



Real-time simulation of the NBI fast-ion distribution

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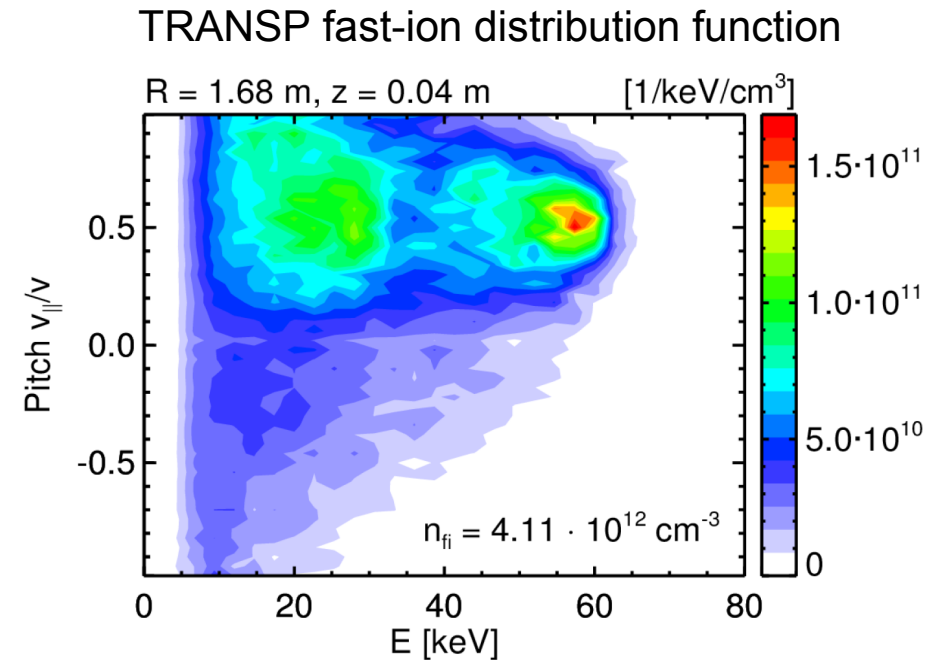
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Motivation:

- Fast ion distribution function is required for instance:
 - Heating profiles for transport calculations
 - pressure and current-drive for equilibrium reconstructions
- Sophisticated simulation codes exist (e.g. TRANSP/NUBEAM based on Monte Carlo), but long computation time (~ 30 s per time-step)
- \rightarrow Too slow for real-time applications (e.g. discharge control systems, real-time transport solvers like RAPTOR)
- \rightarrow Develop fast model
Rapid Analytical Based Beam Injection Tool – RABBIT [M. Weiland, NF 2018]
(~ 20 ms per time-step)



Kinetic equation for distribution function $f(x, v, t)$

$$\frac{\partial f}{\partial t} + \underbrace{\mathbf{v} \cdot \nabla_x f + \mathbf{a} \cdot \nabla_v f}_{\text{Orbit effects}} = \nabla_v \cdot \Gamma_c(f) + \text{Source}$$

Orbit effects

$$\mathbf{a} = \frac{q}{m} \left(\mathbf{E} + \frac{\mathbf{v}}{c} \times \mathbf{B} \right)$$

Time dependence
(=0 for steady state
solution)

collisions
(e.g. slowing down,
pitch angle scattering)

Source = NBI
deposition

Kinetic equation for distribution function $f(x, v, t)$

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3. Orbit effects

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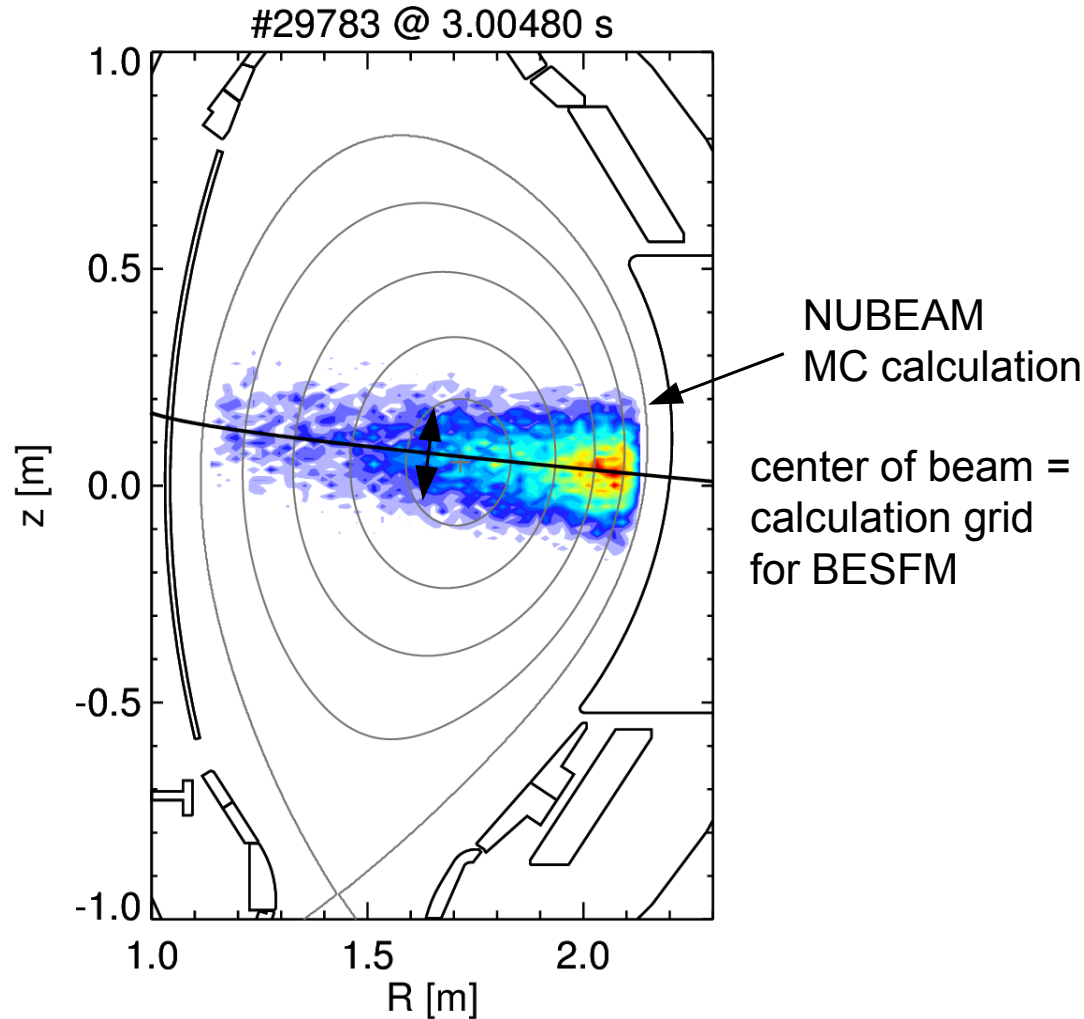
4. Time dependence
(=0 for steady state solution)

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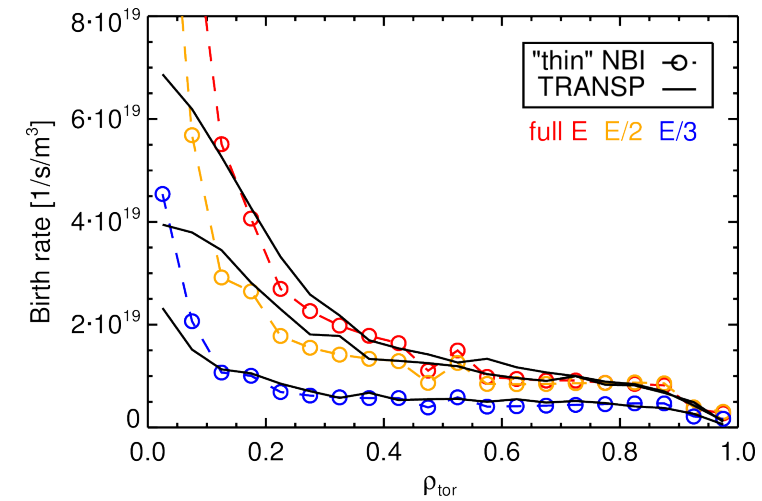
1. Source = NBI
deposition

5. Applications

Beam deposition (birth profile)

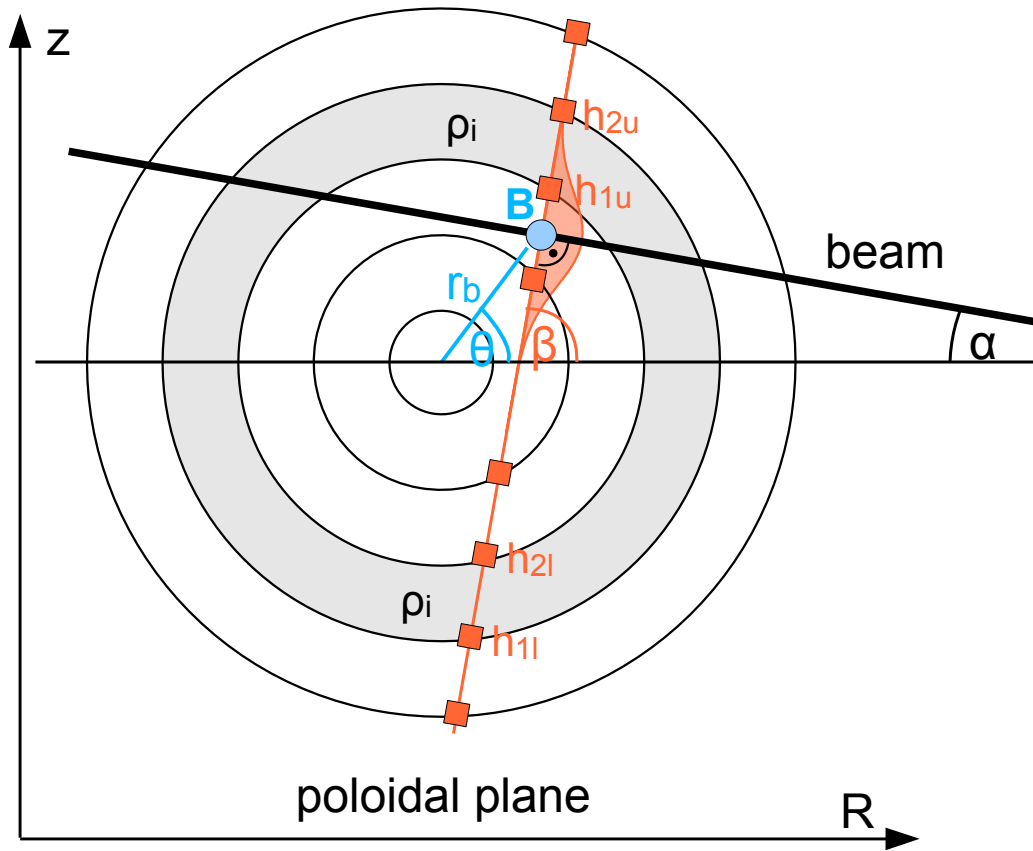


- Injection of fast neutrals into the plasma → Ionization → newly “born” fast ion
- Fast-ion birth rate = - (beam attenuation rate)
- Calculation of beam attenuation:
BESFM Code by A. Lebschy, R. Dux, IPP
- We use the simplest geometry: NBI as thin line
- Good approximation for attenuation – for birth profile, we need to take into account the beam width:



