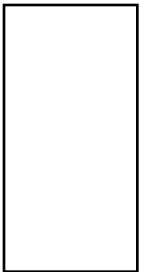
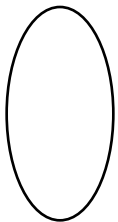


# Novel Radio Frequency Current Drive Systems for Fusion Plasma Sustainment on DIII-D

This is a square



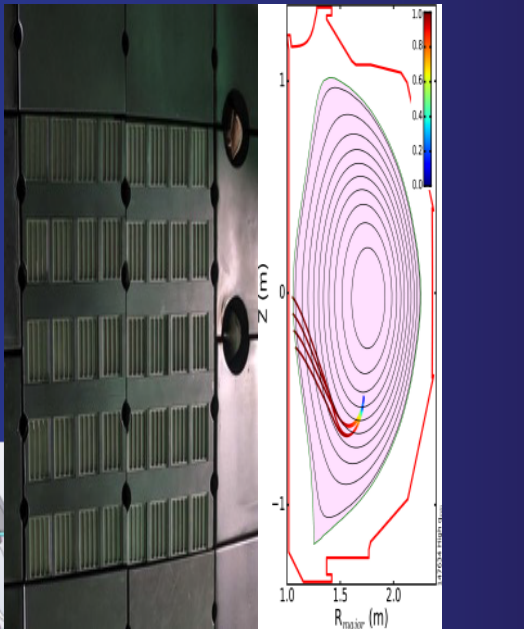
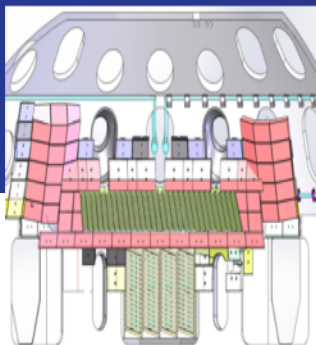
This is a circle



by  
G.M. Wallace  
(MIT PSFC)

Presented at  
2018 IAEA Fusion Energy Conference  
Ahmedabad, Gujarat, India

October 25, 2018



## On Behalf of:

R.C. O'Neill<sup>2</sup>, P.T. Bonoli<sup>1</sup>, M.W. Brookman<sup>2</sup>, J.S. deGrassie<sup>2</sup>, J. Doody<sup>1</sup>,  
J. Ferron<sup>2</sup>, B. Fishler<sup>2</sup>, W. Helou<sup>3</sup>, C. Holcomb<sup>4</sup>, R. Leccacorvi<sup>1</sup>, M. LeSher<sup>2</sup>,  
C. Moeller<sup>2</sup>, C. Murphy<sup>2</sup>, A. Nagy<sup>5</sup>, R.I. Pinsker<sup>2</sup>, S. Shiraiwa<sup>1</sup>, M Smiley<sup>2</sup>,  
J.F. Tooker<sup>2</sup>, H. Torreblanca<sup>2</sup>, R. Vieira<sup>1</sup>, S.J. Wukitch<sup>1</sup>

<sup>1</sup>MIT Plasma Science and Fusion Center, Cambridge, MA USA

<sup>2</sup>General Atomics, La Jolla, CA USA

<sup>3</sup>CEA, IRFM, F-13108 St-Paul-Lez-Durance, France

<sup>4</sup>Lawrence Livermore National Laboratory, Livermore, CA USA

<sup>5</sup>Princeton Plasma Physics Laboratory, Princeton, NJ USA



# Efficient, Reliable, Off-axis Current Drive is Required on Future Tokamak Reactors; Better Actuators are Needed

Most steady-state reactor concepts require off-axis non-inductive current drive to supplement bootstrap current

Efficiency is critical for current drive in a reactor to keep recirculating power down

New CD actuators needed to meet all requirements

Off-axis

High efficiency

Survivability/lifetime

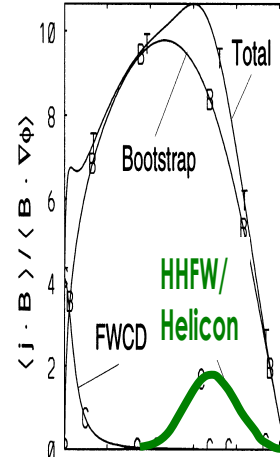
Two novel RF current drive actuators under development at DIII-D:

4.6 GHz high field side (HFS) launch lower hybrid current drive (LHCD)

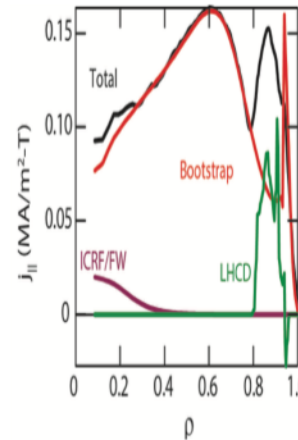
Optimized at higher B and lower  $n_e$

476 MHz "helicon" or fast lower hybrid wave

Optimized at higher  $n_e$  and lower B



Adapted from [ARIES-RS](#) Najmabadi et al., *FED* **38**, 1997.

