

# Using variations in divertor magnetic topology and geometry to optimize divertor detachment

- ✧ Need for more and quicker divertor design guidance/analysis
- ✧ Using ‘experiments’ in SOLPS to quantify the effect of divertor design characteristics on **control of divertor detachment onset**
  - ✧ Strike point angle
  - ✧ Baffling
  - ✧ Total flux expansion
- ✧ Implications for improving the design process

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Most of the thoughts presented are based on the paper – A. Fil et al., ‘Separating the roles of magnetic topology and neutral trapping in modifying the detachment threshold in TCV’, submitted to Plasma Phys. & Contr. Fusion.

1. The core plasma conditions are set based on reactor goals
  - (Q, B, current, aspect ratio,..)
  - Magnetic flux equilibrium developed
2. Space allocated to the divertor based on the coil size
3. Run SOL/divertor fluid codes to determine whether the divertor performs 'adequately'
  - Close the loop on the reactor design both with engineering and core plasma performance

# Reactor divertor design process

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  - (Q, B, current, aspect ratio,..)
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Bottleneck for optimization

# Are there ways to enhance the feedback between divertor design, engineering and core characteristics?

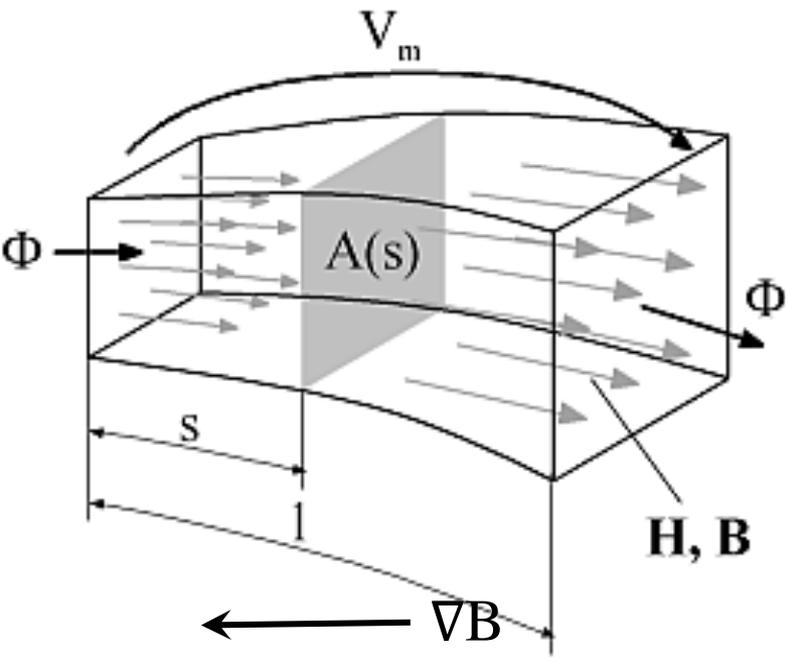
- Are there more ways to enhance the feedback between divertor design and core characteristics?
  - Can simpler (than SOLPS) calculations be properly used?
  - Can one more quickly determine the core operational space compatible with detachment?
  - **Can we be quantitative about how those divertor characteristics control detachment access and its characteristics?**
    - We have addressed this question through a SOLPS study of TCV detachment threshold in upstream density,  $n_{u,d}$

## Reminder – what is total flux expansion

- Increase target strike point radius,  $R_t$ 
  - $|B_t|$ , drops. Area of flux tube increases
  - The heat flux parallel to  $B$ ,  $q_{||,t}$  drops

$$B \cdot A_{\text{fluxtube}} = \text{const}$$

**Flux tube area increases as total B drops**



$$q_{||} \cdot A_{\text{fluxtube}} = \text{const}$$

$$\Rightarrow q_{||} \propto |B| \sim \frac{1}{R}$$

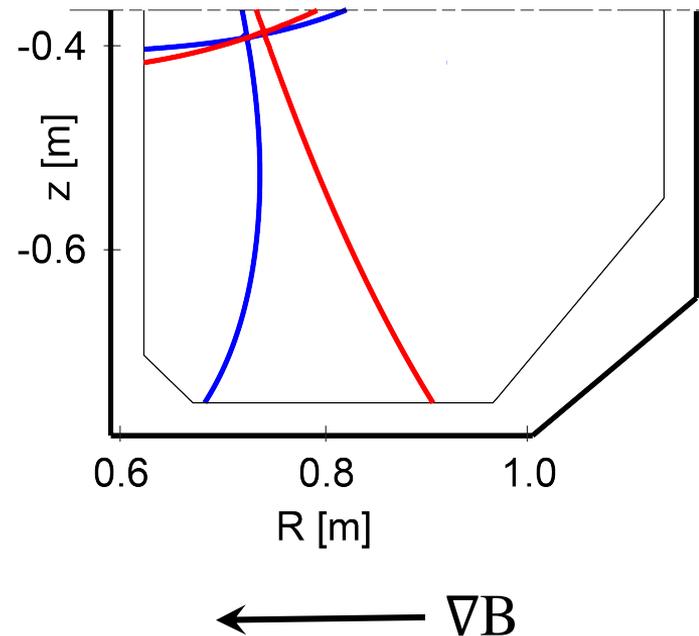
**Not a new effect! Already in SOL/Div codes**

# Simple effect of total flux expansion predicted to lower the detachment threshold

- Increase target strike point radius,  $R_t$ 
  - $|B_t|$ , drops. Area of flux tube increases
  - The heat flux parallel to B,  $q_{||,t}$ , drops
  - lowering the detachment threshold in upstream density,  $n_{u,d}$

$$n_{u,d} \propto \frac{1}{|B_x| / |B_{tar}|} \frac{P_{SOL}^{5/7}}{L^{2/7}} \sim \frac{R_x}{R_t} \frac{P_{SOL}^{5/7}}{L^{2/7}} *$$

Total flux expansion

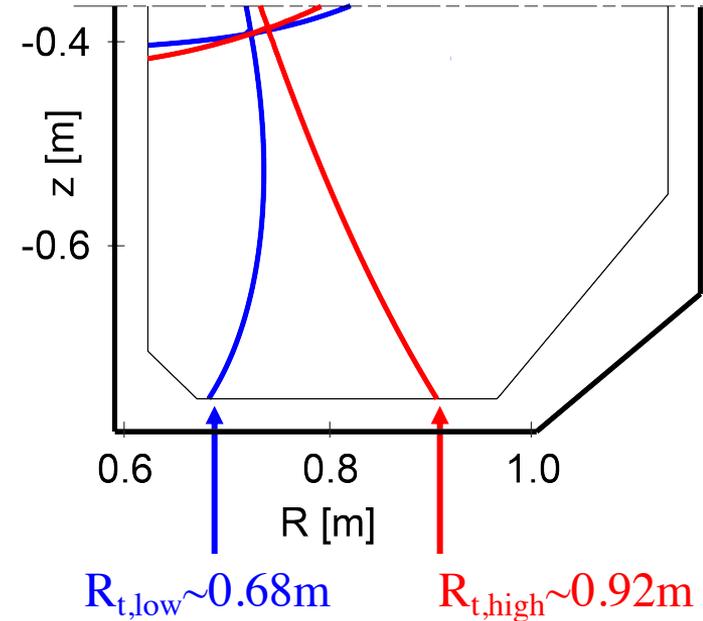


\*M. Kotschenreuther et al., Nucl. Fus. **50** (2010) 035003, TW Petrie et al, J. Nucl. Mat. **438**(2013) S166, B. Lipschultz et al., Nucl. Fus. **56** (2016) 056007, D. Moulton et al., PPCF 59 (2017) 065011

# Prediction of the effect of total flux expansion for TCV

- Predict the ratio of detachment thresholds for the low and high target radius,  $R_t$ :

$$D_{\text{predicted}} \equiv \frac{n_{u,d}^{R_{t,\text{high}}}}{n_{u,d}^{R_{t,\text{low}}}} \sim \frac{R_{t,\text{low}}}{R_{t,\text{high}}} = \frac{0.68}{0.92} = 0.76$$



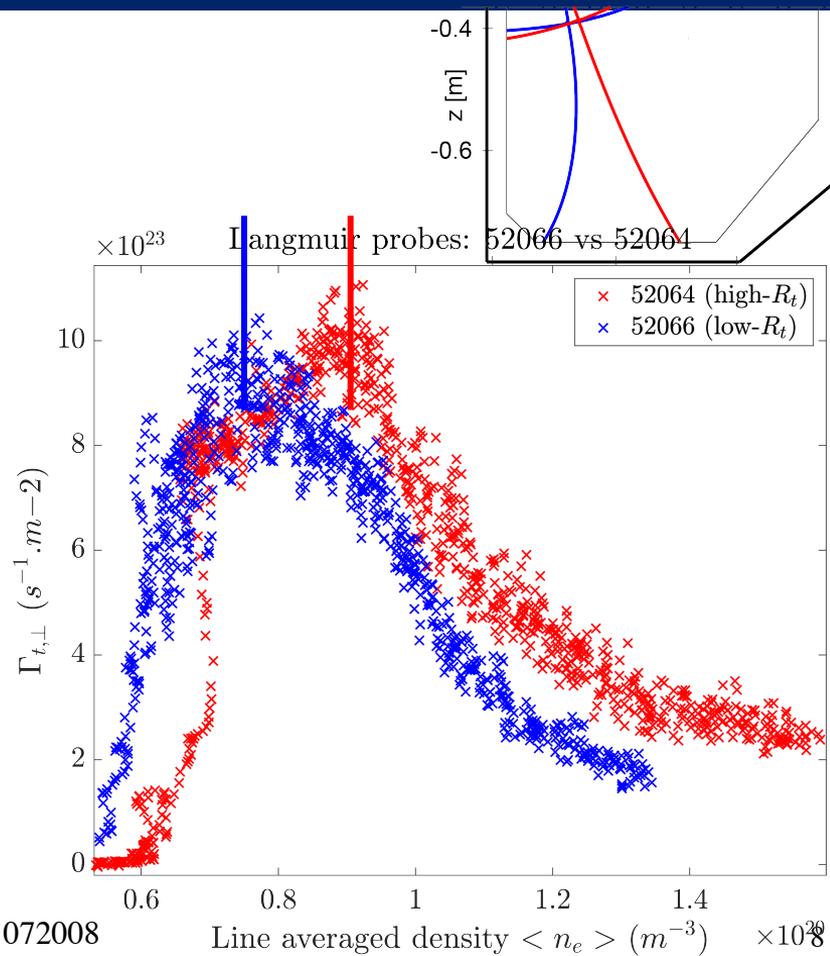
# Experiments contradict simple predictions for total flux expansion