- Assume a Gaussian broadening with standard deviation $\sigma(l)$, l = coordinate along beam, $\sigma(l)$ defined by NBI parameters (e.g. divergence)

Analytic model for the poloidal beam width



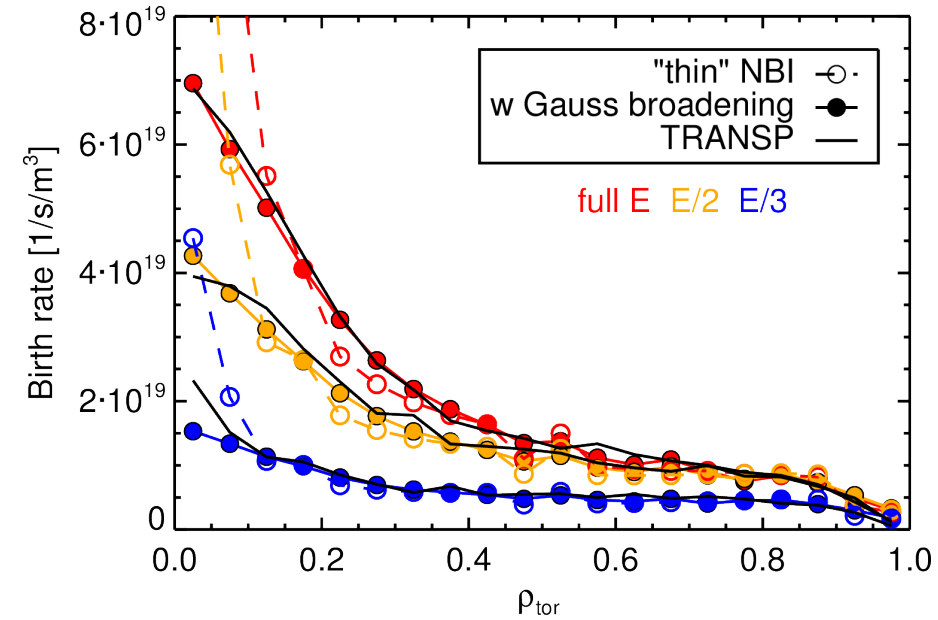
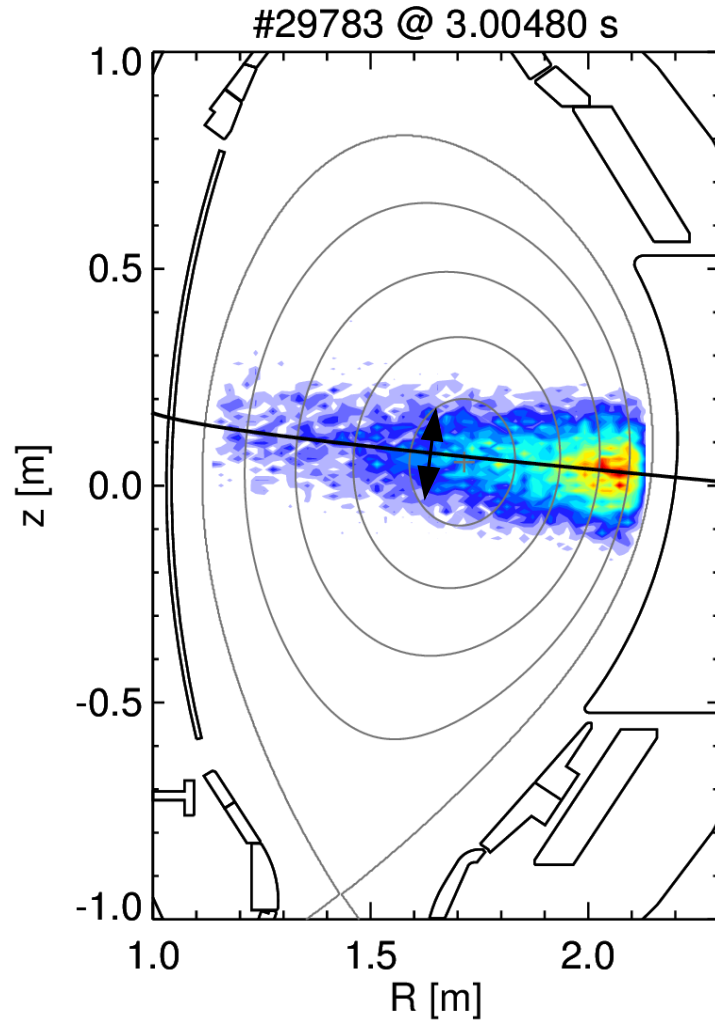
- We assume Gaussian spreading along orange line (standard deviation σ)
- Assume circular concentric flux surfaces
- Transformation between flux coordinate ρ and geometric radius r based on ratio at **B**:
 $r(\rho) = \rho * (r_b / \rho_b)$
- → Crossings \blacksquare with ρ -cells can be calculated analytically
- → Contribution into i -th cell ρ_i :

$$\frac{1}{2} \left(\operatorname{erf} \frac{h_{2u}}{\sqrt{2}\sigma} - \operatorname{erf} \frac{h_{1u}}{\sqrt{2}\sigma} \right) + \frac{1}{2} \left(\operatorname{erf} \frac{h_{2l}}{\sqrt{2}\sigma} - \operatorname{erf} \frac{h_{1l}}{\sqrt{2}\sigma} \right)$$

- Correction for plasma elongation:
 Scale beam width σ according to elongation b/a at **B**.

$$\sigma = \sigma_0 \cdot \sqrt{\frac{(a \cos \theta)^2 + (b \sin \theta)^2}{(a \cos \beta)^2 + (b \sin \beta)^2}}$$

Beam deposition (birth profile) with beam-width correction



- Taking into account a Gaussian broadening of the beam leads to good agreement with TRANSP/NUBEAM

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(=0 for steady state solution)

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(e.g. slowing down, pitch angle scattering)

1. Source = NBI deposition

5. Applications

Analytic solution of the Fokker-Planck equation

$$\frac{1}{\tau_s v^2} \frac{\partial}{\partial v} [(v^3 + v_c^3) f] + \frac{\beta v_c^3}{\tau_s v^3} \frac{\partial}{\partial \xi} (1 - \xi^2) \frac{\partial f}{\partial \xi} + \frac{1}{\tau_s v^2} \frac{\partial}{\partial v} \left[\left(\frac{T_e}{m_{fi}} v^2 + \frac{T_i}{m_{fi}} \frac{v_c^3}{v} \right) \frac{\partial f}{\partial v} \right] = \frac{\partial f}{\partial t} - \frac{S}{2\pi v^2} \delta(v - v_0) K(\xi)$$

slowing down

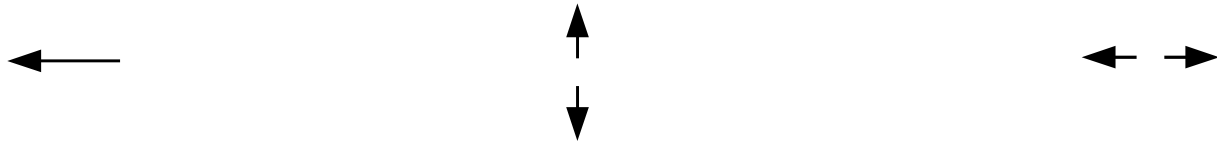
pitch angle scattering

speed diffusion

source term

S: deposition, v0: injection velocity (mono-energetic)

K(ξ): broad pitch distribution



• Solution [Cordey/Core 74]:

Legendre polynomials

$$f(v, \xi) = \frac{1}{2\pi} \frac{S \cdot \tau_s}{v^3 + v_c^3} \cdot \sum_{l=0}^{\infty} \left(l + \frac{1}{2} \right) u^{l(l+1)} P_l(\xi) K_l \cdot H(v_0 - v)$$

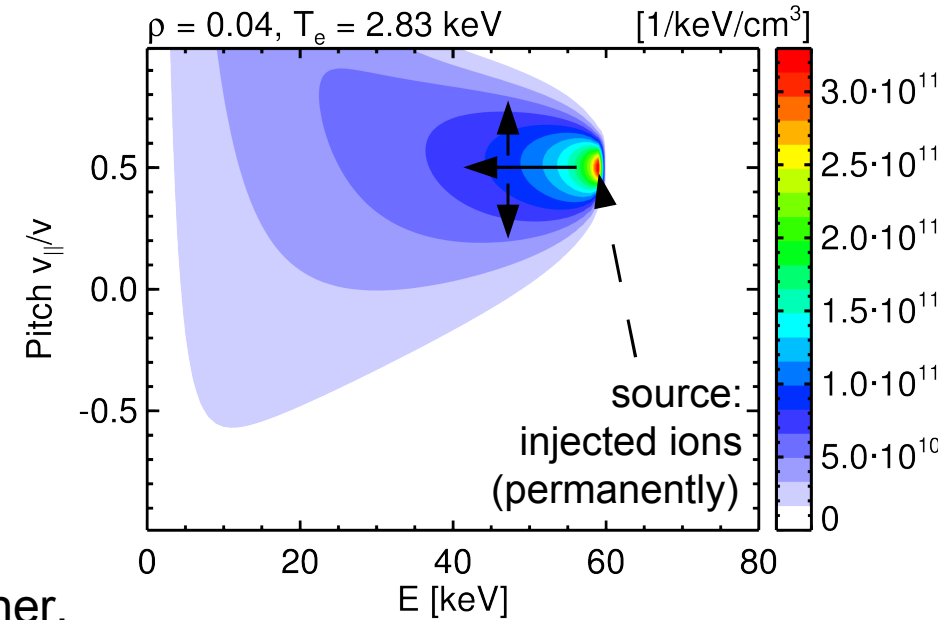
v_c, v_0 : critical, injection velocity

$$K_l = \int K(\xi) P_l(\xi) d\xi$$

$$\tau_s = 6.27 \cdot 10^8 \cdot \frac{A_b}{Z_b^2 \ln \Lambda_e} \cdot \frac{(T_e [\text{eV}])^{3/2}}{n_e [\text{cm}^{-3}]} \text{ s}$$

$$u = \left(\frac{v_0^3 + v_c^3}{v^3 + v_c^3} \frac{v^3}{v_0^3} \right)^{\pm \beta/3} \quad \beta = \frac{Z_{\text{eff}}}{2} \frac{m_i}{m_{\text{beam}}}$$