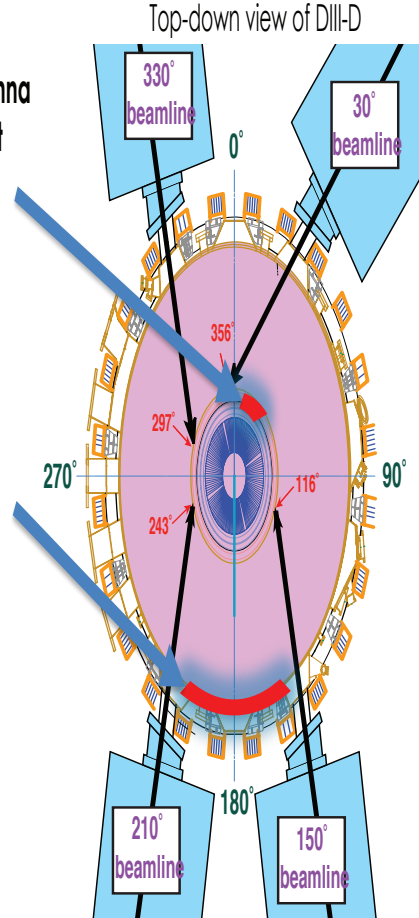


Adapted from [ARIES-ACT1](#) Kessel et al., *FST* **67**, 2015.

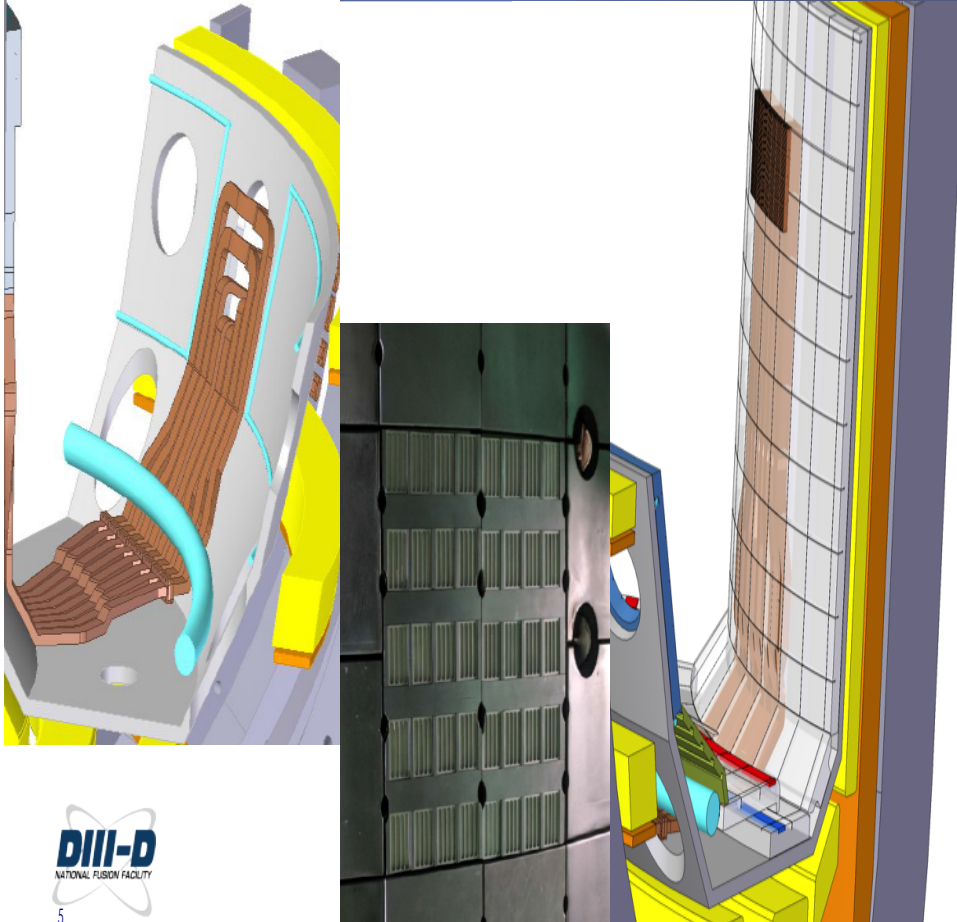
# Two Novel RF Current Drive Actuators Under Development at DIII-D: HFS LHCD and Helicon

