

# **Development of a Lithium Vapor Box Divertor for Controlled Plasma Detachment**

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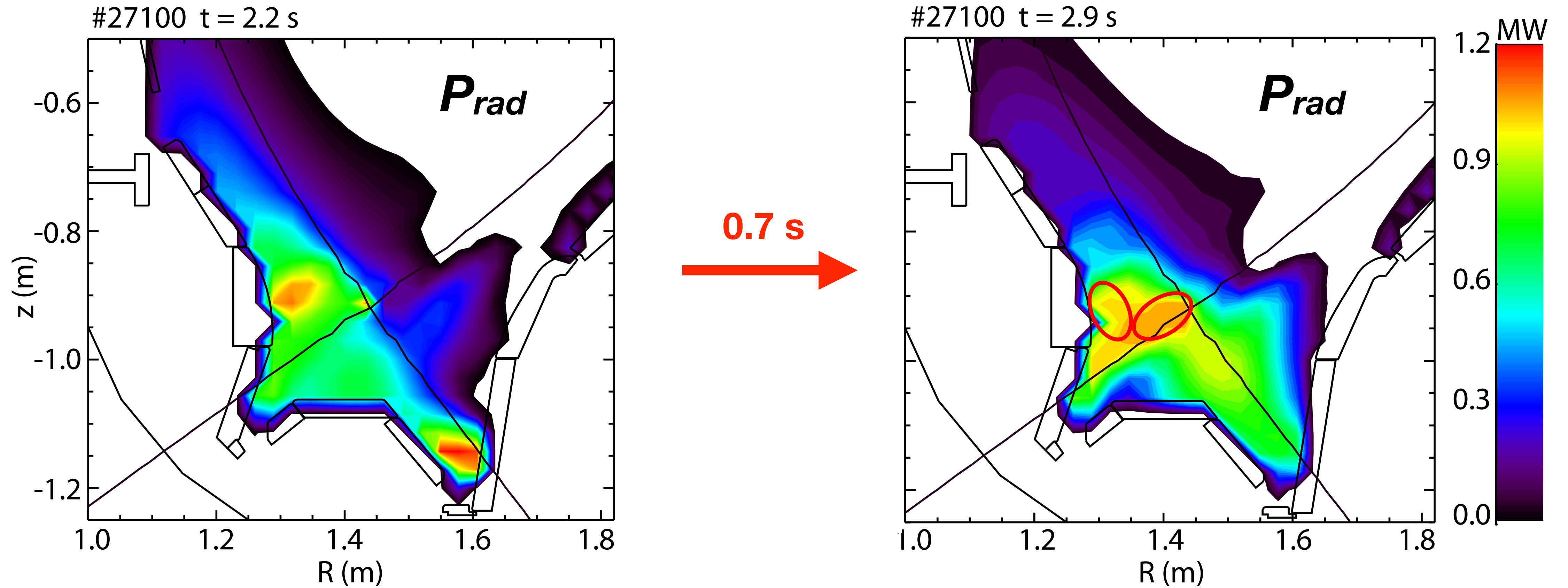
Lawrence Livermore National Laboratory

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# Divertor Detachment Front Easily Runs up to the Main Plasma

