SLOWLY ROTATING 3D FIELD FOR LOCKED MODE AVOIDANCE AND H-MODE RECOVERY IN DIII-D

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Abstract

A slowly rotating 3D field has been considered a promising approach for preventing the locking and growth of NTM-driven disruptions in high beta plasmas, or enhancing the H-mode recovery. Recently, M3D [1], numerical simulations have found new properties of the q=1 modes in these plasmas that suggest the possibility of using the rotating 3D field to sustain the plasma core against quasi-interchange (QI)-driven sawtooth crashes, at the same time as avoiding NTMs locking at q>1. The characteristic q=1 QI modes are found to have dominant n=1 and 2 toroidal harmonics of comparable magnitude that are well suited to interact with the external 3D field. Preliminary experimental observations in hybrid configuration discharges support the possibility of quasi-interchange mode control with the slowly rotating 3D field and suggest that it can be explored simultaneously with the control of NTM locking avoidance.

1. INTRODUCTION

The high beta plasmas with slowly rotating 3D field have been explored as a promising approach for avoiding the locking of neoclassical tearing modes (NTMs) and improving H-mode recovery against NTM-driven disruptions. Recently, numerical MHD simulations of these plasmas using M3D simulation code [1,2] have revealed the external 3D field may have an additional advantage for the sustainment of the core in the quasi-interchange (QI) regime. This is based on the unique characteristics of the QI instability in these plasmas, namely multiple toroidal harmonics at the
lowest toroidal harmonic mode numbers n=1 and 2 with magnetic perturbations that extend well outside q=1 domain. This paper reports preliminary experimental observations in an ITER baseline scenario development discharge in DIII-D that support these simulation predictions. The experiments indicate that control of the quasi-interchange mode over q ≤ 1 can be explored simultaneously with the locking avoidance of NTMs at q>1, using the same slowly-rotating 3D field.

The paper first briefly summarizes MHD simulation results on QI modes with an applied rotating resonant magnetic perturbation (RMP) DIII plasma using the M3D code [3] that are very useful to understand the experimental observations. The plasma configuration considered in this paper is the hybrid plasma with the central safety factor q(0) just above unity. We show the 3D field of the I-coil that was applied for the m/n = 2/1 (m is the poloidal harmonic) NTM locked-mode avoidance can also contribute to regulating the QI mode instability by controlling the core Te collapse, consistent with the suggestion by the numerical simulation. The preliminary experimental observations include several elements. The core Te collapse deforms the plasma column in a helical manner. The experimental analysis confirms the existence of internal n=1 and n=2 harmonics. The phasing control between the applied 3D field and the instantaneous plasma response through feedback [4, 5] indicates that it is possible to control the couplings between the n=1 and n=2 harmonics. The reduction of coupling between internal n=1 and n=2 harmonics may make it simpler to stabilize NTMs in hybrid configurations.

Disruptions due to the locking and growth of neoclassical tearing modes are one of potential obstacles remaining for successful tokamak-based fusion burning in ITER and beyond. The external application of a slowly rotating n=1 RMP could stabilize the most dangerous tearing-locking at q=1, in particular the 2/1 mode at q=2. New results show a possibility that the rotating RMP also produces general plasma conditions favorable for central fusion burning, through a unique set of effects. Small sawteeth driven by QI-modes (here called QI-driven crash) are much more favorable for fusion burning than the larger amplitude internal kink-driven sawteeth at q(0)<1.

2. QUASI INTERCHANGE INSTABILITY AND QUASI-STeady STATE

Numerical simulation with the extended MHD code M3D[1,2] was carried out for the DIII-D ITER-baseline plasma shape discharge with q(0)~1 and q95=4.0 (#166564 at t=3445ms), when an n=1 rotating RMP was applied to prevent the rotational locking of the 2/1 NTM[3]. It showed that the central low magnetic shear q≤1 region is unstable to a nearly ideal quasi-interchange (QI) mode that causes a sawtooth-type crash. The simulation used the experimental profiles and parameters of discharge after the original 2/1 NTM at q=2 had been successfully suppressed by the applied RMP. The RMP itself was not included, due to its very slow rotation frequency.

