



RESEARCH FOR GRAND CHALLENGES

Increasing irradiation and thermo-hydraulic performance of breeding blankets by ODS steel plating

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Introduction



Advanced DEMO blanket: 50 dpa

- Hardening and embrittlement due to high neutron dose
- Helium bubbles due to transmutation
- Fatigue due to pulsed high heat flux load

Mitigation of hardening and embrittlement





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Helium embrittlement

What do we know?

- At temperatures >0.5 T_m, stress and transmutation lead to He migration to grain boundaries.
- At grain boundaries, the formation of large intergranular bubbles significantly degrade strength and toughness.
- The critical helium amount is estimated to be 200-500 appm, corresponding to 20-50 dpa for a DEMO first wall
 Proof by IFMIF/DONES

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Mitigation of helium embrittlement



High density of effective helium sinks

Finely distributed oxide dispersoids in ODS steels can trap helium and prevent the formation of critical big bubbles.



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ODS vs. standard EUROFER



ups

- Better irradiation performance
- 👍 Higher fatigue lifetime
- 👍 Higher creep strength

downs

- High fabrication costs
- Reduced production capacities
- Limited welding processes: only diffusion bonding or friction welding

Reduction of material needs



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A volume of about 0.3 m depth from the surface of the first wall would require an amount of ODS steel in the order of **several 100 tons**. → important long-term goal (not followed in this study)



nboard blanket ield dpa/FPY esse 120 140 160 Central inboard blanket steel shield

rst wall



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FC

shield

60 80 100 120 140 160

Vacuum vessel

Objectives of this project



- Design an advanced blanket first wall mock-up with superior thermo-mechanical properties and potentially higher irradiation resistance for longer component operating-times by the use of ODS steel plating.
- Select, optimize, apply industrial fabrication processes for the mock-up manufacturing.
- Demonstrate the performance of the mock-up by cyclic high heat-flux tests in a helium cooling loop.
- Analyze the highest loaded areas of the mock-up after the tests.

ODS steel production



Production of thin plates (2-3 mm) from a ~100 kg batch of



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ODS steel plates



More than 0.5 m² plates produced from 2 consolidated blocks of 15 kg each

→ 2 plates: 1200 mm x 230 mm x 2 mm → 2 plates: 1000 mm x 100 mm x 3 mm → 2 plates: 1300 mm x 100 mm x 2 mm

One advanced DEMO blanket module \rightarrow 100-400 kg Complete DEMO blanket first wall \rightarrow 20 to 40 tons

 Verification of 100 kg ODS steel production route successful
 Several 10-ton ranges feasible



Mockup design



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from the plasma is only **3 mm**.

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Mockup after ODS steel plating and fabrication of cooling channels

Mockup fabrication





NOTE: The height of the middle channel was intentionally increased to 11 mm, so that the upper part runs into the ODS steel plate. Therefore, the middle channel includes two weld seams along both upper corners. Since the corners are the highest stressed regions in the mockup plate, we have produced artificial crack initiators, which we expected to develop cracks or even fracture during the high heat flux tests.

Installation layout





helium distributors

- mass flow rate
- CFD simulations
- velocity profiles





Connectors at both ends of the mock-up plate



- TIG welds performed
- post-welding heat treatment (PWHT)
- 980 °C/1 hour + quenching + 750 °C/2 hours
- liquid penetration tests
- ultra-sonic tests

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Installation in the Helium Loop Karlsruhe (HELOKA)



Fixation on mounting plate

Instrumentation

- Surface temperature (IR-camera)
- Inlet temperature
- Outlet temperature
- Total mass flow
- Inlet pressure

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Outlet pressure



He cooled divertor mockup

Plasma sprayed W coated FW mockup

ODS plated FW mockup

High heat flux tests



Test sequence	No. of cycles performed	Heat flux	Puls length (on/off)	Surface temperature
#1	100	0.7 MW/m ²	2 min / 2 min	~550 °C
#2	100	0.8 MW/m ²	2 min / 2 min	~600 °C
#3	100	0.9 MW/m ²	2 min / 2 min	~650 °C
#4	7	0.9 MW/m ²	2 hours / >2 min	~650 °C





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High heat flux tests





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Experimental results





No peculiar changes in the operating parameters.
 This indicated that the structural integrity was most probably not affected.

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Post testing examination





Mockup pieces with labels 1-4 in top-down view (upper left). Sideview of piece #3 from which the SEM sample was cut (upper right). Technical drawing and identification of the cooling channel cross-sections A, B, C (lower part).

Post testing examination





Comparison of the BSE images acquired in the ODS/EUROFER97 interfacial region close to channel C (left) and channel A (right).

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Post testing examination





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In both areas, three phases were found: Fe/Cr matrix, (Cr/W) carbides, and Ti carbo-nitrides.

- Heat affected zones formed at the EUROFER/ODS-steel interface in cold and hot areas as well.
- Coarser Cr carbide precipitates are located in the ODS steel part of the interface.
- Effect: carbon diffusion from EUROFER into the ODS steel.
- Cracks, "Kirkendall bubbles", or other obvious defects not observed.

Conclusions

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- Production route of 100 kg ODS steel powder and plate fabrication verified
- Up-scaling to the several 10-ton ranges feasible
- Industrial fabrication processes with very high tolerances against manufacturing imperfections for advanced

The mockup did not develop cracks or show tendencies to fail. Even at intentionally introduced weak points (i.e., the weld seams that were placed in one of the five cooling channels), crack formation did not occur.







 WpMAT

 Partners:

 France

and joined universities

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