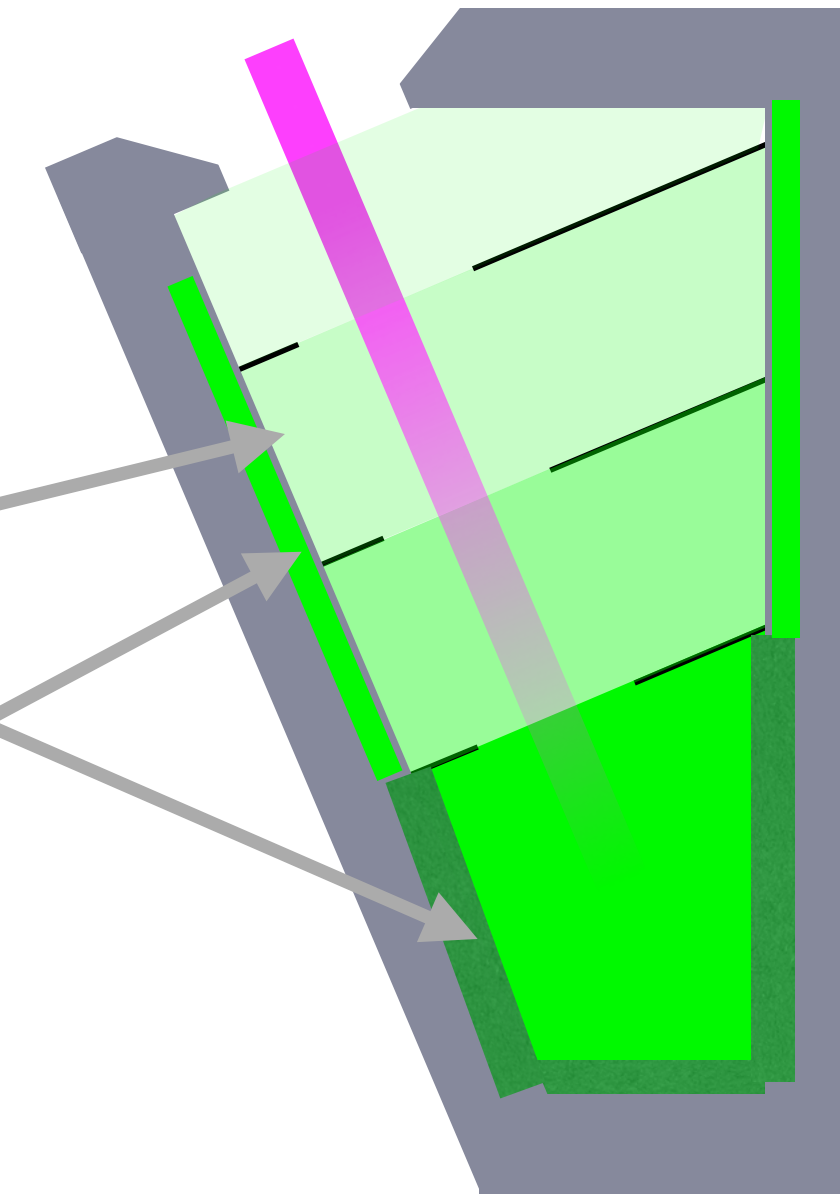
Potzel, NF 2014, AUG



**Deleterious effect on H-Mode pedestal.**

# Lithium Vapor Box Divertor Concept

- Provide a localized cloud of Li vapor away from main plasma
- Evaporation at  $\sim 750^\circ\text{C}$
- Condensation at  $\sim 3-400^\circ\text{C}$  (determines DT pumping)
- Return liquid lithium to evaporator.
- Creates strong vapor gradient.
- Detachment front cannot run up to x-point.
- Detachment front location is resilient to variable heat flux.
- Cannot be achieved with gaseous impurities – pumping is too weak



# UEDGE Model with Lithium

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- **UEDGE has a purely diffusive model for lithium vapor transport.**
  - **Based on collisions of lithium atoms with plasma ions.**  
**No Li-Li collisions.**
  - **Inaccurate in regions dominated by lithium convection/viscosity:**  
**Navier-Stokes regime.**
- **Transports lithium in plasma, calculates radiation self-consistently.**
  - **Issues with thermal force model at high impurity fraction.**
- **Achieves detached plasma in Fusion Nuclear Science Facility (FNSF) with nearly 100% lithium radiated power. In “real” world would include other (seed) impurities.**
- **Upstream lithium fraction depends on upstream electron density.**