The simulation followed the QI instability from very small amplitude to its maximum growth rate and the central QI-driven crash that flattened the core profiles of temperature T and the toroidal current density Jφ, followed by profile healing and eventual establishment of a perturbed quasi-steady QI state over q=1. Figure 1 shows the details, taken from the case of Ref. [3]. Due to the low magnetic shear, the QI modes in the initial stages of the crash are fundamentally nonlinear, characterized by two toroidal numbers n=1 and 2 of comparable magnitude that grow at the same rate (Fig.1(b,c)). At low amplitude, these are 1/1 and 2/2 inside q=1, respectively. The sawtooth-like crash, shown by the temperature profile evolution in Fig.1(a), resemble experimentally observed QI-driven crash in DIII-D 153967 (as shown in Section 3.1), which differs from the resistive internal kink.

The QI crash is dominated by smooth interchange flows transverse to the magnetic field. The simulated mode initially has n=1 and 2, but becomes strongly n=1 at the height of the crash (Fig.1 (b,c)). The interchange flows determine the plasma and magnetic field motion. The flows steadily displace the hotter plasma core and separate its contact region with the q=1 surface in two halves. The two contact regions continue to narrow poloidally, until a strong localized interchange process expels the remaining core pressure out to a mixing radius well outside the q=1 (see Fig. 11 in Ref. [3]). There are no resonant X-points or large-scale magnetic reconnection at q=1. The final expulsion is strongly n=1. Because the entire central q region remains close to unity, the perturbed magnetic field l0BI remains small. After the crash heals, a quasi-steady state develops, with sustained strong n=1 and n=2 harmonics inside the low shear q=1 region and a hollow axisymmetric temperature profile. Many of the QI mode properties predicted in the simulation [3], including the stability analysis, are seen in the actual plasma 166564 and in the discharges discussed in this paper.
The existence of the large n=2 harmonic in the simulated q=1 QI mode at low amplitude, and its higher m=n+1 sidebands that extend well outside q=1, suggest that the n=2 harmonics of the rotating RMP might be used for MHD control of the QI driven-crash, while the n=1 RMP harmonic were used to suppress the 2/1 NTM (Dual n=1 & n=2 combined system). Control using n=2 is unlikely to be possible for the conventional resistive internal kink sawtooth, because it is n=1 until shortly before the final crash. Preliminary discussion of n=2 involvement in the control experiment is reported in this paper.

3. EXPERIMENTAL OBSERVATIONS

Figure 2 shows an example of how the NTM behaves around $\beta_N \sim 3$ in hybrid configuration with q(0) nearly unity and the H-mode recovery[6]. In this shot, H-mode was formed just after the initial plasma current ramp-up around t=1600ms (not shown). The edge pedestals of electron temperature Te and density ne profiles were kept in a steady manner over a few hundred milliseconds. In this shot, the onset of NTM which unexpectedly caused the massive gas inflow (seen in the burst in saturated D$\alpha$ signal at $t \sim 1980$ms) inducing a fast Te pedestal decay and loss of the H-mode. The magnetic sensor signal monitoring the NTM amplitude and growth rate activated the application of 3D field. The general concern is that if the NTM grows too large, it may be impossible for a n=1 only system to control the mode locking. Just after the L-mode began, the preprogrammed frequency began at 20 Hz and quickly increased in time with the rate of 100Hz over 100ms. At the H-mode recovery time, the frequency was around 50Hz[6]. The magnetic sensor signal shows the MHD mode was synchronized with the RMP I-coil current and did not lock to the wall. The plasma condition was a typical hybrid scenario with $\beta_N \sim 2.1$, q95=4.0 and density 4.1x10$^{19}$ m$^{-3}$ when the coils locked the mode. The mode structure and QI mode behavior was monitored with the Electron Cyclotron Emission (ECE) signal.

3.1. EXPERIMENTAL RESULTS

The time period of QI-driven crash around H-mode recovery is shown in Figure 3. The development of the QI-driven crash and Te flattening evolution in time was illustrated by the perturbed electron temperature $\delta$Te calculated from ECE Te by subtracting the running average over one cycling period of 3D field around the time of interest. Although the critical QI-driven crash activity began around $t \sim 2152$ms, $\delta$Te flattening by QI-activity started much earlier just after the main NTM started to synchronize with the applied 3D field around $t \sim 2100$ms. The partial QI-driven flattening was visible when the tearing mode (NTM) was locked to the applied 3D field around 2150ms.
Around that time period, the dominant oscillatory component of the NTM began to vanish away. With the 50Hz range of 3D field rotation, the main plasma began to show a response unified from the core to near the edge. This led to the initiation of a periodic QI-driven crash at every other cycle of I-coil current. The initial boundary behavior (around $\rho=0.2-0.3$) began to change from H-mode recovery around $t=2252\text{ms}$. The following crash ($t=2300\text{ms}$) was formed with two off-centered cool regions. With further recovery of the H-mode, the central crash is sharper around $t=2335\text{ms}$. The blue-colored area indicates a large sharp $T_e$ drop was taking place with longer recovery time. The QI-driven crash became regularly repetitive at every 3D field cycle with a frequency of $\sim150$ Hz later in time (not shown). Next, using the reproducible time period, we look at the mode structure as the numerical simulation suggested.