- TCV experiments<sup>1</sup> studying just the upstream density detachment threshold,  $n_{u,d}$ , contradict the simple scaling.

$$D_{\text{predicted}} \equiv \frac{n_{u,d}^{R_{t,\text{high}}}}{n_{u,d}^{R_{t,\text{low}}}} \sim \frac{R_{t,\text{low}}}{R_{t,\text{high}}} = \frac{0.68}{0.92} = 0.76$$

$$D_{\text{measured}} \equiv \frac{\bar{n}_{e,d}^{R_{t,\text{high}}}}{\bar{n}_{e,d}^{R_{t,\text{high}}}} \sim 1.2^* \quad \leftarrow$$

\*Difficult to obtain  $n_{u,d}$



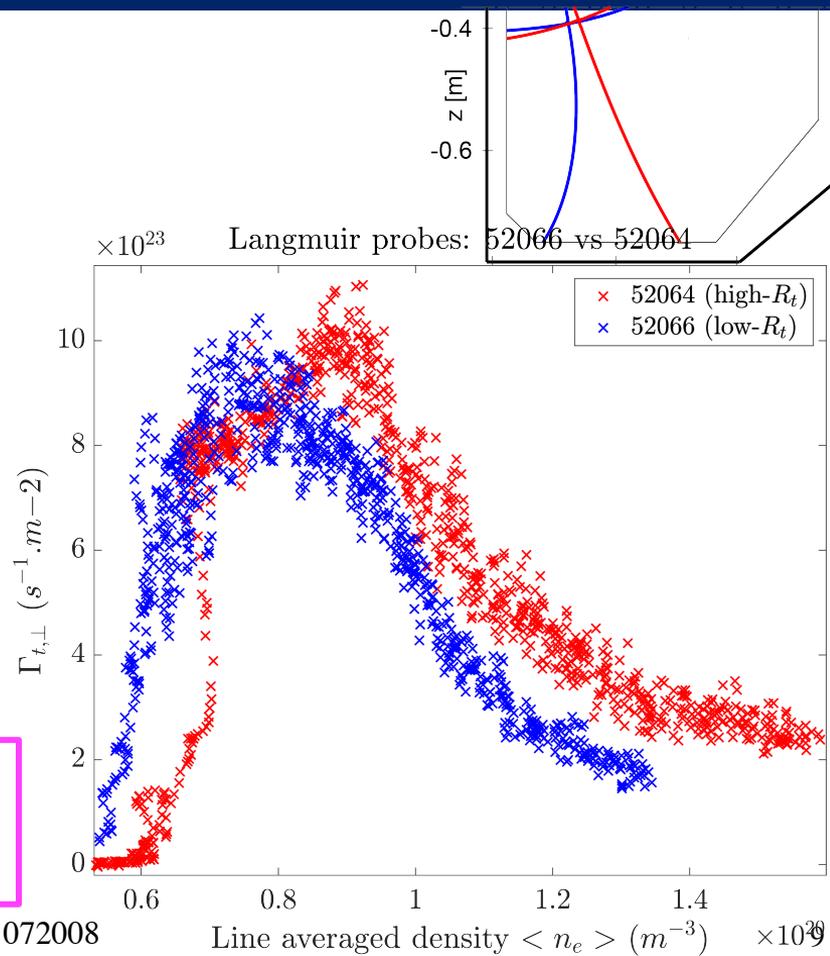
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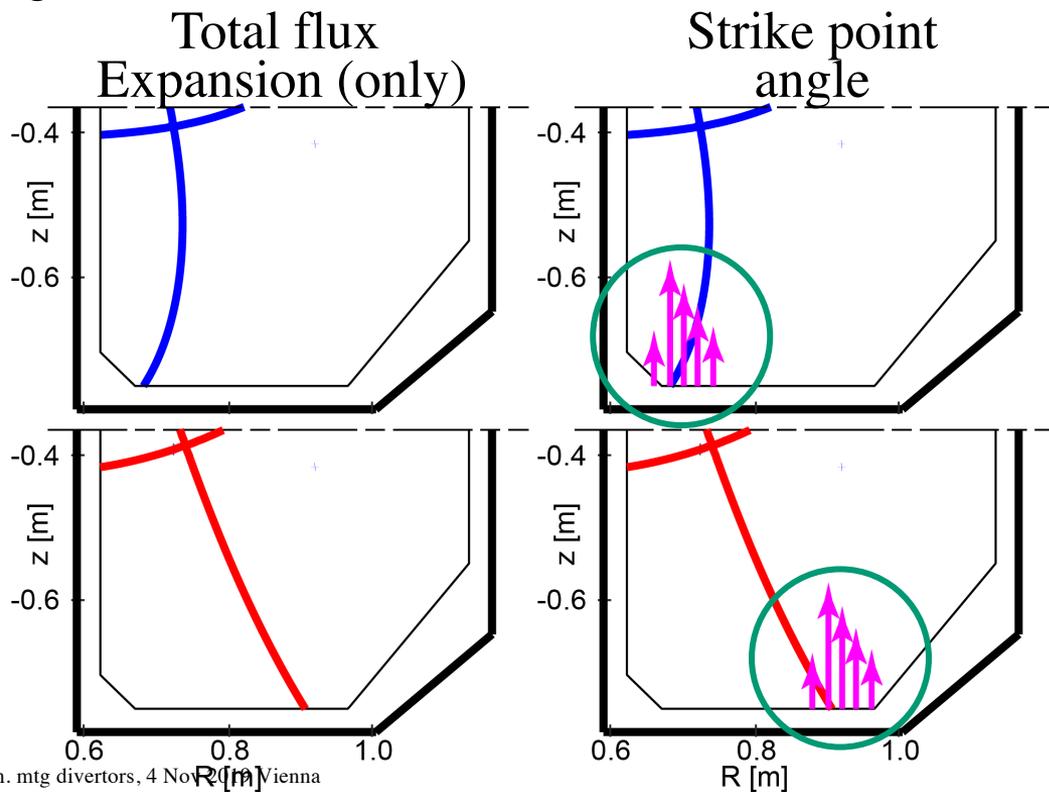
$$D_{\text{measured}} \equiv \frac{\bar{n}_{e,d}^{R_{t,\text{high}}}}{\bar{n}_{e,d}^{R_{t,\text{high}}}} \sim 1.2^*$$

- What leads to this difference between simple prediction and measurement?



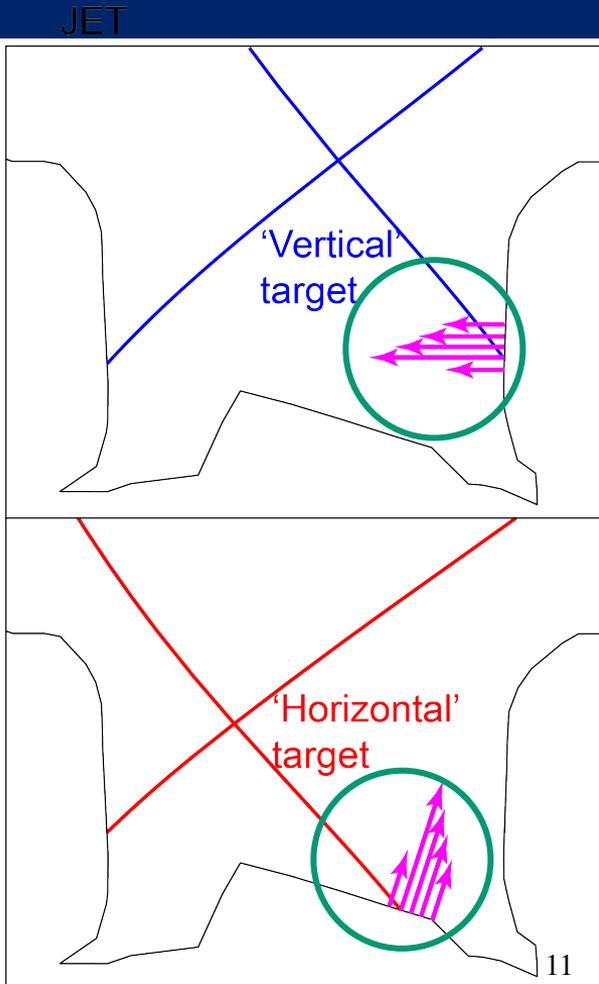
# Strike point angle is another important divertor characteristic and is different for low- and high- $R_t$ in TCV

