



# Drift-kinetic Simulation Studies on Neoclassical Toroidal Viscosity in Tokamaks with Small Magnetic Perturbations

## S. Satake, H. Sugama, R. Kanno

National Institute for Fusion Science, Japan

## J.-K. Park

#### Princeton Plasma Physics Laboratory, U.S.A.

24<sup>th</sup> IAEA-FEC : TH/P2-24, Oct. 9, 2012 @ San Diego, USA

This work was supported by JSPS Grant-in-Aid for Young Scientists (B), No. 23760810, and the NIFS collaborative Research Programs 11KNST014. Part of calculations was carried out using the HELIOS supercomputer at International Fusion Energy Research Centre, Aomori, Japan, under the ITER-BA collaboration between Euratom and Japan, implemented by Fusion for Energy and JAEA.

E-mail: satake@nifs.ac.jp

## **Outlines**

Non-axisymmetric magnetic field perturbations in tokamak (RMP coils, toroidal ripples, MHD modes, ...)  $\delta B/B_0 = O(10^{-3} \sim 10^{-4})$ 

 Even small perturbation can damp the toroidal rotation drastically by neoclassical toroidal viscosity (NTV) (in JET, DIII-D, NSTX, ...).

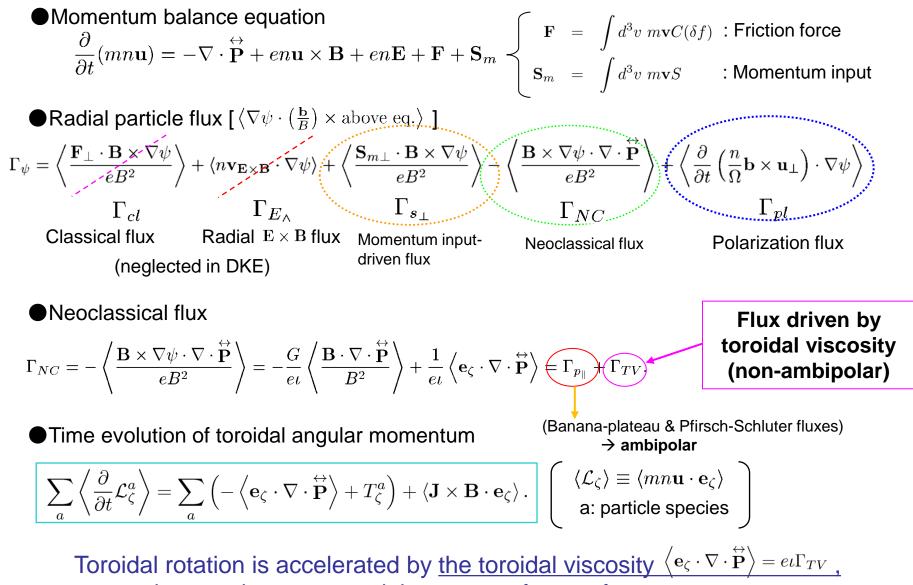
- RMP can mitigates ELMs, but toroidal rotation is related to other stabilities (RWM, locked modes, ...).
- Perturbation field penetration is shielded by plasma rotation.

Accurate calculation method for NTV is required to predict / control the effect of magnetic perturbations on NTV and rotation damping.

♦ FORTEC-3D δf drift-kinetic code is applied to NTV calculations.
 ♦ Verification of the numerical method has been done with Park's analytic formula for E × B → 0 case. → good agreement. (Satake, PRL 2011)

Here, new benchmark results for the finite-*E* × *B* cases are reported.
 It is found that the magnetic shear and the resonant drift motion of passing particles makes a double-peak profile of NTV when *E* × *B* rotation is fast enough.

#### **Basic relations for NTV calculations**



external torque input  $T_{\zeta}$ , and the torque of  $\mathbf{J} \times \mathbf{B}$  force.