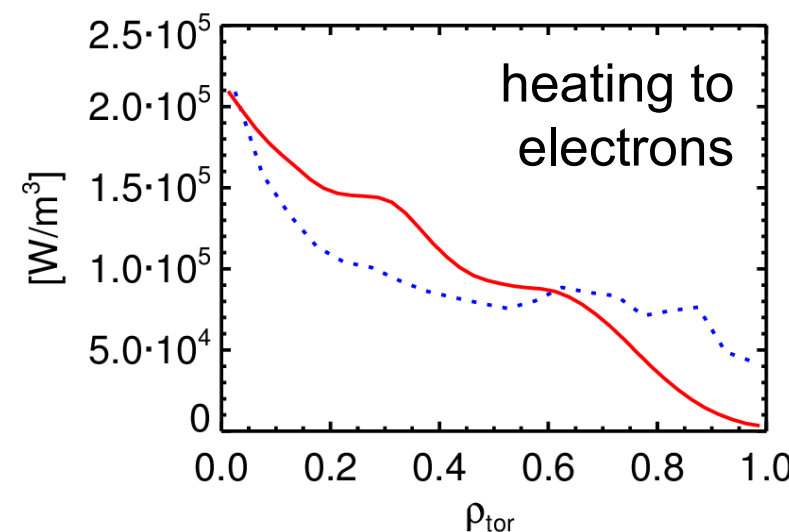
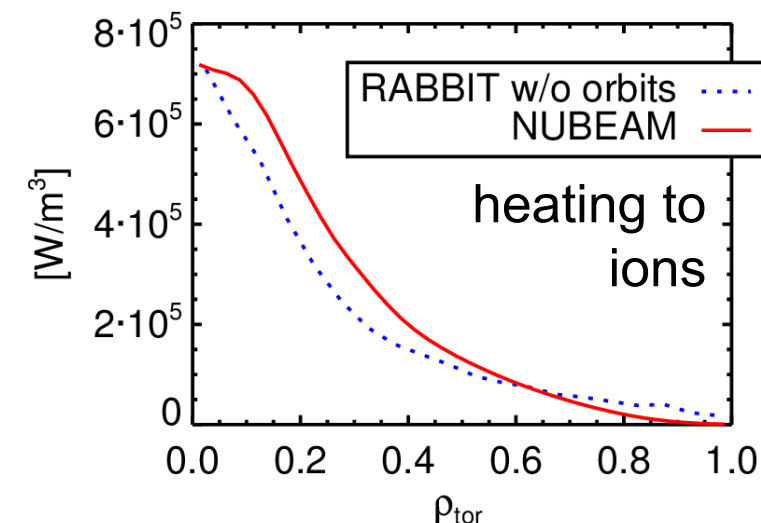
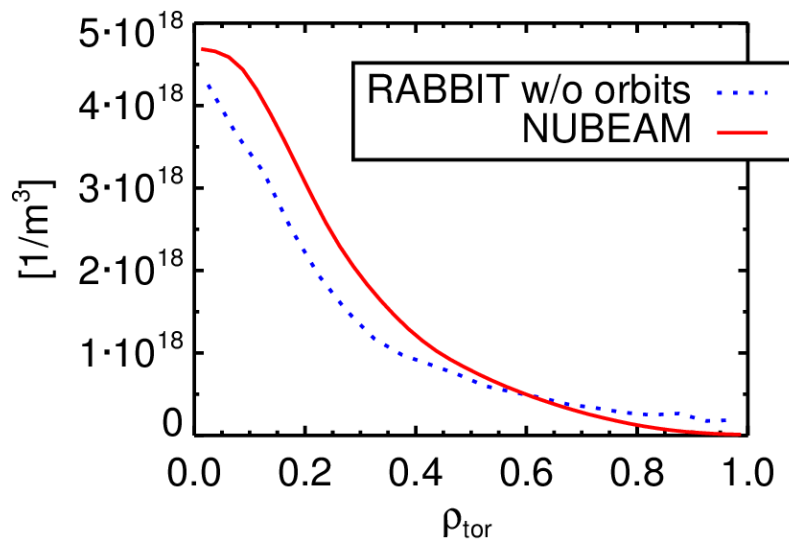
$$v_c^3 = 1.51 \cdot 10^{14} \cdot (T_e [\text{eV}])^{3/2} \cdot \frac{\sum_i n_i Z_i^2 \ln \Lambda_i / A_i}{n_e \ln \Lambda_e}$$



- Uniform plasma solution, i.e. each radial cell is independent of each other, no particle trapping etc.
- A correction for speed diffusion is applied above injection energy.

Density and heating profiles

- In the end we are interested in integrals of f , e.g.:
Heating power (to electrons and ions), fast-ion pressure and current drive
- These integrals can also be solved analytically. Due to orthogonality of the Legendre polynomials, only first few moments are necessary ($l=0, 1$)
- E.g. fast-ion density: $n_{fi} = \iint 2\pi v^2 \cdot f(v, \xi) dv d\xi = \frac{S\tau_s}{3} \ln\left(\frac{v_0^3 + v_C^3}{v_C^3}\right)$



- Profile shapes do not (yet) agree well, due to missing orbit-effects
- Under-estimation in the core, over-estimation at the edge

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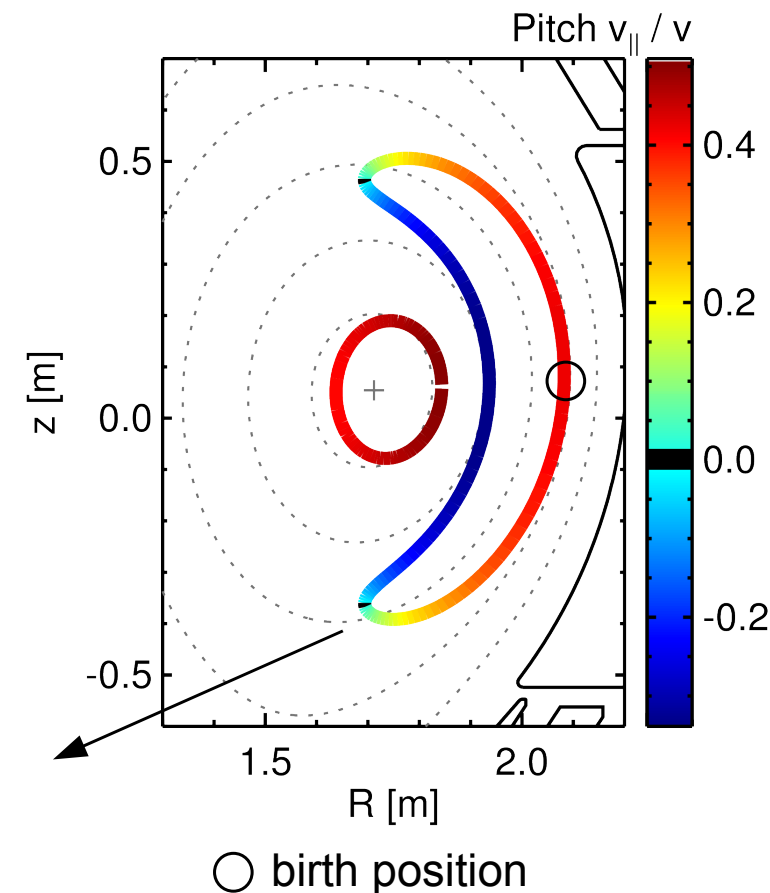
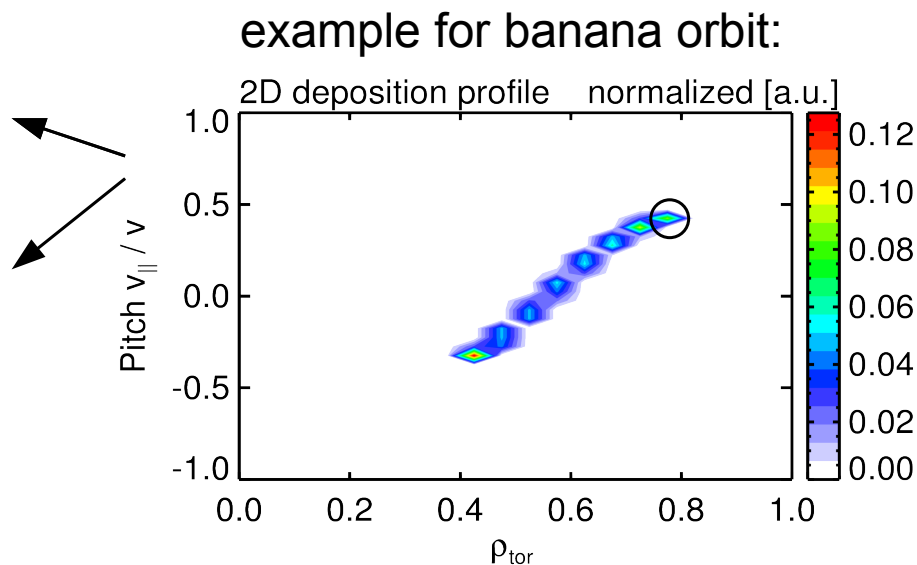
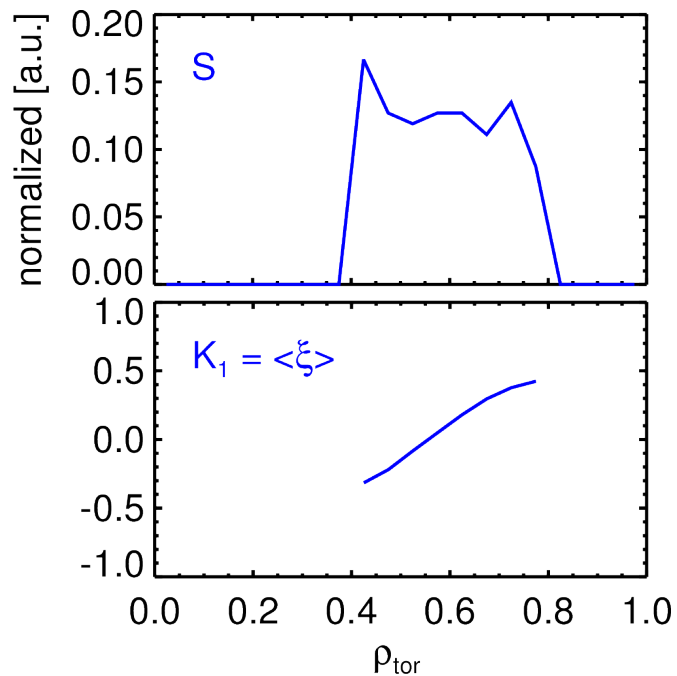
1. Source = NBI
deposition

- In MC codes (e.g. NUBEAM)
 - MC representation of source
 - Calculate orbits for each MC marker
 - Apply collision operator during orbit steps
- For real-time: Only ad-hoc treatment of orbit effects possible