- Recycled neutrals are launched towards different parts of the divertor plasma for low- and high- $R_t$



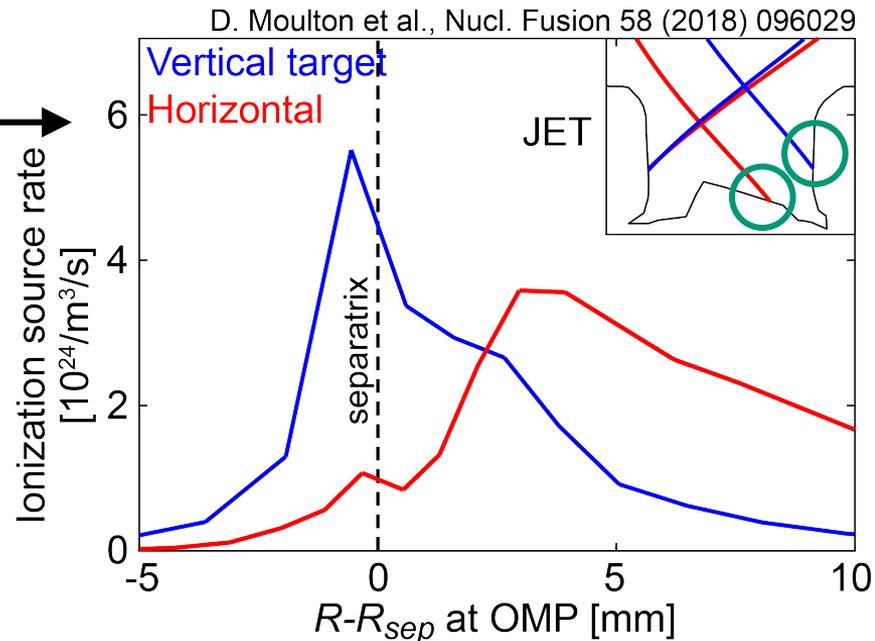
# Strike point angle to the surface affects the ionization profile

- JET is a good example of the effect of varying strike point angle
- Recycling neutrals ionize in different plasma regions for 'vertical target' and 'horizontal target'



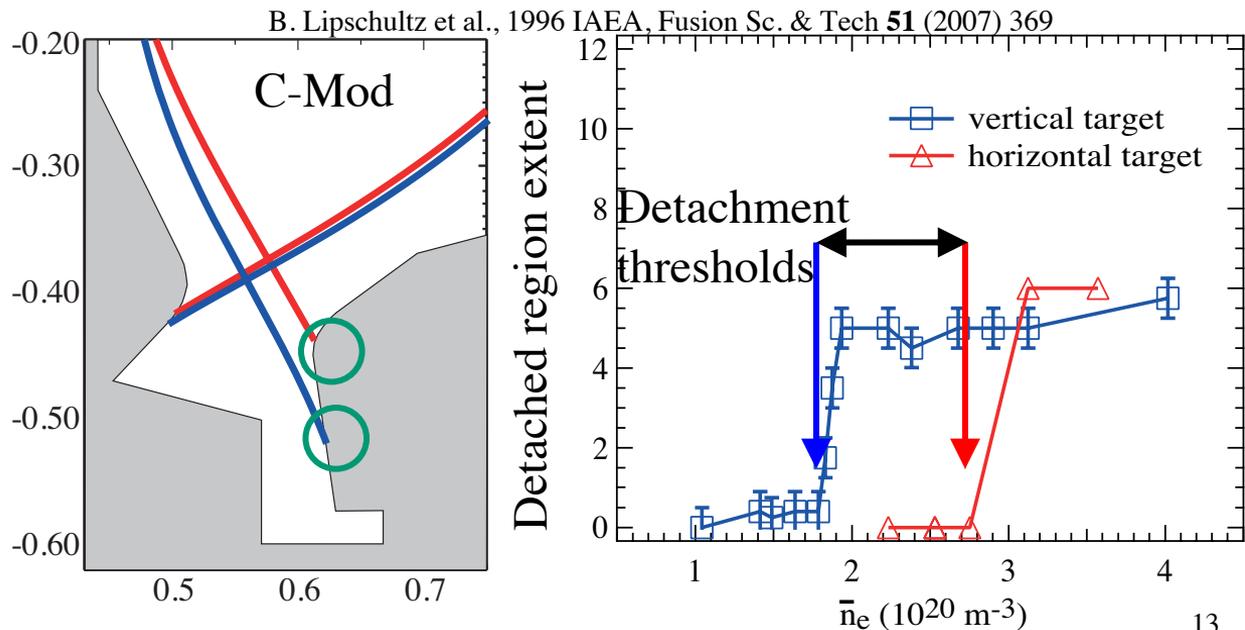
# Strike point angle to the surface affects the ionization profile

- EDGE2D-Eirene calculations demonstrate difference in ionization
  - ‘Vertical target’
    - ionization near separatrix
    - increase density; lower temperature
    - **lowers detachment threshold**
  - ‘horizontal target’
    - ionization farther from the separatrix



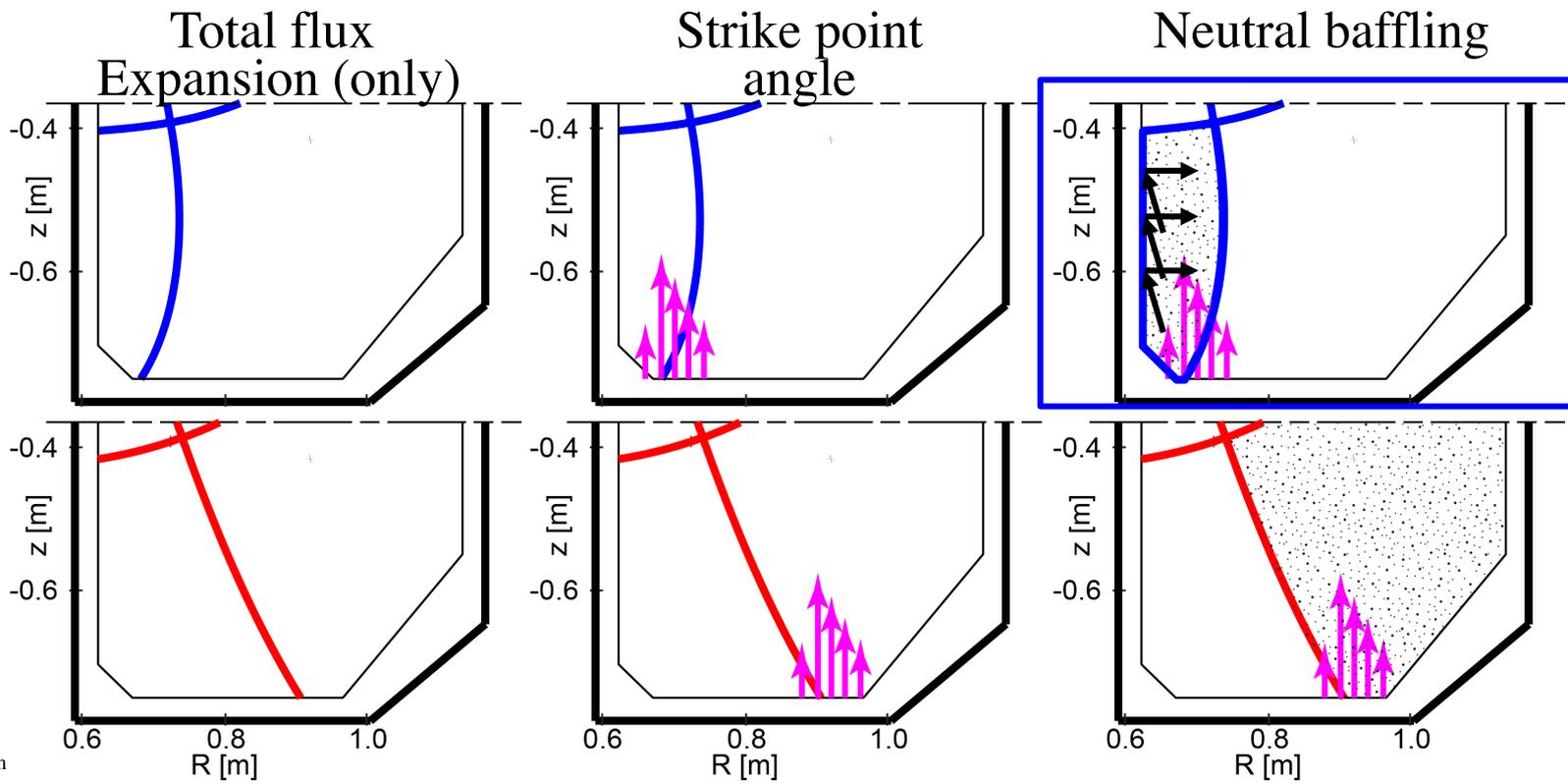
# The effect of the strike point angle on detachment was realized experimentally, early in divertor studies

- Experimental comparison:
  - vertical target ~40% lower detachment threshold,  $n_{ud}$
- Most tokamaks moved to the vertical target geometry in the early 2000s