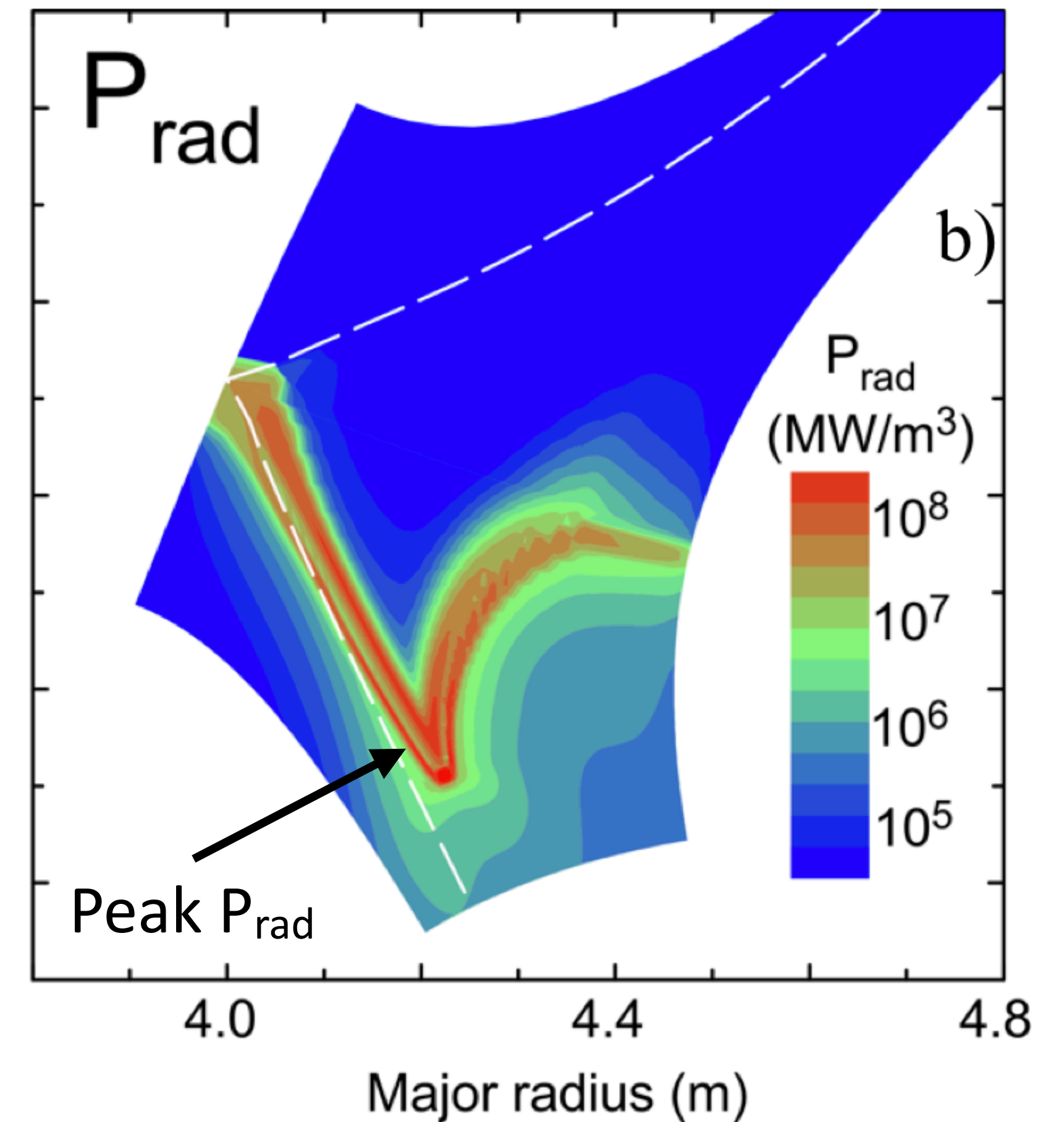
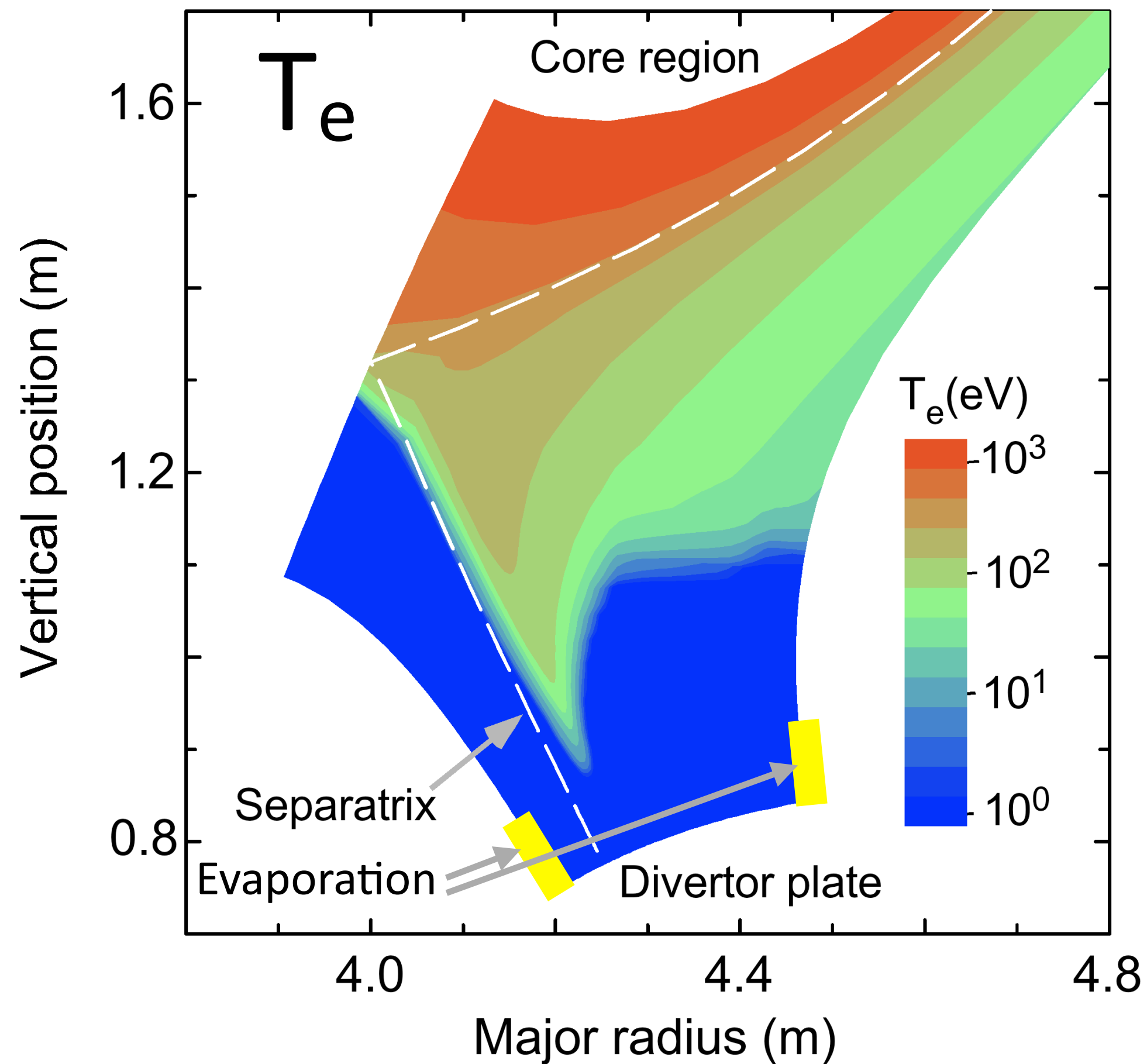
# UEDGE Predicts Detachment in FNSF with Lithium in Simplified Divertor