#### The $\delta f$ Monte-Carlo method in FORTEC-3D code

Drift-kinetic equation for 
$$\delta f(\mathbf{x}, \mathcal{K} = \frac{mv^2}{2}, \mu = \frac{mv_{\perp}^2}{2B}) = f - f_M$$
:  

$$\frac{D}{Dt} \delta f \equiv \left[\frac{\partial}{\partial t} + (\mathbf{v}_{\parallel} + \mathbf{v}_d) \cdot \nabla + \dot{\mathcal{K}} \frac{d}{d\mathcal{K}}\right] \delta f - C_{TP}(\delta f) = -\left[\mathbf{v}_d \cdot \nabla + \dot{\mathcal{K}} \frac{d}{d\mathcal{K}} - \mathcal{P}\right] f_M$$

Linearized collision term (for ion-ion collisions)

 $C_{TP}(\delta f)$  : expressed by random-walk of markers in the  $(v_{\parallel}, v_{\perp})$ -space. (test-particle operator)

 $\mathcal{P}f_M$ : defined so that it satisfies the following properties. (field-particle operator)

$$\int d^3 v \mathcal{M}(C_{TP}(\delta f) + \mathcal{P}f_M) = 0 \text{ for } \mathcal{M} = 1, v_{\parallel}, v^2. \quad \text{(conservation low)}$$
$$C_{TP}(\delta f) + \mathcal{P}f_M = 0 \text{ for } \delta f = (c_0 + c_1 v_{\parallel} + c_2 v^2) f_M. \quad \text{(null-space)}$$

#### The two-weight scheme

For each marker (distribution function: g), two types of weights are assigned that satisfy :

$$wg = \delta f$$
 ,  $pg = f_M$ .

Each marker moves according to the LHS of the linearized DKE, Dg/Dt = 0. Then, the change of these weights are given as follows :

$$\dot{w} = -\frac{p}{f_M} \left( \mathbf{v}_d \cdot \nabla + \dot{\mathcal{K}} \frac{\partial}{\partial \mathcal{K}} - \mathcal{P} \right) f_M - \eta(w - \bar{w}),$$
  
$$\dot{p} = \frac{p}{f_M} \left( \mathbf{v}_d \cdot \nabla + \dot{\mathcal{K}} \frac{\partial}{\partial \mathcal{K}} \right) f_M - \eta(p - \bar{p}).$$

Noise-reduction terms (  $\bar{w},\bar{p} \rightarrow {\rm ensemble}$  average)

 $\bigstar$  In the present study, the radial electric field profile is given as an input parameter.

 $\Rightarrow$  Only ion drift-kinetic equation is solved, and the ion-electron collision is neglected.

#### Evaluation of pressure tensor and NTV in the $\delta f$ simulation

The guiding-center distribution function :  $f = f_M(\psi, v) + \delta f(\psi, \theta, \zeta, v_{\parallel}, v_{\perp})$  $\Rightarrow \quad \stackrel{\leftrightarrow}{\mathbf{P}} = p_0(\psi) \stackrel{\leftrightarrow}{\mathbf{I}} + \delta P_{\parallel} \mathbf{b} \mathbf{b} + \delta P_{\perp}(\stackrel{\leftrightarrow}{\mathbf{I}} - \mathbf{b} \mathbf{b}).$ Taking an flux surface average  $\Rightarrow \langle \mathbf{e}_{\zeta} \cdot \nabla \cdot \stackrel{\leftrightarrow}{\mathbf{P}} \rangle = \frac{1}{2} \langle \frac{\partial}{\partial \zeta} \delta P \rangle$ ,
where  $\delta P = \delta P_{\parallel} + \delta P_{\perp} = m \int d^3 v (v_{\parallel}^2/2 + v_{\perp}^2) \delta f.$ Solution of  $\delta f$  from FORTEC-3D

Instead of evaluating  $\partial \delta P / \partial \zeta$  directly, we make use of the fact that the magnetic field in FORTEC-3D is given in Fourier series in Boozer coordinates.