5. Applications

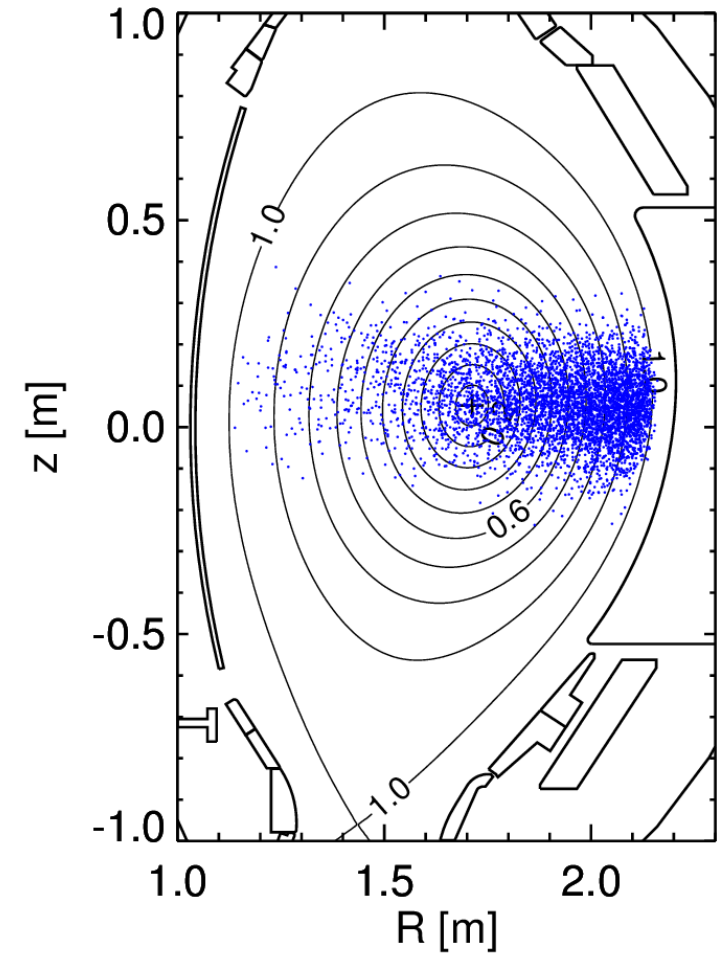
How to include the effect of first fast-ion orbit

- Orbit effects lead to a broadened deposition (towards the plasma center) and to changes of the pitch-distribution in the velocity space
- They can be taken into account, by averaging the deposition over the first orbit:
 - assume that slowing-down process starts on random position of first orbit
 - neglect orbit effects during slowing down



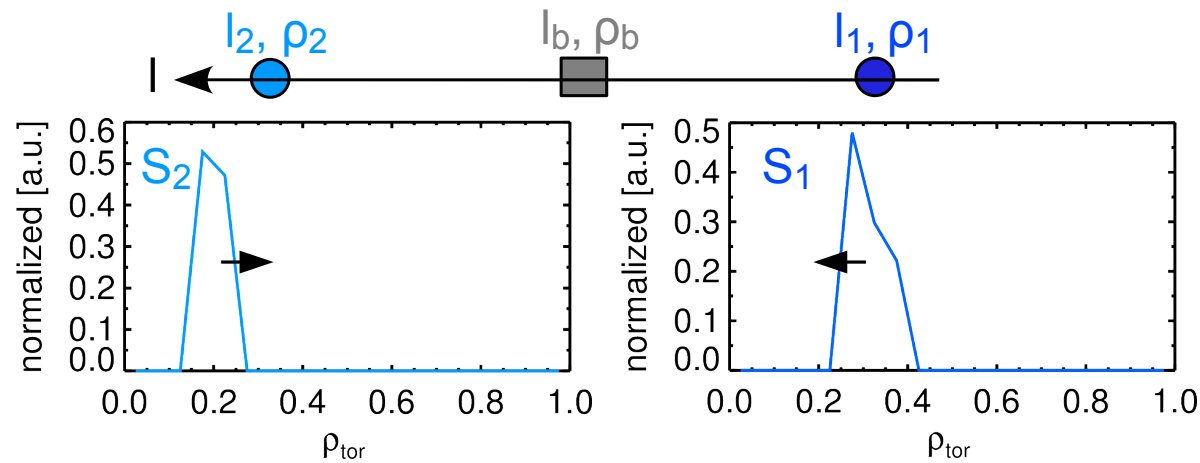
Monte-Carlo orbit-average is too slow for real-time applications

- Monte-Carlo orbit-average:
 - Take MC representation of birth distribution
 - Calculate orbit for each MC marker (e.g. ~5000)
 - → too slow for real-time purposes (takes ~1s)
- Possible solutions:
 - Either: Use approximation formulas for the orbits
 - Or: Reduce number of orbits (strongly)

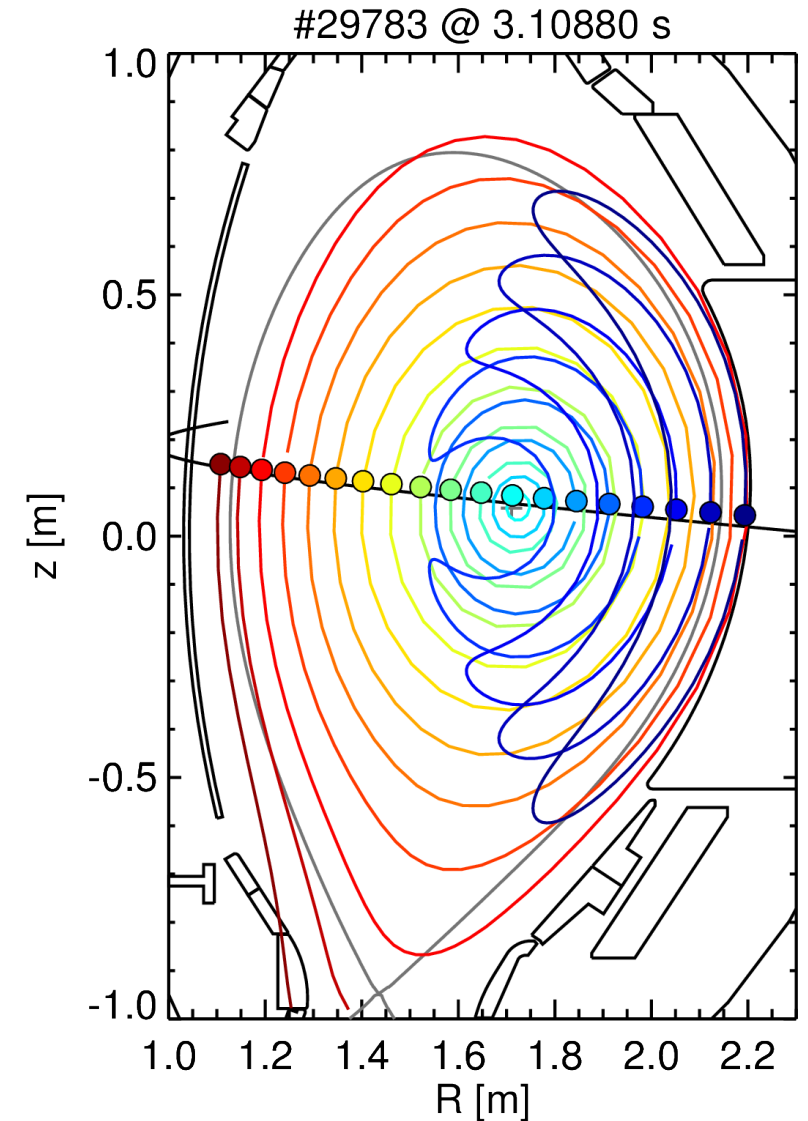


Orbit average in real-time

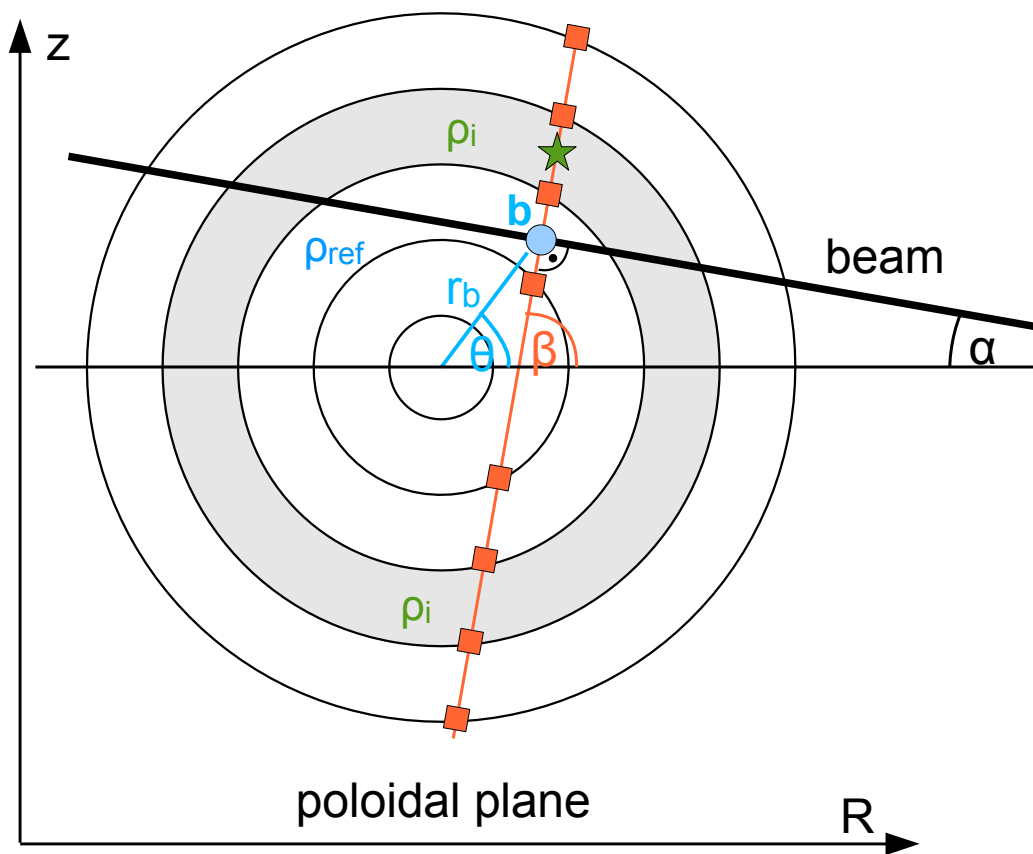
- Calculate orbit only every n-th grid point (4th order Runge-Kutta guiding center integrator)
Right: All calculated orbits for full energy component
- Here: 19 orbits x 3 energy components
→ possible within ~12 ms.
- In between: Shift neighboring profiles and interpolate linearly



$$S_b(\rho) = S_1(\rho - (\rho_b - \rho_1)) \cdot \frac{l_2 - l_b}{l_2 - l_1} + S_2(\rho - (\rho_b - \rho_2)) \cdot \frac{l_b - l_1}{l_2 - l_1}$$

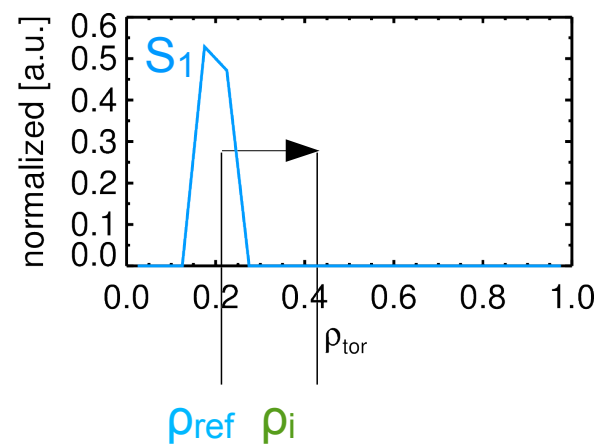


Orbit-average: compatible with beam-width model



- Up to now, we have calculated the orbit-average along the beam (at b).
- For the beam-width correction, we need to extrapolate from the ρ -cell containing b (ρ_{ref}) along the orange line to other radial cells
- E.g. from ρ_{ref} to \star (ρ_i):

$$S_i(\rho) = S_b(\rho - (\rho_i - \rho_{ref}))$$
 (similar to the interpolation method)