4.6 GHz HFS LHCD antenna located on inner wall at  $\sim 20^\circ$  toroidal angle

476 MHz LFS Helicon antenna located at  $\sim 180^\circ$  toroidal angle



# High Field Side Launch LHCD



# HFS Launch of LH Waves Improves Current Drive Efficiency, Antenna Longevity, and Tritium Breeding

## HFS launch improves well established LH wave physics<sup>1</sup>

Lower  $n_{||}$  for higher current drive efficiency

Better wave penetration

Access to inside pedestal in reactor

HFS SOL characteristics extend antenna longevity

Lower heat, neutron, and particle fluxes

Fewer unconfined fast ion orbits

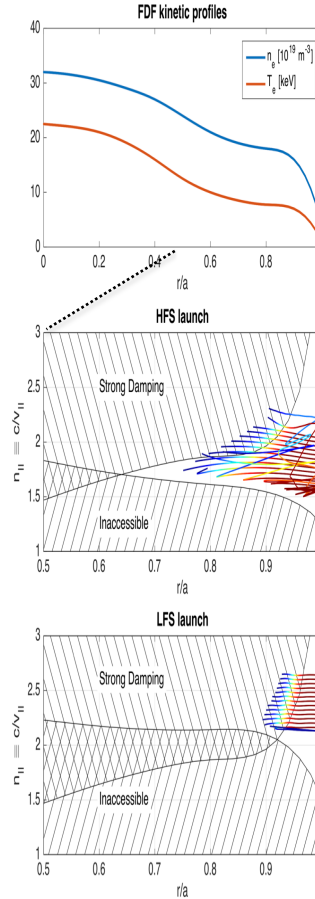
Better impurity screening

Also applies to other HFS RF actuators

**Engineering challenges to fit HFS antenna in existing tokamak designs; more available real estate in a clean slate reactor**



<sup>1</sup>Bonoli, et al, Nuc. Fus. (2018)



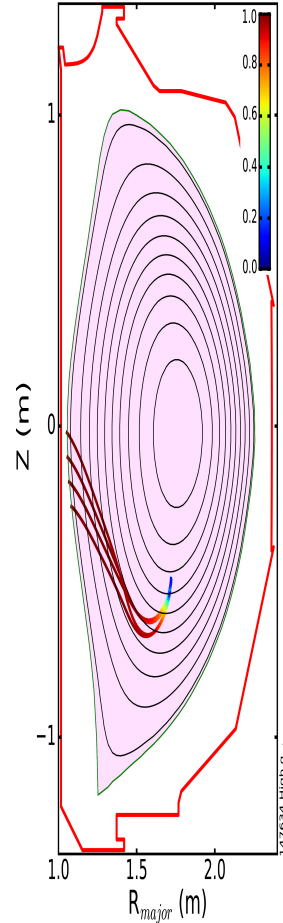
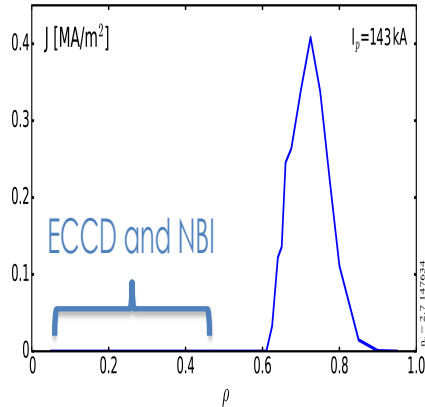
# Excellent Wave Penetration and Efficiency are Predicted for HFS LHCD on DIII-D

High field side lower hybrid current drive (HFS LHCD)  
offers potential efficient off axis current drive

HFS LHCD has good wave penetration and single  
pass absorption

Drives current off axis at  $0.6 < r < 0.8$

For high  $q_{\min}$  discharges, simulations indicate 143  
kA/MW coupled, 0.4 MA/m<sup>2</sup> at  $r/a \sim 0.7$



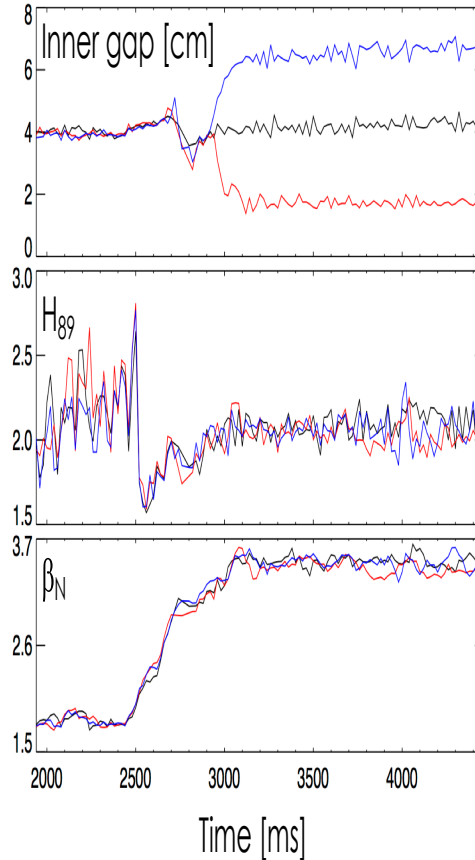
# Experiments Show that Geometry Changes Needed for HFS LHCD have Minor Impact on Plasma Performance

**Coupling of LH waves to plasma requires edge density  $\sim 10^{18} \text{ m}^{-3}$**

Smaller than typical plasma-inner wall gap

**2.5 cm thicker inner wall tiles needed for HFS LHRF**

**Observed only subtle impacts of inner gap on confinement & stability**





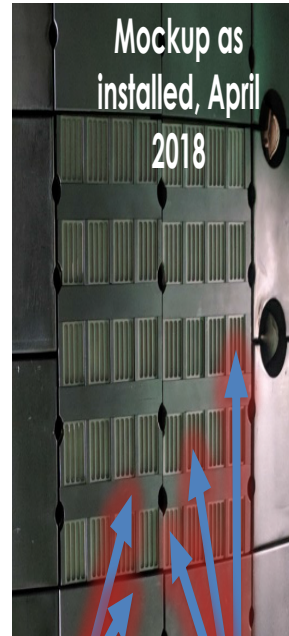
# Mockup Antenna Installed and Operated in DIII-D to Assess Impact of High-Z Materials on the Center Post