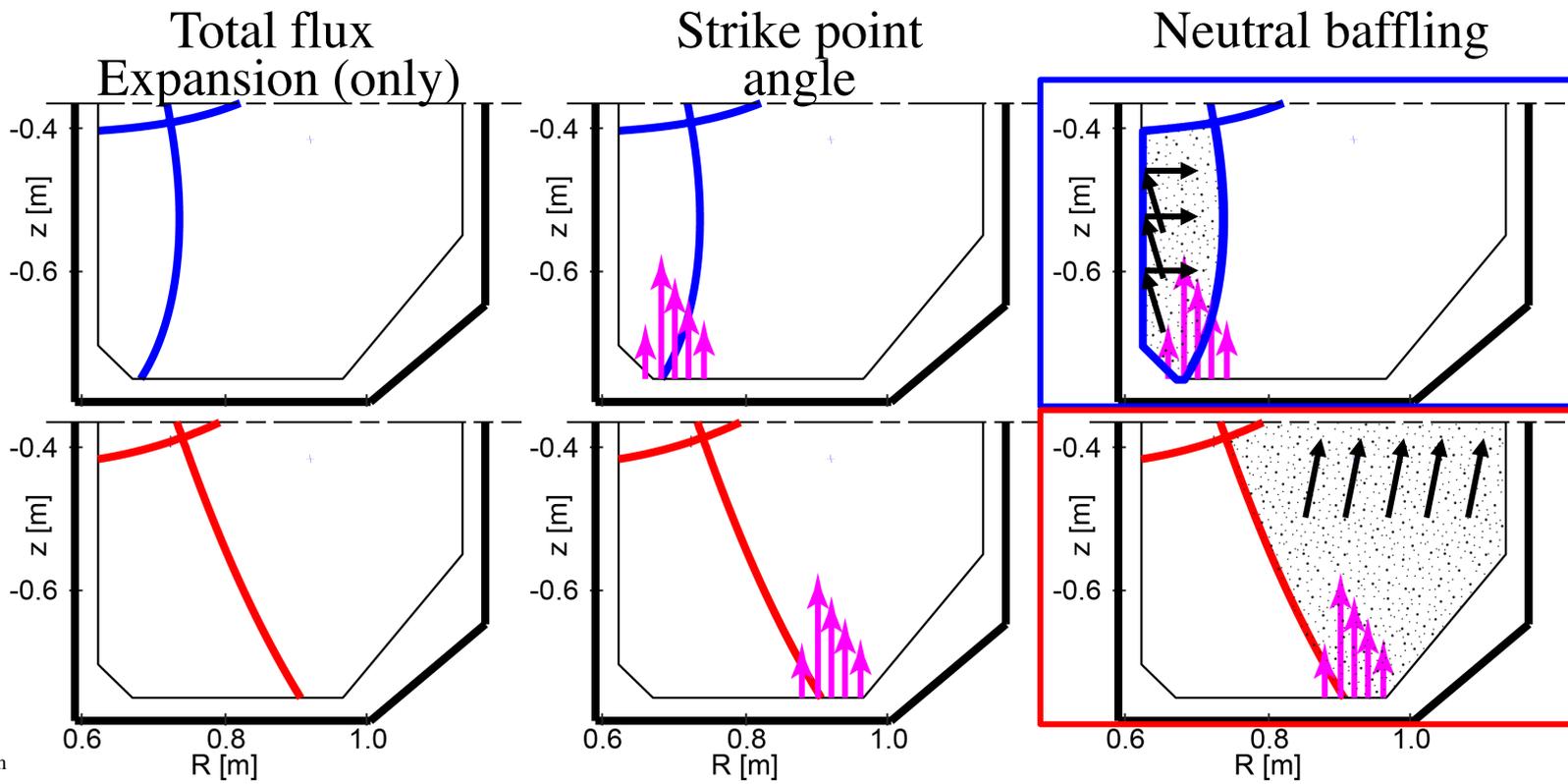
# Baffle geometry also has a strong role in determining the detachment threshold

- Low  $R_t$  divertor traps neutrals between inner wall, inner and outer separatrices



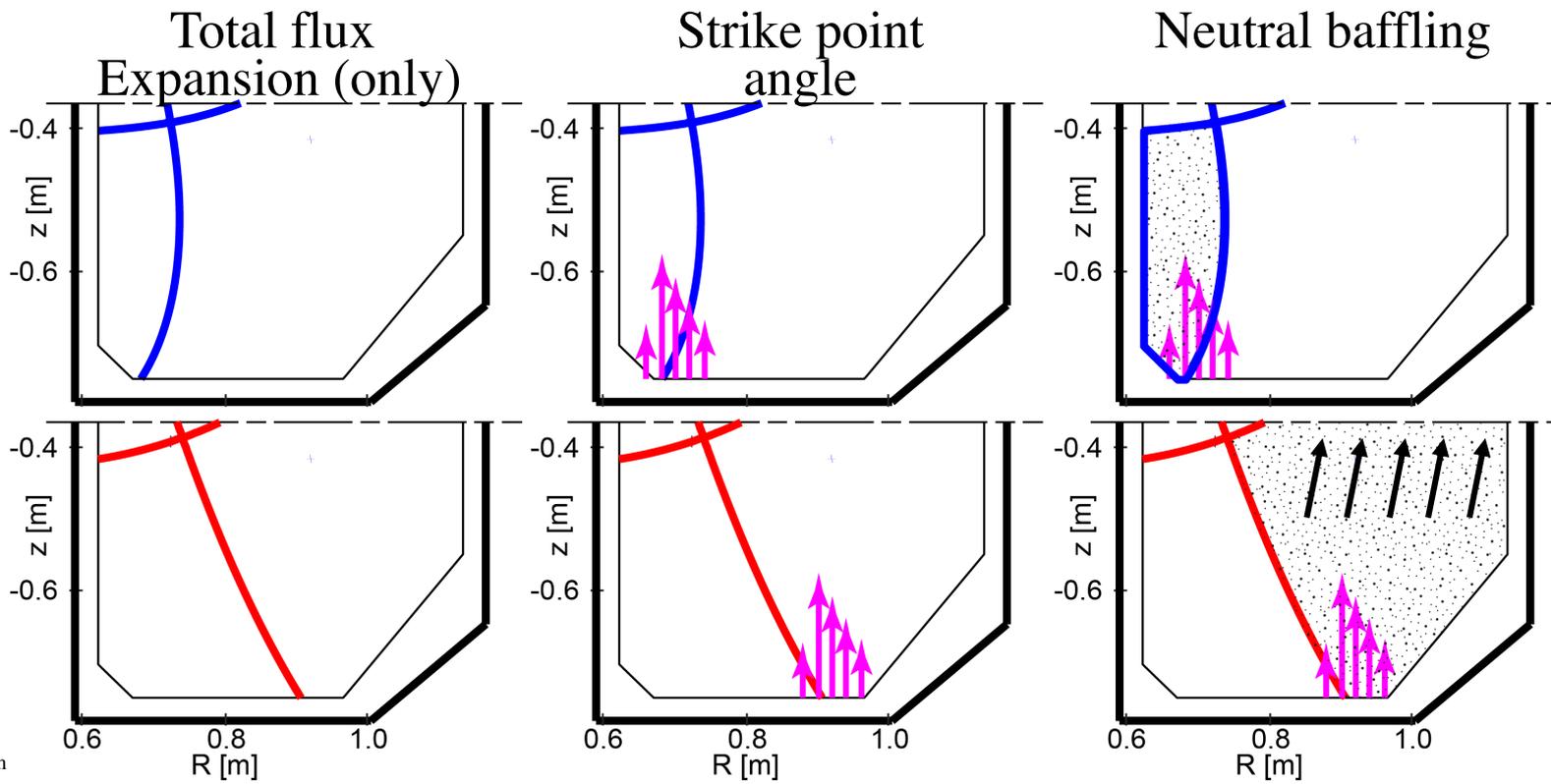
# Neutral trapping in the divertor favors low target R

- Low  $R_t$  divertor traps neutrals between inner wall, inner and outer separatrices
- Neutrals in the high  $R_t$  configuration **easily escape the divertor**



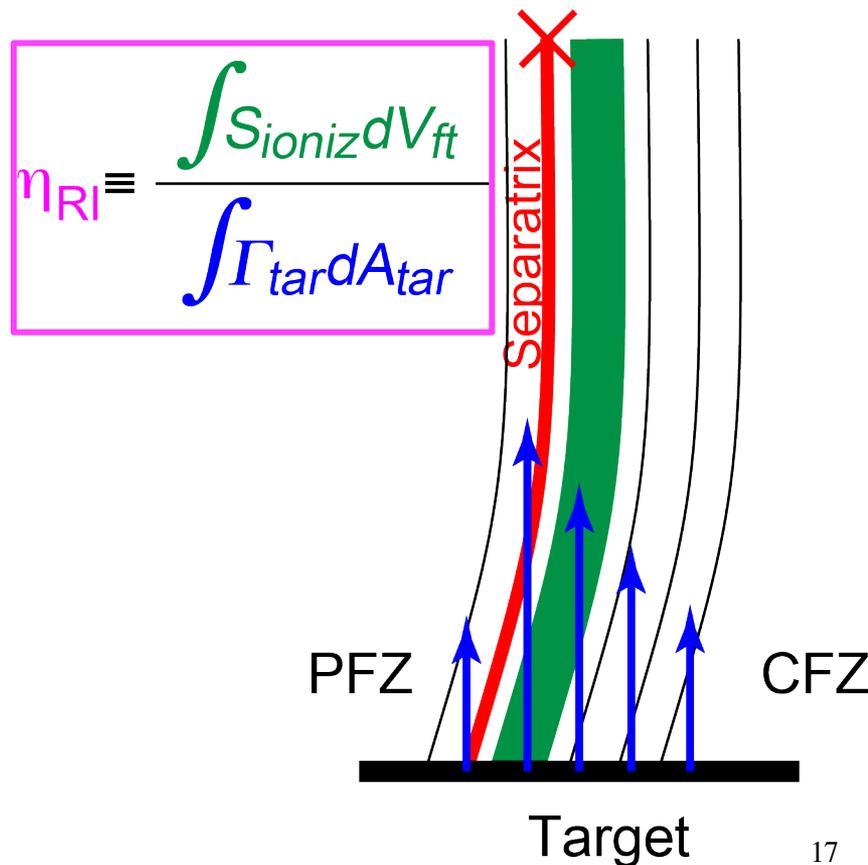
# All three divertor design choices affect the detachment threshold