0.5 m  
outer divertor leg,  
Open geometry

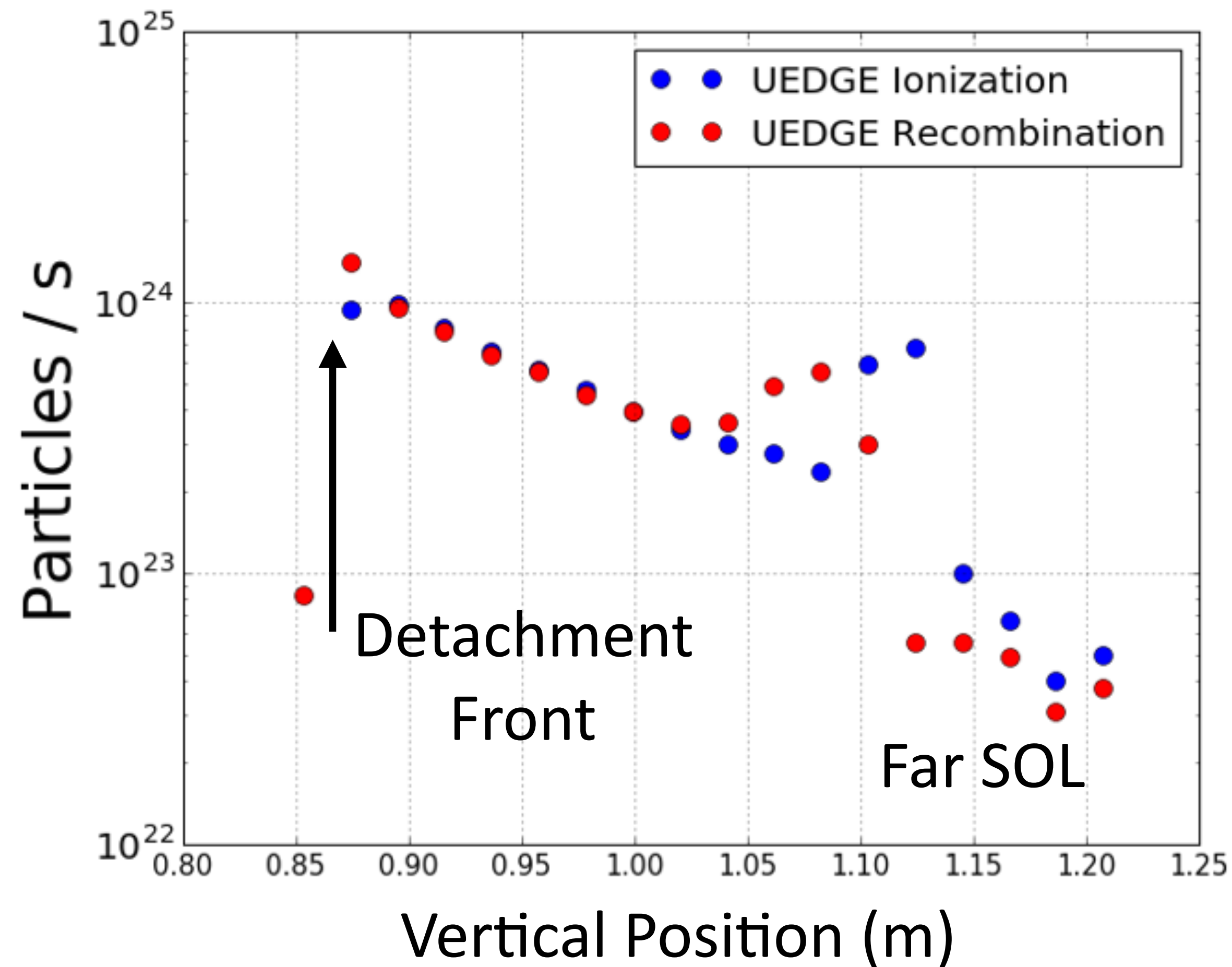
Localized  
evaporation,  
absorbing walls.

60 eV radiation  
per ionization

Divertor region  
heat flux  
All radiative!  
 $\sim 2 \text{ MW/m}^2$



# UEDGE Lithium Ionization & Recombination in Near Local Balance



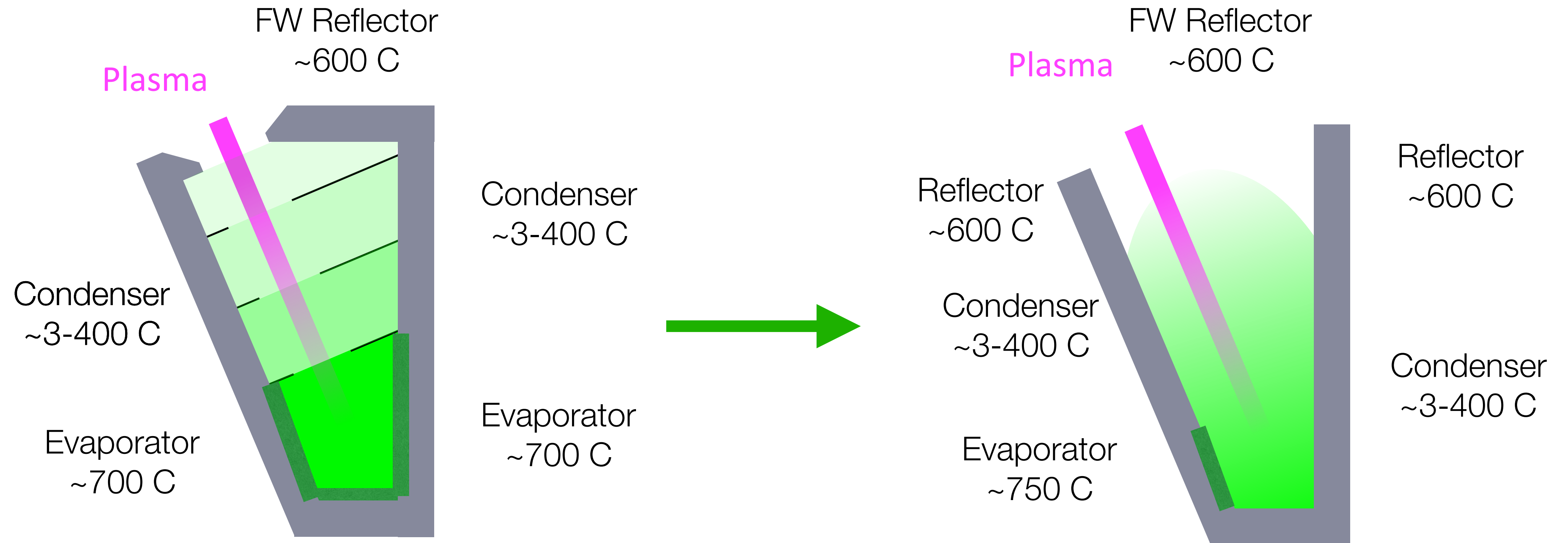
**Recombination roughly equals ionization at a given Z position.  
In effect, plasma acts like a mirror (with a cricket bat).**