**Mock-up is located same vertical position as planned coupler but at  $\sim 300^\circ$  toroidally vs  $\sim 20^\circ$**

Molybdenum (TZM alloy) dummy waveguides  
TZM structure recessed  $\sim 1$  mm behind carbon protection limiters

**Demonstrated that the HFS LHCD coupler will not interfere with general DIII-D operations**

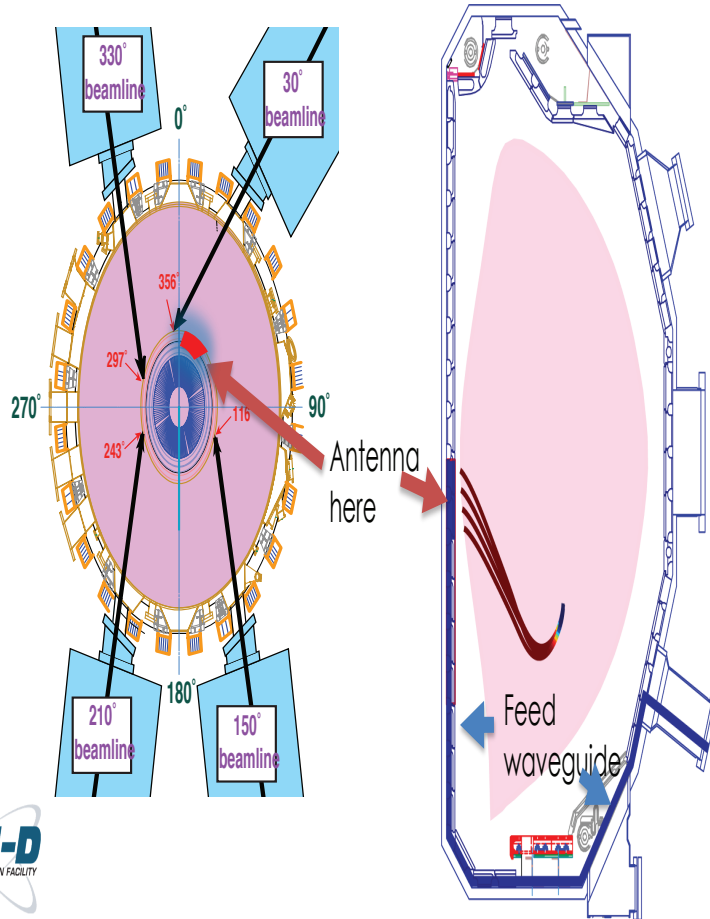
Negligible molybdenum source from HFS antenna mockup  
No impact on plasma performance



Graphite

Molybdenum

# Real Estate is Limited on HFS Wall; Antenna Must be Compact in Radial Dimension



# Antenna Design Based on Toroidal Multijunction + Poloidal T-junction Waveguide Antenna

## Multijunction (MJ) concept proven on many tokamaks (Tore Supra, JET, FTU, EAST)

Self-matching characteristics reduce reflected power towards transmitter

Conventionally oriented radially in LFS port

## T-junction (TJ) poloidal splitter

Similar to successful LH2 antenna on C-Mod

Also tested at low power on COMPASS

## Combine two concepts in series

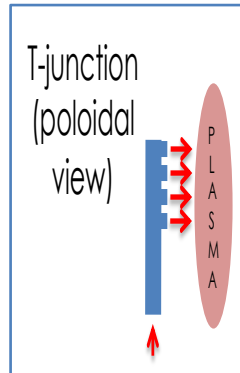
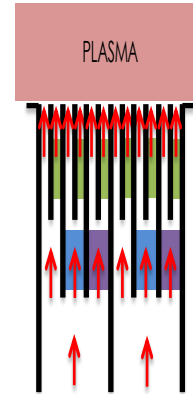
Low reflection coef.

Compact radial build

Toroidal & poloidal split



Multijunction (top view)



Phase Shifters



# Antenna Design Based on Toroidal Multijunction + Poloidal T-junction Waveguide Antenna

## Multijunction (MJ) concept proven on many tokamaks (Tore Supra, JET, FTU, EAST)

Self-matching characteristics reduce reflected power towards transmitter

Conventionally oriented radially in LFS port

## T-junction (TJ) poloidal splitter

Similar to successful LH2 antenna on C-Mod

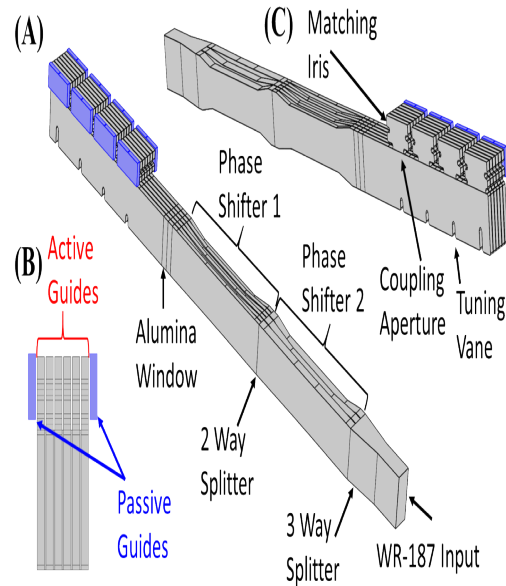
Also tested at low power on COMPASS

## Combine two concepts in series

Low reflection coef.

