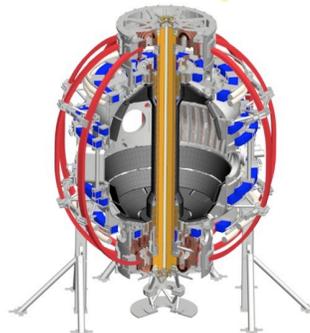


Snowflake Divertor as Plasma-Material Interface for Future High Power Density Fusion Devices

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J. E. Menard, A. G. McLean, T. D. Rognlien,
D. D. Ryutov, F. Scotti, A. Diallo, R. Kaita, R. Maingi,
M. Podesta, R. Raman, A. L. Roquemore**

Poster EX/D P5.021

October 8-13, 2012
San Diego, California, USA

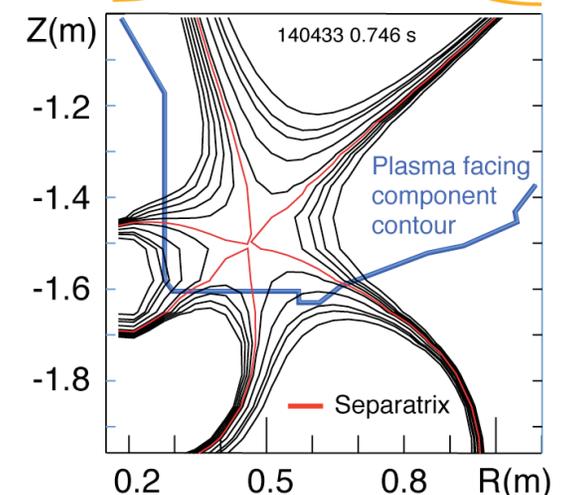
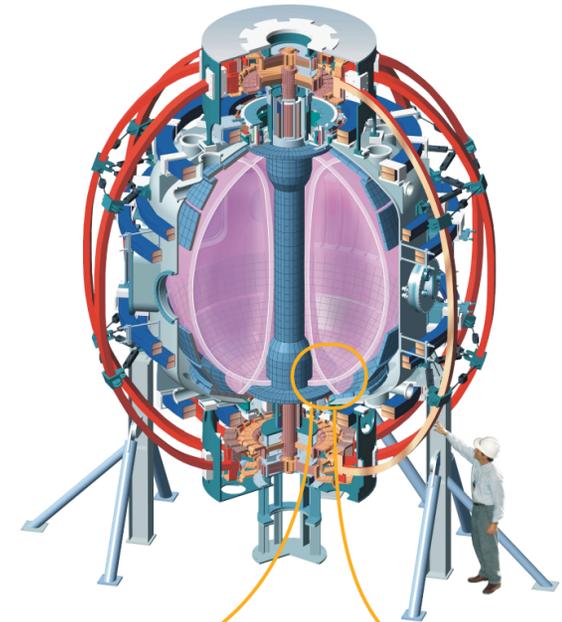


*Coll of Wm & Mary
Columbia U
CompX
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Ioffe Inst
TRINITI
Chonbuk Natl U
NFRI
KAIST
POSTECH
Seoul Natl U
ASIPP
CIEMAT
FOM Inst DIFFER
ENEA, Frascati
CEA, Cadarache
IPP, Jülich
IPP, Garching
ASCR, Czech Rep*

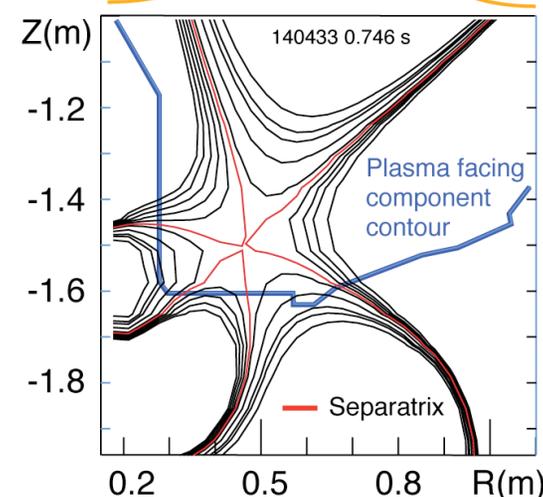
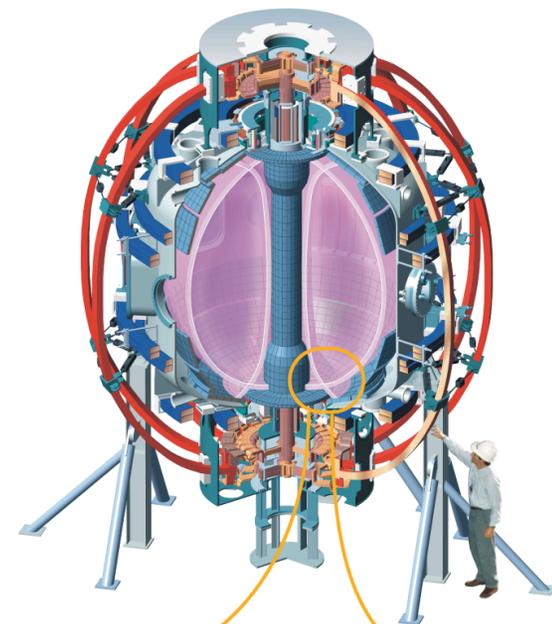
Snowflake divertor is a promising solution for mitigating divertor heat loads, and projects favorably to future fusion devices

Recent NSTX results demonstrate that the snowflake divertor (SFD) configuration may provide a promising solution for mitigating steady-state and transient divertor heat loads and target plate erosion, and project favorably to future fusion devices. In NSTX, a large spherical tokamak with high divertor heat flux $q_{peak} \leq 15 \text{ MW/m}^2$, $q_{||} \leq 200 \text{ MW/m}^2$, steady-state SFD configurations lasting up to 0.6 s ($10 t_E$) were obtained using the existing divertor poloidal field coils. The SFD geometry significantly increased the plasma-wetted area, the parallel connection length, and the divertor volumetric losses compared to the standard divertor configuration. The SFD formation led to a stable partial detachment of the outer strike point otherwise inaccessible in the standard divertor geometry at $P_{SOL} = 3 \text{ MW}$ and $n_e/n_G \sim 0.6-0.8$ in NSTX. Peak divertor heat fluxes were reduced from 3-7 MW/m^2 to 0.5-1 MW/m^2 between ELMs, and from 5-20 MW/m^2 to 1-5 MW/m^2 at peak times of Type I ELMs ($D W_{MHD} / W_{MHD} = 7-15 \%$). H-mode core confinement was maintained albeit the radiative detachment, while core carbon concentration was reduced by up to 50 %. Additional divertor CD_4 seeding increased divertor radiation further. Based on the NSTX experiments, the SFD configuration is being developed as a leading heat flux mitigation technique for the NSTX Upgrade device. An edge transport model based on the two-dimensional multi-fluid code UEDGE favorably projects SFD properties to NSTX-U, showing a significant reduction of the steady-state peak divertor heat flux from 15 to about 3 MW/m^2 expected in 2 MA discharges with 12 MW NBI heating.



Snowflake divertor is a promising solution for mitigating divertor heat loads, and projects favorably to future fusion devices

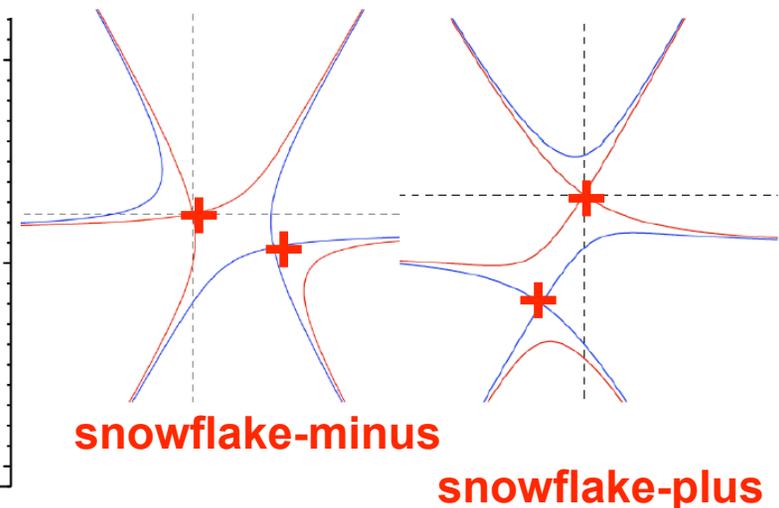
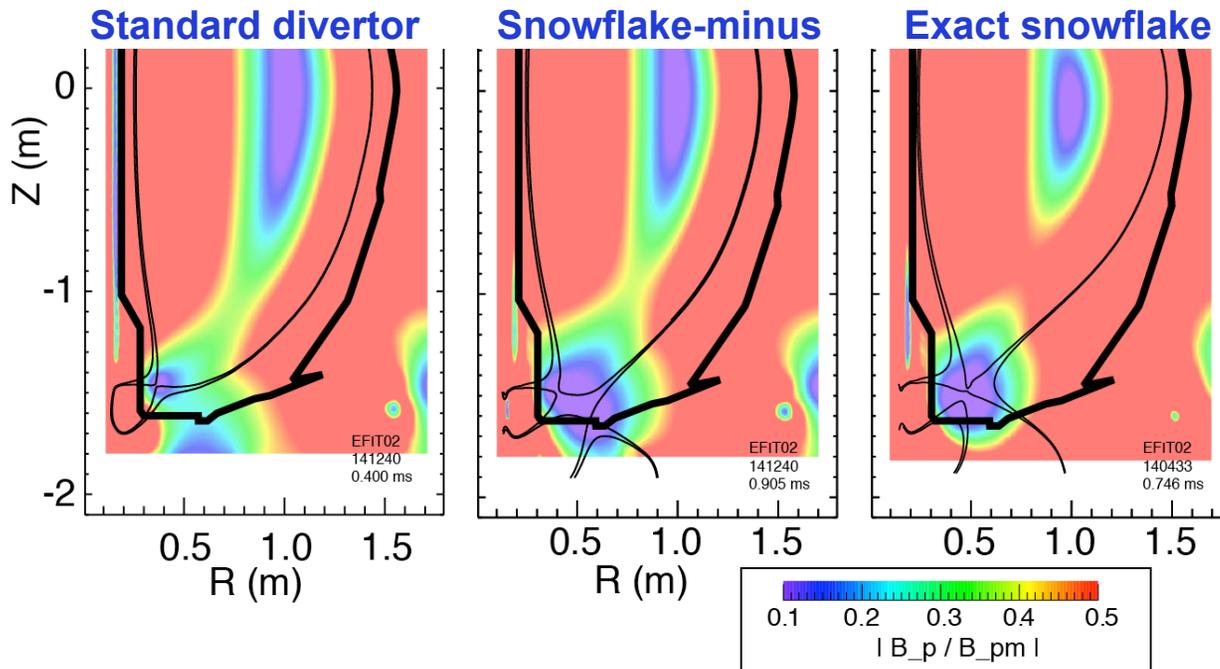
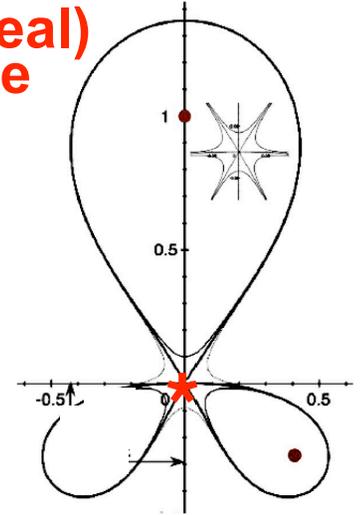
- Snowflake divertor configuration in NSTX
 - Core H-mode confinement unaffected, core carbon concentration reduced
 - Pedestal stability modified: suppressed Type I ELMs re-appeared
 - Divertor heat flux significantly reduced
 - Between-ELM reduction due to geometry and radiative detachment
 - ELM heat flux reduction due to power sharing between strike points, radiation and geometry
- Snowflake divertor is a leading candidate for NSTX-U
 - Divertor coils enable a variety of snowflakes
 - In 2 MA, 12 MW NBI-heated discharges
 - SOL power width $\lambda_{SOL} = 3$ mm projected
 - $q_{div} \leq 15 - 25$ MW/m² projected in standard divertor
 - $q_{div} \leq 3$ MW/m² projected in snowflake divertor