$$B(\psi,\theta,\zeta) = B_0 \left[ 1 - \sum_{m \ge 1} \epsilon_m(\psi) \cos(m\theta) + \sum_{m \ge 0, n \ne 0} \delta_{m,n}(\psi) \cos(m\theta - n\zeta) \right]$$

$$\frac{1}{2}\left\langle\frac{\partial}{\partial\zeta}\delta P\right\rangle = \frac{G+\iota I}{2V'}\oint d\theta d\zeta \frac{1}{B^2}\frac{\partial\delta P}{\partial\zeta} = \frac{G+\iota I}{V'}B_0\oint d\theta d\zeta \frac{\delta P}{B^3}\sum_{m,n}n\delta_{m,n}\sin(m\theta-n\zeta).$$

Then, the toroidal viscosity is evaluated by decomposing into the following form:

$$\left\langle \mathbf{e}_{\zeta} \cdot \nabla \cdot \overset{\leftrightarrow}{\mathbf{P}} \right\rangle = \sum_{m,n} \left\langle \mathbf{e}_{\zeta} \cdot \nabla \cdot \overset{\leftrightarrow}{\mathbf{P}} \right\rangle_{m,n} = B_0 \sum_{m,n} n \delta_{m,n} Q_{m,n} .$$
$$Q_{m,n} \equiv \left\langle \frac{\delta P}{B} \sin(m\theta - n\zeta) \right\rangle.$$

In this expression, one needs to evaluate only the  $Q_{m,n}$  components which has corresponding non-zero  $\delta_{m,n}$   $(n \neq 0)$  perturbations applied.

٦

#### Settings of the numerical simulation model

Large-aspect-ratio, circular cross-section tokamak  $(R_0 = 10m, a = 2.5m, B_0 = 10T)$ . For simplicity,  $T_i = 0.4$ keV= *const*. Banana width is small,  $\Delta_b/a \sim 10^{-3}$ .

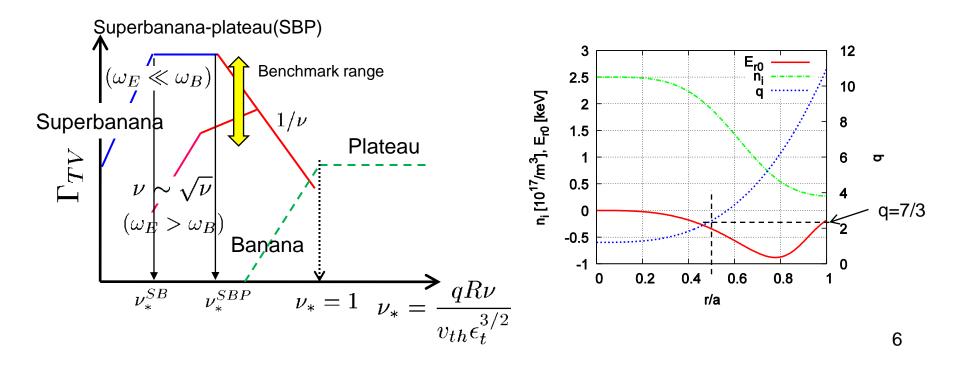
 $\rightarrow$  Finite-orbit-width effect in FORTEC-3D is negligible when comparing with local theory.

> Single-helicity perturbation,  $\delta_{7,3} = 0.01x^2 \cos(7\theta - 3\zeta)$  where x = r/a, is superimposed on the equilibrium tokamak field.

> Plasma collisionality is in the  $1/\nu$ -regime,  $\nu_* \approx 0.06$ .

>q-profile is  $q(x) = 1.2 + 9.8x^3$ . Resonant flux surface exists at r  $\doteq 0.49a$ , where q=7/3.

> Dependence of NTV on  $E \times B$  rotation speed is investigated by varying the  $E_r$  profile.