- Total flux expansion lowers  $n_{u,d}$  for the **high- $R_t$**
- Strike point angle and neutral baffling lower  $n_{u,d}$  for the **low- $R_t$**



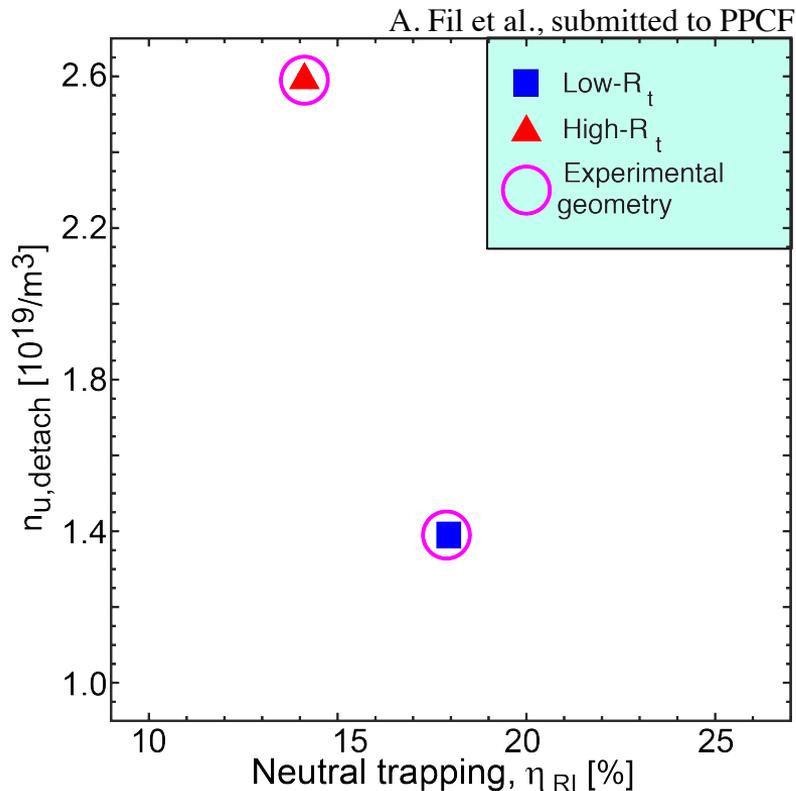
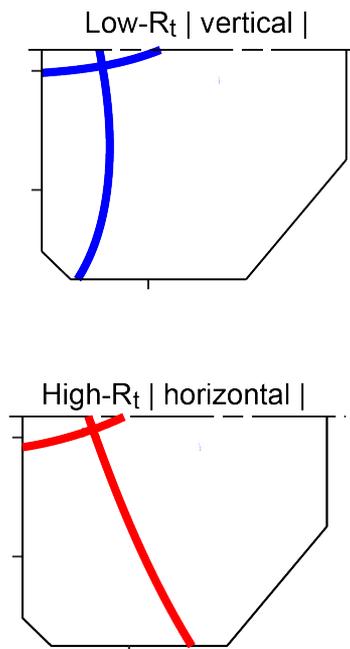
# Define 'neutral trapping' to aid in comparing various effects

- We quantify the relative contributions of strike point angle and neutral baffling on the detachment threshold
  - $\eta_{RI}$  is the fraction of the **total** divertor ionization source that occurs **in a flux tube near the separatrix**
  - We make this 'measurement' for TCV SOLPS cases



# As expected – an anti-correlation between $n_{u,d}$ and $\eta_{RI}$

- Detachment threshold  $n_{u,d}$  appears sensitive to  $\eta_{RI}$



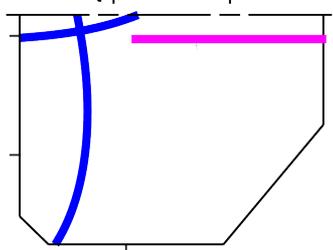
$$D_{predicted} \sim 0.76$$

$$D_{code} = \frac{n_{u,d}^{R_{t,high}}}{n_{u,d}^{R_{t,low}}} \sim 1.86$$

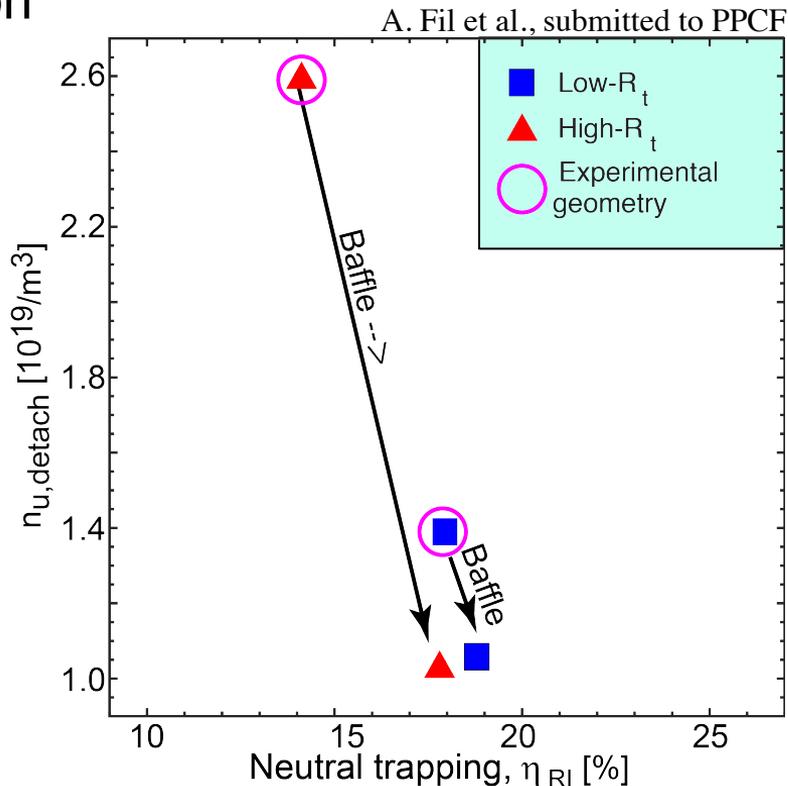
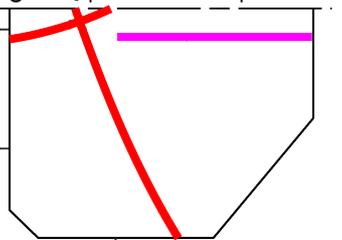
# The baffle strongly strongly affects detachment threshold for high- $R_t$ case

- Similar neutral confinement for high- & low- $R_t$ ; better match to total flux expansion prediction

Low- $R_t$  | vertical | baffled



High- $R_t$  | horizontal | baffled



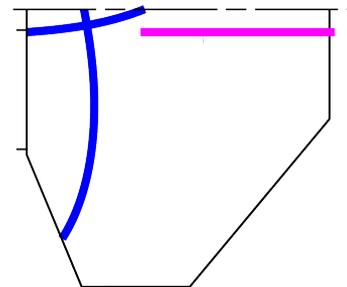
$$D_{predicted} \sim 0.76$$

$$D_{code} \equiv \frac{n_{u,d}^{R_{t,high}}}{n_{u,d}^{R_{t,low}}} \sim 1$$

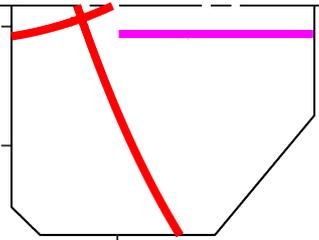
# Having baffling AND strike point angle the same for low- and high- $R_t$ : isolate total flux expansion effect

- Match predictions for total flux expansion!
- What else can we learn?

