

TECH/2 DEMO & Advance Technology

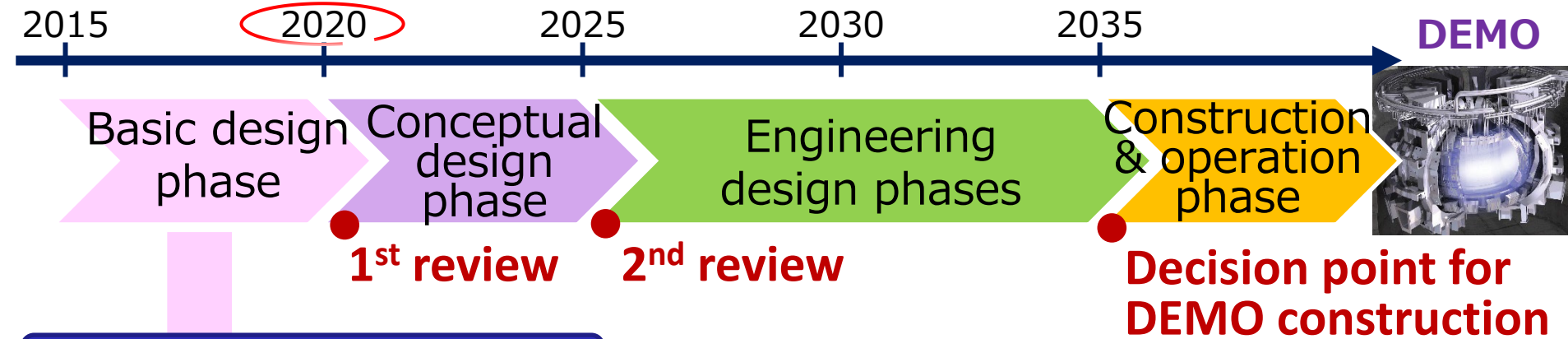
TECH/2-1 : Progress in design and engineering issues on JA DEMO

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Objective of DEMO

- ✓ Steady and stable power generation beyond several 100 MW
- ✓ Reasonable availability leading to commercialization
- ✓ Overall tritium breeding to fulfil self-sufficiency of fuels

Design principle in the basic design phase

- ✓ Application of as reliable technology as possible

Pre-conceptual design of JA DEMO

Plasma operation

- Major radius, $R_p = \sim 8.5$ m
Arrangement of large CS coil for a few hour pulse operation in the commissioning phase
- Plasma perform., $\beta_N = 3.4$, $HH = 1.3$
Study-state operation
- Fusion power $P_{fus} = 1.5$ GW
Allowable divertor heat load (Div. des. based on ITER technol.)

Engineering technology

→ ITER technol. as much as possible

- T breeding blanket:

➤ JA TBM strategy

- Divertor:

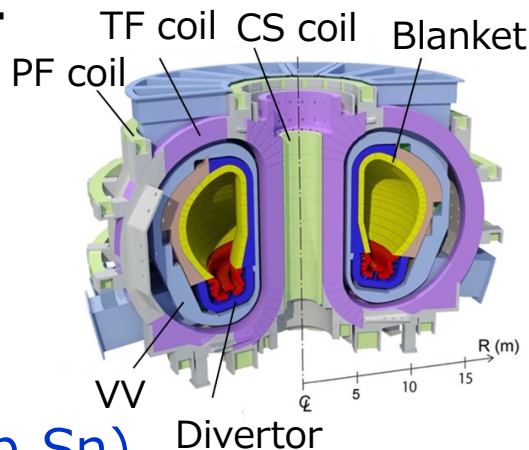
➤ Water cooling

➤ W mono block

- Magnet:

➤ Radial Plate struc.