Snowflake divertor geometry takes advantage of second-order poloidal field null properties

- Snowflake divertor configuration
 - Second-order null
 - $B_p \sim 0$ and $\text{grad } B_p \sim 0$ (Cf. first-order null: $B_p \sim 0$)
 - Obtained with existing divertor coils (min. 2)
 - Exact snowflake topologically unstable
 - Deviation from ideal snowflake: $\sigma = d / a$
 - d – distance between nulls, a – plasma minor radius

Exact (ideal) snowflake



D. D. Ryutov, PoP 14, 064502 2007
 EPS 2012 Invited, subm. to PPCF

Snowflake divertor geometry has benefits over standard X-point divertor geometry

- Predicted geometry properties in snowflake divertor (cf. standard divertor)
 - Increased edge shear :ped. stability
 - Add'l null: H-mode power threshold, ion loss
 - Larger plasma wetted-area A_{wet} : reduce q_{div}
 - Four strike points : share $q_{||}$
 - Larger X-point connection length L_x : reduce $q_{||}$
 - Larger effective divertor volume V_{div} : incr. P_{rad} , P_{CX}

$$q_{pk} \simeq \frac{P_{heat} (1 - f_{rad}) f_{out/tot} f_{down/tot} (1 - f_{pfr}) \sin \alpha}{2\pi R_{SP} f_{exp} \lambda_{q_{||}}}$$

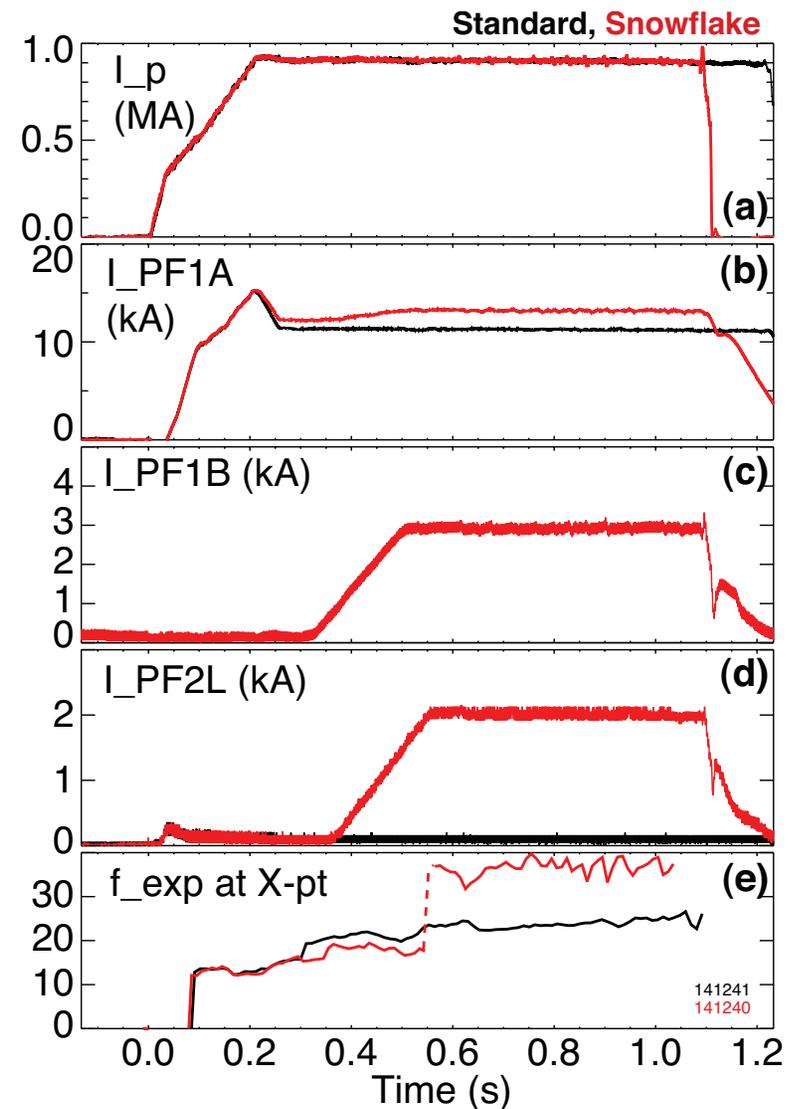
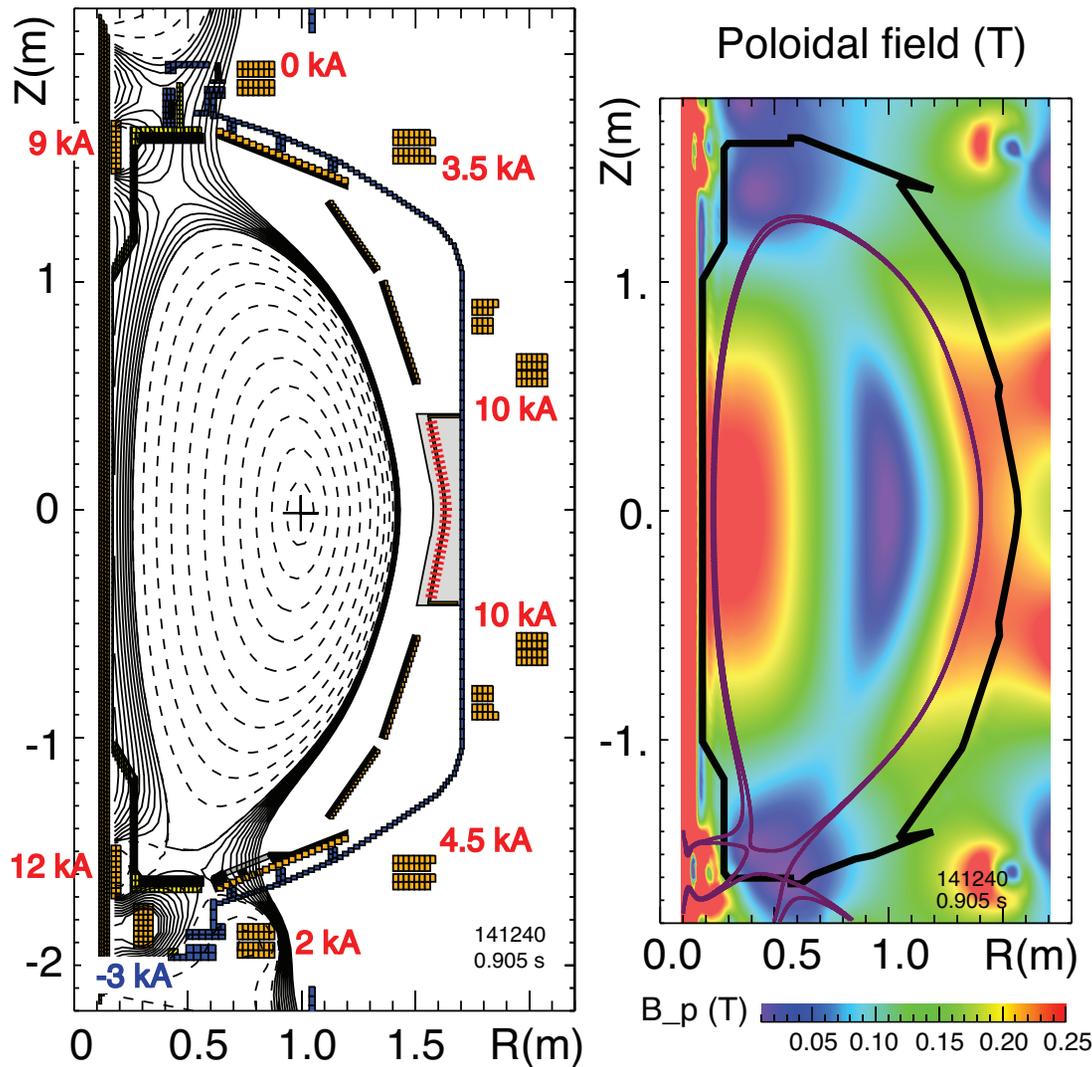
$$f_{exp} = \frac{(B_p/B_{tot})_{MP}}{(B_p/B_{tot})_{OSP}}$$

D. D. Ryutov, PoP 14, 064502 2007

$$A_{wet} = 2\pi R f_{exp} \lambda_{q_{||}}$$

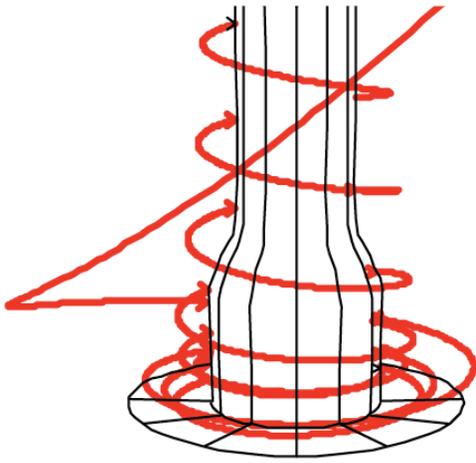


Snowflake divertor configurations obtained with existing divertor coils, maintained for up to $10 \tau_E$



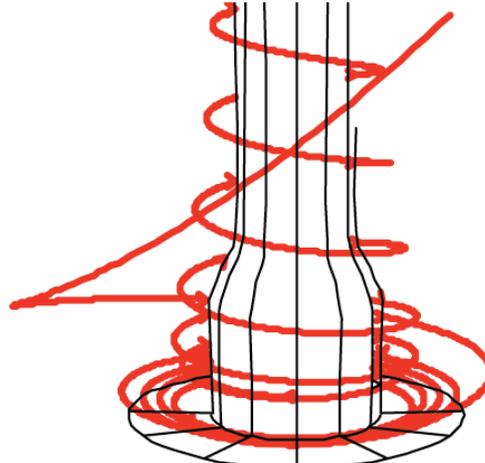
Plasma-wetted area and connection length are increased by 50-90 % in snowflake divertor

Standard divertor



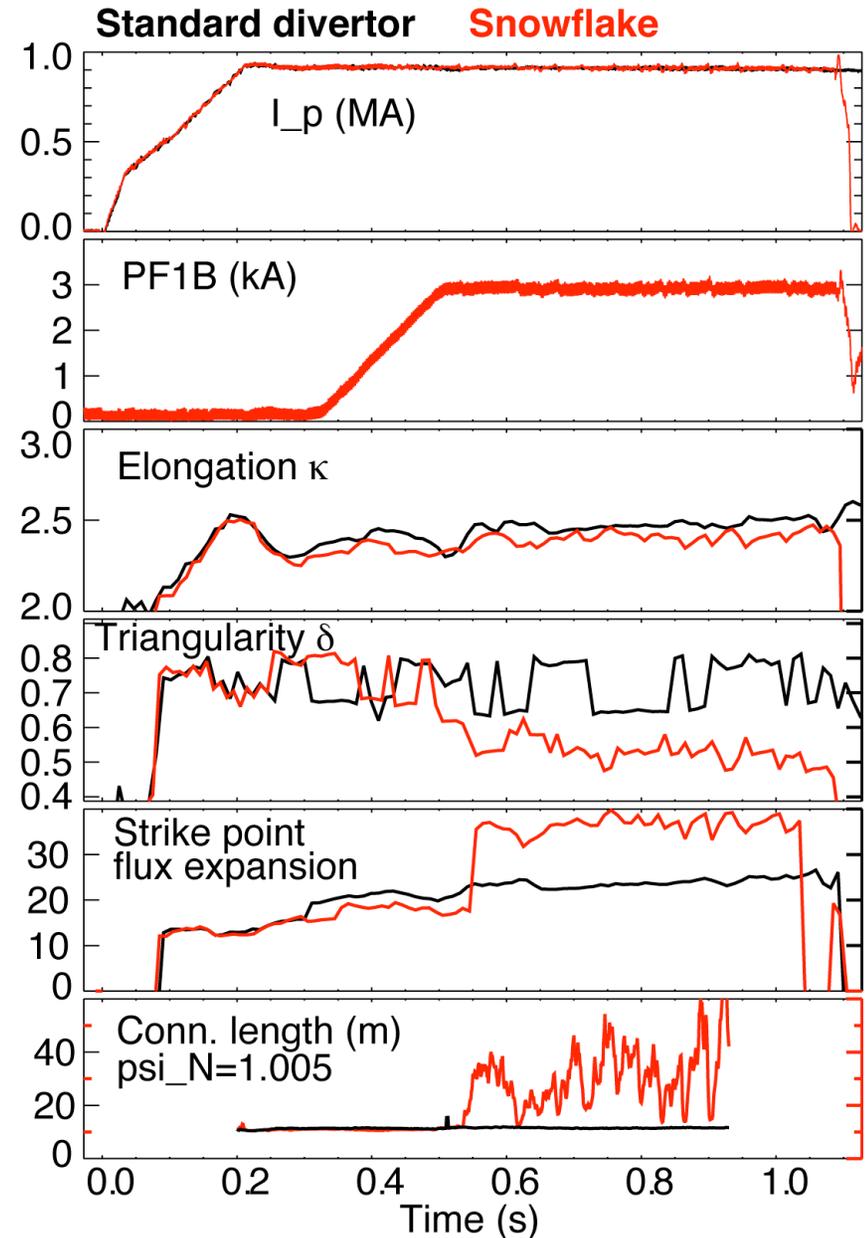
Shot 141241, EFIT02,
time: 0.905 s,
normalized flux: 1.005