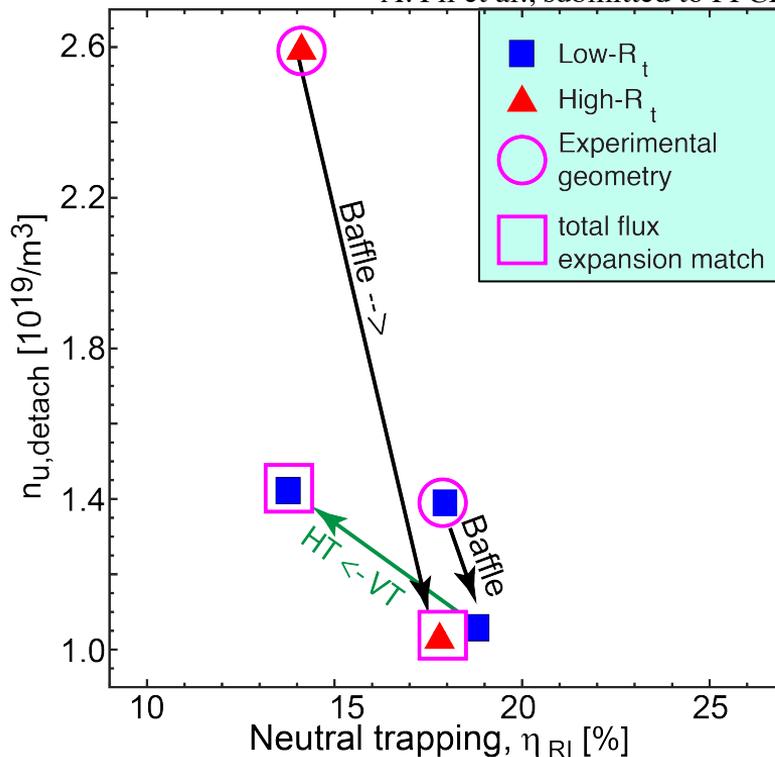
Low- $R_t$  | horizontal | baffled



High- $R_t$  | horizontal | baffled



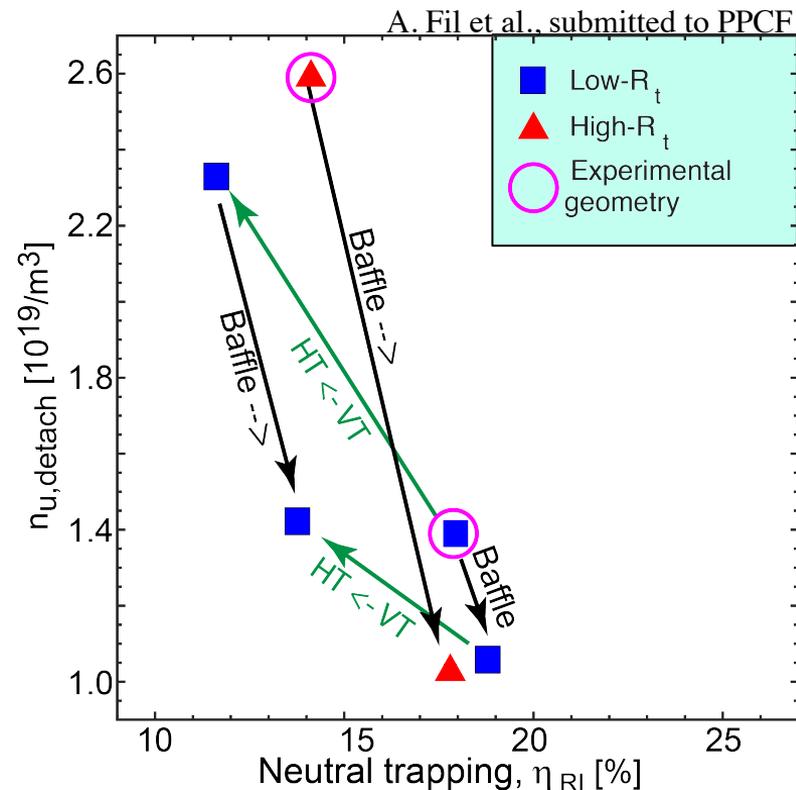
A. Fil et al., submitted to PPCF



$$D_{predicted} \sim 0.76$$

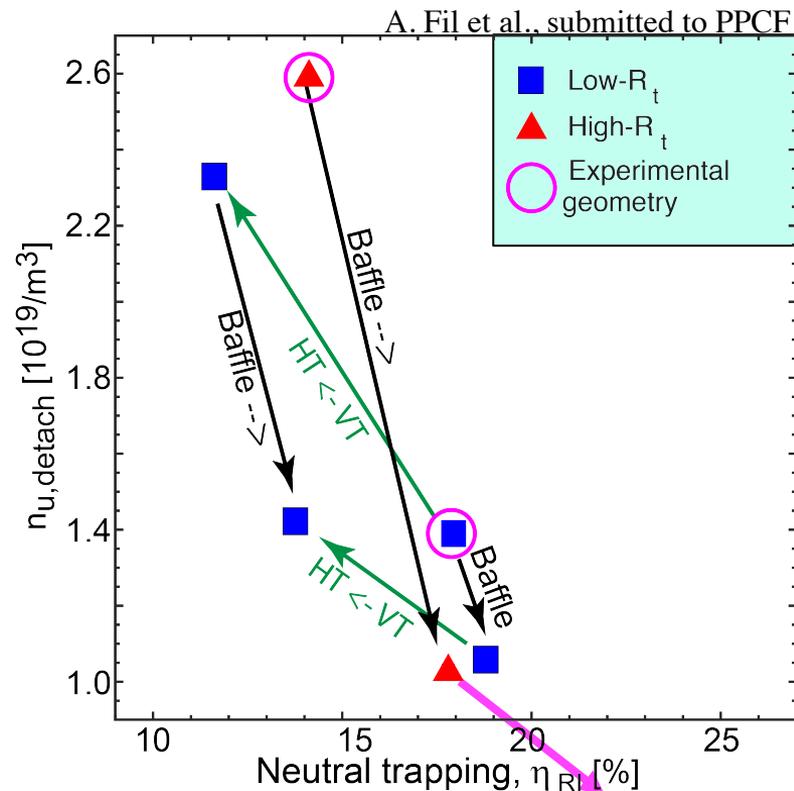
$$D_{code} \equiv \frac{n_{u,d}^{R_{t,high}}}{n_{u,d}^{R_{t,low}}} \sim 0.74$$

- **Baffle** (confining recycling neutrals)
  - Raises neutral density across the entire divertor, raising density and ionization costs, accelerating detachment
  - **Small effect on  $\eta_{RI}$  but large on  $n_{u,d}$**
- **Strike point angle** of 'vertical target'
  - Raises neutral density and ionization costs on a focussed region
  - **Larger effect on  $\eta_{RI}$ , similar for  $n_{u,d}$**

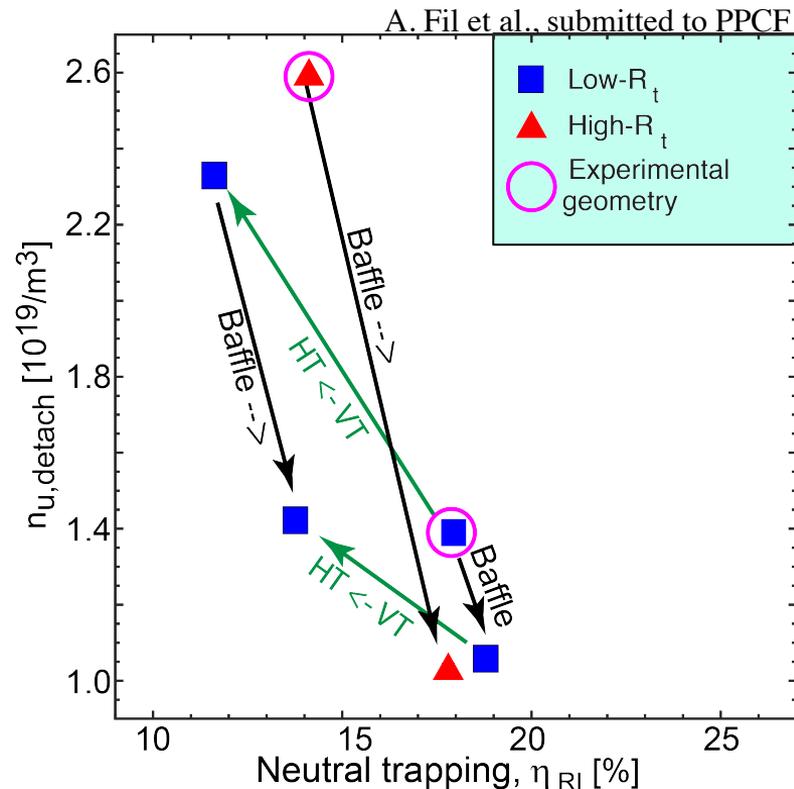


- We expect adding vertical target to high- $R_t$  to reduce  $n_{u,d}$  and raise  $\eta_{RI}$

- Caveat – This analysis presented here is for TCV conditions, far from a reactor
  - However, strike point angle and neutral baffling enhancements are recognized in studies of ITER, C-Mod and AUG
  - The total flux expansion effect is straightforward and already in codes.