➤ CIC conductor (Nb_3Sn)



	Steady state	2hrs pulse
R_p (m) / a_p (m)	8.5 / 2.4	
A	3.5	
K_{95}	1.65	
q_{95}	4.1	
I_p (MA)	12.3	
B_T (T)	5.94	
P_{fus}	~ 1.5	~ 1.0
Ave. NWL (MW/m ²)	1.0	0.7
Coolant water	290-325°C, 15.5MPa	
Q	17.5	13
P_{ADD} (MW)	~ 83.7	
n_e (10^{19} m ³)	6.6	
HH_{98y2}	1.31	1.13
β_N	3.4	2.6
f_{BS}	0.61	0.46
n_e/n_{GW}	1.2	

Plasma operation

- Major radius, $R_p = \sim 8.5$ m
- Arrangement of large CS coil for a few hour pulse operation in the

	Steady state	2hrs pulse
R_p (m) / a_p (m)	8.5 / 2.4	
β	3.5	

13 May 2021, 17:00 (Oral)

ID: TECH/3-2Rb, N. Asakura, et. al.,

Plasma Exhaust and Divertor Designs in Japan and Europe Broader Approach, DEMO Design Activity

Engineering

→ ITER to be as much as possible

- T bre... blanket
- 1M TBM strategy

● Divertor:

- water cooling
- W mono bl...

● Magnet:

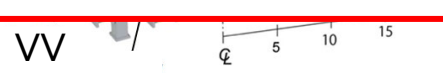
- Radial Plate struc.
- CIC conductor (Nb_3Sn)

13 May 2021, 08:30 (Poster)

ID: TECH/P5-1, H. Utoh et. al.,

Design study of large superconducting coil system for JA DEMO

Avg. NVE (MW/m ²)	1.0	0.7
...



T_{BS}	0.61	0.46
n_e/n_{GW}	1.2	

In order to increase the feasibility of JA DEMO concept, studies on the following engineering issues have been progressed.

1. Countermeasure against a loss of coolant accident inside blanket (in-box LOCA)

→ Blanket concept of a honeycomb shape was proposed with pressure tightness.

- ✓ **Issue_1: Increase in tritium retention due to stagnation of purge gas flow**
- ✓ **Issue_2: Complicated structure of the support rib arrangement**

2. An outlook of the steady and stable power generation beyond several 100 MW

→ The power generation system followed the PWR with close cooling conditions.

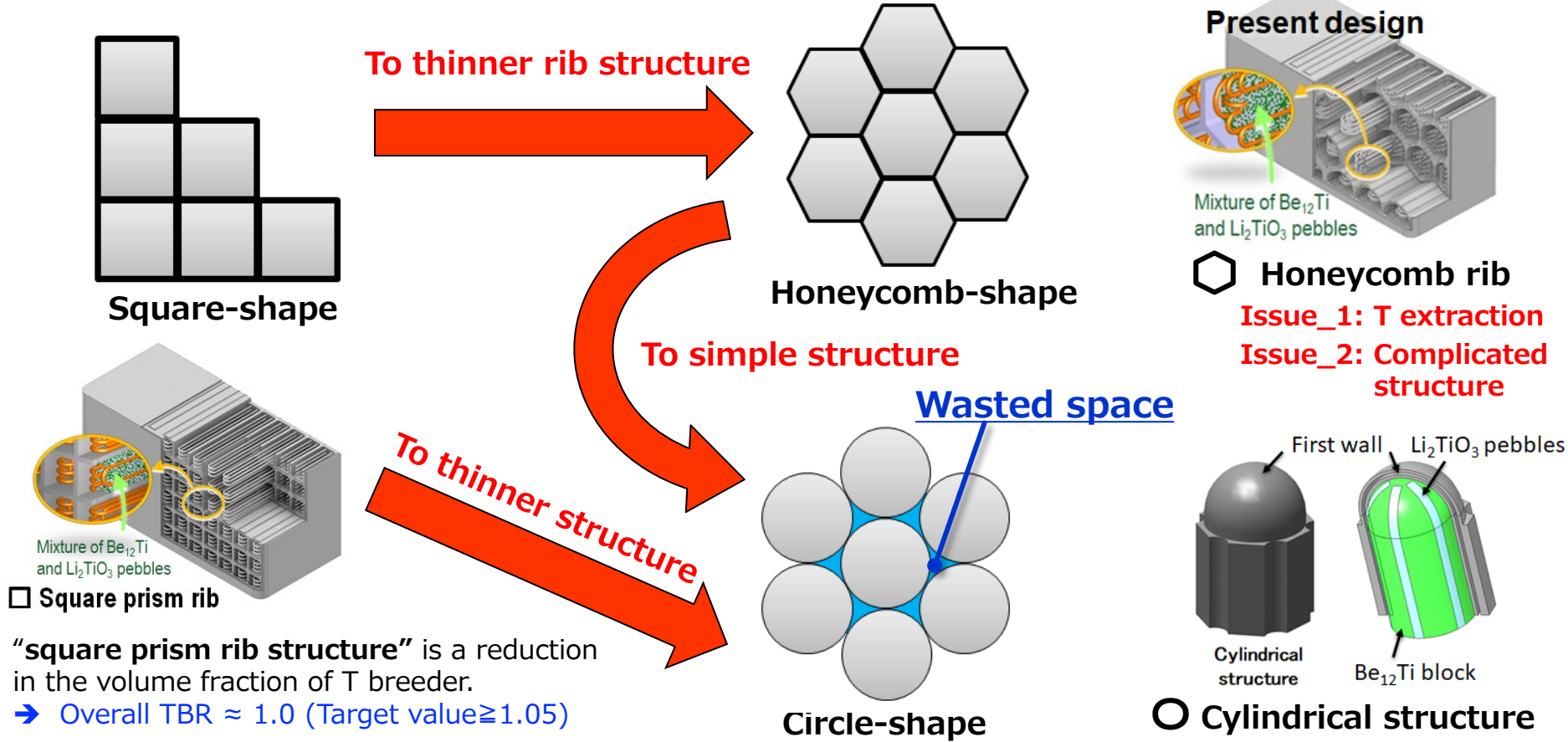
- ✓ **Issue_1: Evaluation of the power for DEMO plant consumption**
- ✓ **Issue_2: Consistency between cooling system and T concentration control**