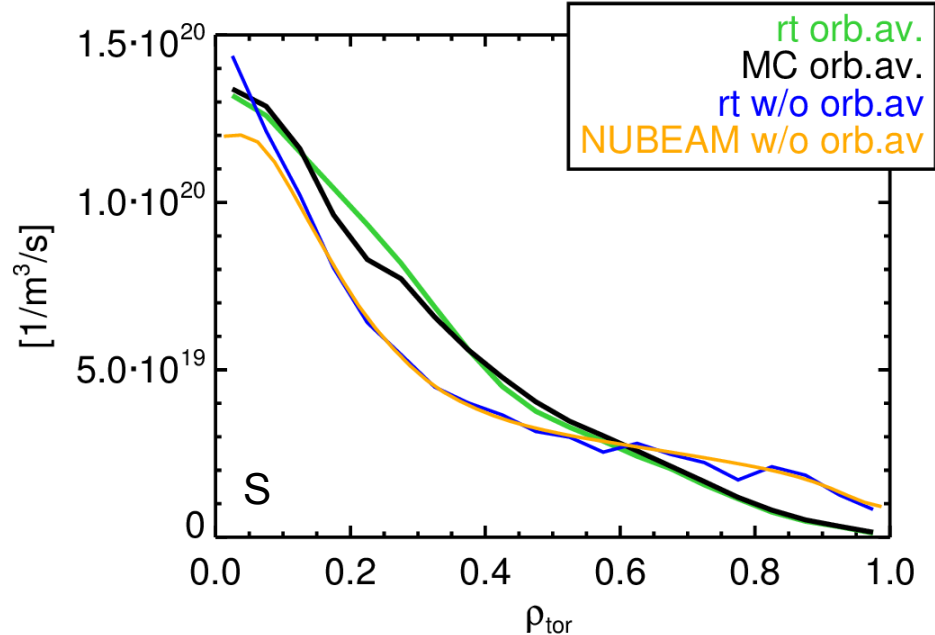


Results of „RABBIT orbit average“ in good agreement with MC orbit average

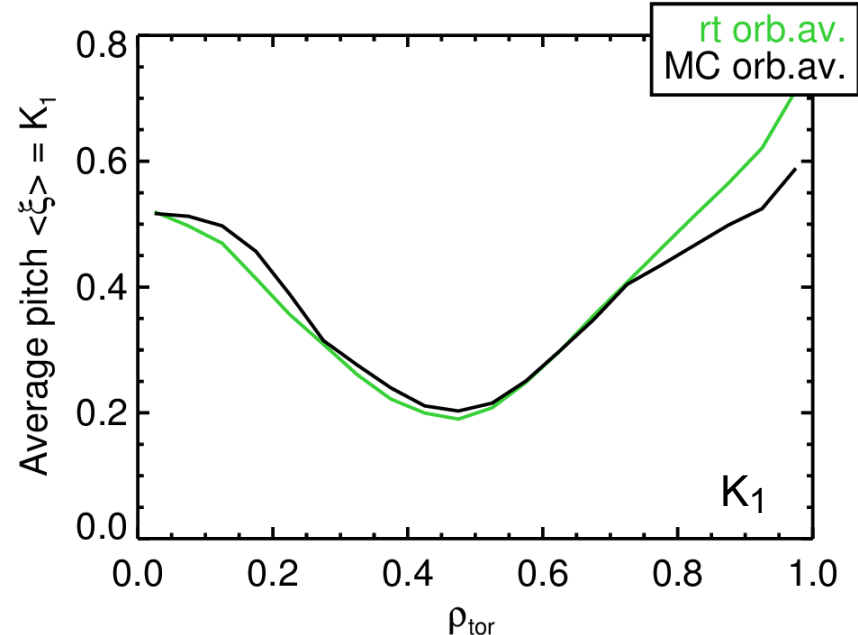


- Test accuracy of the RABBIT rt orbit average:
Compare it to Monte-Carlo orbit average (including fully realistic NBI geometry)
- Very good agreement is found, despite orders of magnitude difference in calculation time (~5000 orbits vs. ~60 orbits)

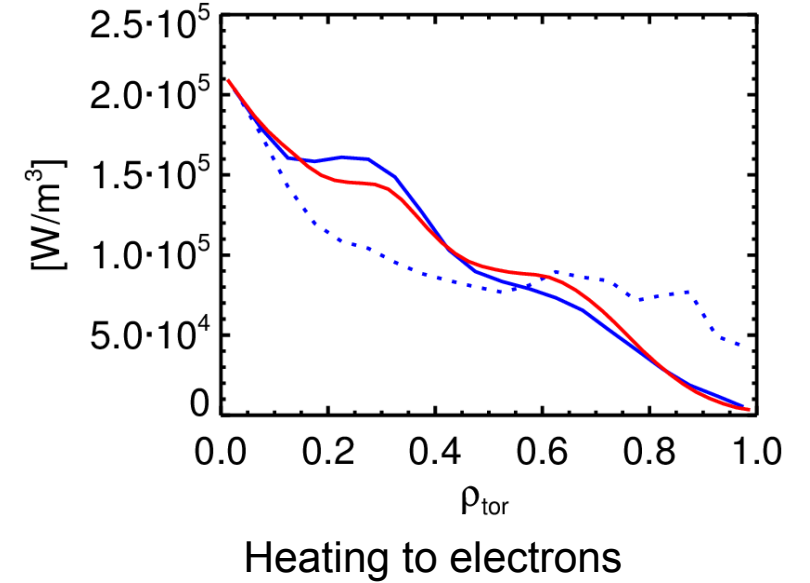
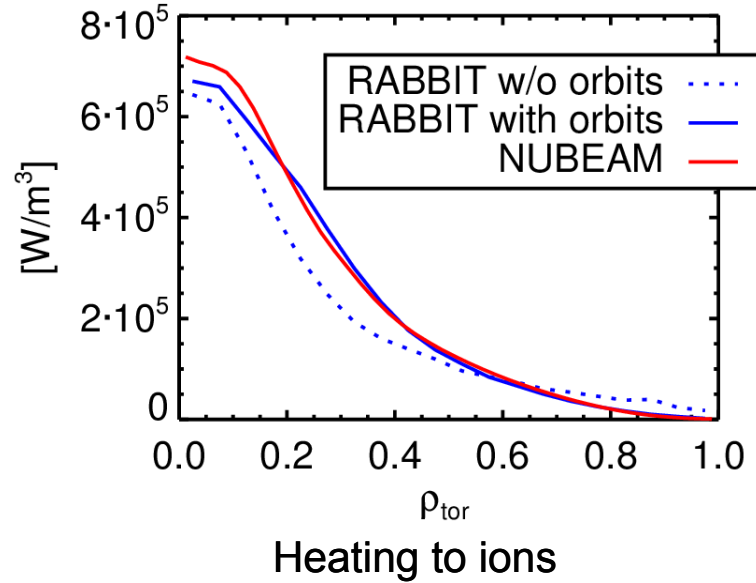
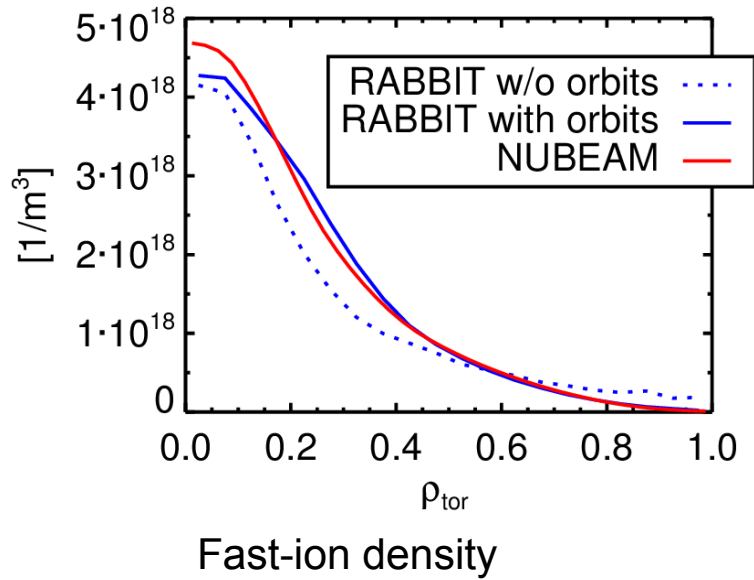
Birth profile (sum over all E components):



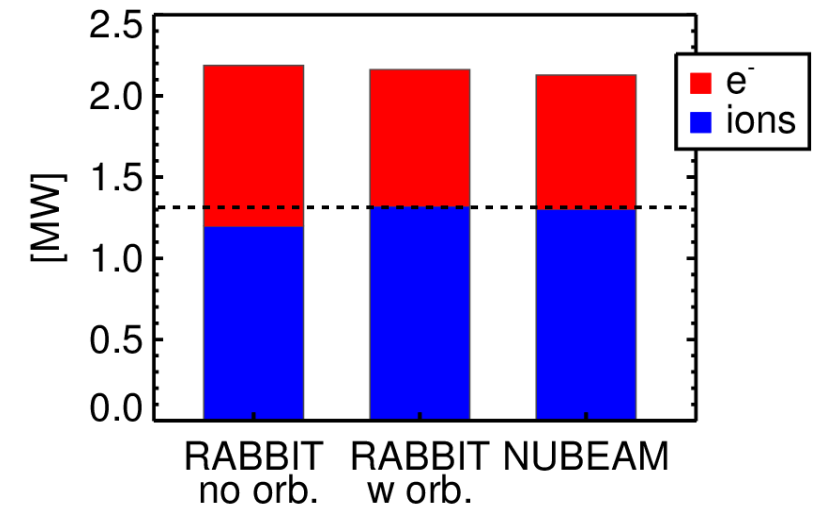
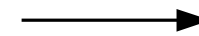
Average pitch $v_{||}/v$ of full-E component:



Comparison to NUBEAM



- Orbit-average leads to good agreement in profile shape
- Slight deviations remain in plasma center, affecting only small fraction of plasma volume
- Orbit-average has also an impact on volume-integrated heating distribution to electrons/ions and improves agreement