Figure 4 shows the QI-driven crash with an RMP frequency of 120 Hz, about 150 ms after the onset of H-mode. The Thomson scattering shows a well-established $T_e$ and $n_e$ H-mode edge profile during this time (not shown). The details of the formation of $T_e$ collapse and perturbed $T_e$ profile were calculated from the ECE by subtracting the DC profile offset at $t=2480\text{ms}$ to minimize the uncertainty due to the possible $T_e$ profile rapid change during the crash event. The $q$-profile (Figure 4(a)) was obtained from the EFIT calculation with MSE Bz measurement but no kinetic correction included. The $\delta T_e$ behavior shown in the Figure 4(b) contour and the expanded contour (Figure 4(d)) shows two small radially-localized cool regions first appears off-axis: $\rho = 0.25$ in the Low Field Side (LFS) and $\rho = 0.25$ at the High Field Side (HFS). These two initial growing cool cells drift toward the axis in a manner of avalanche, of which time evolution is visible in Figure 4(d). The one initiated at LFS might have not propagated smoothly until it reached a little toward the core axis as shown in Figure 4(d). The plasma equilibrium may be slightly asymmetric so that the initial tiny crashes at HFS/LFS evolve differently until the penetration reached below $\rho =0.2$. The two cool regions took a few hundred microseconds to reach the magnetic axis, producing a crescent-shaped cliff of a few hundred electron-volt drop on the ECE signals. The QI observation on the midplane such as mode structure (Fig. 4(e)) and its resulting to the crescent shape collapse in time is in a good agreement of the 3D simulation results of Fig.1 (a). The simulation [3] shows at the complete process takes place through the poloidal interchange flow mechanism without any resonant reconnection at $q=1$.

Fig. 3. The Core-$T_e$-collapse behavior around H-mod onset (#153967) (a) The electron density and beta-$n$, $\beta_n$. (b) I-coil current and the perturbed $\delta T_e$ (c) the $q$-profile(x-axis) vs. rho(y-axis).
This local Te profile drop by crash decays away with a 7-10 ms decay time constant. These slow time-developments indicate that transport processes are involved in the setting-up condition and the onset of QL-driven collapse. It is also possible that the QL-mode itself influences the transport properties. Next, we look at the possible involvement of low-n components as the numerical simulation suggested using the reproducible time period.

3.2. THE RECONSTRUCTED MULTI-TOROIDAL COMPONENTS WITH MAGNETIC SENSORS

The information of radial perturbation toroidal wavenumber is highly desirable. However, the radial profile measurement is available at only one toroidal location. On the other hand, magnetic sensors are located at various toroidal angles outside the plasma and provide the amplitude and phase with sub-millisecond time resolution over multi-toroidal harmonics.

By assuming that the information from the internal events dominantly involved in the magnetic process is transmitted outward without additional dissipation to the plasma boundary, we can relate the magnetic sensor signals to the perturbed-profile components. Here, $\delta Te$ from the ECE signals is decomposed as a sum over the lowest toroidal harmonics as

$$\delta T_{e,j} = \sum_{n=1,2,3} C_{n,j}(r,j) * \delta B_n(t)$$

The $\delta B_n(t)$ is expressed by complex components determined from magnetic sensor signal decomposition. The complex coefficient $C_{n,j}$ is determined by taking average over one cycling time period of 3D field with the error minimization each observation surface. Thus, the toroidal phase shift such as due to resistivity can be included by the complex coefficient radial profile. Reconstructed toroidal component is given by,

$$\delta T_{e,n,j,\text{reconst}}(r,t_{sampling}) = C_{n,j} * \delta B_n$$

The examples are shown in Figure 5 and 6 corresponding to the time period before the crash (2480-2493 ms) as shown in Figure 4(a,b). We did not include the collapse dominated time period here, since the coefficient $C_{n,j}$ is assumed to be constant over each surface. Figure 4 (a) shows the I-coil current and the inputs to the analysis, namely the magnetic sensor signals of $n=1,2,3$. (I-coil current was not used for the calculation). The fitting results (blue curves) and the input ECE signals (black) are shown in Figure 5(b).