3. Safety

→ An accident sequences and mitigation systems are being sorted out.

- ✓ **Issue_1: Identification of an accident sequences**

A conceptual design of breeding blanket with pressure tightness against in-box LOCA has been carried out for safety of the JA DEMO.



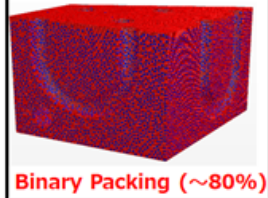
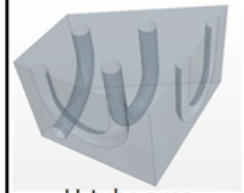
- ① T extraction is confirmed by CFD analysis with “**honeycomb-shape**”
- ② Simple concept of “**cylindrical structure**” is designed to meet the target TBR in the condition of the pressure tightness.

- Target of TBR (≥ 1.05) was achievable with a honeycomb-rib
- For the achievement of TBR target, P.F. to 80% with B.P. is necessary.
- **Issue:** Amount of tritium retained in the breeding area may increase, due to the increase in pressure drop as a result of binary packing.
 - The flow of He-purge gas was analyzed to confirm tritium retention

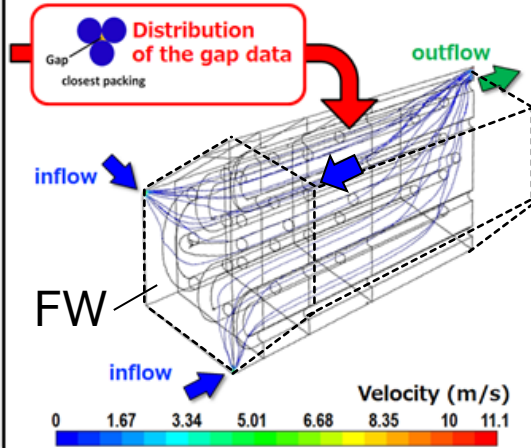
Analysis method

1. Gap distribution is evaluated by DEM.
2. The flow analysis is performed in the distribution of binary packing area which is modelled as a porous body.