## **Combined analytic NTV theory**

- Including the missing components in conventional bounce-average theories:
  - Resonance between bounce motions and electric precession
  - Resonance between magnetic and electric precession (SBP and SB)
- Do not use assumptions that limits the range of collisionality (such as  $1/\nu$ , superbanana, etc.)
- Combined formula for NTV torque has been derived with effective Krook collision operator

$$\langle \hat{\phi} \cdot \vec{\nabla} \cdot \vec{\Pi}_{a} \rangle_{\ell} = \frac{\epsilon^{-1/2} p_{a}}{\sqrt{2} \pi^{3/2} R_{0}} \int_{0}^{1} d\kappa^{2} \delta_{w,\ell}^{2} \int_{0}^{\infty} dx \mathcal{R}_{a1\ell} \left[ u^{\varphi} + 2.0\sigma \left| \frac{1}{e} \frac{dT_{a}}{d\chi} \right| \right]$$
(11)  
Torque (Transport)  $\propto \sum_{m,m'} \delta_{m,n} \delta_{m',n}$  Resonance Rotation with offset  

$$\mathcal{R}_{ay\ell} = \frac{1}{2} \frac{n^{2} (1 + (\frac{\ell}{2})^{2}) \frac{\nu_{a}}{2\epsilon} x (x - \frac{5}{2})^{y} e^{-x}}{\left[ \ell \frac{\pi \sqrt{\epsilon}}{4\sqrt{2}} \omega_{ta} \sqrt{x} - n\omega_{E} - n\sigma \frac{q^{3}}{4\epsilon} (\omega_{ta}^{2}/\omega_{ga}) x \right]^{2} + \left[ (1 + (\frac{\ell}{2})^{2}) \frac{\nu_{a}}{2\epsilon} \right]^{2} x^{-3}}.$$
(12)  
Bounce Frequency  $\omega_{b}$  Electric Magnetic Collisionality Precession  $\omega_{B}$   $\nu_{K}$ 

[Park et al, PRL<u>102</u>, 065002 (2009)]

#### **Benchmark of NTV : Finite-***E*<sub>*r*</sub> **case**

#### How are simulations with $E \times B$ rotation compared with theory?

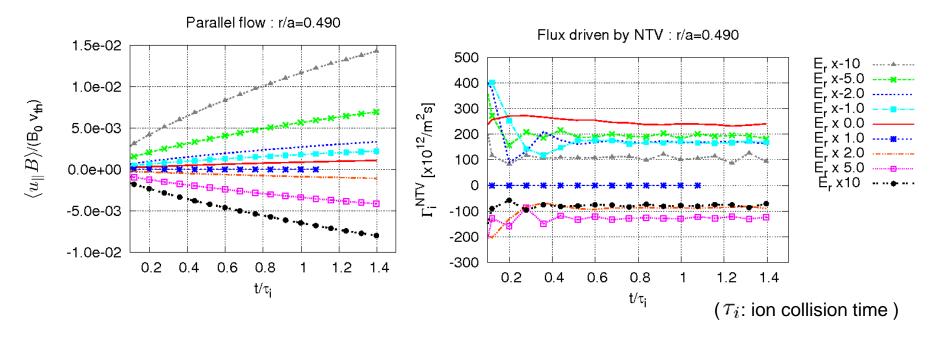
Park's formula ( $\chi =$  poloidal flux)

$$\begin{aligned} \langle \mathbf{e}_{\zeta} \cdot \nabla \cdot \mathbf{\Pi} \rangle &\simeq -\frac{\sqrt{\epsilon} p u_l^{\zeta}}{\sqrt{2} e \pi^{3/2} R_0} \sum_l \sum_{nmm'} \int_0^1 d\kappa^2 \delta_{l;mm'n}^2(\kappa) \int_0^\infty dx \mathcal{R}_{1l}(x), \\ \mathcal{R}_l(x) &\sim \frac{\omega_b \nu_K}{[l\omega_b - n(\omega_E + \omega_B)]^2 + \nu_K^2} \cdot A_1 = \frac{d\ln p}{d\chi} + \frac{e}{T} \frac{d\Phi}{d\chi}, \quad A_2 = \frac{d\ln T}{d\chi} \\ u_l^{\zeta} &\equiv u^{\zeta} - \frac{T}{e} \left[ k + \frac{\int dx \mathcal{R}_{2l}(x)}{\int dx \mathcal{R}_{1l}(x)} \right] A_2, \quad R_{2l}(x) \equiv (x - 5/2) R_{1l}(x) , \\ u^{\zeta} &= -T(A_1 - kA_2)/e \quad \leftarrow \text{From the radial force balance relation} \end{aligned}$$

