

#### **Experimental studies of the nitrogen concentration required for divertor detachment in ASDEX Upgrade**

# S. Henderson<sup>1</sup>, M. Bernert<sup>2</sup>, D. Brida<sup>2</sup>, M. Cavedon<sup>2</sup>, P. David<sup>2</sup>, R. Dux<sup>2</sup>, A. Kallenbach<sup>2</sup>, F. Reimold<sup>3</sup> and the EUROfusion MST1 and ASDEX Upgrade teams

<sup>1</sup> UKAEA, CCFE, Culham Science Centre, Abingdon, OX14 3DB, Oxon, UK <sup>2</sup> Max Plank Institute for Plasma Physics, Garching, Germany <sup>3</sup> Max Plank Institute for Plasma Physics, Greifswald, Germany









This work has been carried out within the framework of the EUROfusion Consortium and has received funding from the Euratom research and training programme 2014-2018 and 2019-2020 under grant agreement No 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission.

#### This talk will describe how we obtain the following scaling law for detachment from experimental measurements, how it compares to a simple model of impurity cooling, and what we should consider for future tokamaks

$$C_N = 5.92 P_{sep}^{0.999 \pm 0.35} I_p^{1.04 \pm 0.66} n_{e,sep}^{-2.63 \pm 0.63} \times (1 + \kappa^2)^{-1} a^{-3}$$







#### Introduction and motivation



Recent derivations, based on Lengyel's work<sup>1</sup>, have attempted to predict the concentration of impurity required to reach detached conditions in future tokamaks

<sup>2</sup> Goldston  $c_Z \propto \frac{P_{sep}}{B_p(1+\kappa^2)^{1.5} f_{GW,sep}^2}$ <sup>3</sup> Reinke  $c_Z \propto B_T^{0.88} R^{1.33}$ <sup>4</sup> Kallenbach  $c_Z \propto \frac{P_{sep}/R}{p_{div}\lambda_{int}R^{rz}}$ 

focus on upstream density focus on machine size scaling focus on momentum and energy loss

However, direct measurements of the impurity concentration in the divertor are difficult to make and therefore currently there are no experimental studies to validate these scaling laws to guide expectations for ITER and DEMO

- <sup>2</sup> R J Goldston et al 2017 Plasma Phys. Control. Fusion **59** 055015
- <sup>3</sup> M.L. Reinke 2017 Nucl. Fusion **57** 034004
- <sup>4</sup> A Kallenbach et al 2016 Plasma Phys. Control. Fusion **58** 045013

<sup>&</sup>lt;sup>1</sup>Lengyel L L 1981 Analysis of radiating plasma boundary layers IPP Report1/191

#### Introduction and motivation



Recent derivations, based on Lengyel's work<sup>1</sup>, have attempted to predict the concentration of impurity required to reach detached conditions in future tokamaks



This talk focuses on a new spectroscopic technique for measuring the divertor nitrogen concentration

### Nitrogen spectroscopy in the divertor



#### The nitrogen concentration in the divertor is calculated using N II line emission



N II emits in a narrow, localised band in the PFR which spreads into the SOL as the divertor temperature cools



#### Impact of plasma transport





If transport is significant, then the N II emission could be shifted to hotter temperatures <sup>1</sup> and compromise the concentration measurement



Experimental line ratios typically indicate  $T_e=3-4 \text{ eV}$ suggesting **transport effects are negligible** for this particular emission region (e.g. N II PFR)

<sup>1</sup> P G Carolan and V A Piotrowicz 1983 Plasma Phys. 25 1065

#### **Divertor detachment state**

# The extent of N II emission through a sightline, which is proportional to the nitrogen concentration, is also dependent on the divertor detachment state

In this analysis, the real-time estimate of the outer divertor temperature, derived from shunt measurements, is used as a proxy for describing the detachment state [1]



**Onset detachment Tdiv = 5-10 eV** 

Partial detachment Tdiv = 0-5 eV

#### Full detachment Tdiv < 0 eV

[1] A. Kallenbach *et al* 2015 *Nucl. Fusion* **55** 053026

### **Deriving the nitrogen concentration**





The intensity measured in the **highlighted sightline** is mostly immune to strike-point position and provides signal in detached conditions



The concentration for detachment is defined as the average between **3-5 eV** 

#### **Database studies**

The database requires N-seeded H-mode discharges with a ramp of divertor temperature in steady conditions (e.g. power, fuelling, stored energy)

Database spans the following parameters:

 $n_{e,core} = 7.00 - 10 \times 10^{19} m^{-3}$   $n_{e,sep} = 1.80 - 4 \times 10^{19} m^{-3}$   $P_{sep} = 1.50 - 5 MW$   $I_p = 0.83 - 1.2 MA$   $\kappa = 1.68 - 1.75$  a = 0.49 - 0.51

Reasonable agreement with scaling law [1]

$$n_{e,sep} = 2.65 p_{div}^{0.32}$$

[1] A Kallenbach et al 2018 Plasma Phys. Control. Fusion 60 045006



#### **Database studies**



The database requires N-seeded H-mode discharges with a ramp of divertor temperature in steady conditions (e.g. power, fuelling, stored energy)