① DEM analysis

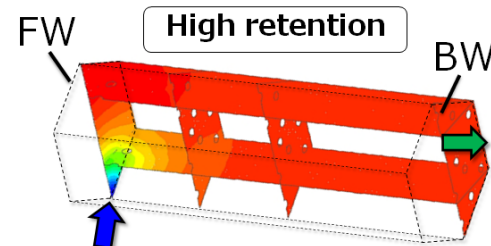


② CFD analysis

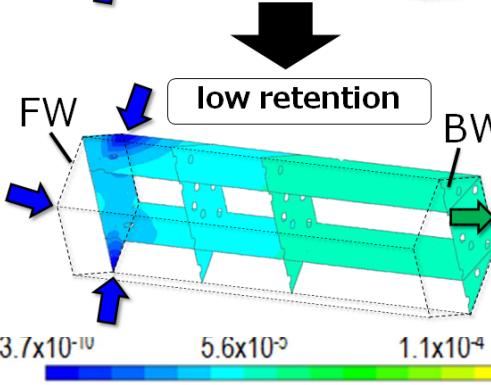


Analysis results

- ➡ Inflow of purge gas line
- ➡ Outflow of purge gas line



- ← Inflow of purge gas: 1 line
- ✓ Velocity : 5 m/s
- ✓ Pressure drop: 12.8 kPa
- ✓ T partial pressure: 17.2 Pa



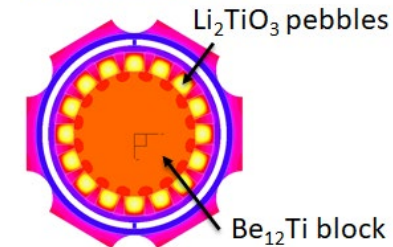
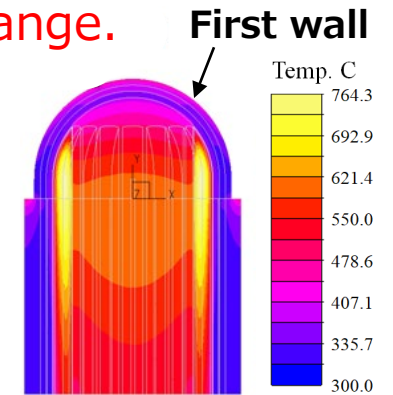
- ← Inflow of purge gas: 3 line
- ✓ Velocity : 5 m/s
- ✓ Pressure drop: 16.0 kPa
- ✓ T partial pressure: 5.7 Pa

3 inflow points of He-purge gas are arranged near the FW
 ➔ Little retention of tritium in the area was found.

A simplified BB structure was proposed with a cylindrical structure .

→ Characteristics of cylindrical concepts with Beryllide(Be_{12}Ti) block.

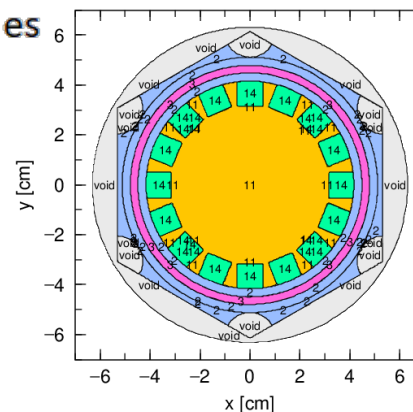
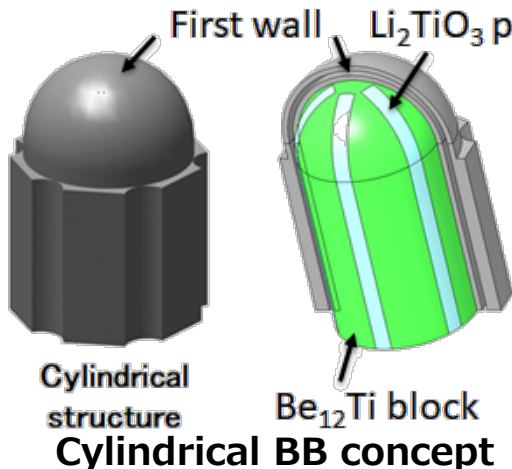
- ✓ Be_{12}Ti has little swelling compared to Be. → Be_{12}Ti can be used as blocks.
- Using blocks with a higher thermal conductivity than pebbles eliminates cooling piping inside the module. (2 to 45 W/m·K)
 - ✓ Allowable temp. of the materials is confirmed on the temp. distribution.
 - ✓ All materials were within the allowable temperature range.
- ✓ The design is embodied with keeping the highest percentage of TBR values (Li_2TiO_3 pebbles = 25%).
Dents around the Be_{12}Ti block are designed to have the Li_2TiO_3 ratio of 25%
- ✓ Target of overall TBR (>1.05) is achievable.