Snowflake-minus

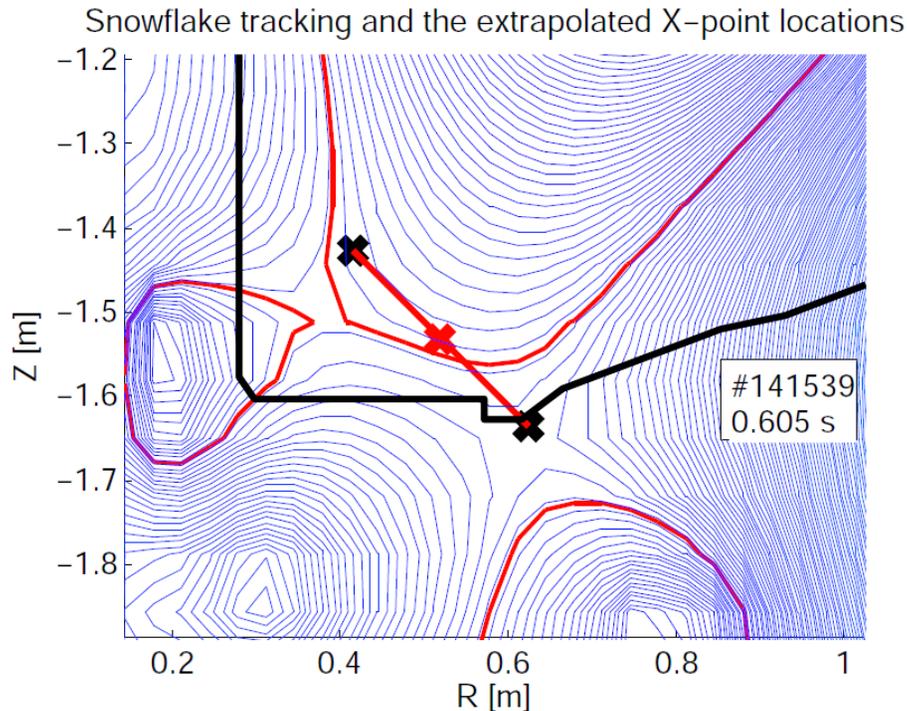


Shot 141240, EFIT02,
time: 0.905 s,
normalized flux: 1.005

- These properties observed in first 30-50 % of SOL width
- B_{tot} angles in the strike point region: 1-2°, sometimes < 1°



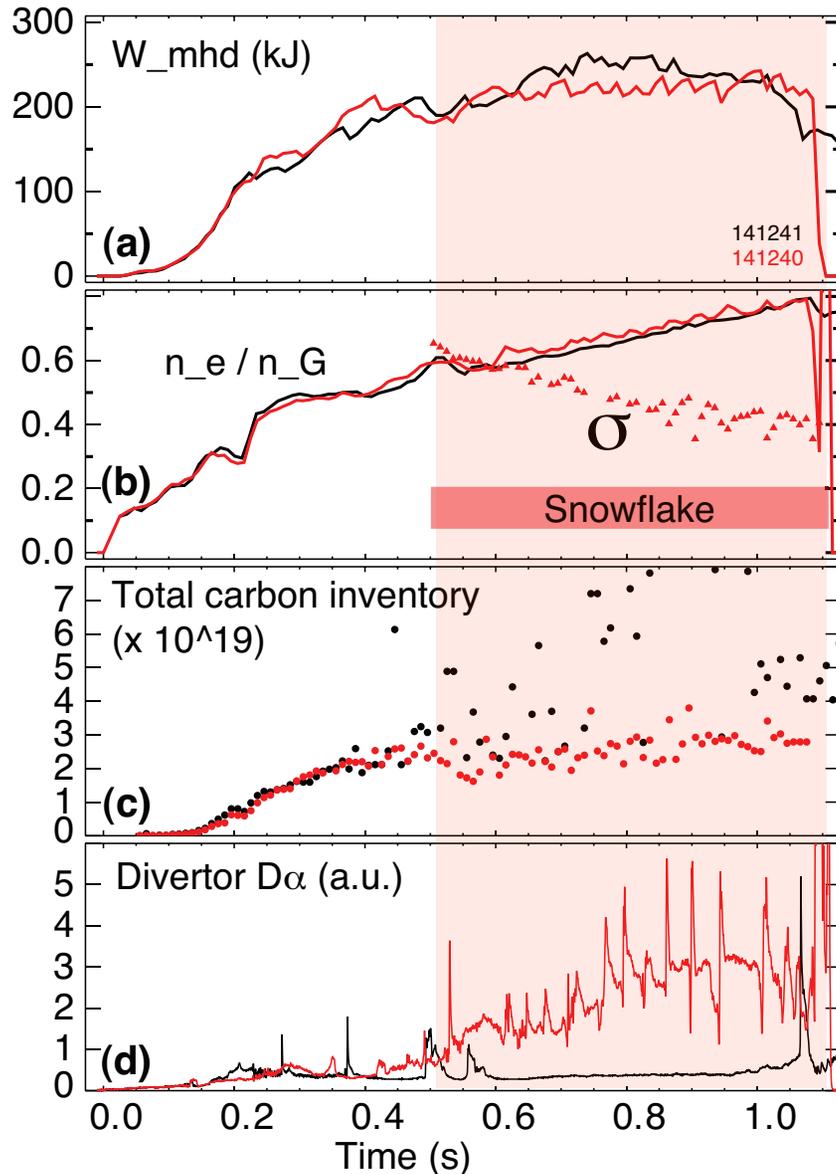
Close-loop feedback control of divertor coil currents is desirable for steady-state snowflake



M.A. Makowski & D. Ryutov, “X-Point Tracking Algorithm for the Snowflake Divertor”

- All configurations are obtained reproducibly under feed-forward control in NSTX
- In NSTX
 - Developed X-point tracking algorithm that locates nulls and centroid
 - Algorithm tested on NSTX snowflakes successfully
 - Implementing snowflake control in digital plasma control system

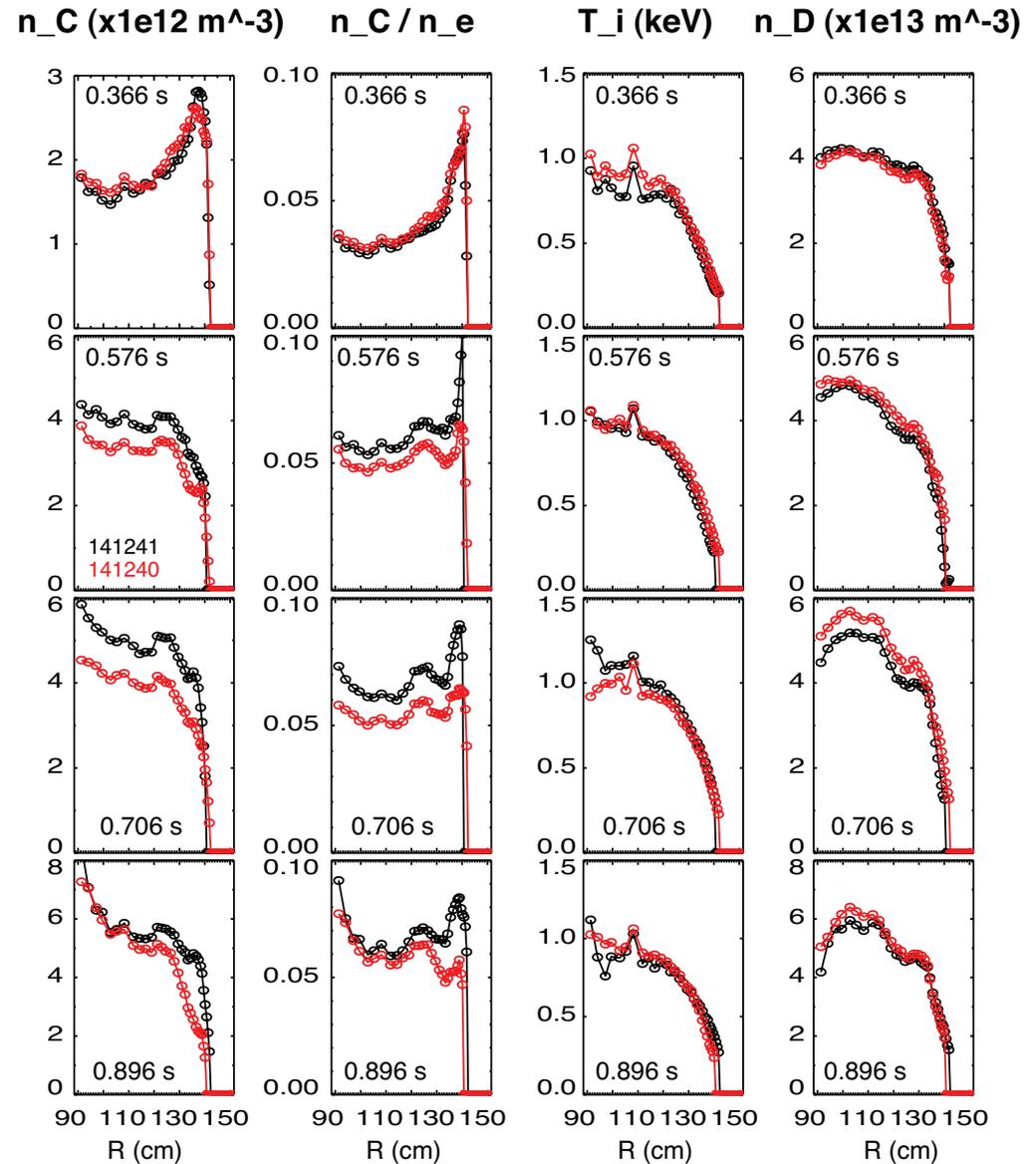
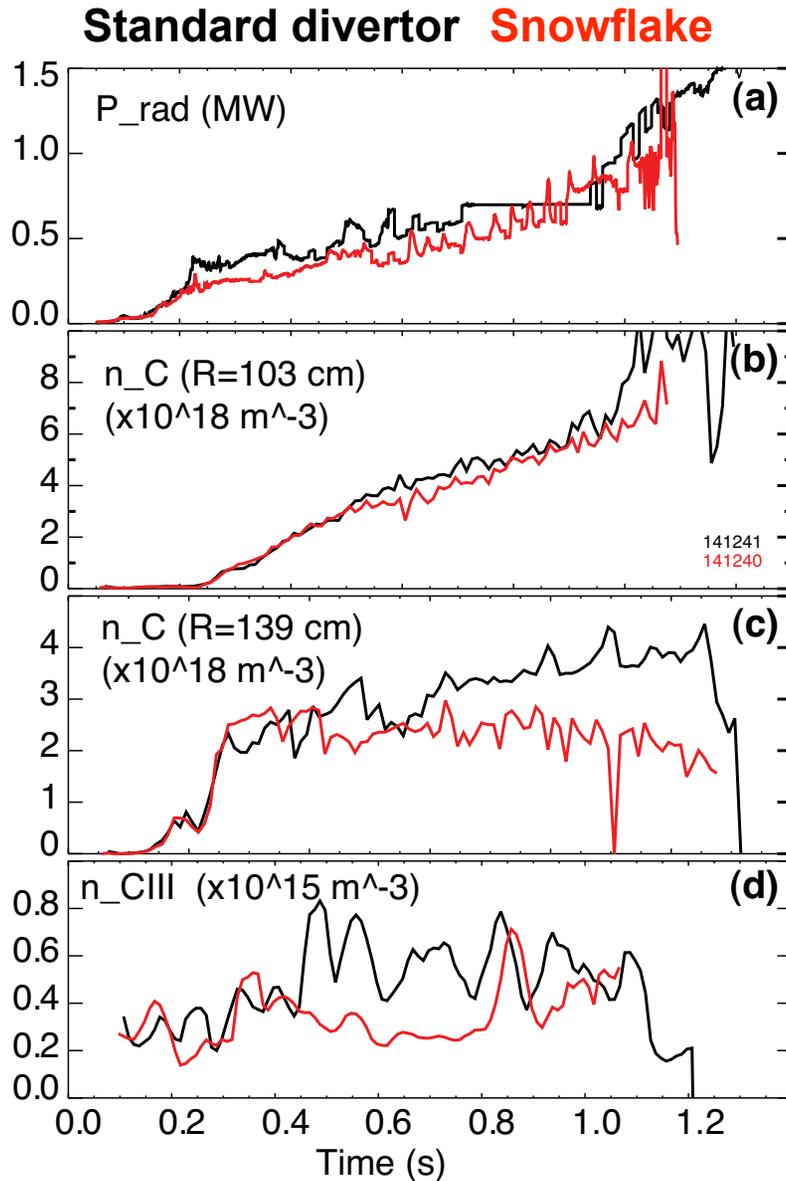
Good H-mode confinement properties and core impurity reduction obtained with snowflake divertor