Database spans the following parameters:

 $n_{e,core} = 7.00 - 10 \times 10^{19} m^{-3}$   $n_{e,sep} = 1.80 - 4 \times 10^{19} m^{-3}$   $P_{sep} = 1.50 - 5 MW$   $I_p = 0.83 - 1.2 MA$   $\kappa = 1.68 - 1.75$  a = 0.49 - 0.51

Reasonable agreement with scaling law [1]

$$n_{e,sep} = 2.65 p_{div}^{0.32}$$





### **Comparison with valve flux estimation**



In steady state conditions, the gas valve fluxes can provide an estimate of  $c_N$  if the wall sticking/release is negligible and the D and N pumping speeds are equal

The ratio of valve fluxes is defined as:

 $c_N = \frac{\Gamma_N}{\Gamma_D + \Gamma_N} [1]$ 

If D & N are pumped equally then it is useful to compare  $c_N$  from flux ratios and spectroscopy in the database of shots

Agreement with spectroscopy is mostly dependent on the intrinsic nitrogen content before seeding which is linked to the wall loading of vessel surfaces



[1] A Kallenbach et al 2016 Plasma Phys. Control. Fusion **58** 045013

### **Comparison with valve flux estimation**



In steady state conditions, the gas valve fluxes can provide an estimate of  $c_N$  if the wall sticking/release is negligible and the D and N pumping speeds are equal

The ratio of valve fluxes is defined as:

 $c_N = \frac{\Gamma_N}{\Gamma_D + \Gamma_N} [1]$ 

If D & N are pumped equally then it is useful to compare  $c_N$  from flux ratios and spectroscopy in the database of shots

Including shots with changing input power shows agreement of the two measurements at higher levels of intrinsic nitrogen



[1] A Kallenbach et al 2016 Plasma Phys. Control. Fusion 58 045013

### Scaling with separatrix density



Goldston's scaling law predicts that the impurity concentration should scale inversely with the square of the normalised separatrix density

By selecting points from the database at reasonably constant  $P_{sep}$ , the trend with normalised separatrix density is assessed

The results suggest that there may be a moderately stronger dependence on the normalised separatrix density than suggested by Goldston's scaling law

A stronger dependence on n<sub>e,sep</sub> is also found from a database of ITER baseline SOLPS simulations with Ne seeding [1]



[1] Pitts et al 2019 Nucl. Mater. Energy **20** 100696

#### **Comparison with scaling laws**



Goldston's scaling law is proportional to  $c_Z \propto \frac{P_{sep}}{B_p(1+\kappa^2)^{1.5}f_{GW,sep}^2}$ 

The absolute magnitude of the scaling law is found by normalising the result to the conditions of a simulation described by Kallenbach et al (2016)

Despite the offset in the absolute experimental concentration, the trends with  $P_{sep}$  and  $f_{GW,sep}$  are reasonably well reproduced by Goldston's scaling law



#### **Regression analysis**



A regression analysis has been performed on P<sub>sep</sub>, n<sub>e,sep</sub> and I<sub>p</sub> to compare against Goldston's scaling law

Re-writing Goldston's scaling in terms of  $I_p$  i.e.  $\langle B_p \rangle \propto \frac{l_p}{a(1+\kappa^2)^{0.5}}$  and  $n_{GW} \propto \frac{l_p}{a^2}$ y = 0.16 + 1.01x $R^2 = 0.97$ Spectroscopy c<sub>N</sub> [%] gives  $c_Z \propto \frac{P_{sep}I_p}{n_{e.sep}^2(1+\kappa^2)a^3}$ regression of  $P_{sep}$  [MW],  $n_{e,sep}$  [10<sup>19</sup> $m^{-3}$ ] and  $I_p$  [MA] gives  $C_N = 5.92 P_{sep}^{0.999 \pm 0.35} I_p^{1.04 \pm 0.66} n_{e,sep}^{-2.63 \pm 0.63} \times (1 + \kappa^2)^{-1} a^{-3}$ 0 2 6 8 10 12 14 Δ Regression  $c_N$  [%]

#### Summary and where to next



#### **Main conclusion**

Future fusion reactors depend on divertor detachment to limit the heat flux to the plasma facing components. This work provides experimental evidence from one device that the impurity concentration needed to reach detachment scales dominantly with  $P_{sep}I_p n_{e,sep}^{-2.6}$ ; a result in reasonable agreement with a simple model for impurity cooling

#### Future experiments to address key points for DEMO

- comparison of measurements from another device would assess machine size scaling
- what role does divertor geometry play, e.g. enrichment/compression?
- in different geometries, do these trends still hold?
- the atomic data and lines exist to perform this analysis on Ne



(f) ROV014

(g) ROV012

(h) ROV010

(i) ROV008

20

30

#### The extent of N II emission through a sightline is dependent on both the divertor detachment state and the strike-point position





#### The extent of N II emission through a sightline is dependent on both the divertor detachment state and the strike-point position





#### The extent of N II emission through a sightline is dependent on both the divertor detachment state and the strike-point position





Nitrogen line ratio