Allowable temp. of material

- ✓ $\text{Be}_{12}\text{Ti} \leq 900^\circ\text{C}$
- ✓ $\text{Li}_2\text{TiO}_3 \leq 900^\circ\text{C}$
- ✓ F82H $\leq 550^\circ\text{C}$

Temp. distribution of BB



Calculation model

- Be_{12}Ti block
- Li_2TiO_3 pebbles
- F82H
- coolant

Structure shape

- ✓ Casing (Out/In) : 102.4 / 83.2 mm
- ✓ Number of cut: 16
- ✓ Center direction: 10mm
- ✓ Width : 10.5mm

● Primary heat transfer system

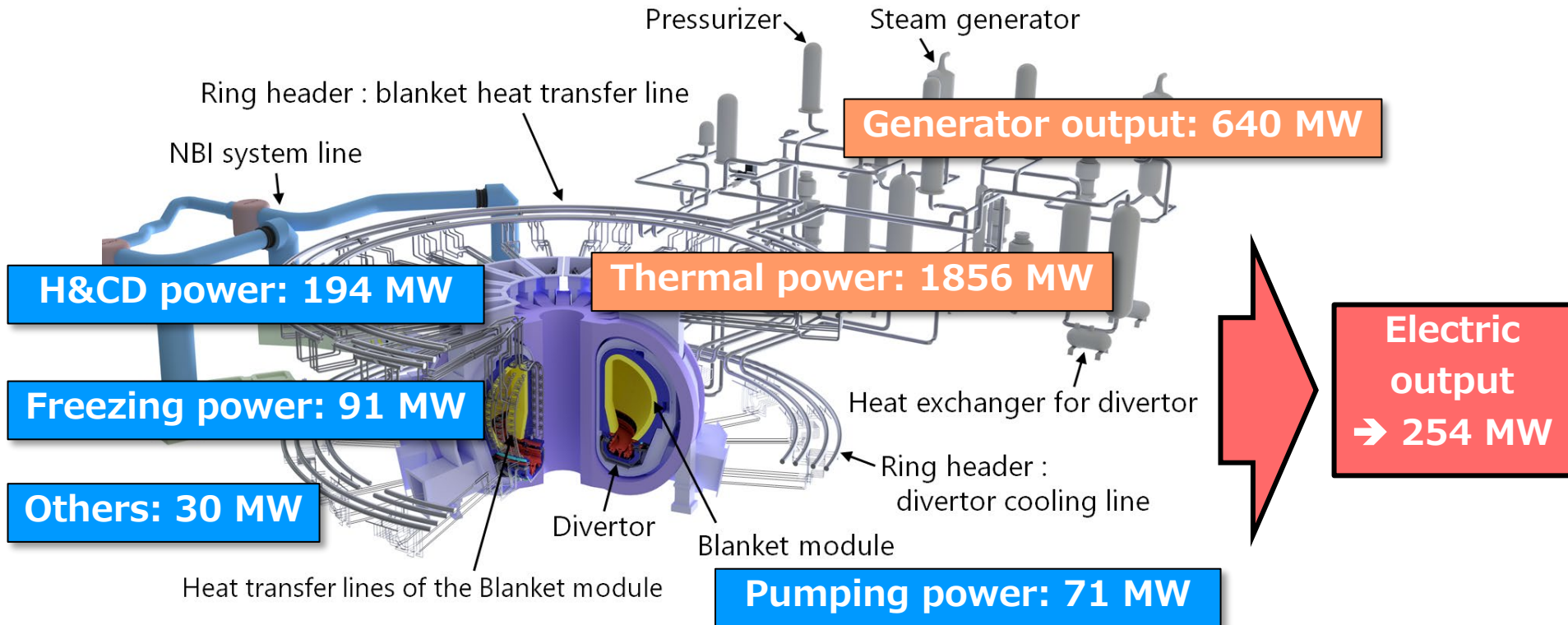
- ✓ PWR coolant water condition
→ 15.5MPa, 290~325°C