- 0.8 MA, 4 MW H-mode
- $\kappa=2.1$, $\delta=0.8$
- Core $T_e \sim 0.8-1$ keV, $T_i \sim 1$ keV
- $\beta_N \sim 4-5$
- Plasma stored energy ~ 250 kJ
- H98(y,2) ~ 1 (from TRANSP)
- ELMs
 - Suppressed in standard divertor H-mode via lithium conditioning
 - Re-appeared in snowflake H-mode
- Core carbon reduction due to
 - Type I ELMs
 - Edge source reduction
 - Divertor sputtering rates reduced due to partial detachment

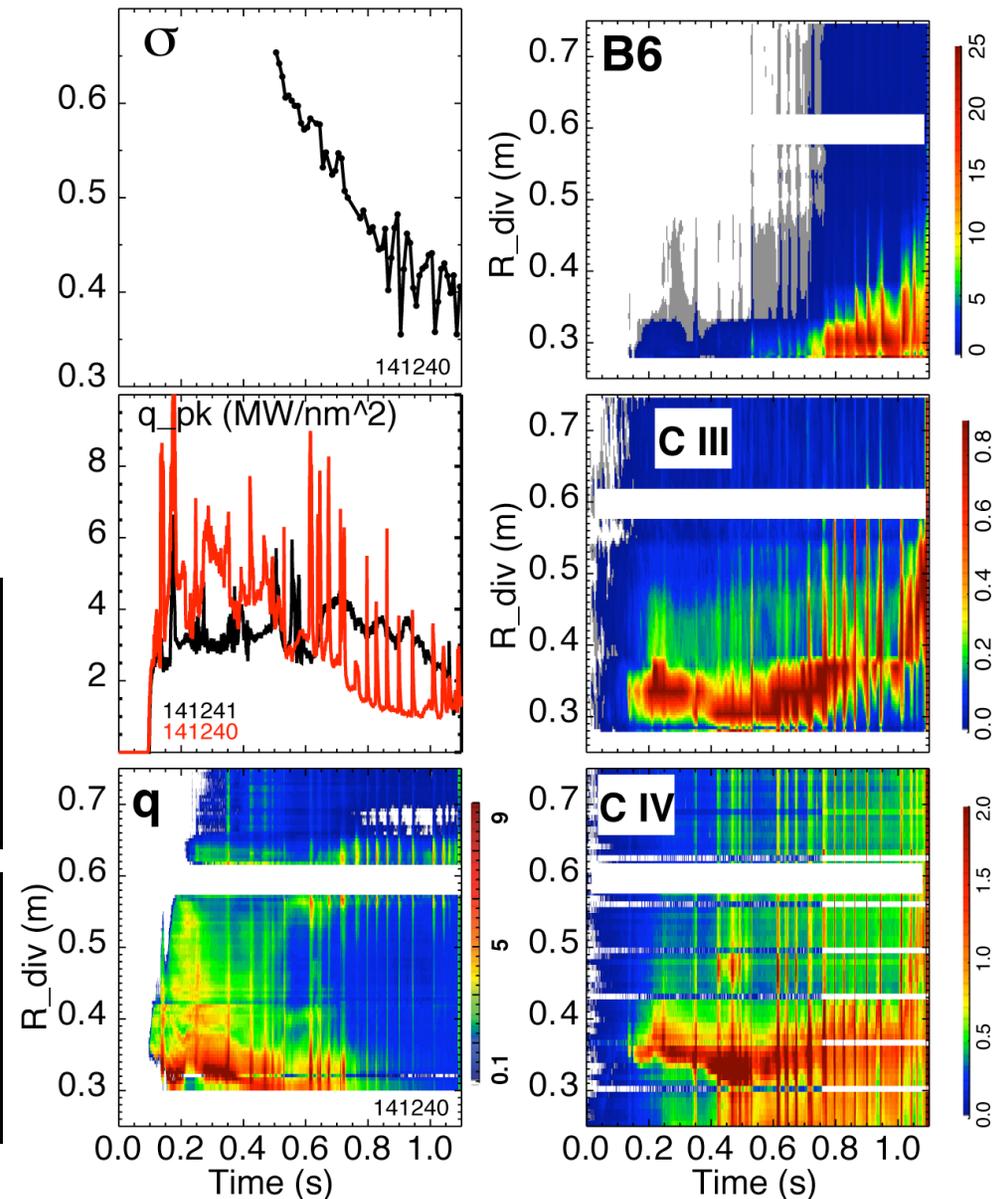
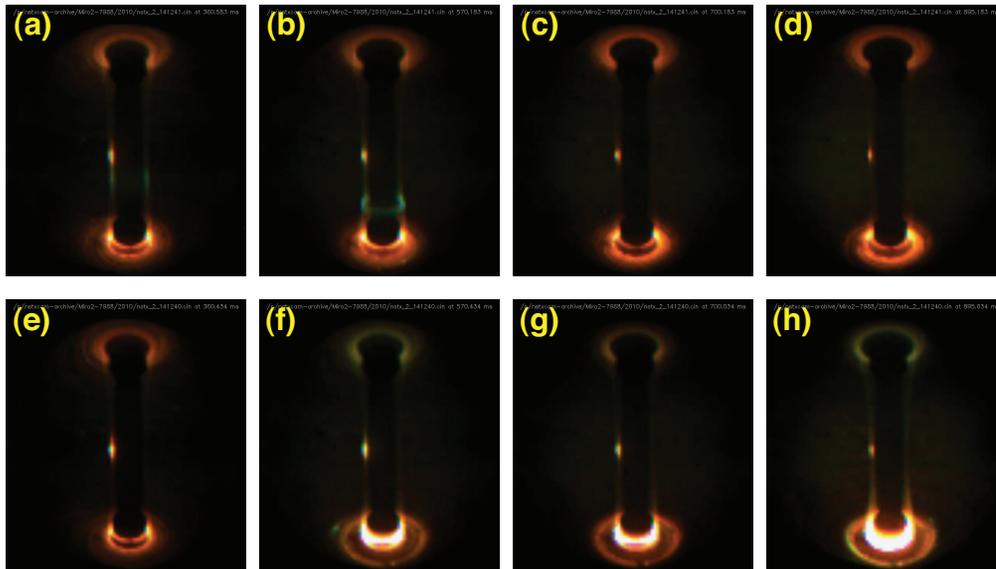


Core carbon density significantly reduced with snowflake divertor

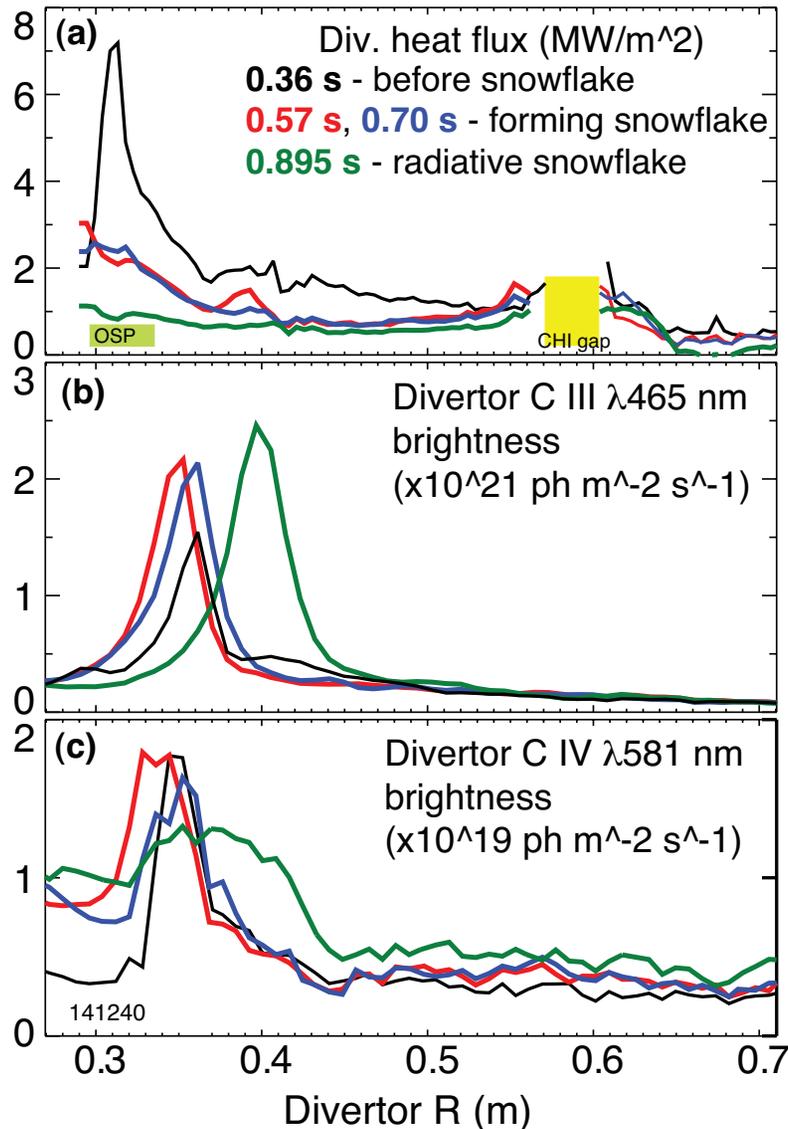


Radiative detachment with strong recombination and high radiated power observed in snowflake divertor

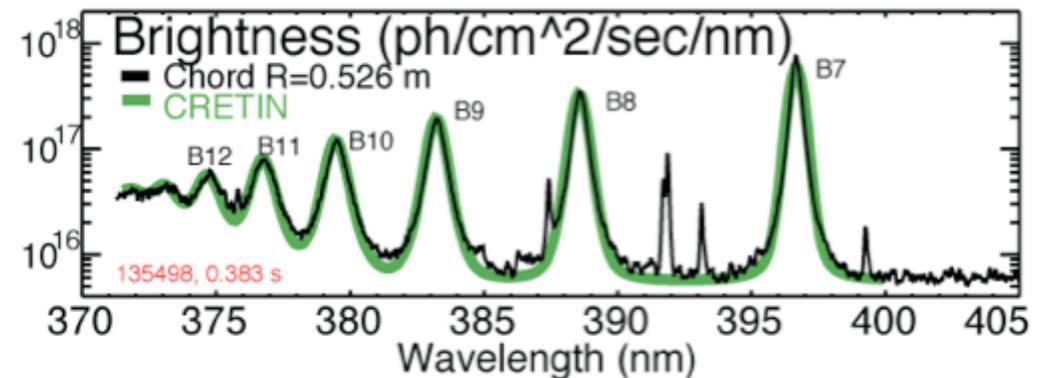
- Attached standard divertor - snowflake transition - snowflake + detachment
- $P_{\text{SOL}} \sim 3 \text{ MW}$ ($P_{\text{NBI}} = 4 \text{ MW}$)
- $Q_{\text{div}} \sim 2 \text{ MW} \rightarrow Q_{\text{div}} \sim 1.2 \text{ MW}$
 $\rightarrow Q_{\text{div}} \sim 0.5\text{-}0.7 \text{ MW}$