# SPARTA Provides Alternative Model for Lithium Vapor, including Convection & Viscosity

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- Using SPARTA Monte-Carlo Direct Simulation code for lithium vapor
  - Li-Li collision model based on known vapor viscosity vs.  $T$ .
  - Model evaporation and condensation based on known equilibrium Li pressure vs.  $T$ , and Langmuir fluxes from surfaces.
- Lithium – Plasma interaction
  - Assume absorption of lithium at  $T_e = 0.2$  eV
  - Recombination at the same point.
    - Lithium leaves along B with  $T_{Li} = E_{||,Li} = 0.2$  eV

# A Simplified Lithium Vapor Box Divertor Based on UEDGE Results



**Allows more Li efflux, but needs less total evaporation**  
**Makes experimental implementation easier,**  
**including starting with a toroidal segment**

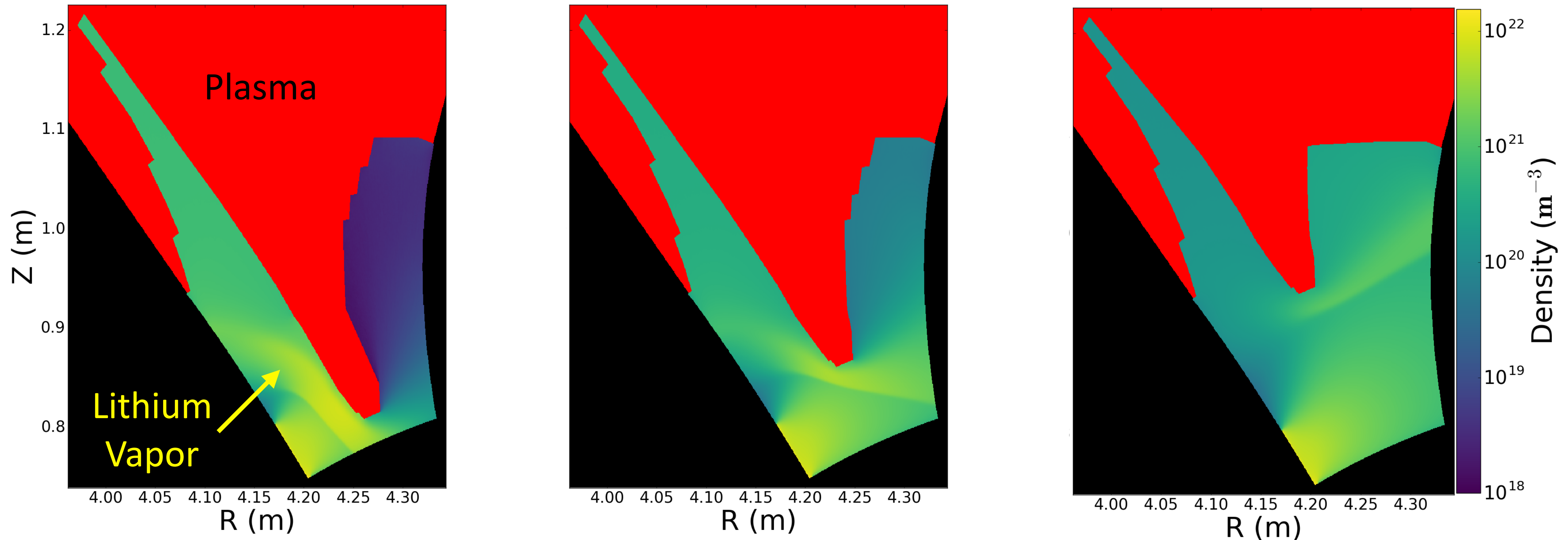