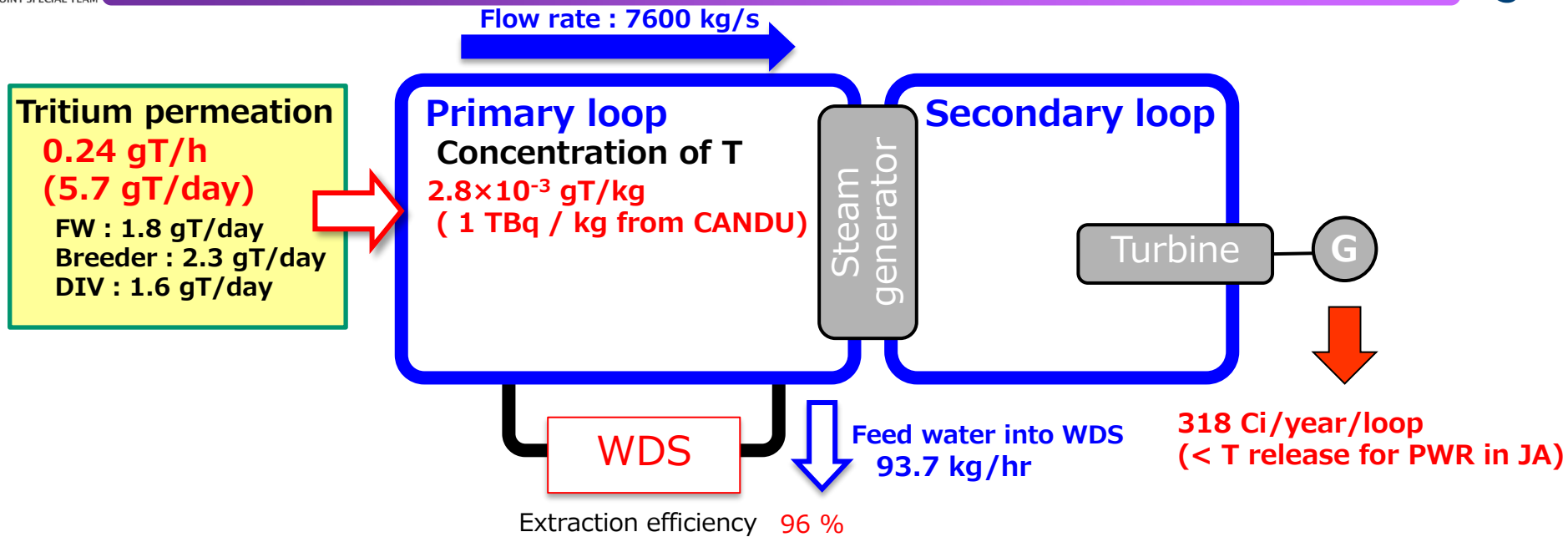
● Turbine system

- ✓ Thermal efficiency : 34.4%
- ✓ Gross power generation : 640MW

Breakdown of power balance

Fusion power	1500 MW
Thermal power	1865 MW
Generator output	640 MW
Power consumption	386 MW
Electric output	254 MW





Tritium impact in the primary coolant line

- T concentration at 1TBq/l was managed to apply the existing WDS for CANDU
 - T permeation was estimated to be as low as 5.7 gT/day at most. [Ref. 1]
 - T permeation reduction factor was estimated to be 2077 from CANDU[Ref. 2]
 - T permeation through a SG to the turbine system evaluated at 318 Ci/y/loop
- This value is less than restricted amount of T release for a PWR in JA[Ref.3]

[Ref1] K.Katayama et al., Fusion science tech.71(2017)261

[Ref2] S. Tosti et al., Fusion Engin. Des. 43 (1998) 29–35

[Ref3] R. Hiwatari et al., Fusion Eng. Des. 143 (2019) 259-266

Previous safety study focus on the “bounding sequences”

→ Lessons learned from “bounding sequences”

- Even for extremely hypothetical accidents, environmental release of tritium will be within a dose for evacuation-free. [Ref.]
[Ref.] Nakamura, et al., IEEE Trans. Plasma Sci. 44, 1689 (2016)
- However, in-vessel LOCA due to a large scale break of cooling pipe could result in a failure of VV (primary confinement boundary).