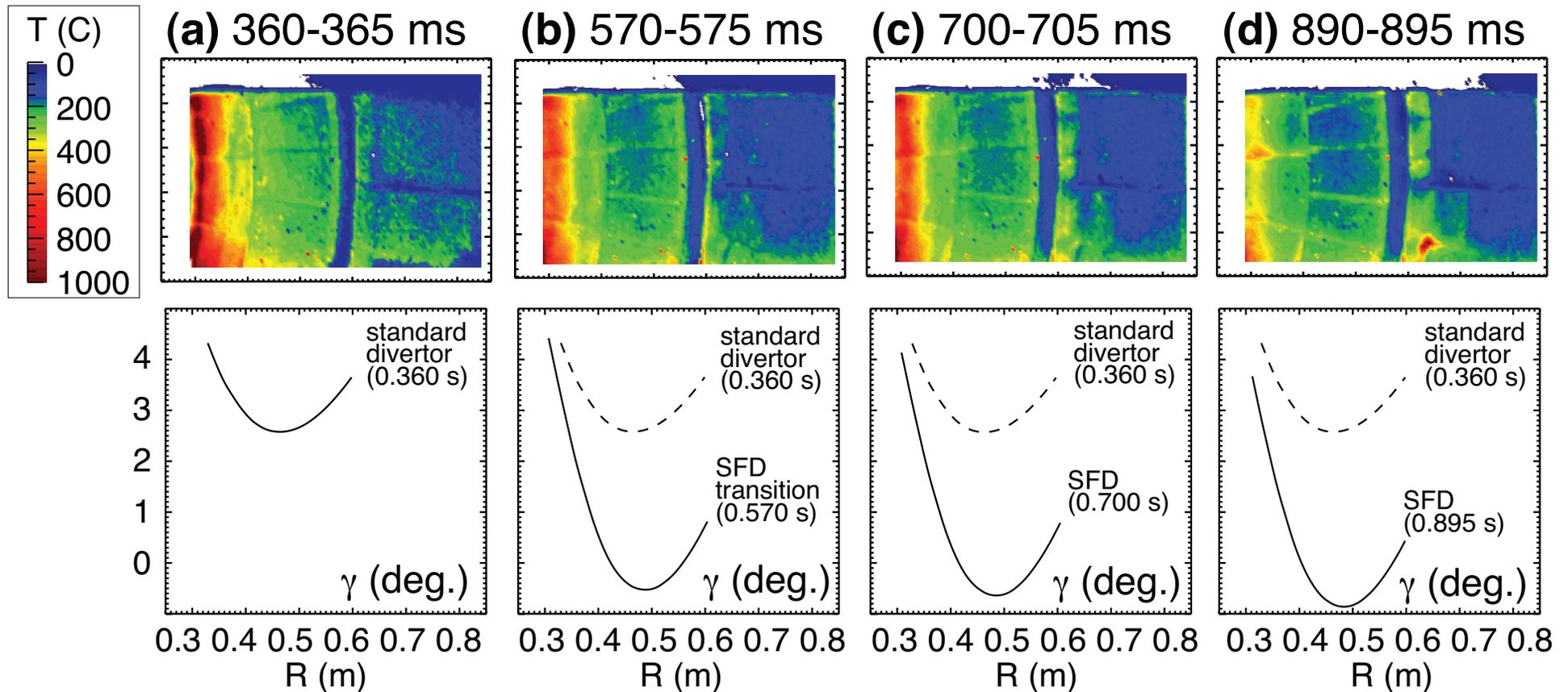
Divertor profiles show low heat flux, broadened C III and C IV radiation zones in the snowflake divertor phase



- Heat flux profiles reduced to nearly flat low levels, characteristic of radiative heating
- Divertor C III and C IV brightness profiles broaden
- High- n Balmer line spectroscopy and CRETIN code modeling confirm outer SP detachment with $T_e \leq 1.5 \text{ eV}$, $n_e \leq 5 \times 10^{20} \text{ m}^{-3}$
 - Also suggests a reduction of carbon physical and chemical sputtering rates



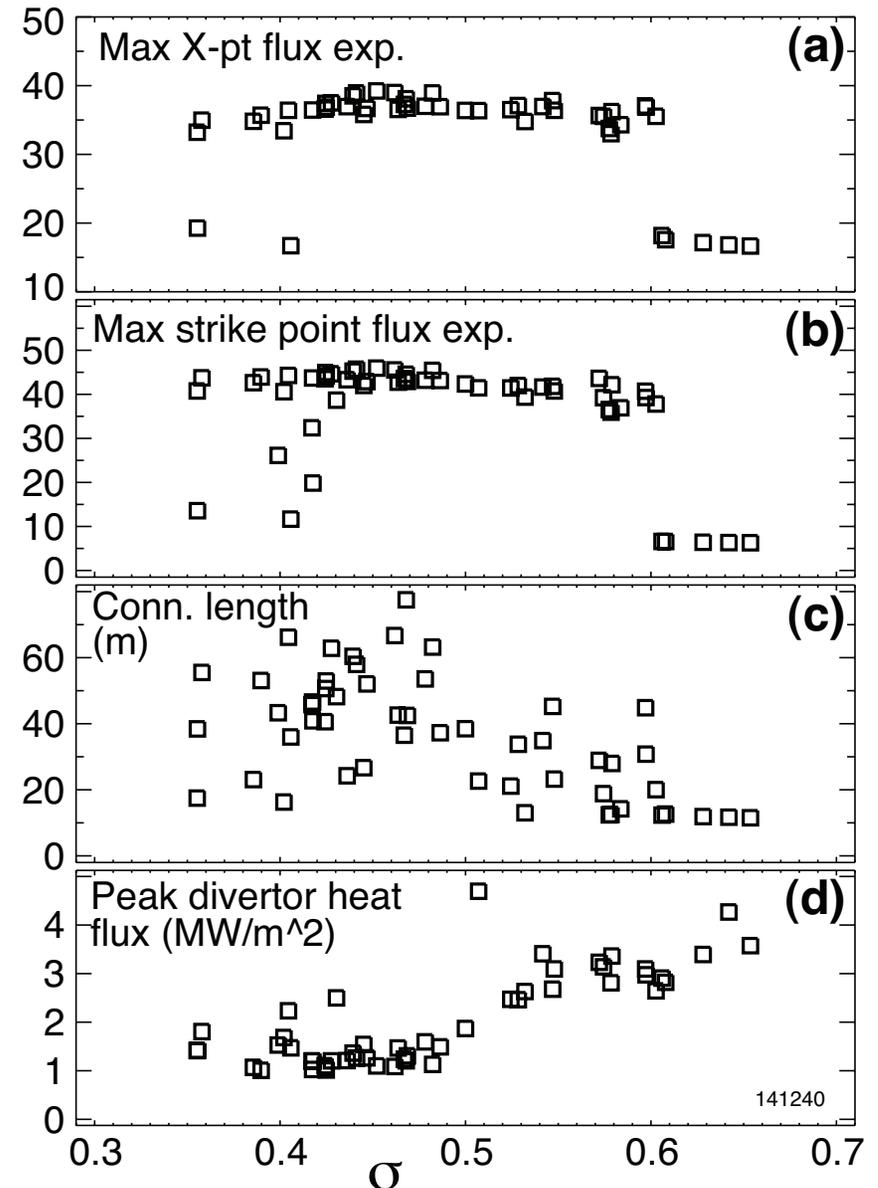
No leading edge PFC tile heating observed at shallow magnetic field incidence angles



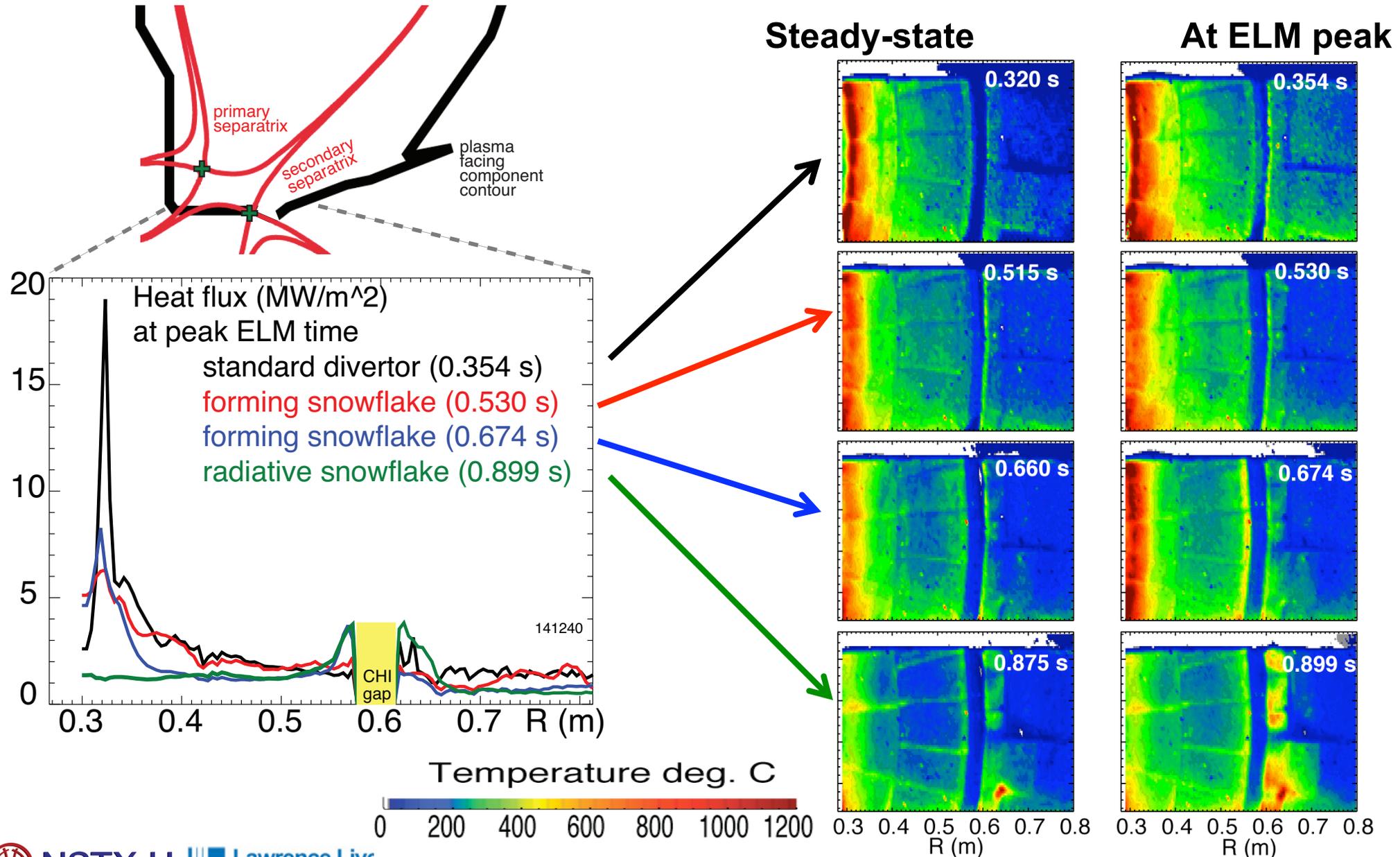
- Reduction of q_{\parallel} due to radiative detachment is considered

Peak divertor heat flux decreases with stronger snowflake effects (lower σ)