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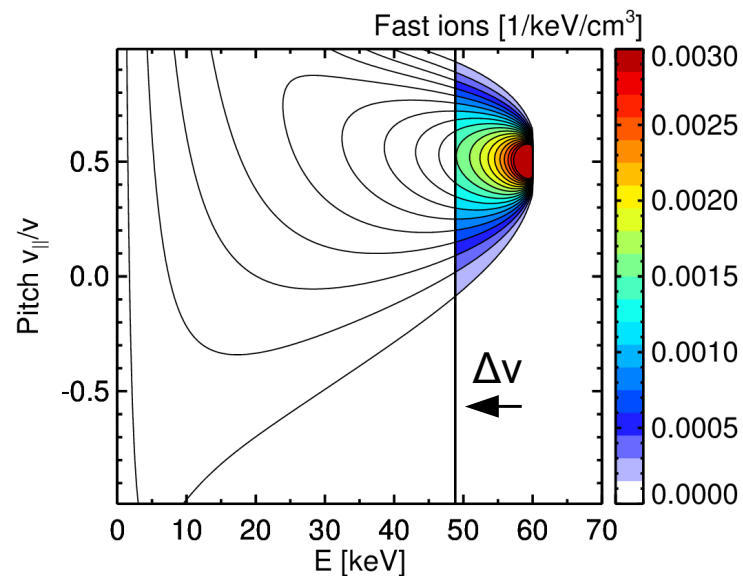
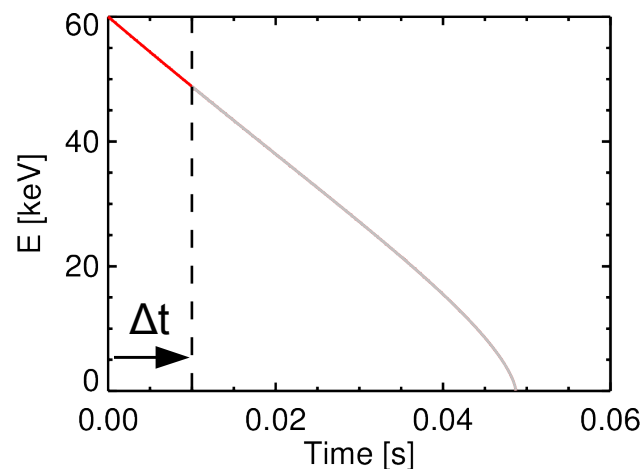
5. Applications

Time dependence

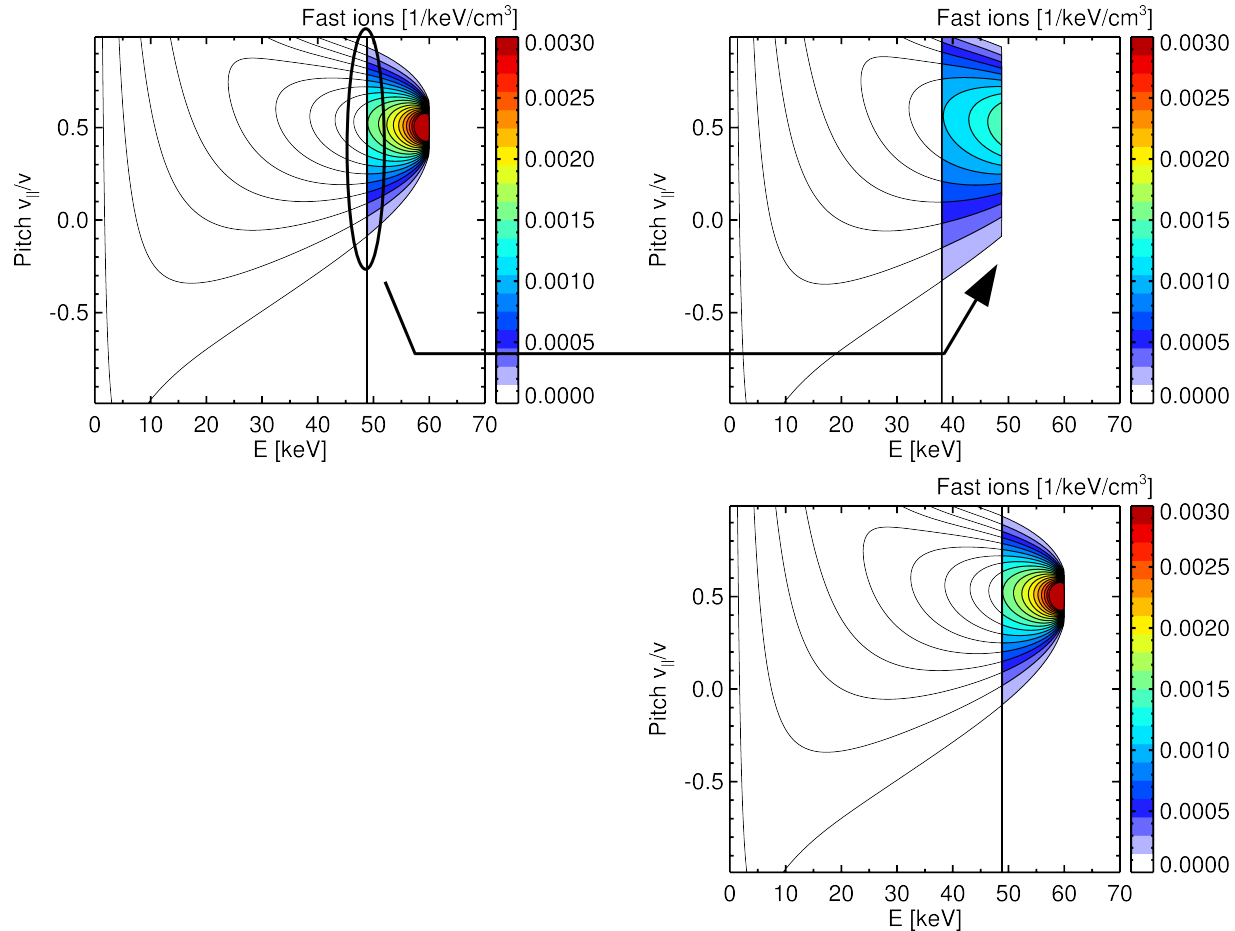
- For time-dependent simulation: Discrete time steps Δt
- Calculate how far the fast-ions slow down during time-step:

$$v_{\text{final}}^3 = (v_{\text{start}}^3 + v_c^3) \cdot \exp\left(\frac{-3 \cdot \Delta t}{\tau_s}\right) - v_c^3$$

→ multiply steady state solution with box function



Time dependence via train of fast-ion pulses



• Final state of „step 1“ is starting point of „step 2“

...

• If beam is still turned on in „step 2“, add a new pulse at nominal injection energy

...

• continue ...
(add new rows each time-step, sum over rows)

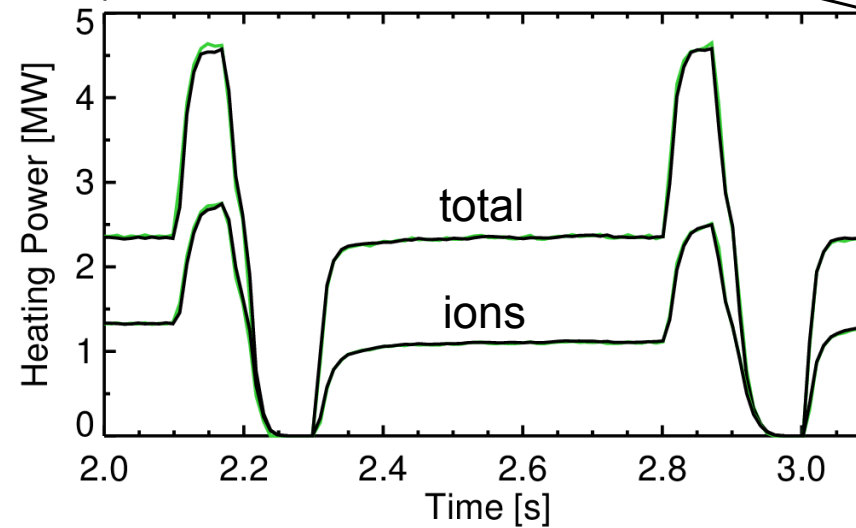
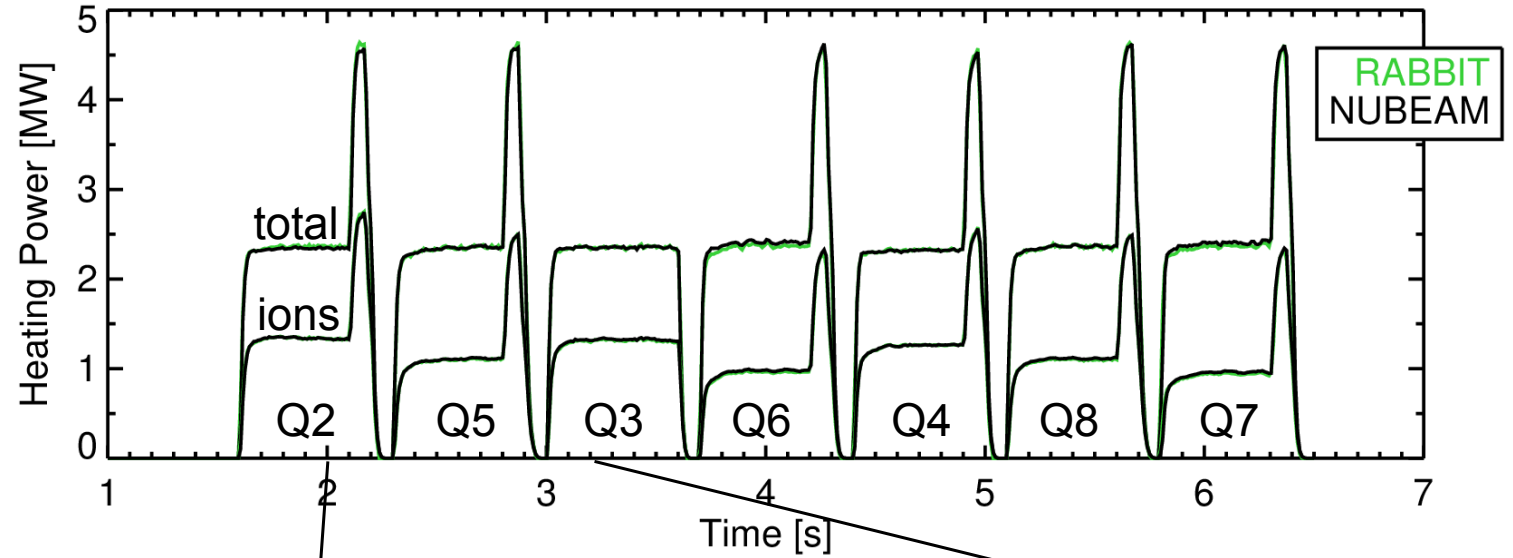
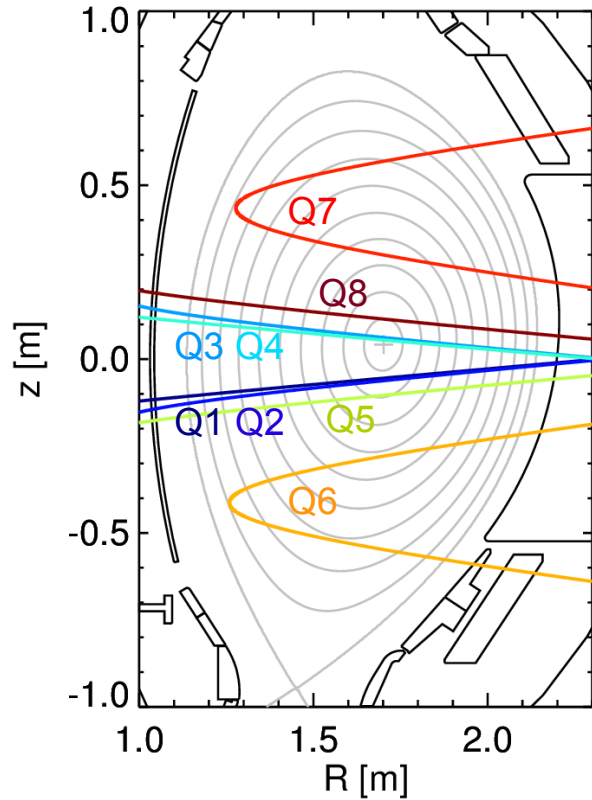
...