- ▷ In order to avoid ambiguity coming from approximating  $k(\epsilon_t, \nu_*) \approx 1$  used in the definition of  $u_l^{\zeta}$  ( $k \simeq 1.17$  in the  $\epsilon_t, \nu_* \rightarrow 0$  limit), benchmarks are carried out by setting  $A_2 \propto dT/dr = 0$ .
- ► In FORTEC-3D, an  $E_r$  profile is given from the force balance relation with assuming  $u_{\zeta} \simeq 0$ , e.g.,  $E_r = \frac{T_i}{e} \frac{d}{d\chi} \ln n_i$ . This  $E_r$  profile is called "the  $E_{r0}$  case".
- > To see the NTV dependence on  $E_r$ , the  $E_{r0}$  case profile is multiplied by  $\pm 1$ ,  $\pm 2$ , etc.

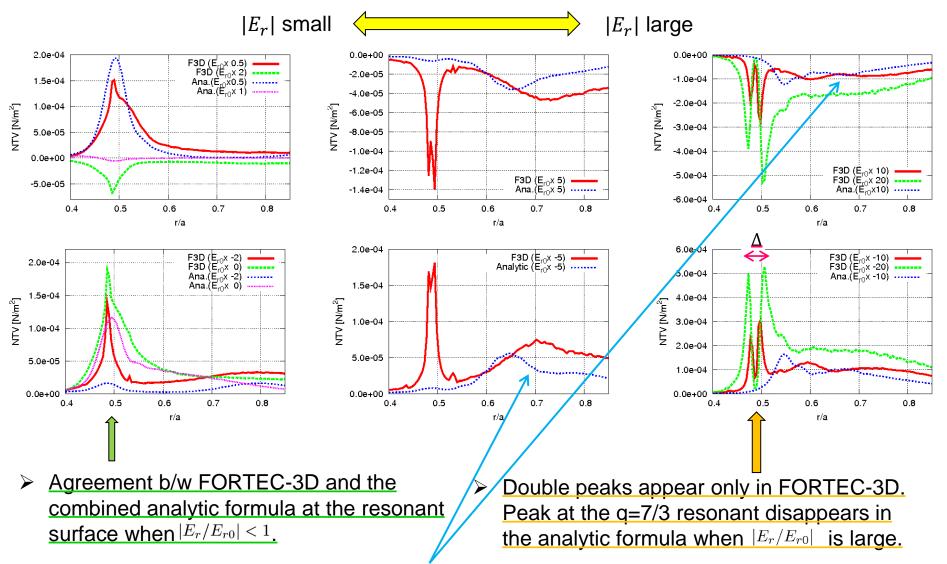
#### **Benchmark of NTV : Finite-***E*<sub>*r*</sub> **case**

#### **Convergence check of the Monte Carlo simulation**



- > Though  $u_{\parallel}$  (and  $u_{\zeta}$ ) evolves slowly in a simulation run, it remains small,  $u_{\parallel}/v_{th} \ll 1$ , in the present benchmark calculations.
- > The evolution of  $u_{\parallel}$  does not affect the evaluation of NTV in the simulations even in the large- $|E_r|$  cases.
- >NTV is evaluated by taking time average in the quasi-steady phase after  $\tau_i > 1$ .
- > Total simulation marker number is  $3.2 \times 10^7$  and the radial mesh points are 240.
- > Each run takes about 20 hours on Helios supercomputer.