Identification of an accident sequences and mitigation systems

→ Mechanisms and countermeasures against threats are sorted out.

Threats **Loss of soundness of VV**

Mechanisms

Overpressure in VV by coolant

→ In-VV LOCA

Overpressure in VV due to decay heat

→ After the in/ex-VV LOCA, LOOP...

Overpressure in VV due to H explosion

→ Air intrusion after In-VV LOCA

Countermeasures

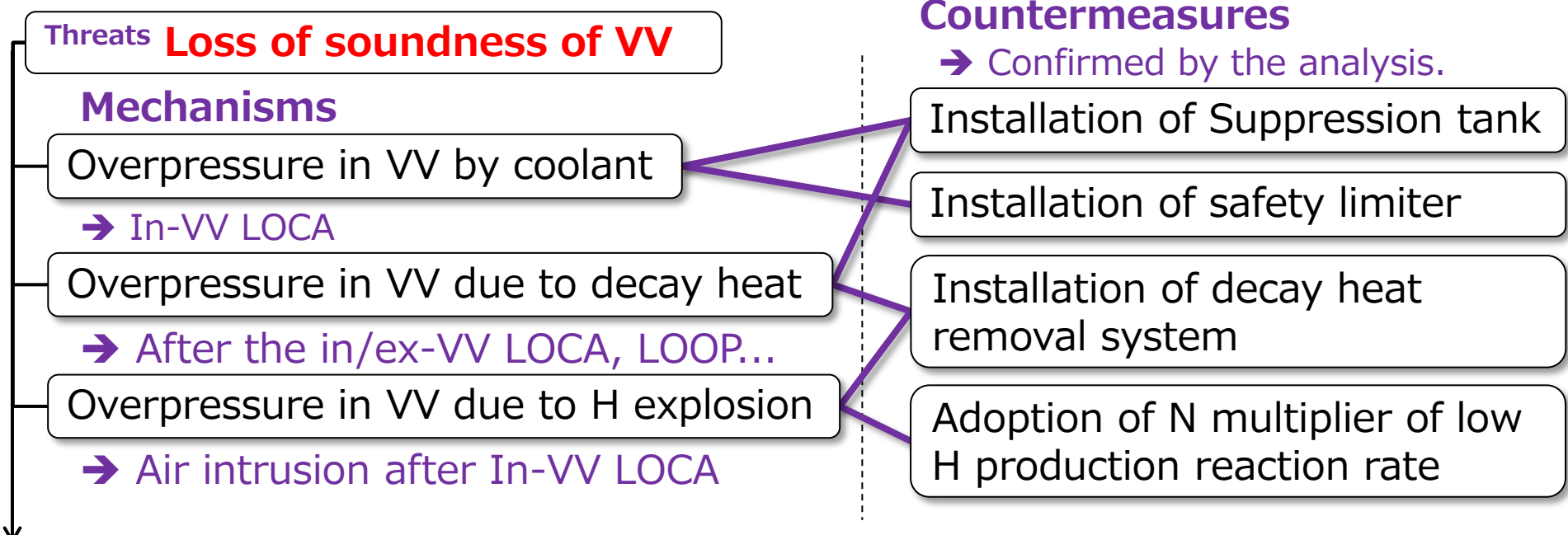
→ Confirmed by the analysis.