Time step 1

step 2

Comparison of time evolution with NUBEAM

- Analyze discharge where different NBI sources (Q#) are interchanged
- Good agreement of temporal evolution



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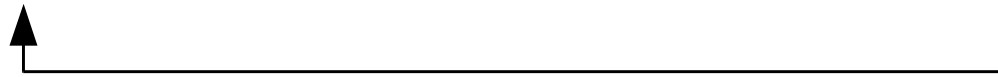
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RABBIT for equilibrium reconstructions with the IDE code

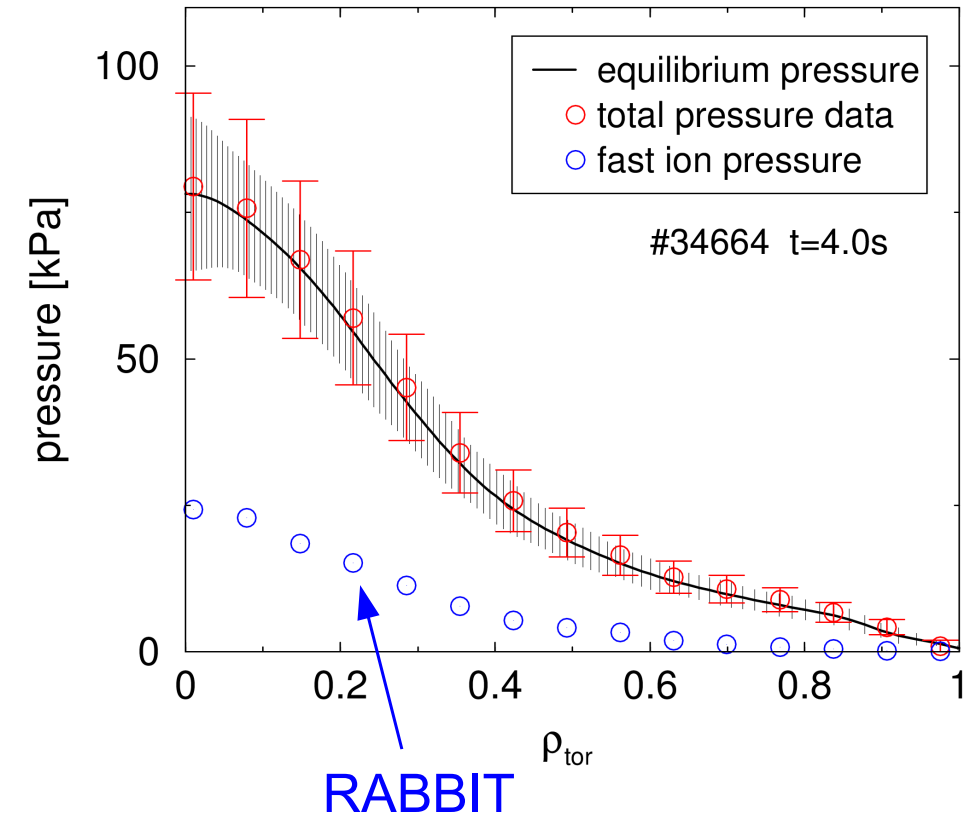


Equilibrium reconstruction: Solve Grad-Shafranov-Schlüter equation for ψ :

$$\Delta^* \psi = R^2 \mu_0 \frac{dp}{d\psi} + F \frac{dF}{d\psi}$$



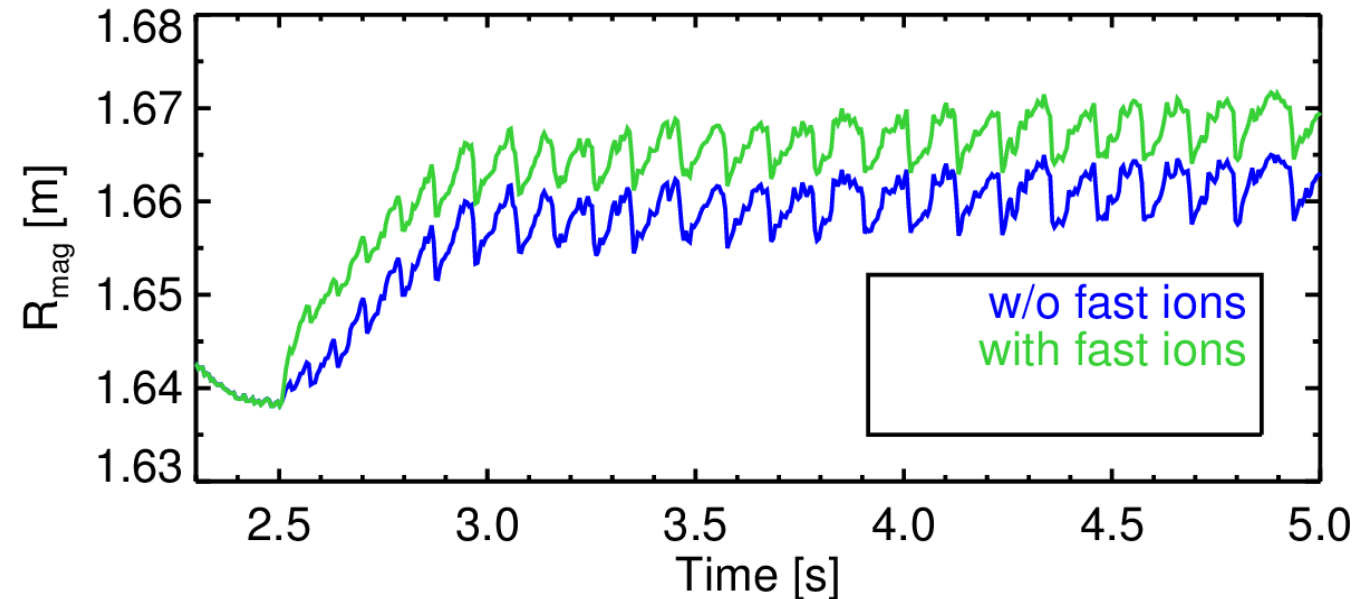
- IDE code: Equilibrium reconstruction based on integrated data analysis [R. Fischer, 2016, FST]
- Fast-ions from NBI can contribute significantly to the **pressure** $p(\psi)$
- Neutral beam **current** drive is relevant for current diffusion equation
- With RABBIT these profiles can be calculated routinely and also directly after the discharge



RABBIT for equilibrium reconstructions with the IDE code



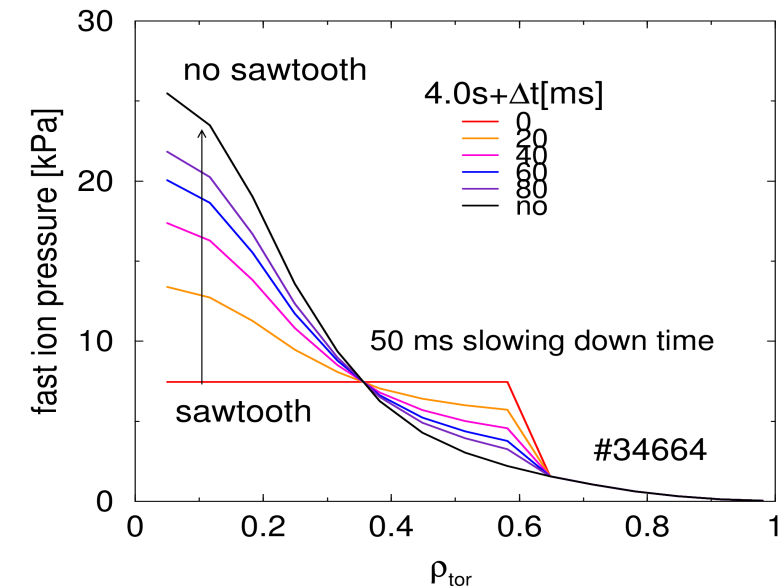
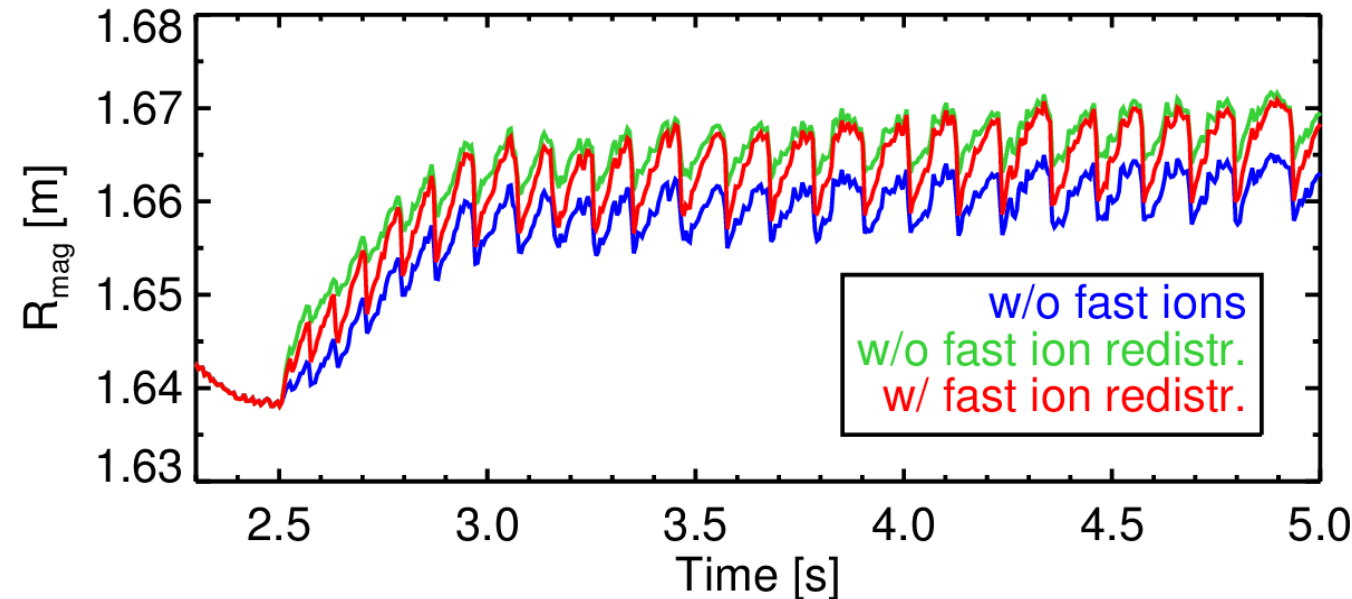
- Fast-ion pressure
 - increases Grad-Shafranov shift
 - correction for magnetic axis
- Relevant for correct interpretation of diagnostics (e.g. MSE)
- In this case: Sawtoothing plasma, sawtooth-induced fast-ion redistribution is relevant, too