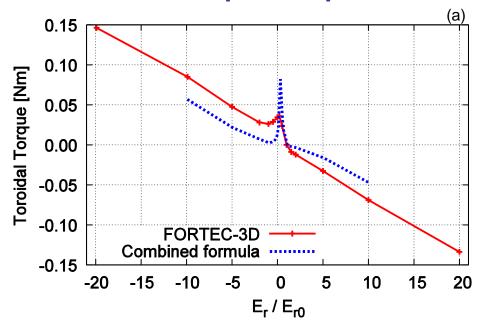
## Comparison of the NTV radial profile in Finite- $E_r$ cases

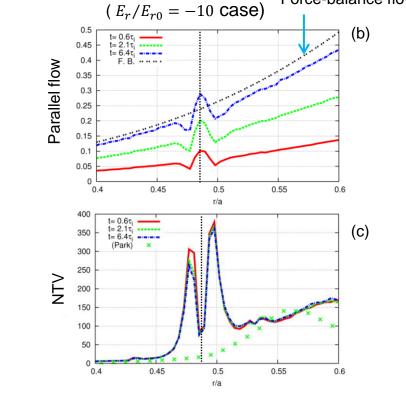


- Even  $|E_r/E_{r0}| \gg 1$ , in the off-resonant region (r/a>0.6) two calculations agree within factor O(1).
- ▶ Distance of the peaks is much larger than the banana width, and  $\Delta \propto |E_r|/B$ .

#### **NTV** Dependence on the $E_r$ amplitude :

Total toroidal torque and parallel flow profile





- The total toroidal torque (NTV integrated on the whole volume) is also compared. (fig. (a))
- The off-resonant region, where FORTEC-3D agrees well with the analytic formula, contributes mainly to the total torque.
- > Both calculation methods shows the same linear dependence of total toroidal viscosity on  $E_r/E_{r0}$ .
- > The peak of NTV at  $E_r \sim 0$  is because of the resonant of the trapped particles,  $\omega_E + \omega_B = 0$ .

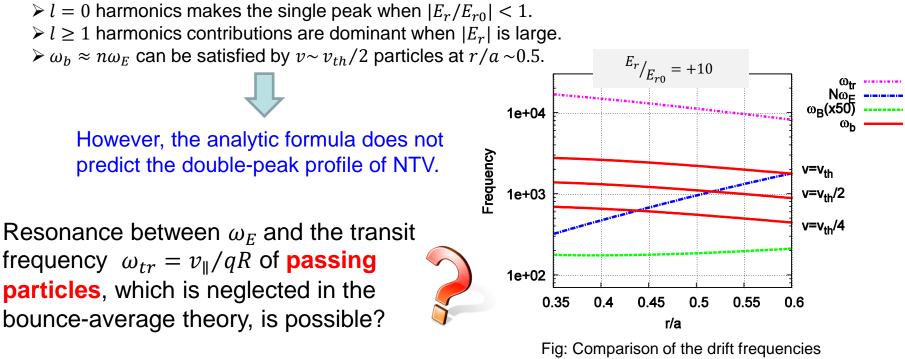
- ➤ In FORTEC-3D simulations, parallel (toroidal) flow evolves so that it satisfies the force balance relation,  $u^{\zeta} = -T(A_1 kA_2)/e$ .
- ▶ In large- $|E_r|$  cases,  $V_{\parallel}$ -shear is observed around the resonant flux surface (fig.(b)).
- However, the evolution of the shear flow does not affect the double-peak profile of NTV (fig. (c)).

Force-balance flow

#### The origin of the double-peak:

From the bounce-average analytic formula  $(T_i = const. case)$ :  $\langle \mathbf{e}_{\zeta} \cdot \nabla \cdot \mathbf{P} \rangle \sim \sum_{l \ge 0} \sum_{mn} u^{\zeta} \delta_{mn}^2 \int d\kappa^2 F_{lmn}(\kappa) \int dx \mathcal{R}_l(x),$  $\mathcal{R}_l(x) \sim \frac{\omega_b \nu_K}{[l\omega_b - n(\omega_E + \omega_B)]^2 + \nu_K^2}, \quad u^{\zeta} = -\frac{1}{e} \left( \frac{d\ln n_i}{d\chi} + e \frac{d\Phi}{d\chi} \right)$   $\begin{pmatrix} \omega_E = d\Phi/d\chi : \\ E \times B \text{ rotation freq.} \\ \omega_B : \text{Bounce freq.} \\ \omega_B : \text{Magnetic drift freq.} \\ \nu_K : \text{Collision freq.} \end{pmatrix}$ 

Strong peak of NTV will occur when  $l\omega_b - n(\omega_E + \omega_B) \approx 0$  is satisfied. (resonance)



Note:  $\omega_{tr}$  in the right fig. is evaluated by  $v_{\parallel} = v_{th}$ .

