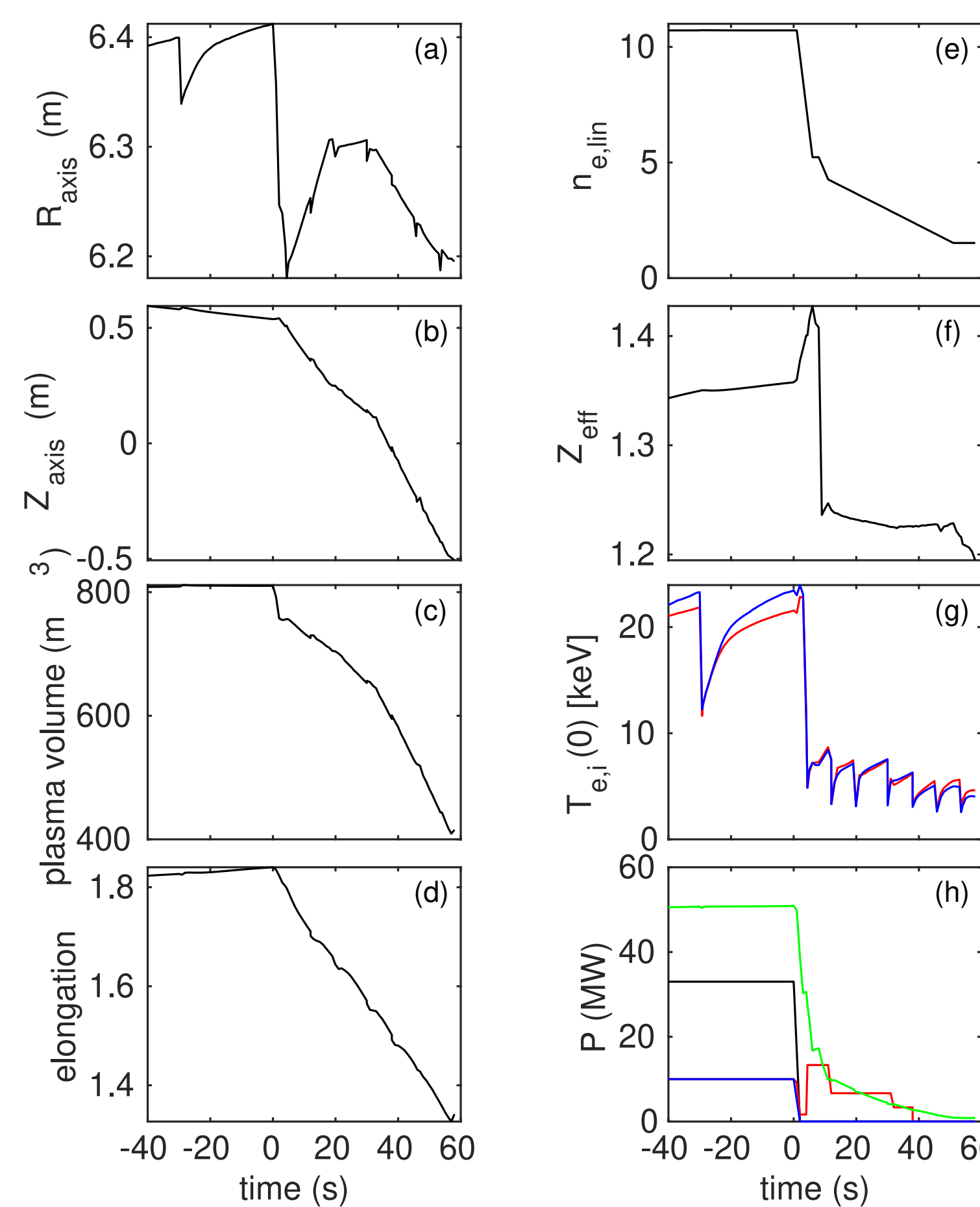
$$\Gamma_{\text{ELM}} = 0.2 n_{\text{ped}} P_{\text{SOL}} / 1.5 V_{\text{ped}}$$

$$q_{\text{pk}} = f(P_{\text{SOL}}, \mu, C_{\text{Z,sep}}, S_{\text{ENG}}, P_{\alpha})$$

Limits of these simulations:

- Do not include ELM regimes
- H-L transition based on scaling
- Density peaking not realistic (either prescribed or based on semi-empirical)
- Uncertainties on dynamical variation of the Greenwald fraction

Initial assessment of H-L transition time



H-L transition at 15MA

- Let the controller do everything
- No NTMs in ramp-down

Risk assessment => high current disruptions

step-down everything together
 => in what sequence? what time scales?
 => Compatibility with DMS response time?

H-L transition around 10MA

Risk assessment => NTM control

w_{EC} naturally broadens => reduced CD efficiency

$q=2$ surface drifts => need to track (m,n)

Compatible with steering capabilities, but what about

=> ECE S/N ratio

=> magnetic equilibrium response

$$m_s = \left[\frac{1.47 (1 + e^{-2\ell_i + 1})}{2(\kappa - 1.13)} - 1 \right] (1 + 0.6(\beta_P - 0.1))$$

Conclusions from initial assessment with reduced models and 0D parametrization:

- H-L transition at higher current is more controllable than transition at lower current
- Because it minimizes the number of combined operations for the PCS
- It minimizes risks with loss of NTM control and ELM heat loads