# **Lithium Accumulation on First Wall will be Very Low**

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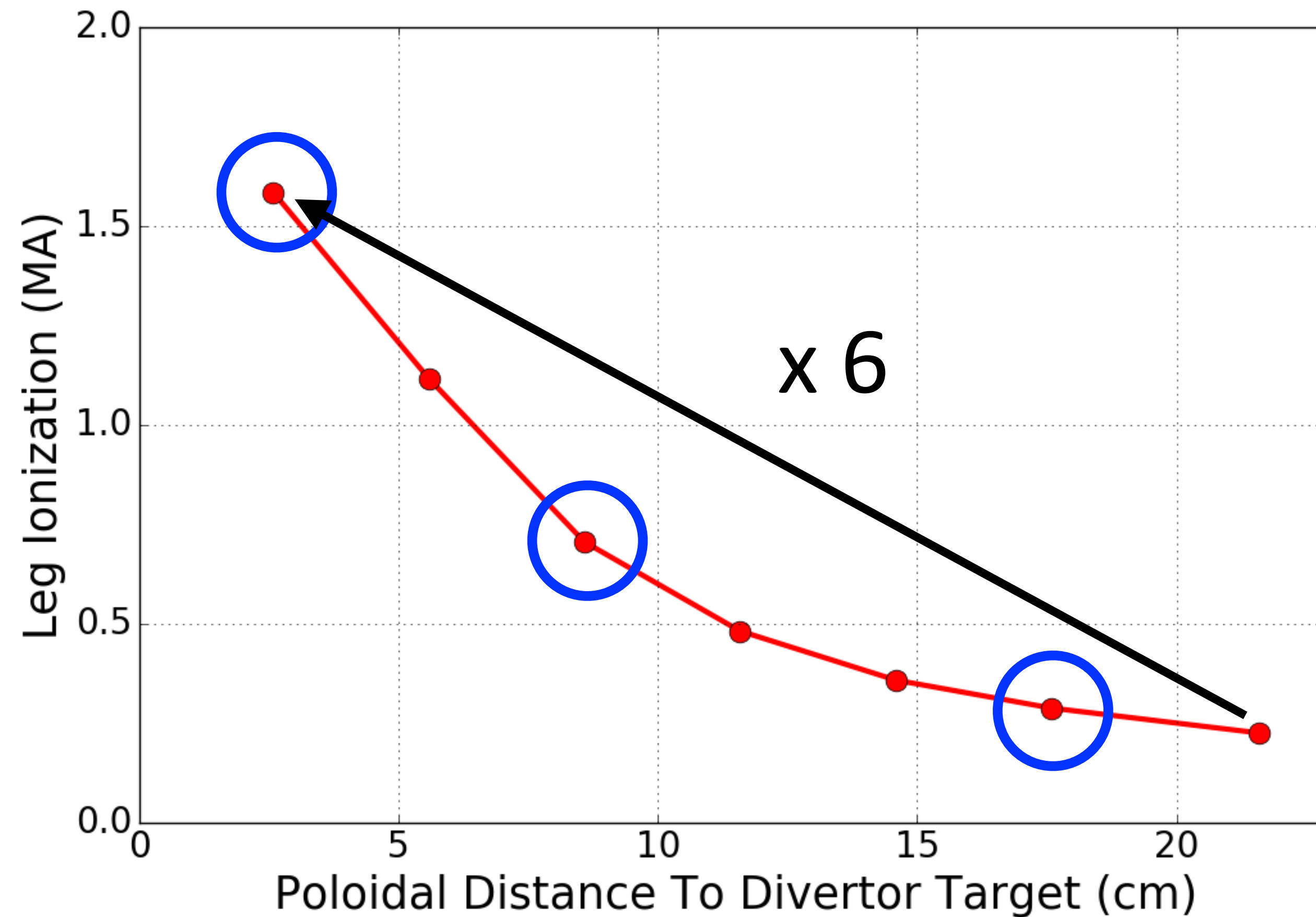
- **140 g/s of lithium evaporated for  $P_{\text{rad}} = 66$  MW.**
- **Assume all of this is deposited on first wall,  $T_w \sim 600$  C.**
- **Evaporation rate at 600 C = 2.66 g/s/m<sup>2</sup>**
- **Area of first wall  $\sim 300$  m<sup>2</sup>**
- **Total evaporation rate with multi-monolayer surface coverage = 800 g/sec**
- **Can't even accumulate a few monolayers of Li**
- **LiH decomposes in  $\ll 1$  sec at 600 C.**

# SPARTA Shows Strong Variation in Lithium Absorption with Detachment Vertical Position



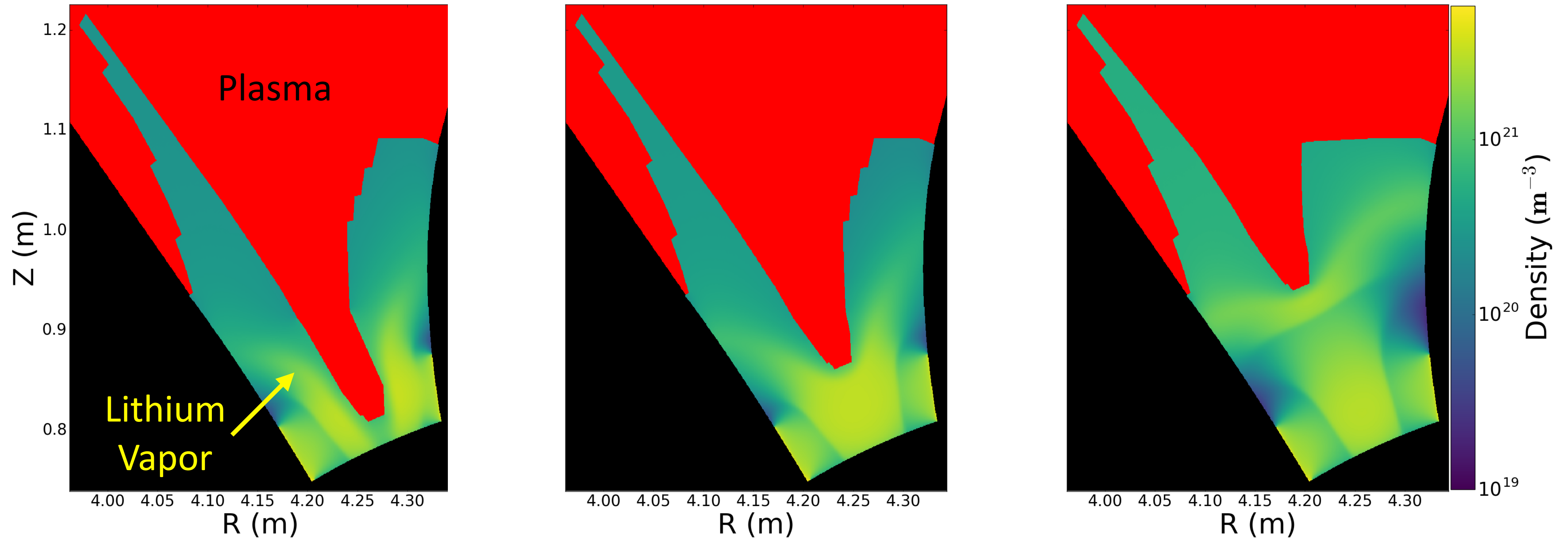
**Lithium evaporation from private flux side is much more efficient when leg is closer to evaporator.**  
**(Does not include radiative heating of evaporator.)**