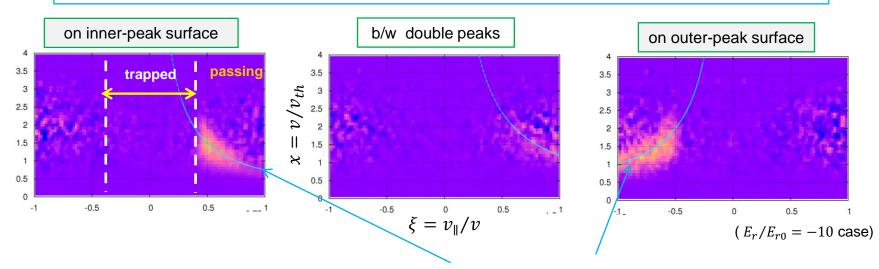
and the bounce frequency.

#### Passing particle resonance makes the double-peak of NTV (1)

In FORTEC-3D, NTV is evaluated as follows:

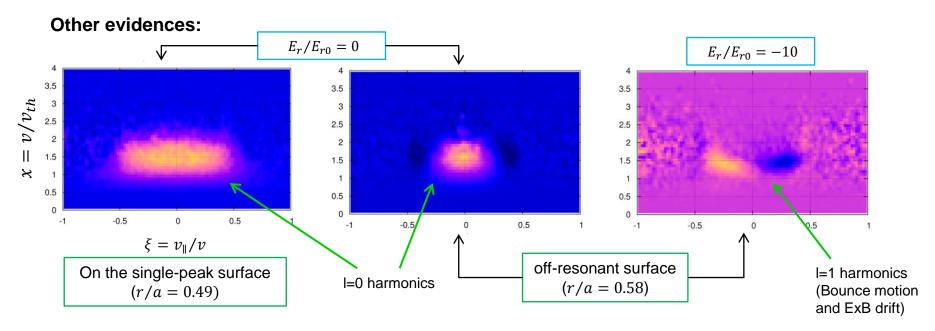
$$\begin{aligned} \mathbf{e}_{\zeta} \cdot \nabla \cdot \mathbf{P} \rangle &= \sum_{m,n \neq 0} \left\langle \mathbf{e}_{\zeta} \cdot \nabla \cdot \mathbf{P} \right\rangle_{m,n} \equiv B_0 \sum_{m,n \neq 0} n \delta_{m,n} Q_{m,n}, \\ Q_{m,n} &\equiv \left\langle \frac{\delta P}{B} \sin(m\theta - n\zeta) \right\rangle = \frac{1}{V'} \oint d\theta \oint d\zeta \frac{J_B}{B} \sin(m\theta - n\zeta) M_i \int d^3 v \delta f\left(v_{\parallel}^2 + \frac{v_{\perp}^2}{2}\right). \\ \hline dQ_{m,n} \end{aligned}$$

To see what kind of particles makes the double-peak NTV, the integrand  $dQ_{m,n}$  in the velocity space  $(x, \xi) = (v/v_{th}, v_{\parallel}/v)$  at  $\theta \cong 0$  is observed.



- In passing region, strong resonant appears <u>on  $v_{\parallel} = \text{const.}$  line</u>.
- •The sign of resonant  $v_{\parallel}$  is opposite b/w the inner and outer peaks.
- •The sign also changes according to the sign of  $E_r$ .
- •When the resonance of  $dQ_{m,n}$  appears at  $x \approx 1$ , strong peak of NTV is created on that flux surface.