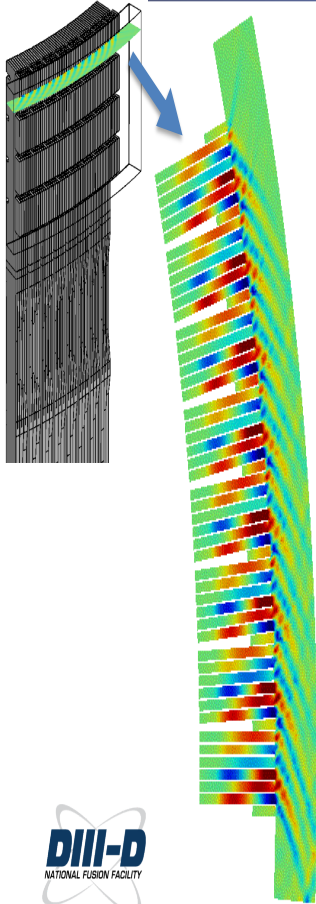
Compact radial build

Toroidal & poloidal split



# Antenna RF Simulations Predict Good Directivity and Coupling at Edge Density

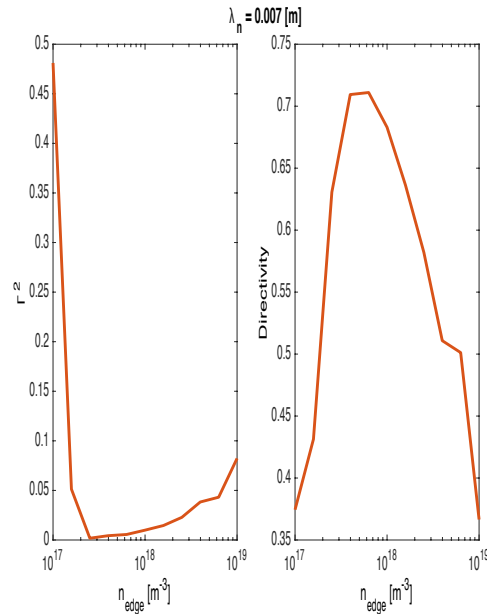
$\sim 0.3\text{-}1 \times 10^{18} \text{ m}^{-3}$



4 rows X 6 columns per MJ/TJ module

Eight MJ/SWA modules launch wave at  $n_{||} = 2.7$

Low reflected power ( $\Gamma^2 < 1\%$ ) and high directivity ( $>60\%$ )



## Antenna will Employ Additive Manufacturing (3D printing)

### **3D printing of copper alloy (GRCo-84) for major multijunction and T-junction components**

Excellent conductivity, heat tolerance, and strength

Able to manufacture complicated geometries

at lower cost vs CNC

### **Molybdenum (TZM alloy) for plasma facing grills**

### **Graphite for protection tiles**

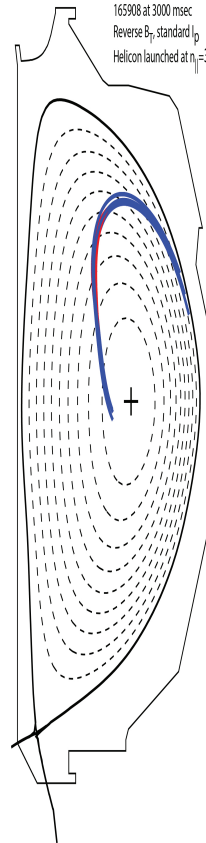
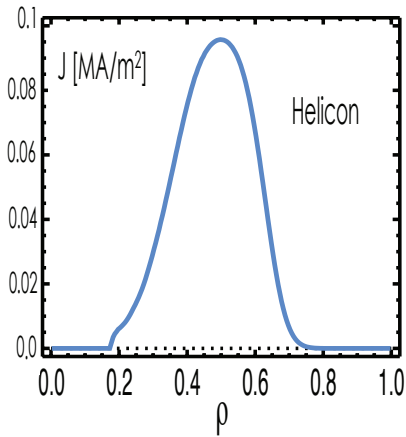
### **Installation of full power antenna in DIII-D in 2020**