# SPARTA Gives Very High Positional Resilience



**Lithium injection from private flux side is much less efficient as leg moves away from evaporator → Positional resilience. (Does not include change in radiative heating of evaporator.)**

# Two-Sided Injection Has Low Resilience



**Little variation in Li absorption as leg moves away from evaporators. Same low resilience with bottom evaporation.**

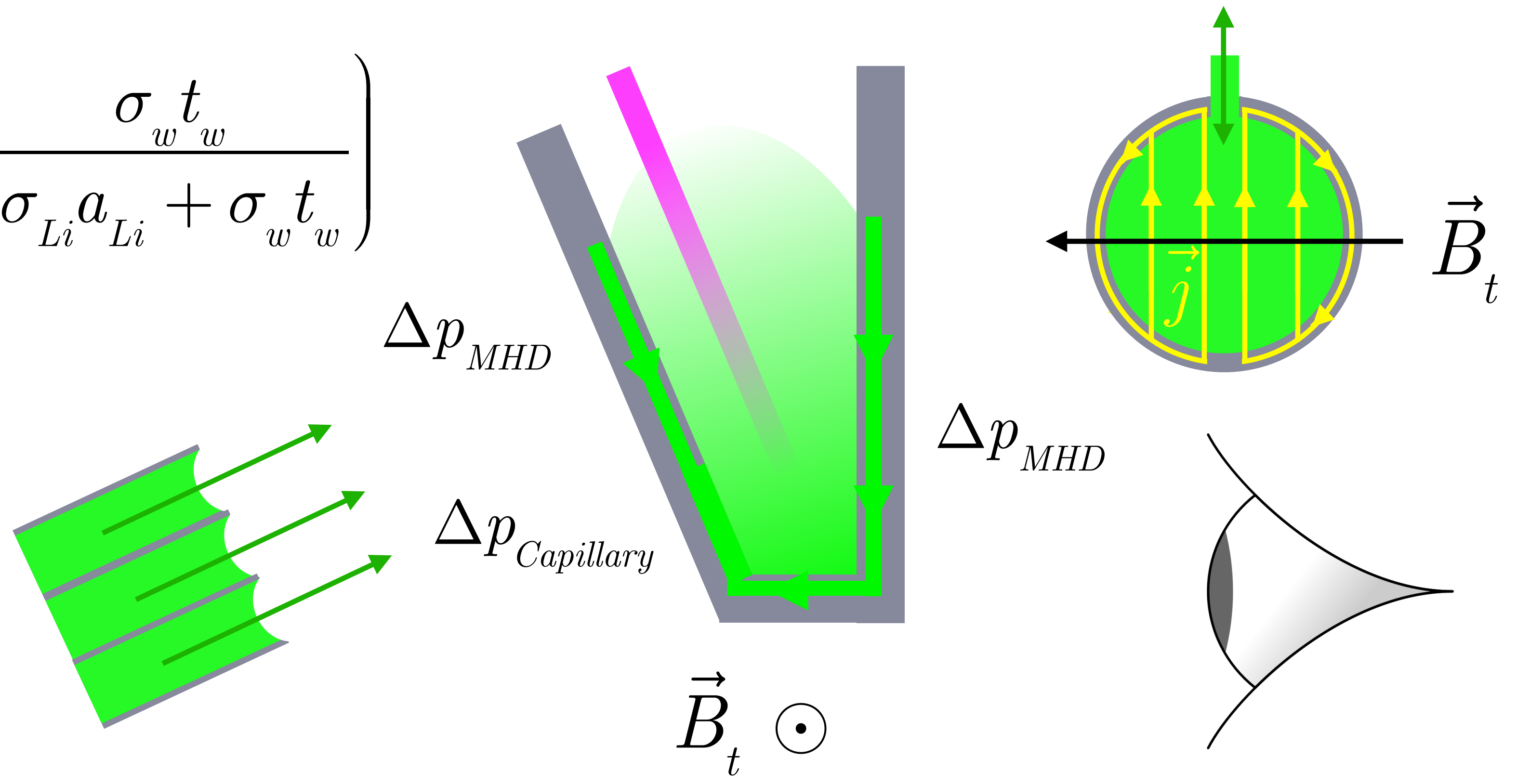
# Lithium Return Flow is Determined by Balance between Capillary Pull & MHD Drag