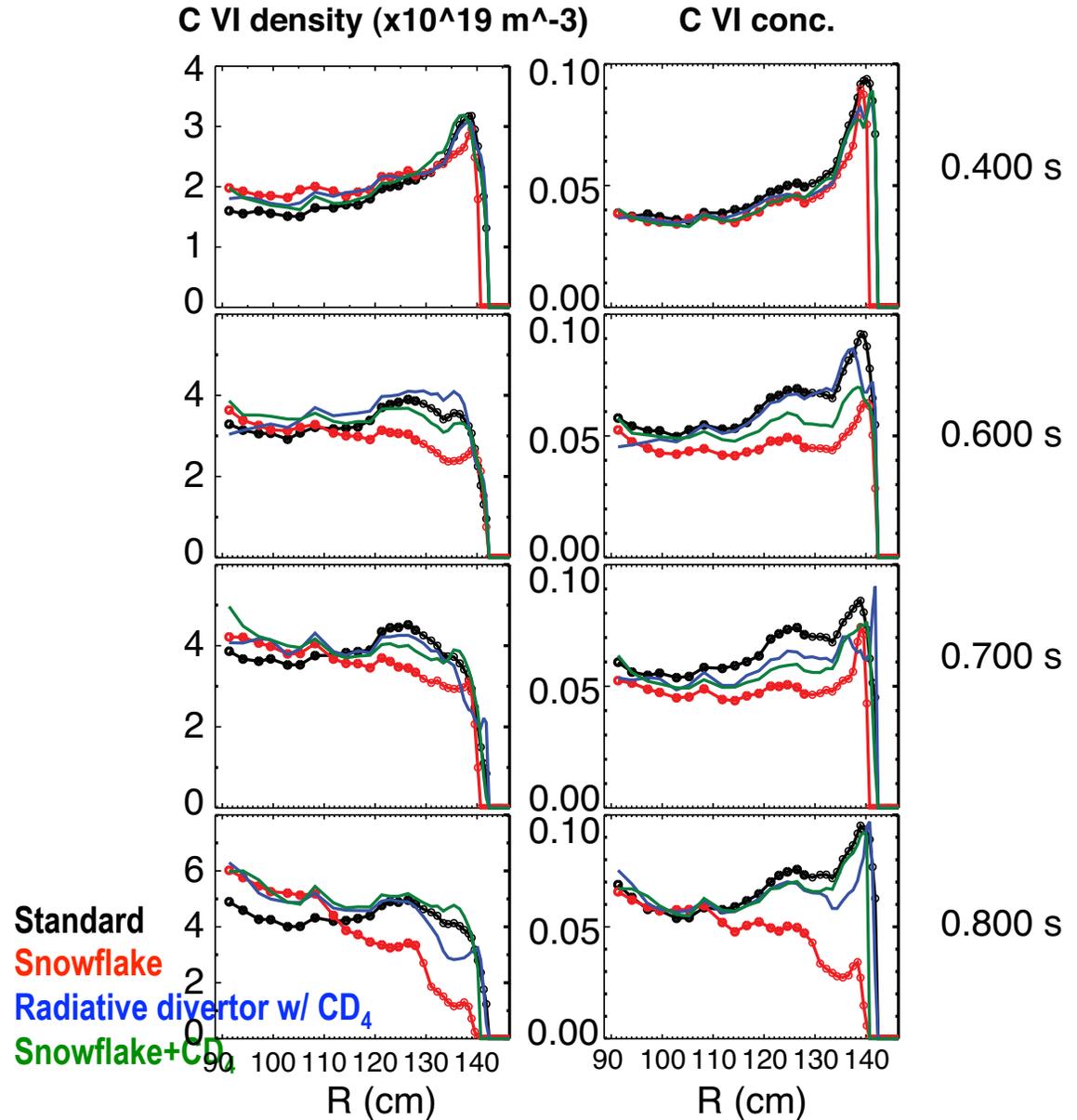
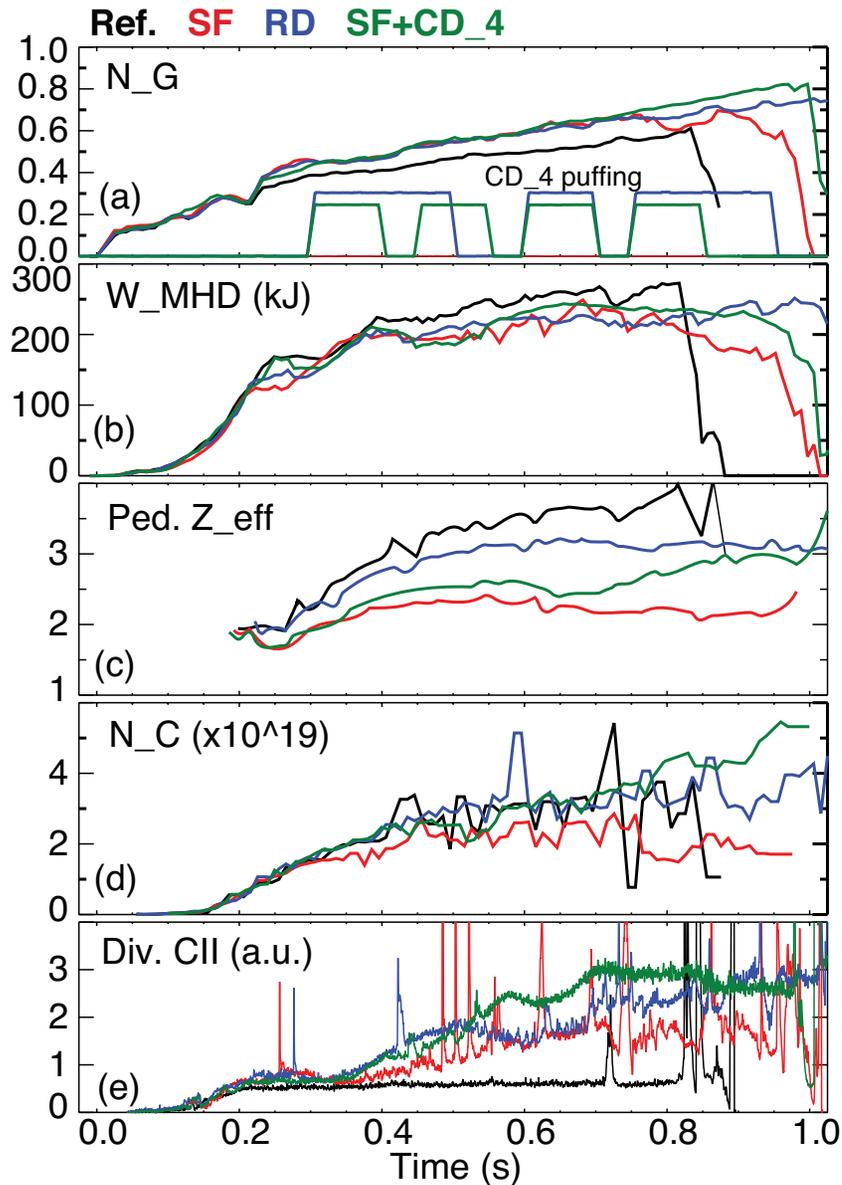
- Deviation from ideal snowflake: $\sigma = d / a$
 - d – distance between nulls,
 a – plasma minor radius
- Clear trends of flux expansion, connection length, and peak heat flux with σ observed



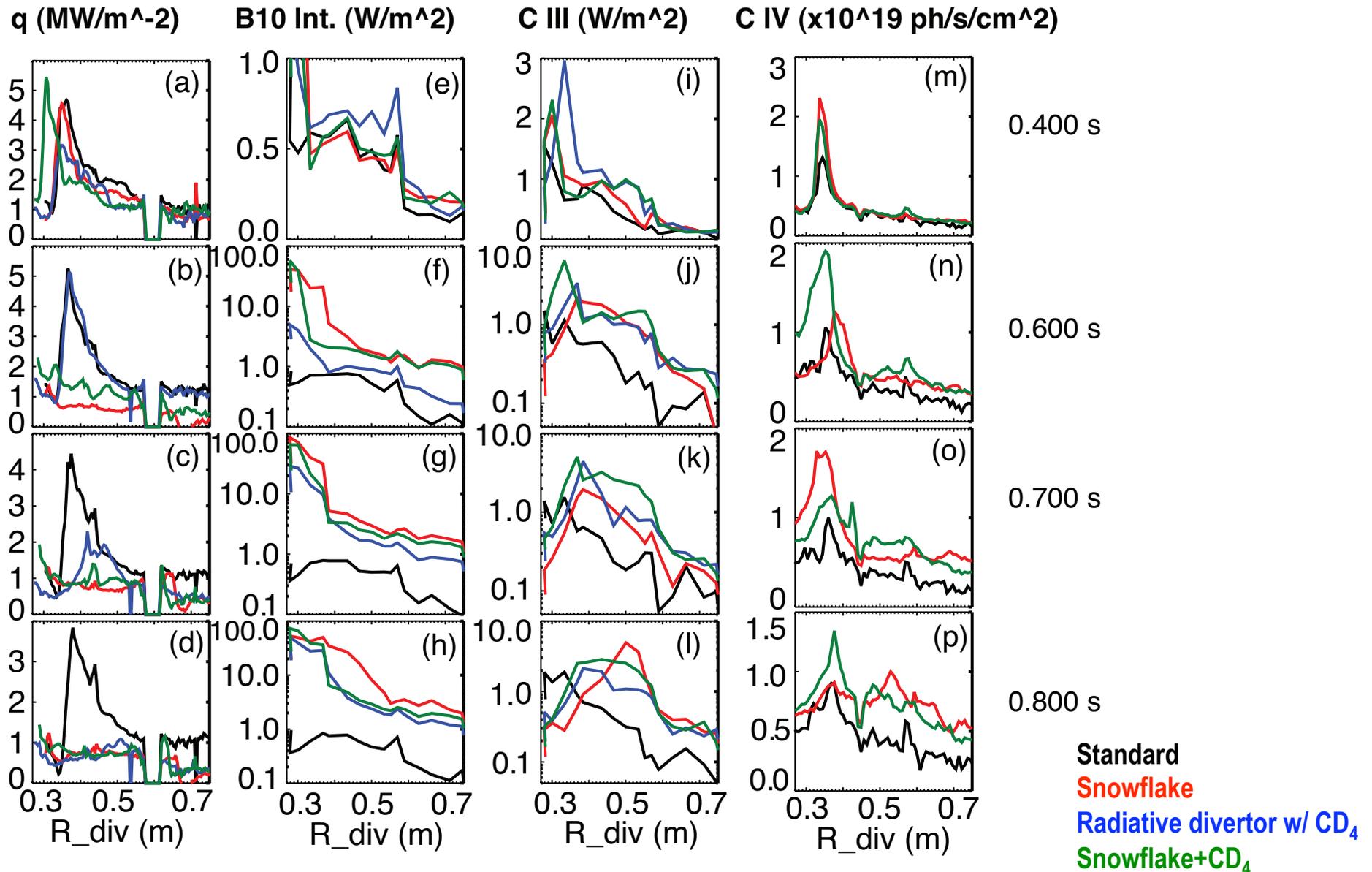
Impulsive heat loads due to Type I ELMs are mitigated in snowflake divertor