Figure 6 shows the reconstructed radial $\delta T_{n=1,j,\text{reconst}}$ profile at various time before the crash. The $n=1$ component of reconstructed $\delta T_{n=1,j,\text{reconst}}$ provides where rational surfaces may exist. The odd-parity behavior seen between $\rho=0.2$ and $\rho=0.2$ at any time slices indicates these two locations are rational surfaces at rho $\rho = \pm 0.2$. The resonant response is also seen at $\rho = 0.65$ corresponding to a 2/1 mode. The radius of $\rho = 0.2$ or $-0.2$ could be attributed to a safety factor of unity. On the other hand, it is hard to explain the rational surface at $\rho = 0.4$ with a monotonic q profile. Thus,
tentatively, we assume that a second helical-q=unity surface exists in this configuration, as suggested by Figure 4(e). We will reexamine this assumption a-priori. The n=2 component of reconstructed $\delta I_{n=2, j_{reconst}}$ magnitude remains finite but show some indication of peaking at $r=0.4$.

4. QUASI INTERCHANGE MODE UNDER TEARING LOCKING AVOIDANCE CONTROL

The M3D simulation in Section 2 showed that the amplitude of the $n=1$ and $n=2$ components are comparable when the QI-driven crash grows and suggested that this was a general property of these DIII-D plasmas with low shear $q=1$ regions. The rotating $n=1$ RMP feedback fits well to the dual purpose of preventing the locking of the 2/1 NTM and investigating the QI-driven crash. The feedback requests the adjustment of the I-coil current to have a finite phase delay relative to the observed mode component as if pushing the observed component behind. The feedback minimizes the phase between the 3D field and the mode excited in plasma. At the same time, the feedback also tries to reduce the amplitude of the observed mode.

Figure 7 shows the results of the 3D feedback control to unlock the NTM which was already locked earlier (~300ms before). The preliminary survey before this shot had indicated that the plasma condition was very sensitive to the extra 3D field application. Thus, the DC component of I-coil current was gradually increased to a typical error field correction level of 1kA after the locking to the wall (the error field correction was provided separately by the C-coil system). Here, the AC frequency feedback range was set to around 30 Hz, which is a factor of five slower than the preprogrammed operation discussed in section 3. After the 3D field was applied initially as shown in Figure 7(b,d) at t=2520ms, the relative phase difference at the maximum amplitude between the 3D field and $n=1$ mode (also $n=2$) became small. However, the mode amplitude was gradually increased. The better coupling between the 3D field and the plasma response is likely to have helped reduce the applied frequency. At the same time, the core-collapse structure began to evolve in time. The balance of $n=1$ and $n=2$ components remains to be improved.

The first core Te collapse at $t=2510.5$ms in Figure 7(d) is similar to the H-mode recovery case as shown in Figure 4(b,d). The details of first collapse are shown in Figure 8. The small Te perturbations appearing at HFS and LFS at the startup arrive at the axis at $t=2510.5$ms [Figure 8 (d)], similar to the case in the section 3, but in the second crash at $t=2542$ms, no trigger cooling spot at the LFS seemed visible and the crash started only at HFS persisted and drifted toward into the LFS. This situation became more clear with the crash of third cycle at $t=2582$ms and fourth cycle at $t=2622$ms. These crashes show that the radial extension of Te collapse is now connected beyond $r \sim 0.4$.

Figure 9 shows how the $n=1$ and $n=2$ responses at off-axis extend inward to the $p=0.4$ domain, reaching the boundary of helical-q unity region, $p=0.4$, where interacts with the QI-driven core crash (Fig.9(a)). The $n=1$ reconstructed response (Fig. 9(b)) becomes maximum around $p=0.65$ corresponding to the 2/1 surface and extends radially inward with a nearly constant amplitude and sharply decay around $p=0.4$ helical-q unity area. The $n=2$ component amplitude (Fig.9(c)) increases both at slightly-outer/inner sides of $q=2/1$ area with the variation at 2/1 minimum as if the $n=2$ structure deforms by the even-flattening, at same time with smooth radial-extension toward $\rho=0.4$ with constant amplitude, similar to the $n=1$ behavior toward the $p=0.4$. The 3/2 resonant-type response is
visible at q=3/2 around \( \rho = 0.52 \). The \( n=1 \) and \( n=2 \) components are in the same magnitude \( \sim 0.1 \text{keV} \), significant by considering the overall \( \Delta T_e \) is \( \sim 0.3 \text{keV} \). The handshaking around \( \rho = 0.4 \) takes place in the very stable manner. The further increase of the \( n=1 \) and \( n=2 \) component later in time eventually causes a minor collapse, but taking place outside \( \rho = 0.4 \), while the perturbation inside of \( \rho = 0.4 \) remains minimum (detail discussion in a separate paper).