$$\Delta p_{Capillary} = \frac{2\gamma \cos \alpha}{r_p} \geq \Delta p_{MHD} =$$

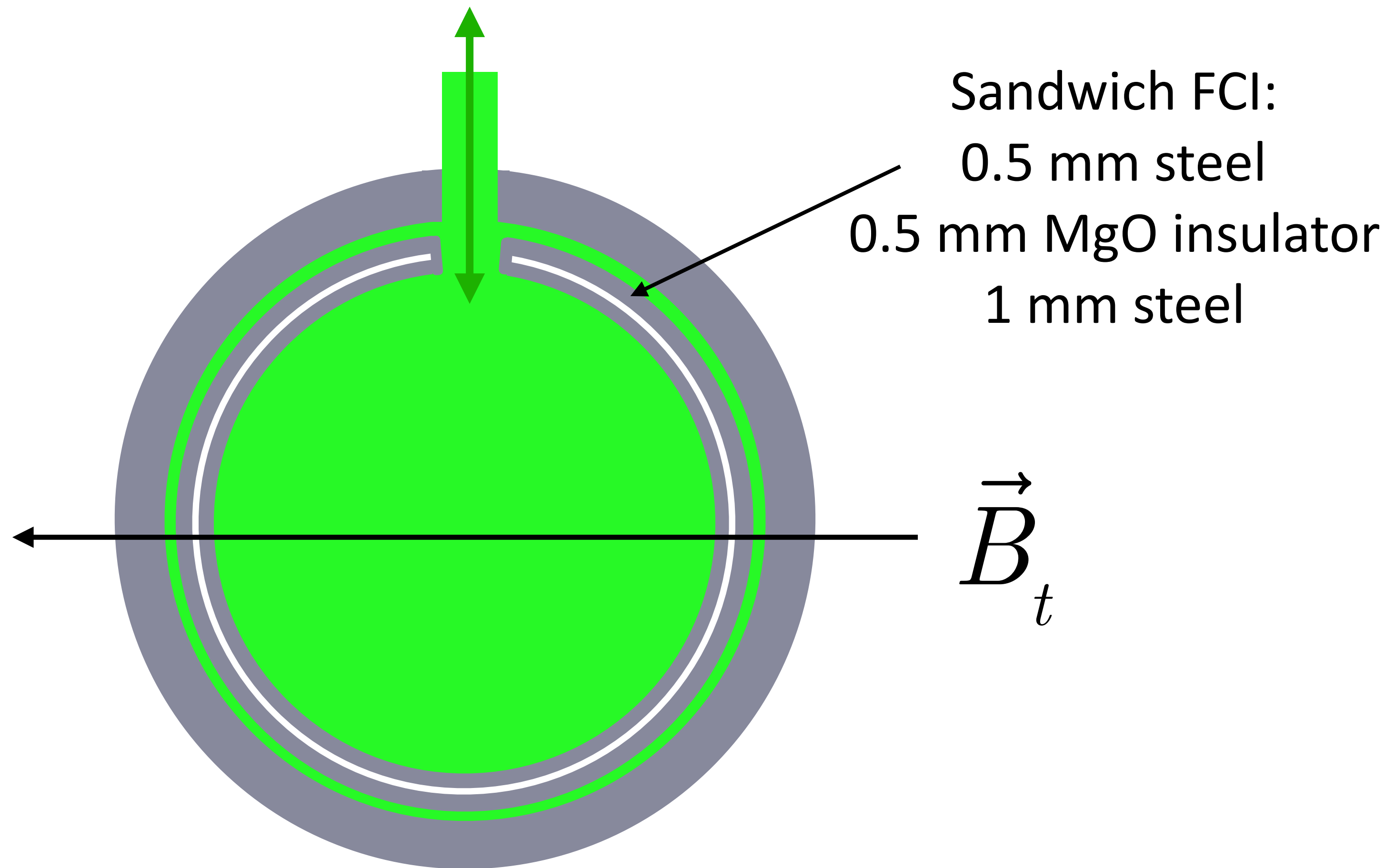
$$\int \vec{j}_{Li} \times \vec{B} \cdot d\vec{l} = \int v \sigma_{Li} B^2 dl \left( \frac{\sigma_w t_w}{\sigma_{Li} a_{Li} + \sigma_w t_w} \right)$$

$2a_{Li} = \text{pipe ID}$   
 $t_w = \text{wall thickness}$

$\gamma \equiv \text{surface tension}$   
 $\alpha \equiv \text{contact angle}$   
 $r_p \equiv \text{pore radius}$



# Sandwich Flow Channel Inserts Reduce $\Delta P_{MHD}$



*2 cm ID pipes spaced  
10 cm apart toroidally*

$$\Delta p_{MHD} = 0.22 \Delta p_{Capillary}$$

$$@ r_p = 40 \mu m$$

$$v \leq 2.9 \text{ mm/s}$$

$$\phi = 0.4 \text{ mV}$$

**Gap in Flow Channel Insert orients towards divertor surface.  
Works top and bottom, leaves margin for other effects.**

# Conclusions

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- **UEDGE predicts detachment in FNSF with Li alone, shows lithium dynamics at detachment front.**
- **This provides a preliminary physics basis to optimize Lithium Vapor Box Divertor using SPARTA.**
- **A divertor with private-flux-side lithium evaporation near the bottom of the divertor leg –**
  - **Provides adequate lithium for detachment.**
  - **Provides strong positional resilience of the detachment front, without baffles. No issue of Li accumulation on 600 C surfaces.**
  - **Sandwich Flow Channel Inserts facilitate capillary force to return 140 g/s of lithium across 7T magnetic field.**
- **Integrated modeling, design, & experiments are needed.**