- Results indicate the the effect of total flux expansion is occurring but may be hidden by neutrals effects
  - It is 'additive', or 'subtractive' in this case, so an independent effect



# Other implications of this study for divertor design

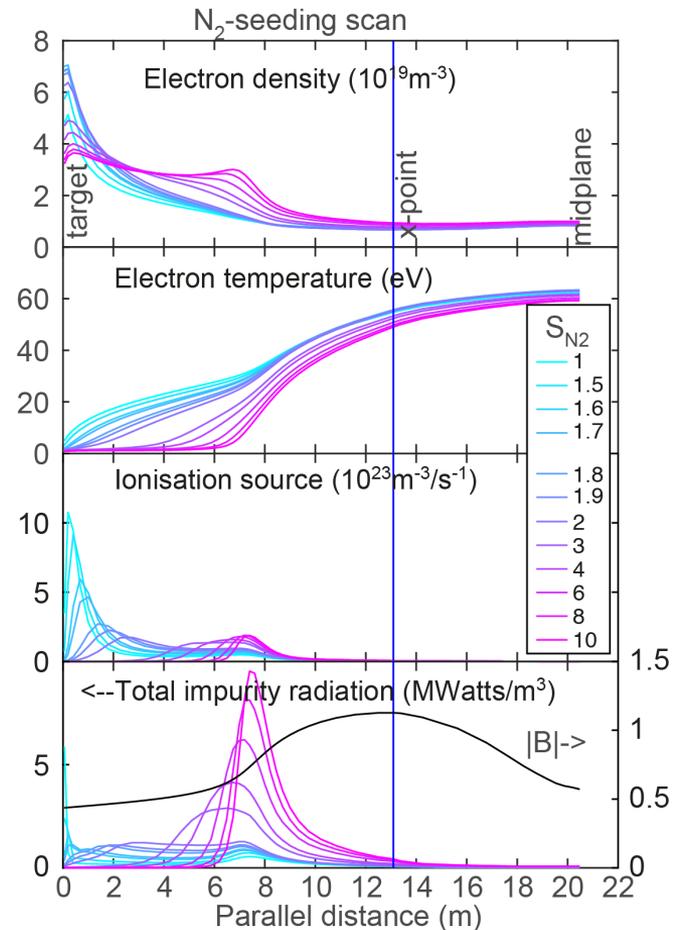
- These results can be generalized using the Lengyel radiation formulation to include two other 'control' variables<sup>1</sup> – impurity concentration,  $C_z$ , and  $P_{SOL}$ :

$$\left[ \frac{n_u C_z^{1/2}}{P_{SOL}^{5/7}} \right]_{detach} \propto \frac{|B_{tar}|}{|B_x|} f(L, z_x / L)$$

- Lower  $n_{u,d}$  is equivalent to detaching at higher  $P_{SOL}$  or lower  $C_z$

# Other 'experiments' in SOLPS\* on detachment position control

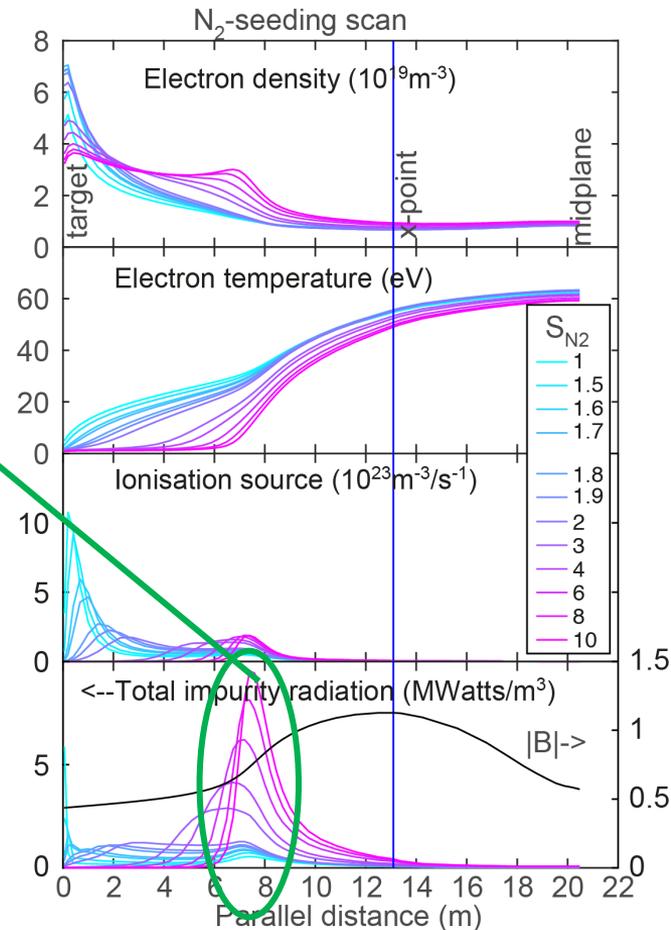
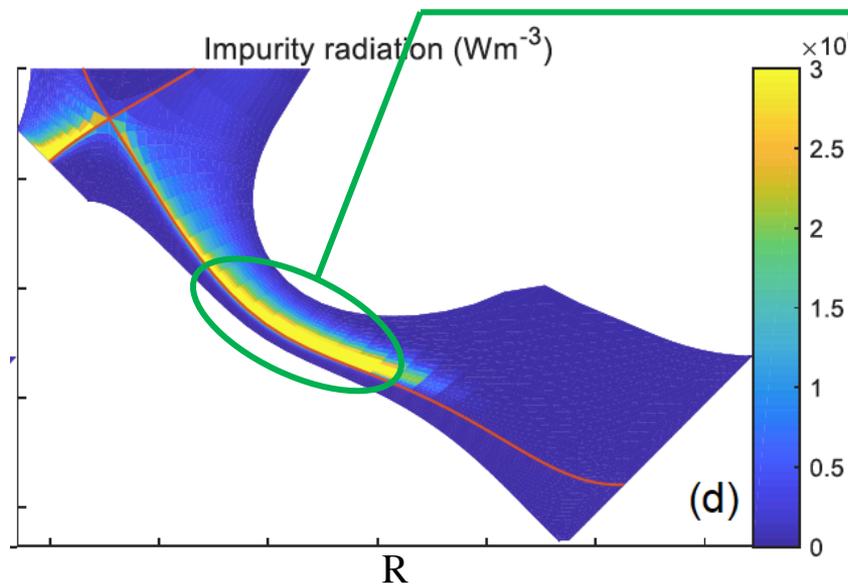
- MAST-U Detachment (seeding):



\*O. Myatra, MAST-U, PSI18 poster

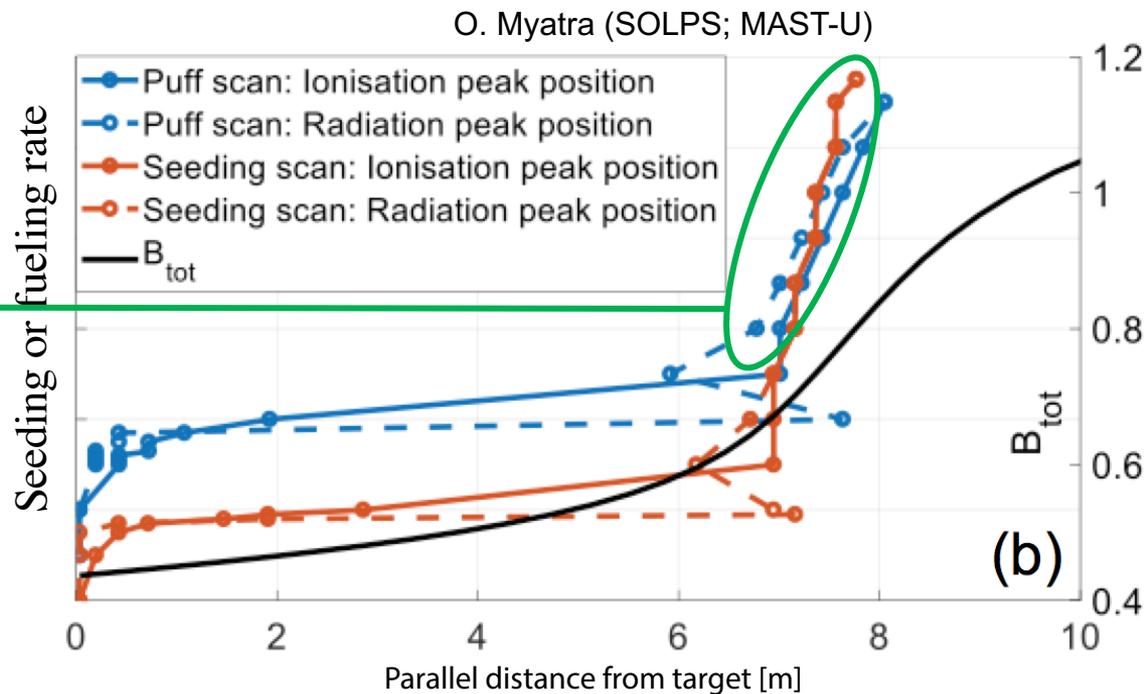
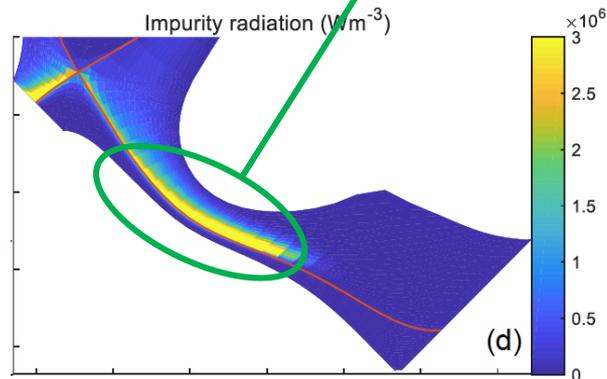
# Other 'experiments' in SOLPS\* indicate control increases with the magnitude of $\nabla|B|$

- Movement slows down even though seeding rate is strongly increased
- Radiation region 'stops' mid-divertor where  $\nabla|B|$  (really  $\nabla|q_{||}|$ ) large