“Helicon” (in this context) is a fast magnetosonic wave in the LHRF

Relatively weak damping allows for penetration to mid-radius in a reactor

55 kA/MW coupled power, 0.1 MA/m<sup>2</sup> at  $r/a \sim 0.5$  in DIII-D



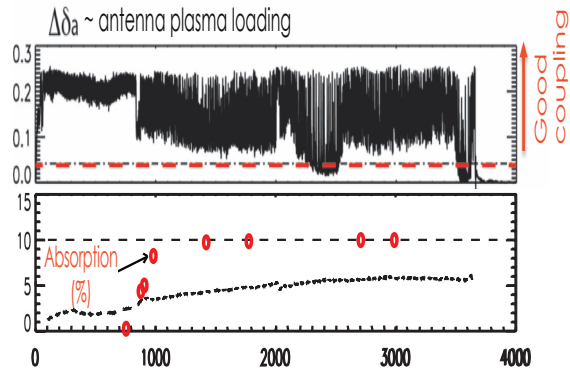
# Low Power Helicon Antenna Tested in DIII-D





## Goal: First Experimental Verification for Helicon Current Drive

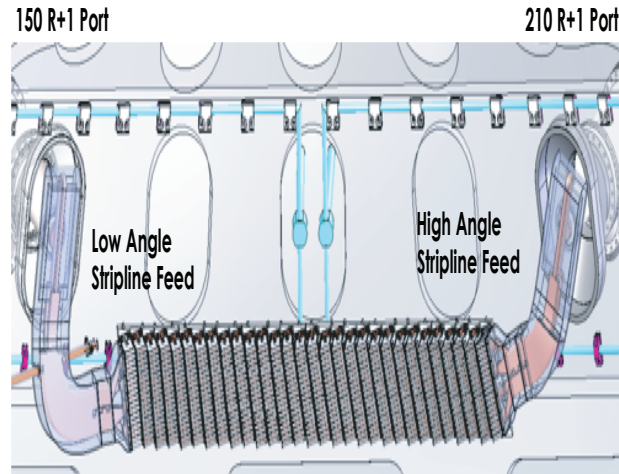
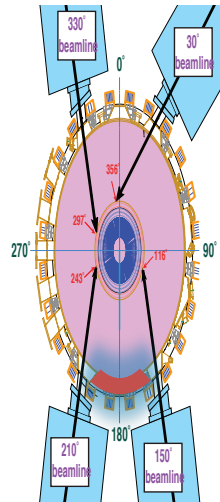
Electron pressure not high enough for single pass absorption in previous tests on other tokamaks  
High  $\beta_e$  discharges on DIII-D will have strong single pass damping at mid-radius  $\rightarrow$  good current drive efficiency



# “Comb-line” Traveling Wave Antenna Launches Fast Wave at 476 MHz

Feedthrus and striplines at each end allow operation in  $\pm I_p$  configuration  
30 mutually coupled antenna modules mounted on water-cooled back plates

1.2 MW klystron from SLAC provides power to antenna



30 Module, 1MW Comb-line Antenna

# Testing at DIII-D Evaluates High Power Antenna Design

Quarter and half-length helicon antenna modules used for 6 kW power testing, validating full design now being manufactured with ASIPP

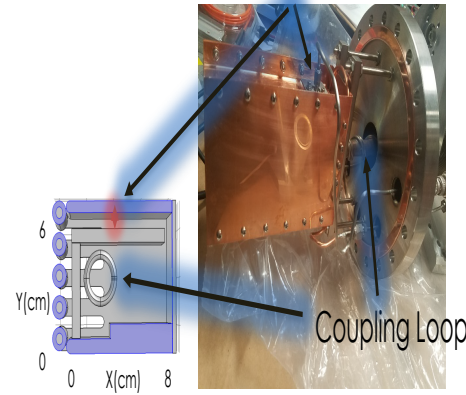
One Antenna Module



## Tests performed:

- Module losses (quality factor)
- Voltage standoff with B-field in vacuum
- Multipactor and discharge cleaning

Capacitive probe measures  $\bar{T}$  in gap



Quarter Module

Expt. Module Setup

## Helicon Antenna Under Construction; Installation in 2019 for Upcoming Run Campaign

**Design finalized for full power (1 MW at 476 MHz) antenna**

**Manufacturing through collaboration between GA and ASIPP**

**Installation of antenna during “long torus opening” period prior to upcoming run campaign**

# Conclusions

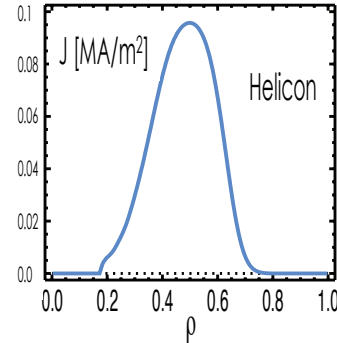
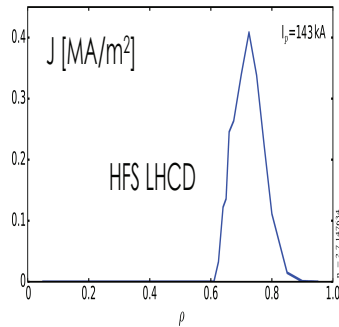
**HFS LHCD and Helicon offer promise of efficient, off-axis RF current drive for DIII-D and future tokamak reactors**