Installation of Suppression tank

Installation of safety limiter

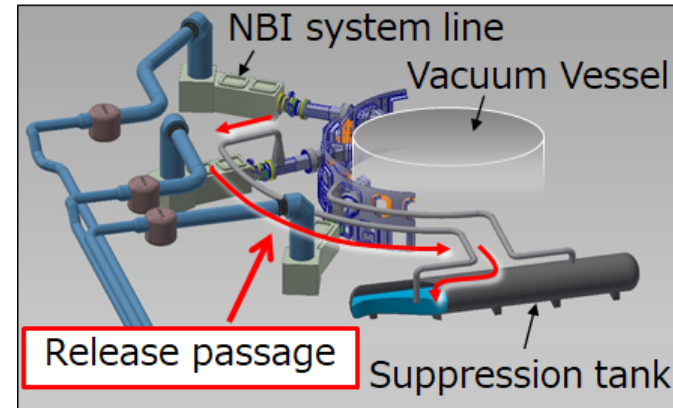
Installation of decay heat removal system

Adoption of N multiplier of low H production reaction rate



✓ Installation of suppression tank on the VV

- Suppression tank is connected via the NBI port.
- Max. pressure at VV could be reduced to 15%.
 - ✓ Tank of volume (water): 5,600 m³ (2,800 m³)
 - ✓ Rupture disk: 0.2 MPa (Differential pressure)
 - ✓ Cross section of the NB port: 4.2 m²



✓ A check valves are arranged to suppress

- Maximum pressure of VV is smaller than design pressure when the check valve arranges in the cooling system of the divertor baffle.
 - ✓ Break area of the div. baffle is assumed to the all of the cooling pipe.
- Since the blanket has more amount of the water coolant than other IVCs, It can hardly contribute to suppress the max. pressure by check valve.
 - ✓ Soundness of BB first wall is protected ← the safety limiter is sacrificed.

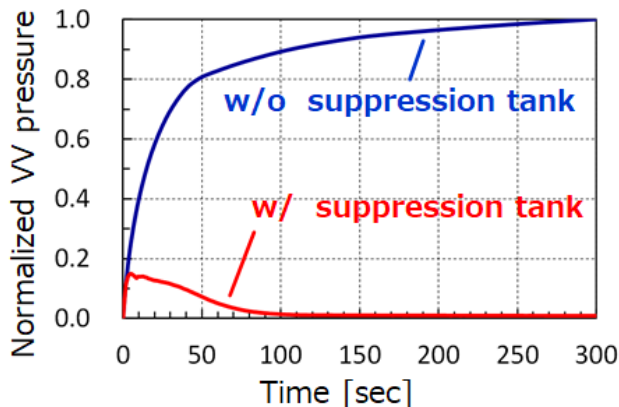


Fig. Effect of a suppression tank on VV

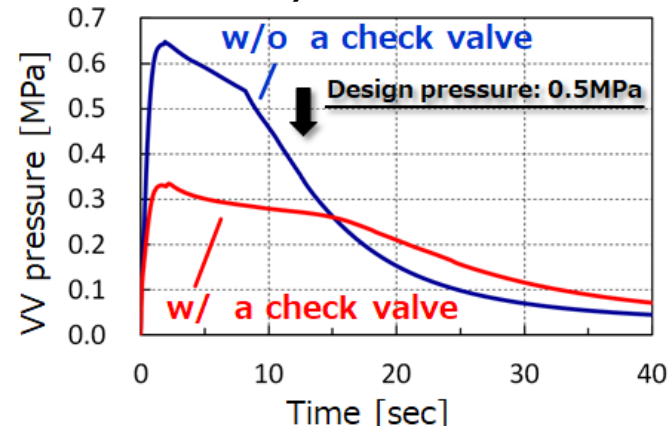


Fig. Effect of a check valve in cooling system for div. baffle

- **In order to increase the feasibility of JA DEMO concept, studies on the following engineering issues were performed.**

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- ➔ In the “honeycomb-shape”, little retention of tritium was found by the flow analysis of the purge gas.
- ➔ Simple concept of cylindrical structure are designed to meet the target TBR in the condition of the pressure tightness.

2. An outlook of the steady and stable power generation beyond several 100 MW

- ➔ The total power consumption was found to be 386 MW, and the electric output was evaluated to be 254 MWe
- ➔ Consistency between cooling system and T concentration control was confirmed for safety management.

3. Safety

- ➔ An accident sequences and mitigation systems are being sorted out.
- ➔ A mitigation systems of the countermeasures were confirmed on the safety analysis
- **The proposed concept as JA DEMO is the foundation for Japan’s DEMO that can be envisioned in the next stage of ITER.**