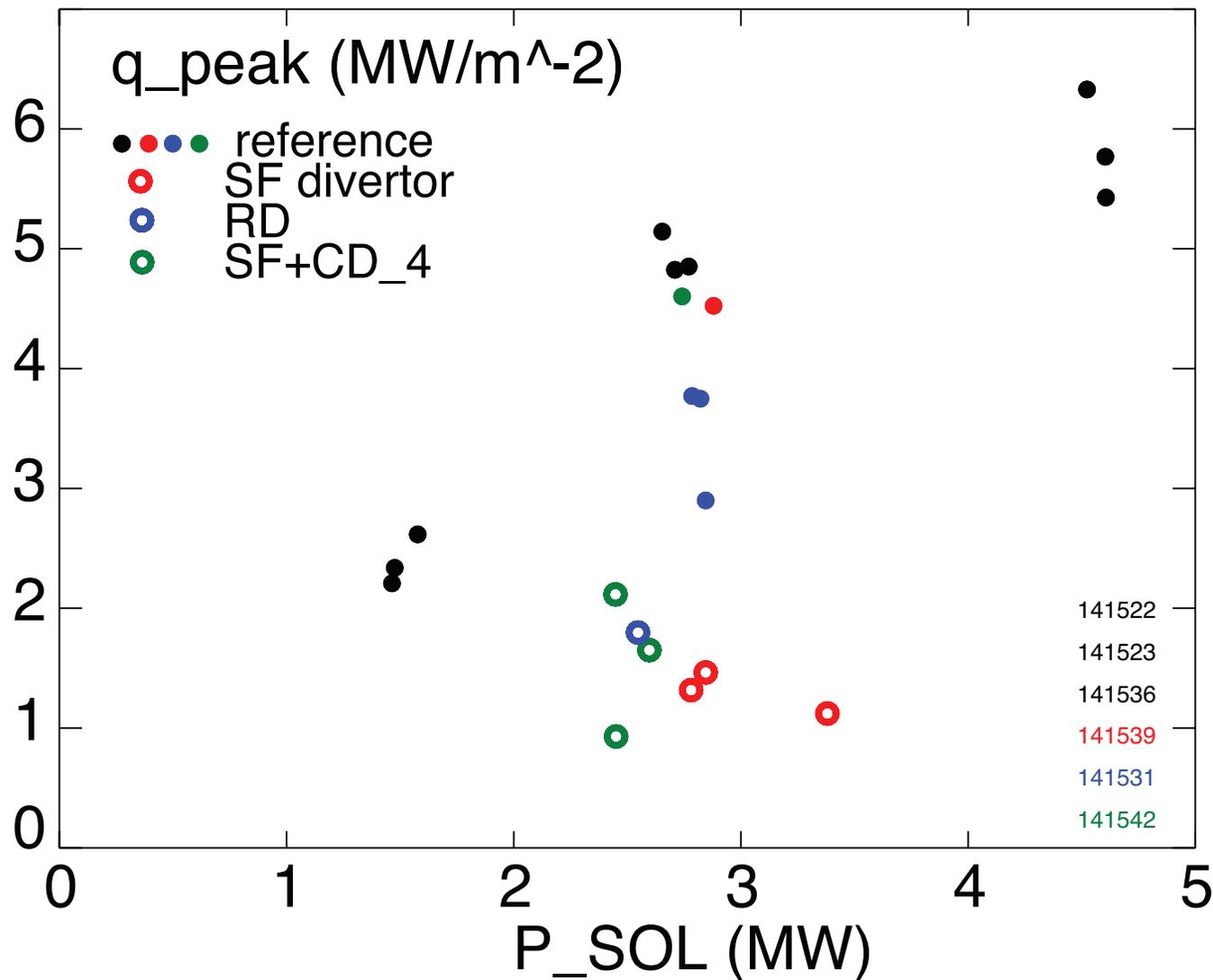
Good H-mode confinement properties retained or slightly reduced with CD_4 -seeded snowflake divertor



Divertor profiles show enhanced radiation and recombination zone in snowflake divertor w/ and w/o CD₄

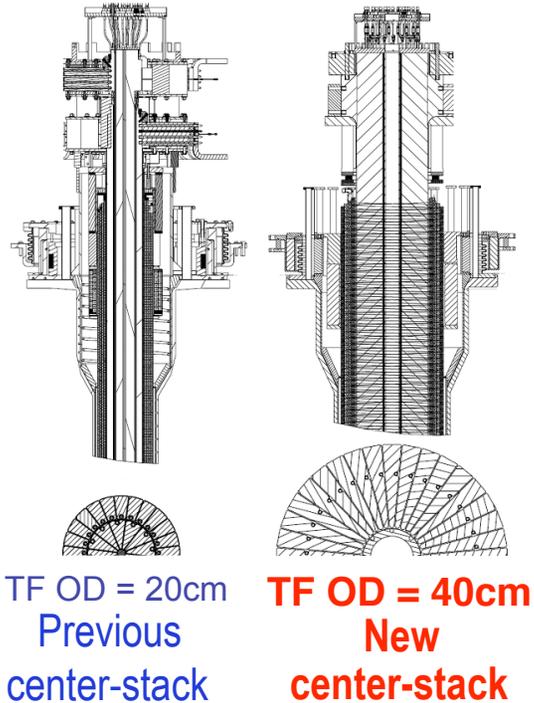


Divertor heat flux reduced by radiation and/or geometry in radiative and snowflake divertors



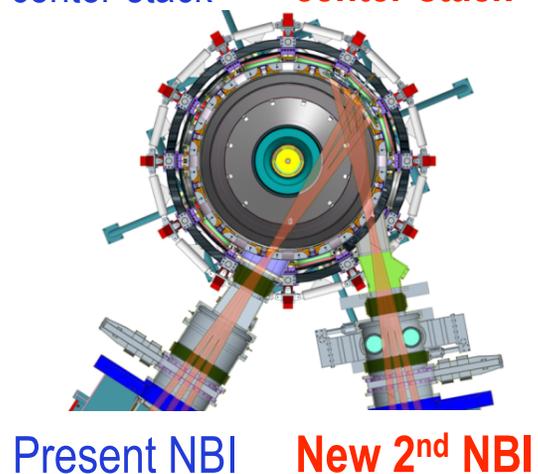
Standard
Snowflake
Radiative divertor w/ CD₄
Snowflake+CD₄

NSTX Upgrade will address critical plasma confinement and sustainment questions by exploiting 2 new capabilities



New center-stack

- Reduces v^* → ST-FNSF values to understand ST confinement
 - Expect 2x higher T by doubling B_T , I_p , and NBI heating power
- Provides 5x longer pulse-length
 - $q(r,t)$ profile equilibration
 - Tests of NBI + BS non-inductive ramp-up and sustainment

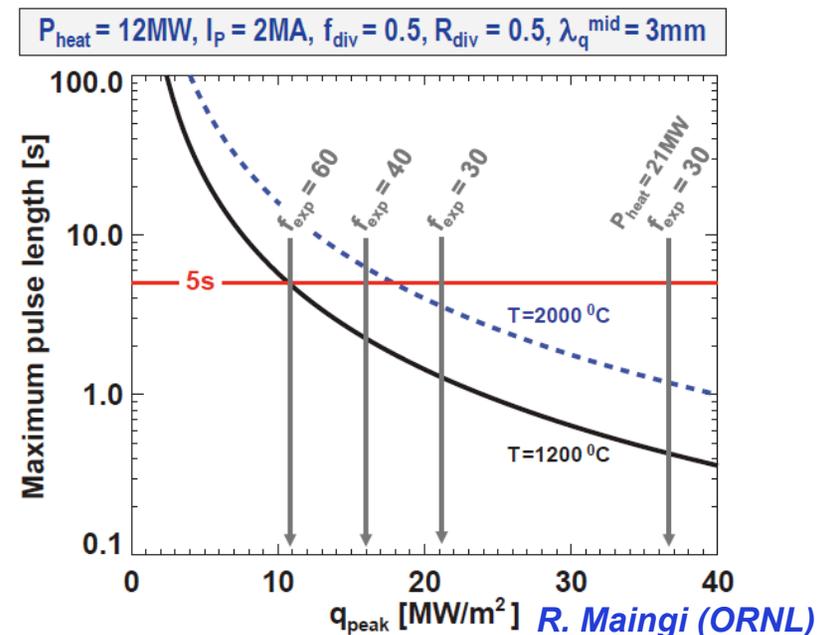
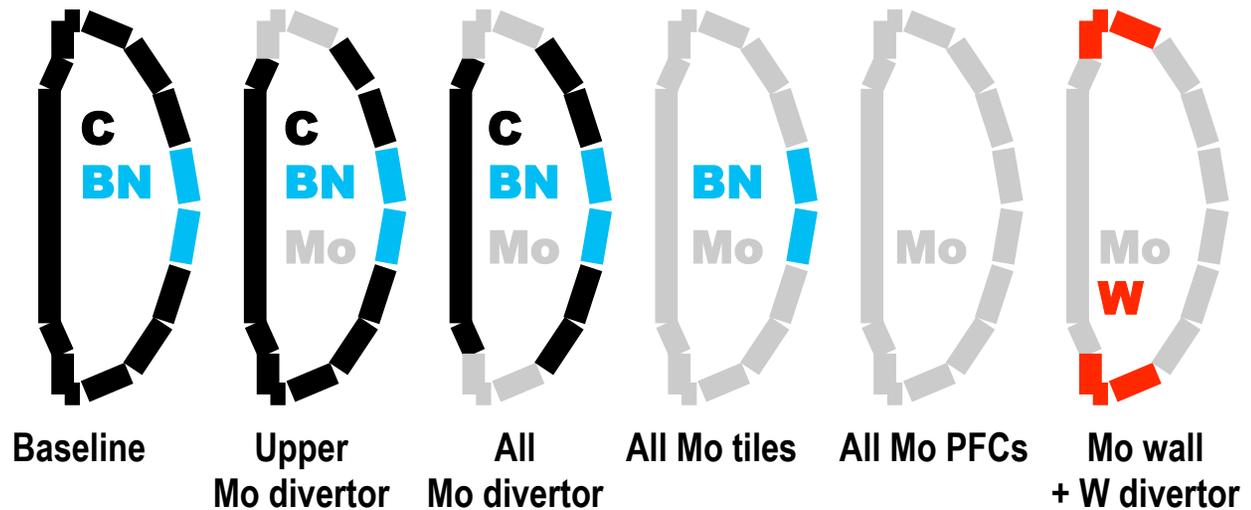


New 2nd NBI

- 2x higher CD efficiency from larger tangency radius R_{TAN}
- 100% non-inductive CD with $q(r)$ profile controllable by:
 - NBI tangency radius
 - Plasma density
 - Plasma position

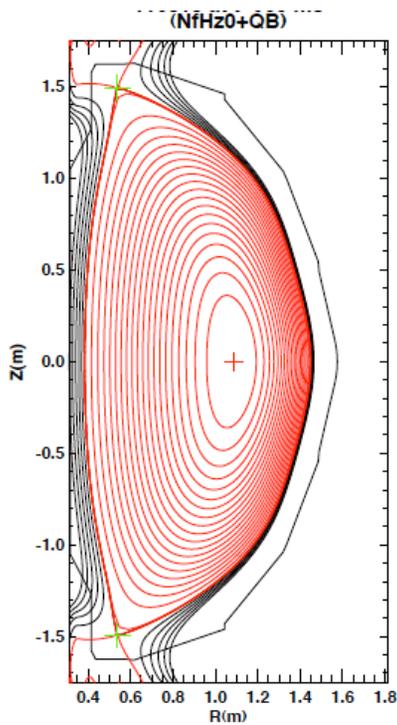
Divertor heat flux mitigation options are affected by NSTX-U plasma-facing component development plan

- Developing PFC plan to transition to full metal coverage for FNSF-relevant PMI development
- Wall conditioning: GDC, lithium and / or boron
- PFC bake-out at 300-350°C
- Divertor impurity seeding:
 - D₂, CD₄, Ne, Ar with graphite PFCs
 - N₂ with molybdenum PFCs
- High $I_p = 2$ MA scenarios projected to have narrow $\lambda_q^{mid} \sim 3$ mm
- Scenarios with high I_p and P_{NBI} are projected to challenge passive cooling limits of graphite divertor PFCs

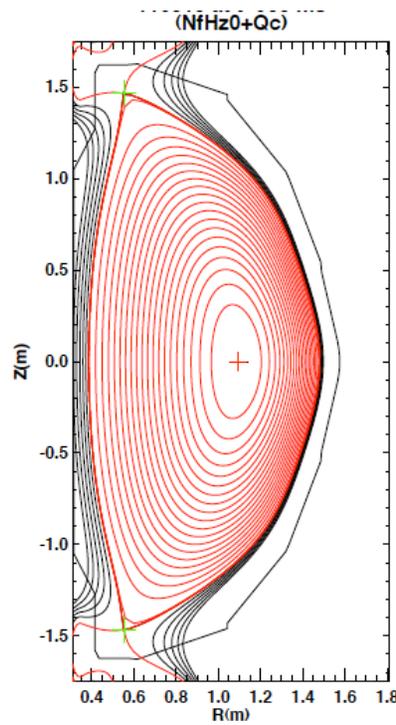


Snowflake divertor is a leading heat flux mitigation candidate for NSTX-U

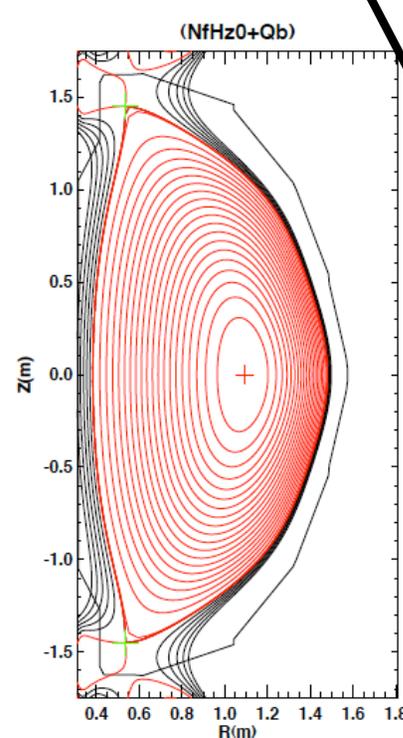
- Single and double-null radiative divertors and upper-lower snowflake configurations considered
 - Supported by NSTX-U divertor coils and compatible with coil current limits
 - ISOLVER modeling shows many possible equilibria
 - Impact of changing I_{OH} on snowflake minimal
 - Reduced divertor coil set can be used for snowflakes