LHCD:  $0.4 \text{ MA/m}^2$  at  $r/a \sim 0.7$ ,  $143 \text{ kA/MW}$

Helicon:  $0.1 \text{ MA/m}^2$  at  $r/a \sim 0.5$ ,  $55 \text{ kA/MW}$

**Installation of Helicon antenna in 2019**

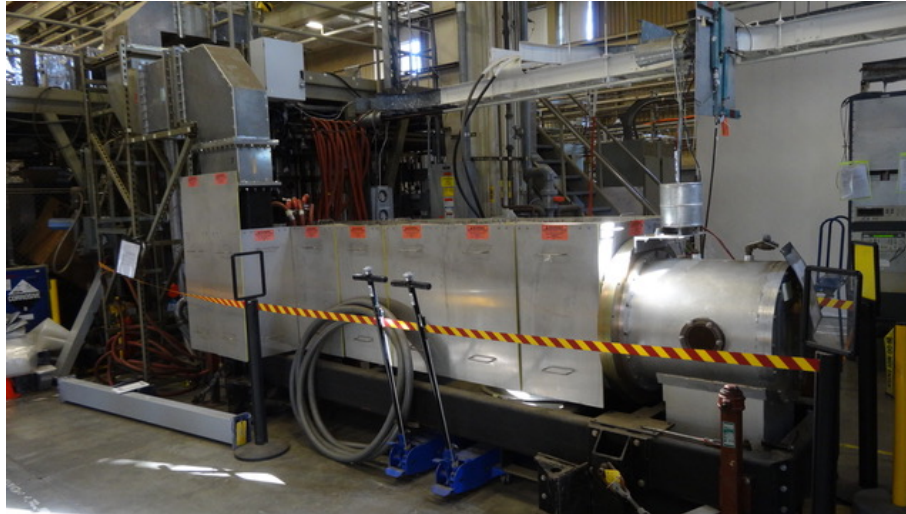
**Installation of HFS LHCD antenna in 2020**



## Additional Slides

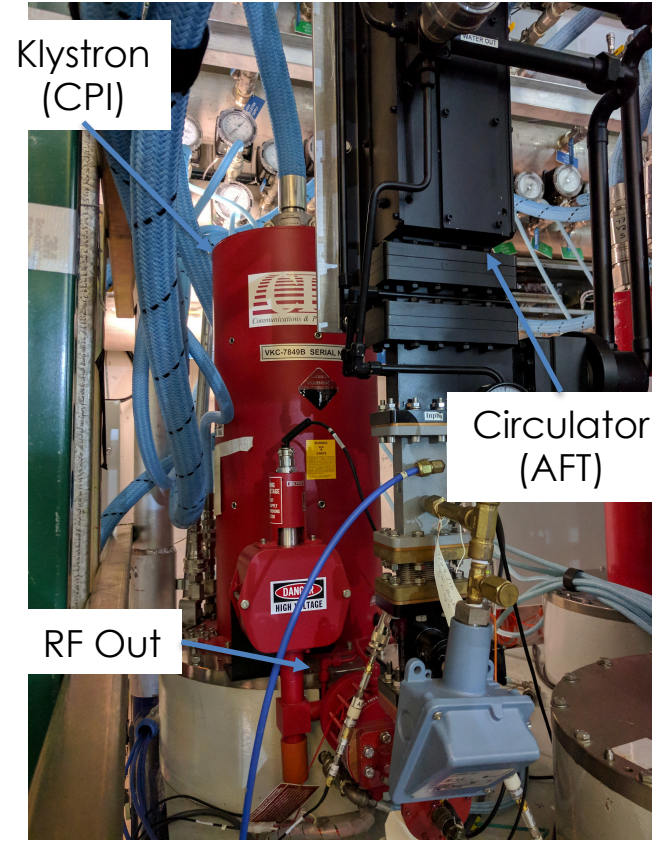
# Single Klystron Provides 1.2 MW at 476 MHz

- Klystron and associated hardware provided by SLAC
- Beam power provided by 2 MW, 80 kV high voltage power supply
- Snubber and circulator protect klystron from faults