5. DISCUSSION

Slowly rotating 3D fields have been considered as a promising approach for locking avoidance and H-mode recovery against NTM-driven disruptions. This 3D field application approach has been found effective, but, near the operational limit, the application is not always successful. Recently, M3D numerical simulations\cite{3} of locking-avoidance experiment discharge suggest there exists an additional MHD advantage of the rotating 3D field for sustaining the off-axis domain separated from the quasi-interchange. The preliminary experimental observations in the hybrid configuration discharge suggest that it may be possible to control the quasi-interchange mode stability together with the NTM-driven disruptive mode using separate aspects of the same slowly-rotating 3D field by considering the coupling between \( n=1 \) and \( n=2 \) components. Based on the core \( T_e \) collapse evolution and the fluctuation behavior measured by ECE, we tentatively conclude that the QI sawtooth seen in the simulation is consistent with experimental observations and that the experimentally observed stability appears to follow the multiple criteria identified in the simulation paper, although the complete picture of QI-driven stability also depends on many other factors. Some interesting remarks and uncertainties are summarized here.

(1) Measured behavior of the \( T_e \) collapse is qualitatively consistent with the QI-driven crash seen in the simulation.

(2) Timing of the \( T_e(0) \) crash is independent of the phase of the rotating RMP phase for i-coil frequencies up to 200 Hz. The feedback of the RMP reduced the frequency of the repetitive crashes to the 30 Hz level.

The experimental observation is qualitatively consistent with the QI-type crash seen in the simulation, despite the different plasma conditions between two cases, which are listed as follows. Here, we use the shot number as the identifier: simulation (166564) and the present experiment (153967 and 153974).

(1) Profile shape. Discharge 166564 was completely sawtooth stable because the actual central pressure profile was hollow (\( T_e \) was hollow and the density profile slightly hollow over \( q<1 \)), yielding an effective negative poloidal \( \beta_p \) for \( 1/1 \) mode stability (instability requires \( \beta_p > \beta_p, \text{crit} > 0 \) where \( \beta_p \) is a poloidal beta defined by the average of pressure gradient inside the \( q=1 \) surface and \( \beta_p, \text{crit} \) is the critical value for the stability\cite{7} while 153967 had centrally peaked density and temperature. The simulation used the slightly peaked pressure profile from the experimental EFIT

(2) Plasma shaping. The plasmas had different flux surface shapes that increased the interchange stability (of the magnetic well parameter) of 166564 compared to 153967. The simulation shot,166564 was a D-shaped ITER baseline plasma that scales to a 20 keV ITER burning state. Interior flux surfaces had ellipticity combined with significant triangularity, which has a stabilizing effect on the \( n=1 \) interchange modes \cite{8}. The shot reported here (153967) was elliptical, with little triangularity, corresponding to greater interchange instability.

(3) Plasma beta: 166564 had higher beta (\( \beta_N=2.3 \) compared to 1.5 in 153967) and a larger Shafranov shift of the magnetic axis, which increases the stabilization due to triangularity in the interchange magnetic well criterion.
Since triangularity is stabilizing for most MHD modes, 153967 is generally more unstable than the simulation shot 166564.

In summary, we have started to extend the application of an n=1 rotating 3D field for mode-locking avoidance to the control of the core QI-driven crash at the hybrid configuration q=1 as well. The quasi-interchange stability in hybrid regimes with central q=1 has dual low toroidal harmonics n=1, 2 that make its spectrum well suited to interact with an external 3D field. This is very helpful to integrate the MHD understanding from the core to the edge, in particular, in higher temperature less-collisional regime. The extended approach to control from core to the off-axis should contribute to develop paths attractive for successful realization of fusion reactors.

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REFERENCES