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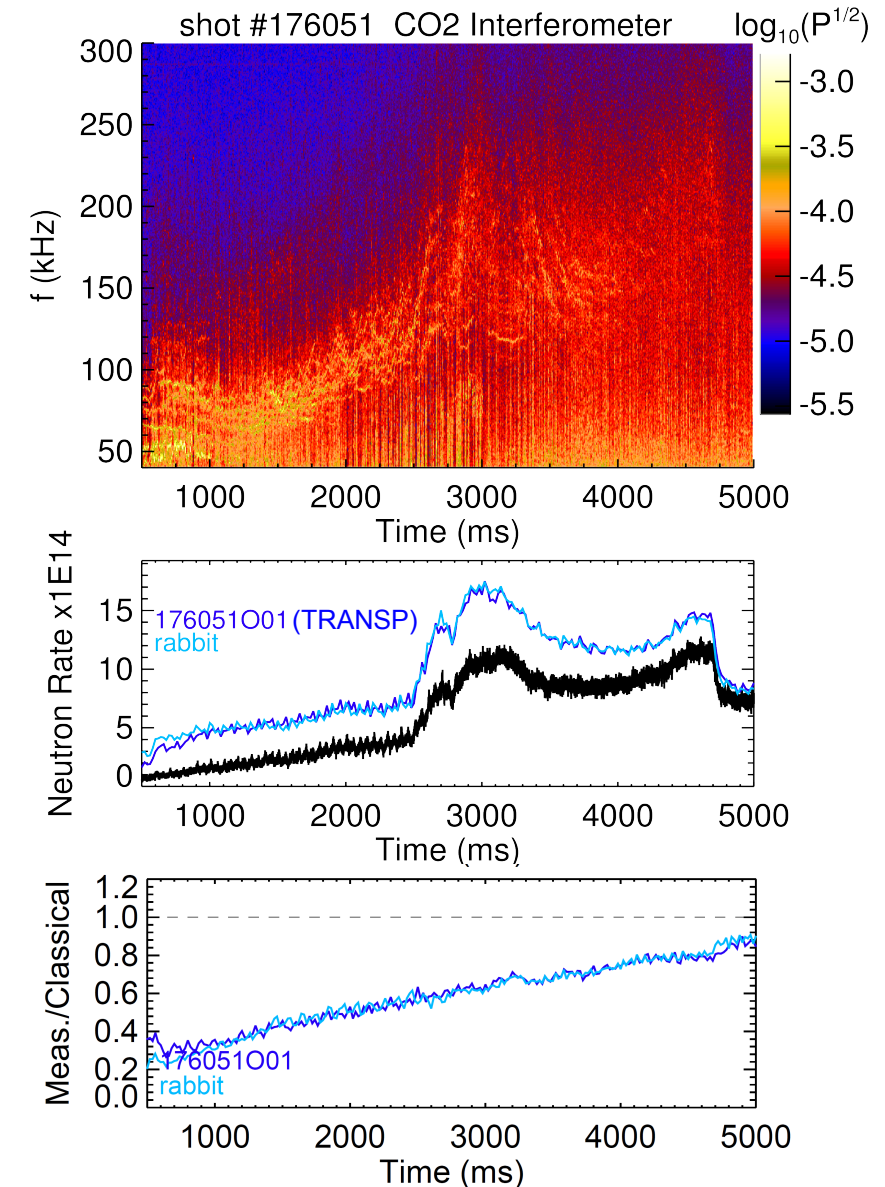
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- Relevant for correct interpretation of diagnostics (e.g. MSE)
- In this case: Sawtoothing plasma, sawtooth-induced fast-ion redistribution is relevant, too
 - here modeled by post-processing RABBIT profiles
 - Outlook: implement redistribution directly in RABBIT.



Detect AE-induced fast-ion transport by analyzing neutron rates

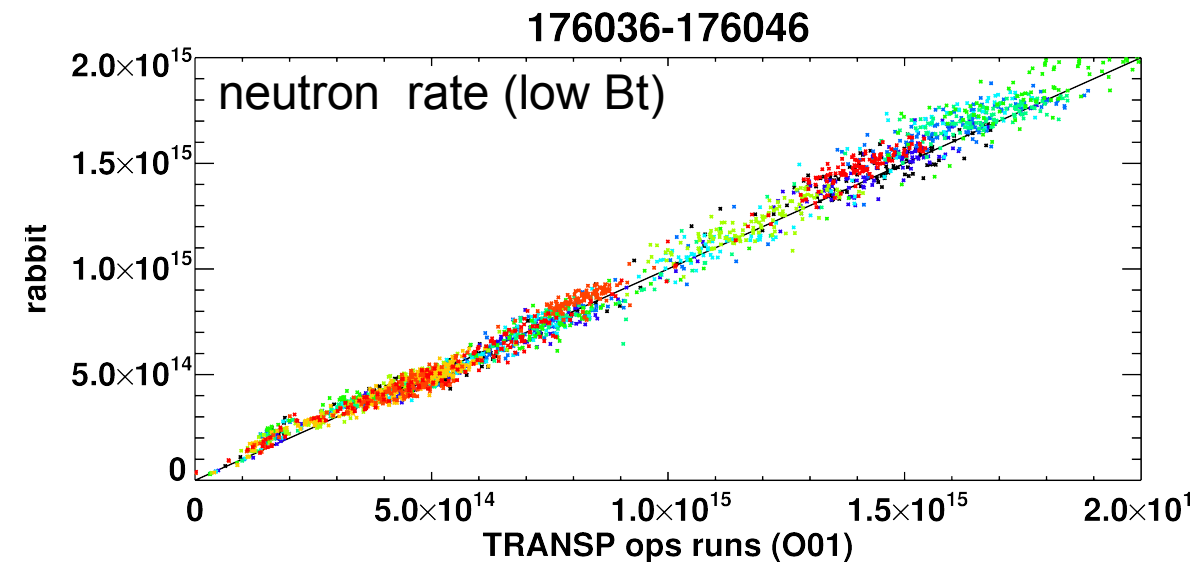
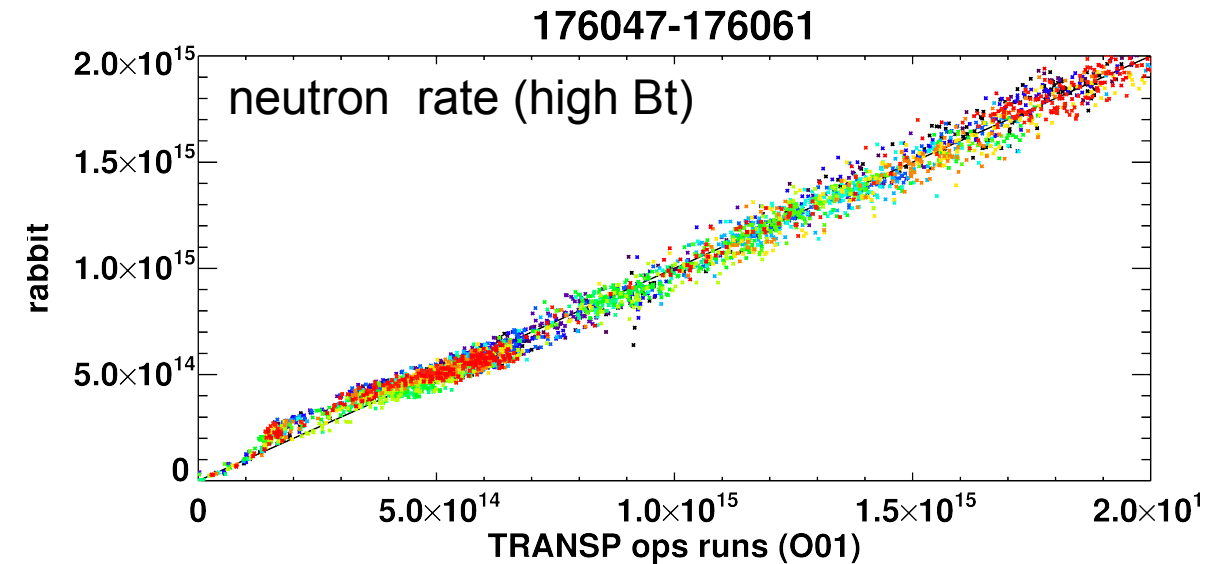
- Alfvén eigenmodes (AE) can be measured directly by fluctuation diagnostics
- Do they cause strong fast-ion transport?
→ can be assessed by comparing measured neutron rate with neo-classical prediction
- With RABBIT, this information is available directly after the discharge or even in real-time

- Used in scenario development for reversed shear steady state scenario experiments
→ Goal: Reduce fast-ion transport to optimize performance
→ RABBIT useful for decision making between discharges



Database comparison between TRANSP and RABBIT

- Comparison between RABBIT and TRANSP for all shots from the experimental session
→ Good agreement
- Outlook: Use for real-time control of AE modes
→ use ECE to detect AE amplitude
→ use RABBIT to detect detrimental fast-ion transport
→ trigger counter-measures, e.g. reduce NBI power (=AE drive)
- Use for data-mining (plan to run Rabbit on every historic DIII-D discharge)



real-time
diagnostics

real-time codes

Magnetics

Te, ne raw data
from:
Interferometry,
ECE

RT equilibrium
JANET/LIUQE

RT profile
estimator
RAPTOR

ne(ρ)
Te(ρ)
Ti(ρ)

TORBEAM
(ECRH)
RABBIT
(NBI)
...

Profiles of:
Heating, current-
drive, particle
source...

- RAPTOR is 1D real-time transport solver → relies on realistic inputs of sources by auxiliary heating
- Status of RABBIT implementation:
Hardware is installed, software is being finalized, first tests/results are expected in few weeks

Summary – RABBIT: A high-fidelity real-time NBI code



Three parts:	Calc. time:	Method:
• 1. Beam attenuation – birth profile	~ 7 ms	Simplified geometry (“thin beam”), analytic treatment of beam width
• 2. Orbit average	~ 12 ms	Conventional GC-integrator, but for very few orbits (~20 per E-comp.)
• 3. Time dep. solution of FP equation	~ 1 ms	Fully analytic

- In total ~20 ms per time-step (1 thread per beam) - faster than NUBEAM by roughly a factor of ~1000
- Good agreement with NUBEAM e.g. for heating profiles, neutron rates, fast-ion pressure tested so far on ASDEX Upgrade, DIII-D and JET

Applications / Outlook:

- For improved equilibrium reconstruction (e.g. IDE)
- Neutron rates allow to assess fast-ion transport (e.g. at DIII-D, intershot and real-time)
- Real-time control applications (with RAPTOR) at ASDEX Upgrade and TCV
- In ASTRA for the currently developed ASDEX Upgrade flight simulator
- In integrated modeling frameworks (IMAS, ETS, JINTRAC, OMFIT, ...)

Intel Xeon E5-2680 v3 (2.5GHz) CPUs,