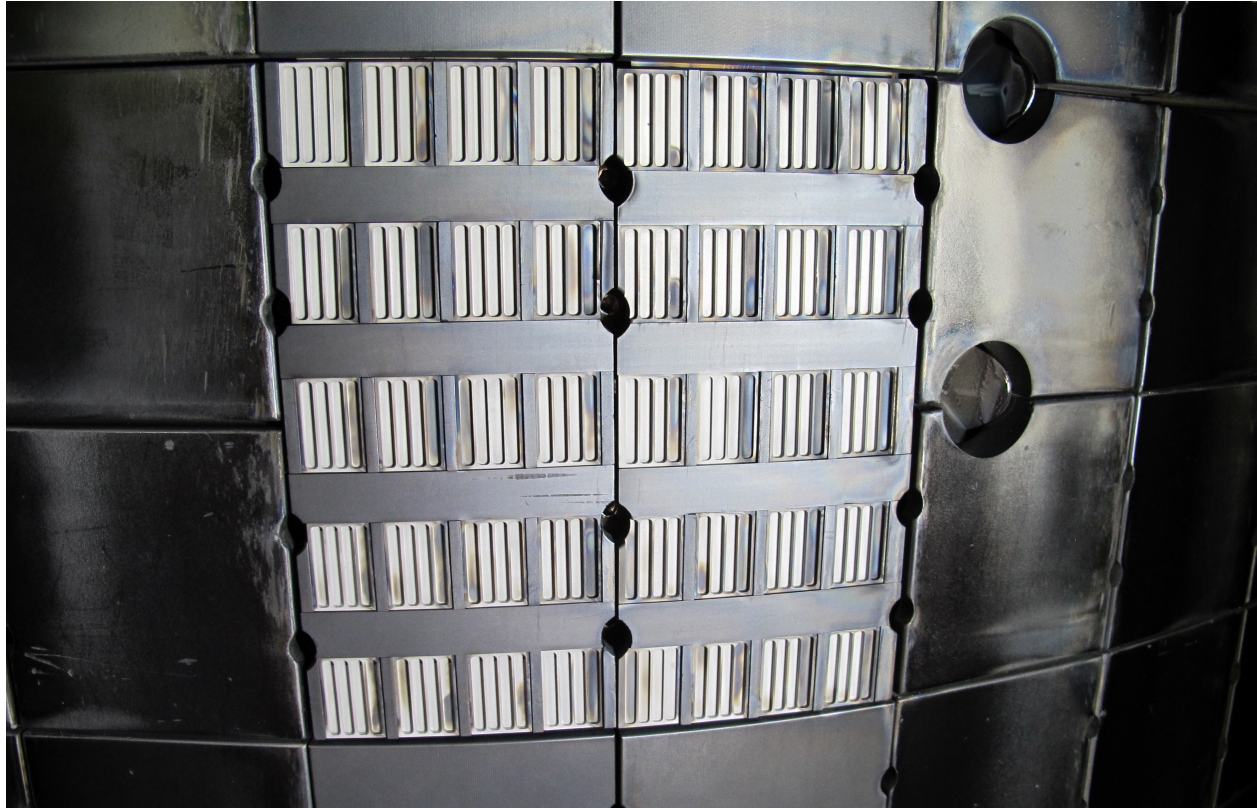
# Multi MW Source Power at 4.6 GHz for DIII-D HFS LHCD

- $f_0 = 4.6$  GHz
- $P_{RF} = 0.25$  MW/klystron
- Gain = 55 dB
- $V_b = 46.5$  kV
- $I_b = 13$  A
- Efficiency = 41%
- 8 klystrons to be located adjacent to DIII-D cell → 2 MW source
- Thales/Ampegon HVPS to be installed in high voltage yard outside DIII-D building
- Power systems and antenna designed for 5 s full power pulses at 1% duty cycle



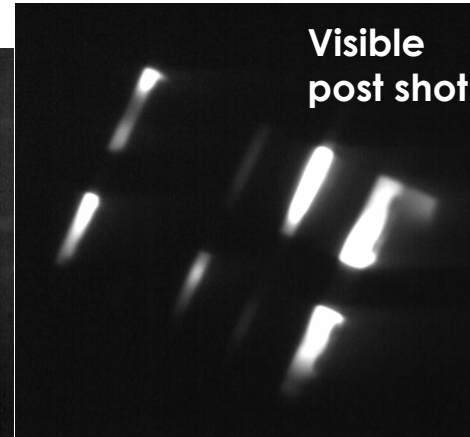
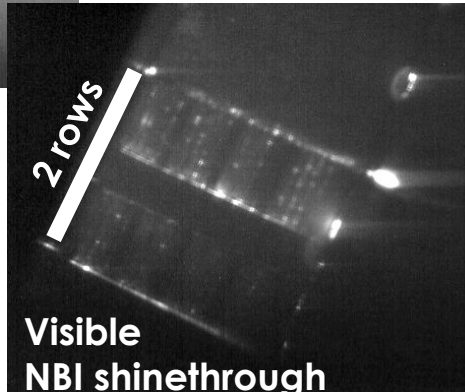
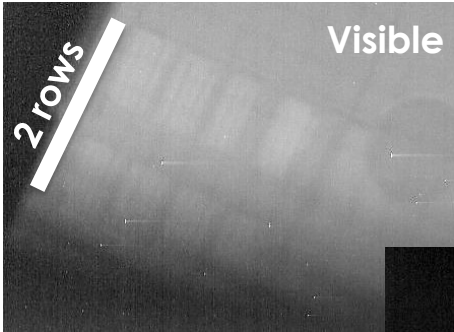


# Post-run Inspection of Mockup: Excellent Condition



# Inner Wall Limited with Rotating $n=1$ was Most Severe Test for Antenna Mockup

- **Mock-up carbon files have had strong plasma-material interaction**
  - Visible and IR camera confirm protection tiles were significantly heated during inner wall limited discharges



# Two Novel RF Current Drive Actuators Under Development at DIII-D

- DIII-D uses NBI and ECCD with considerable success at  $r/a < 0.5$
- Strong bootstrap current in edge region due to  $\nabla p$
- Need actuator in off-axis region around  $0.6 < r/a < 0.8$
- Two novel RF current drive actuators under development at DIII-D have the potential to fill this hole:
  - High field side (HFS) launch lower hybrid current drive (LHCD)
    - Optimized at higher B and lower  $n_e$
  - “Helicon” or fast lower hybrid wave
    - Optimized at higher  $n_e$  and lower B