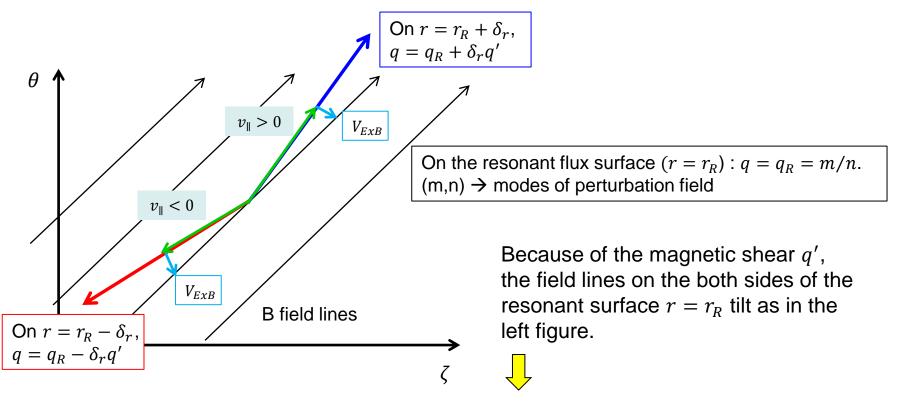
### Passing particle resonance makes the double-peak of NTV (2)



- When  $E_r \approx 0$ , the single peak of NTV on the resonant surface (q = m/n) is created mainly from the trapped particles. Passing contribution is non-zero, but small.
- In the off-resonant region (away from the resonant surface), NTV is almost determined by the trapped particles.
- The l = 0 ( $E_r \approx 0$ ) and l = 1 ( $|E_r/E_{r0}| \gg 1$ ) type harmonics in the velocity space, which is predicted in the analytic theory, can clearly be distinguished in FORTEC-3D simulation, as shown in the right two figures.

The difference between FORTEC-3D and the combined analytic formula comes from the passing particles' resonance when  $\omega_{tr} \sim \omega_E$ .

#### The passing particle resonance condition



- If the *E* × *B* drift is large enough and <u>the drift velocity</u> *v*<sub>||</sub>b + v<sub>E×B</sub> for *v* ≈ *v*<sub>th</sub> passing particles on *r* = *r*<sub>R</sub> ± δ<sub>r</sub> surfaces is aligned with the *q* = *m*/*n* field lines on the resonant surface, such passing particles continuously feel the constant phase of perturbed magnetic field, δ<sub>m,n</sub> ∝ cos(mθ − nζ).
- If such condition is satisfied, the resonant passing particles' orbits are affected by the perturbed magnetic field, resulting in non-ambipolar radial flux and therefore NTV.
- Large V<sub>E×B</sub> → Large δ<sub>r</sub> is required to satisfy the condition for  $v ≈ v_{th}$  particles. This explains why the distance b/w the double peaks increases with |E<sub>r</sub>|.

### Summary



FORTEC-3D code was applied to calculate neoclassical toroidal viscosity in tokamak plasmas with asymmetric magnetic field.
 Benchmark tests were carried out with the combined analytic formula for finite-*E<sub>r</sub>* cases .

- ✓ NTV profile shows significant difference b/w two calculations when  $|E_r/E_{r0}| \gg 1$ . In FORTEC-3D simulations, a **double-peak profile of NTV** appears around the resonant rational flux surface as  $|E_r/E_{r0}|$  increases.
- ✓ Passing particle resonance, which occurs if magnetic shear dq/dr and large  $E_r$  coexist near the resonant flux surface, makes a significant contribution to NTV to make the double-peak profile.

✓ The localized double-peak of NTV will also affect the toroidal rotation damping there.

#### Future Tasks

- > Investigate the collisionality dependence of NTV when  $E_r \neq 0$ .
  - Is NTV really scales as  $\nu \sim \sqrt{\nu}$  as asymptotic formula predicts?
- Include the passing-particle resonance effect in the combined analytic formula.
- What if the perturbed field makes explicit island structure (the present model is vacuum approximation).
  - Use  $\delta \mathbf{B} = \sum_{m,n} \nabla \times (\alpha_{m,n} \mathbf{B})$ -type expression, for example.
- Application to helical devices : EX/P3-27 "Transition to Improved Confinement Mode by Electrode Biasing in the Large Helical Device" by Kitajima et al.