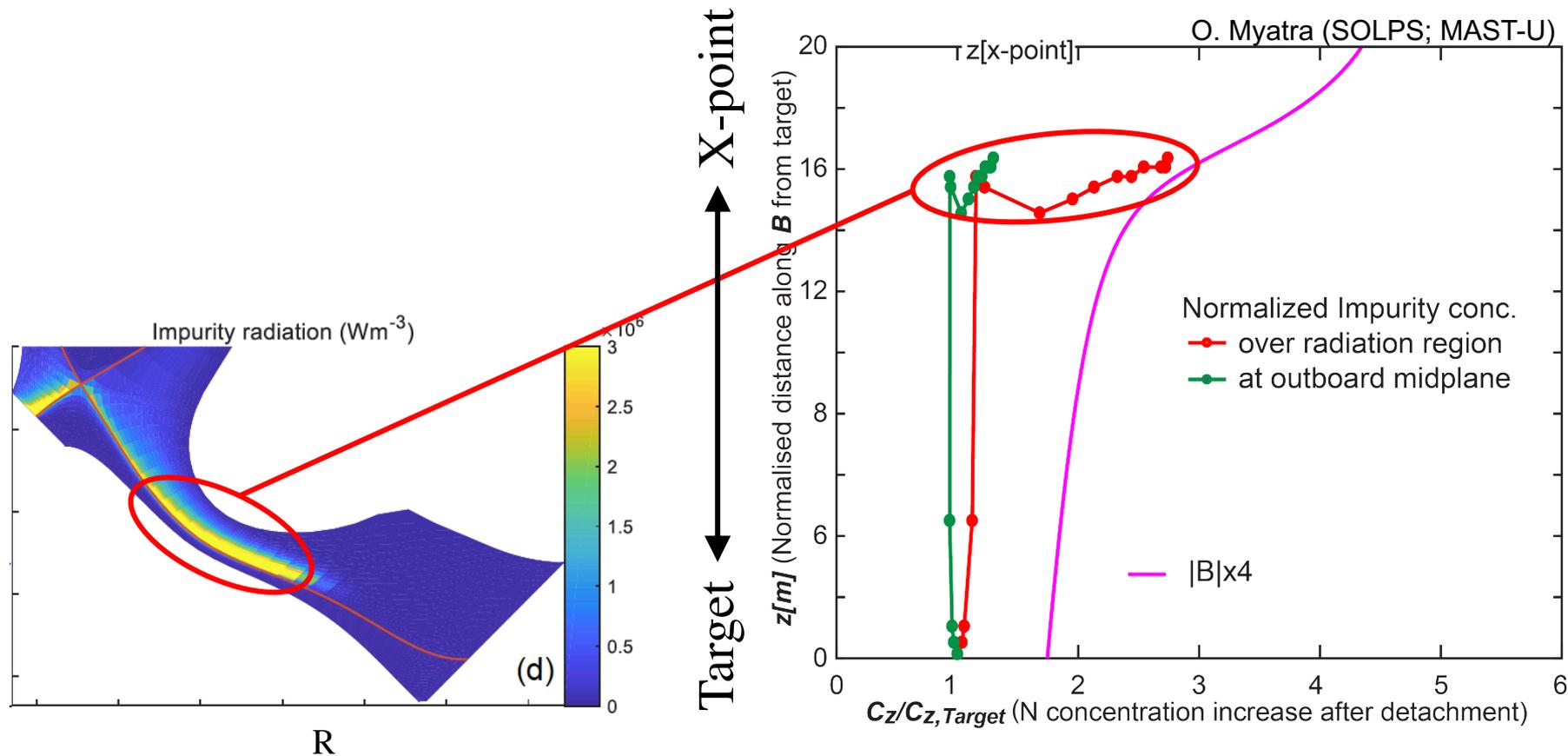


# Strong $\nabla|B|$ correlates with ‘slowing’ front movement\*

- Could be  $\nabla|B|$  (really  $\nabla|q_{||}|$ ) location stabilizing effect<sup>4</sup>

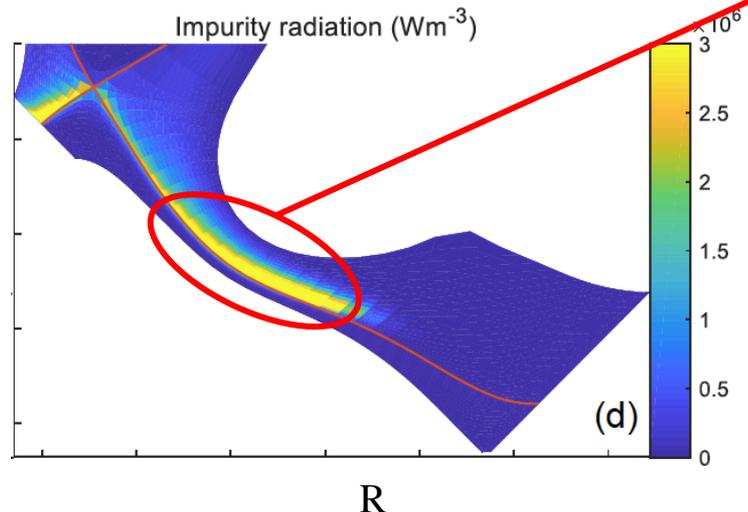


# Detachment position vs normalized impurity fraction, $C_z/C_{z,target}$ , correlates with position vs $|B|$

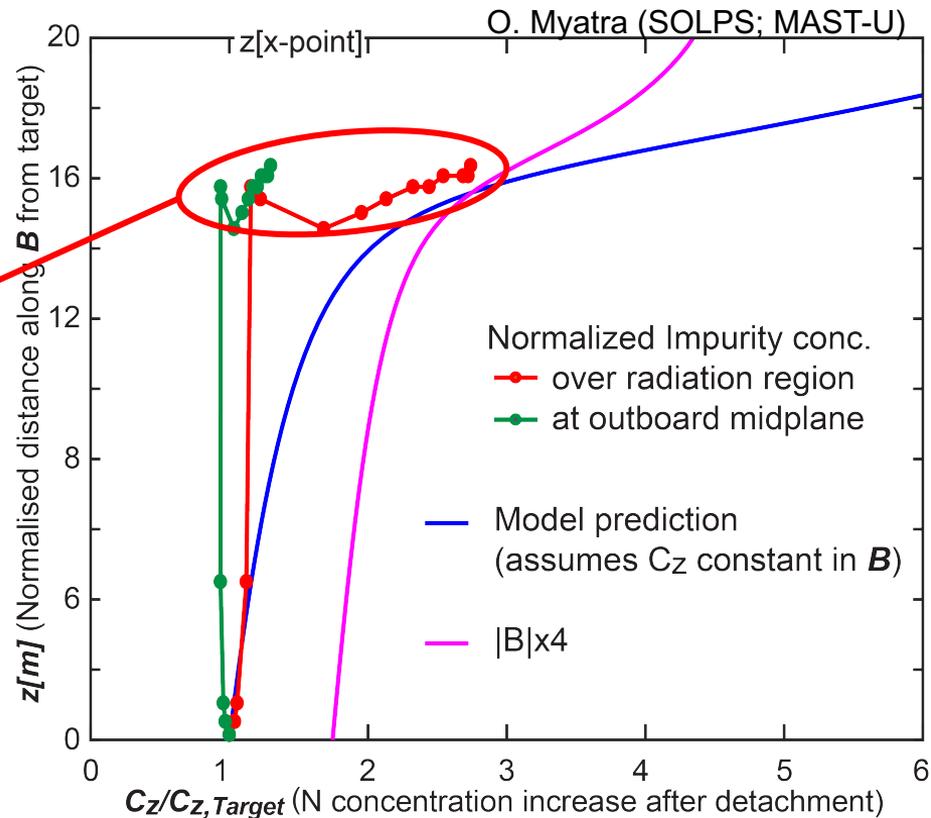


# Model prediction<sup>1</sup> of movement fair approximation of SOLPS 'experimental' results

- Reasonable agreement with **model prediction\***
  - Tests with more equilibria needed
  - $\nabla|B|$  ( $\nabla|q_{||}|$ ) could be another 'tool' in divertor design



X-point  
↑  
Target  
↓



# Summary - Control of detachment threshold and movement

To optimize minimization of the detachment threshold:

- Divertor designs should enhance baffling & optimize strike point angle
  - If total flux expansion can be accommodated it will
    - Lower  $n_{u,d}$  further (and potential to optimize control of location)

Further studies needed:

- A full study over a range of strike point angles would help optimize strike point angle choice over a range of divertor plasma densities and  $q_{||}$
- More study is needed of how divertor design choices affect:
  - Divertor impurity confinement (e.g. forces on impurity ions)
  - Detachment control after onset

# Backup slides

# Model prediction<sup>1</sup> of detachment location movement can be used to compare to SOLPS results

- Useful for predicting general sensitivity of detachment movement,  $z$ , to changes in one or more control variables,  $C_x$  and their derivative  $dz/dC_x$  (and detachment thresholds)
  - Many simplifications required for such an analytic model

$$\frac{n_u f_{imp}^{1/2}}{P_{SOL}^{5/7}} \propto \frac{B[z]}{B_x} \left[ \frac{(z_x - z)}{3} \left( 1 + \left| \frac{B[z]}{B_x} \right| + \left| \frac{B[z]}{B_x} \right|^2 \right) + \frac{(L - z_x)}{2} \right]^{2/7}$$

$$\frac{C_{nu} C_{imp}^{1/2}}{C_{PSOL}^{5/7}} \propto A[z]$$

- Initial control variables,  $C_x$  - impurity concentration,  $P_{SOL}$  and upstream density,  $n_u$
- Movement in  $z$  related to
  - magnetic field profile (affects  $\nabla|B|$  and  $\nabla|q_{||}|$ ) and  $z_x/L$
  - Variation in control variables,  $C_x$ , leads to a different solution and  $z$

<sup>1</sup> B. Lipschultz et al,  
 Nucl. Fusion **98** (2016)  
 056007