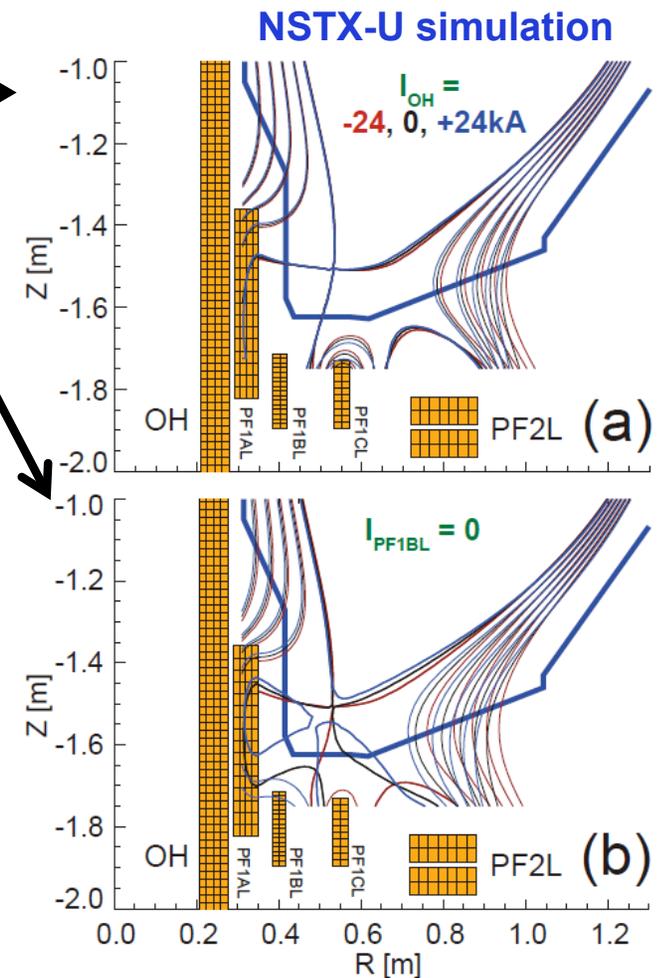
NSTX-U double-null



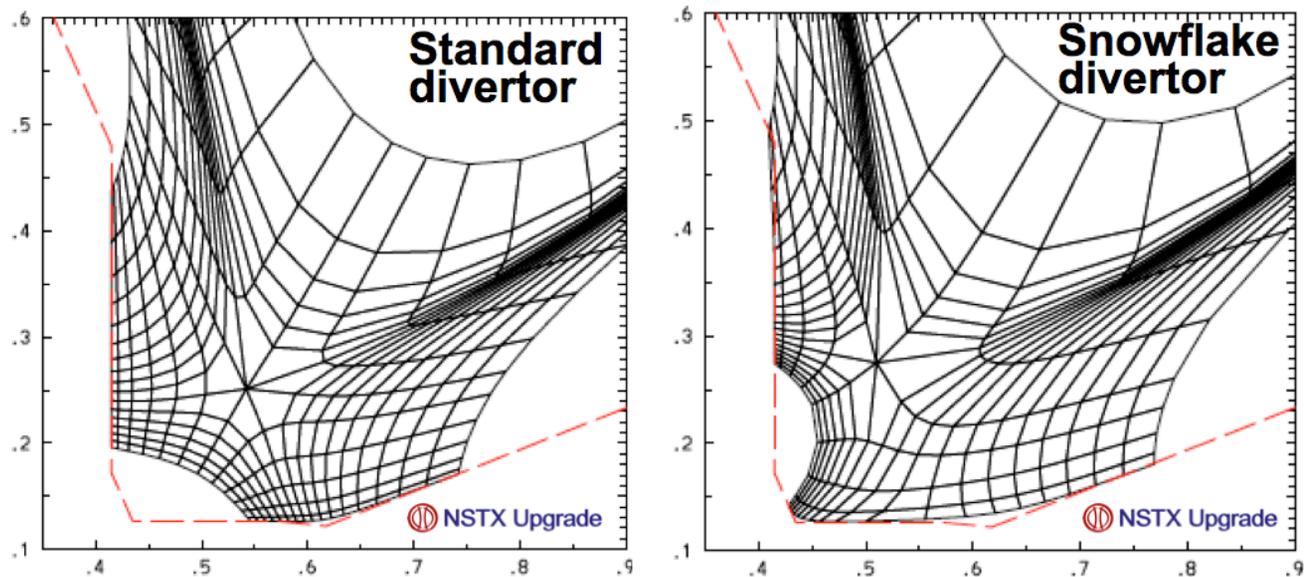
NSTX-U double-snowflake-plus



NSTX-U double-snowflake-minus



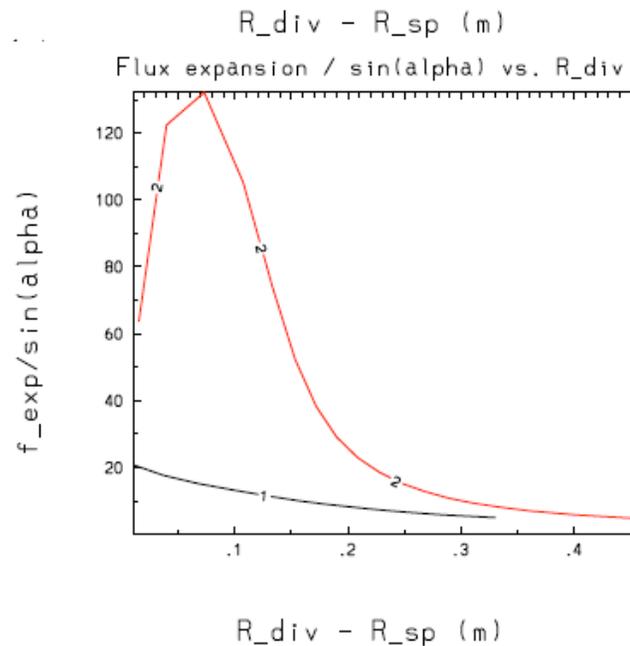
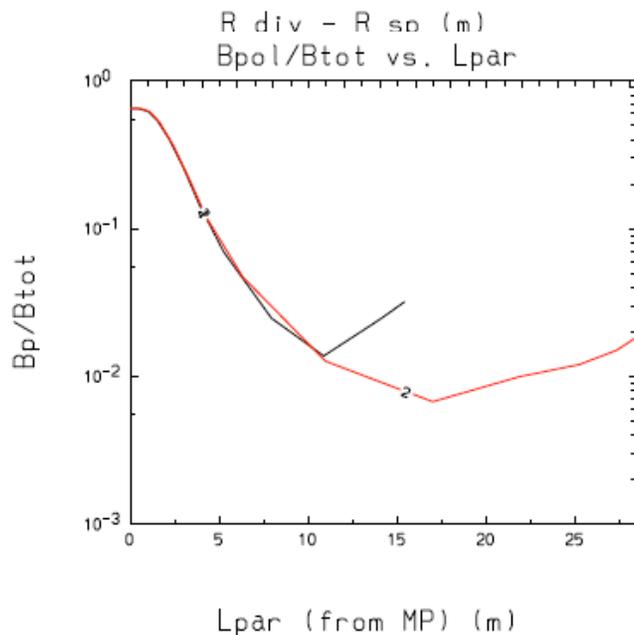
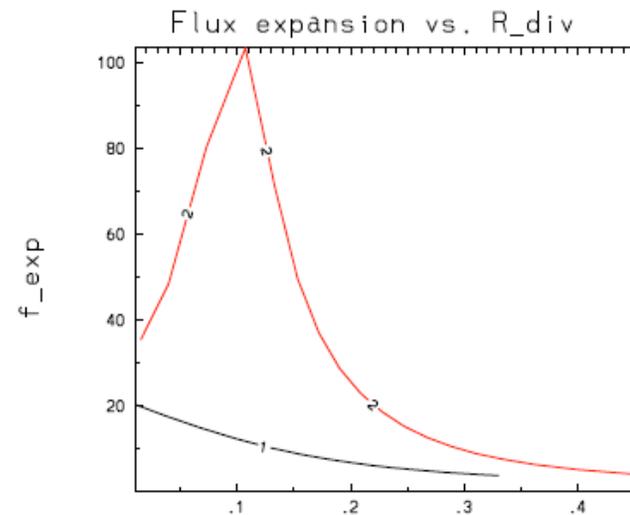
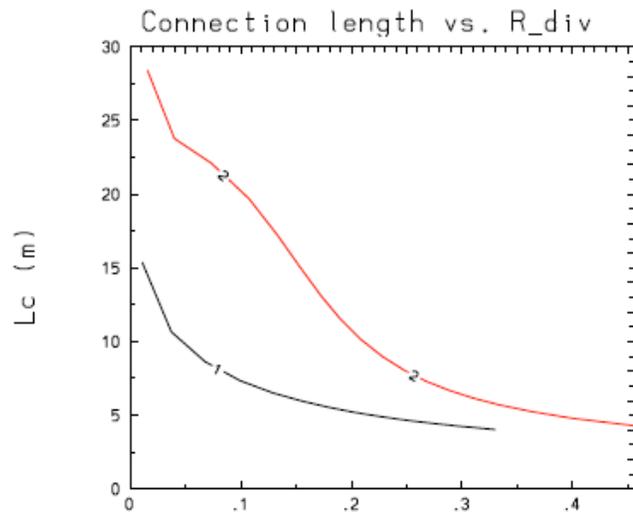
Projections with UEDGE edge multi-fluid model for NSTX-U are optimistic



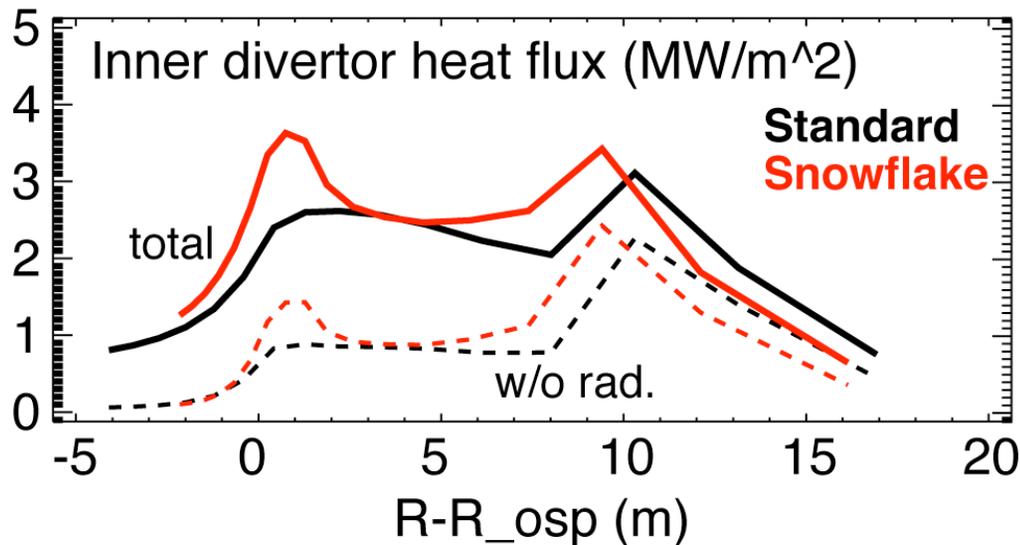
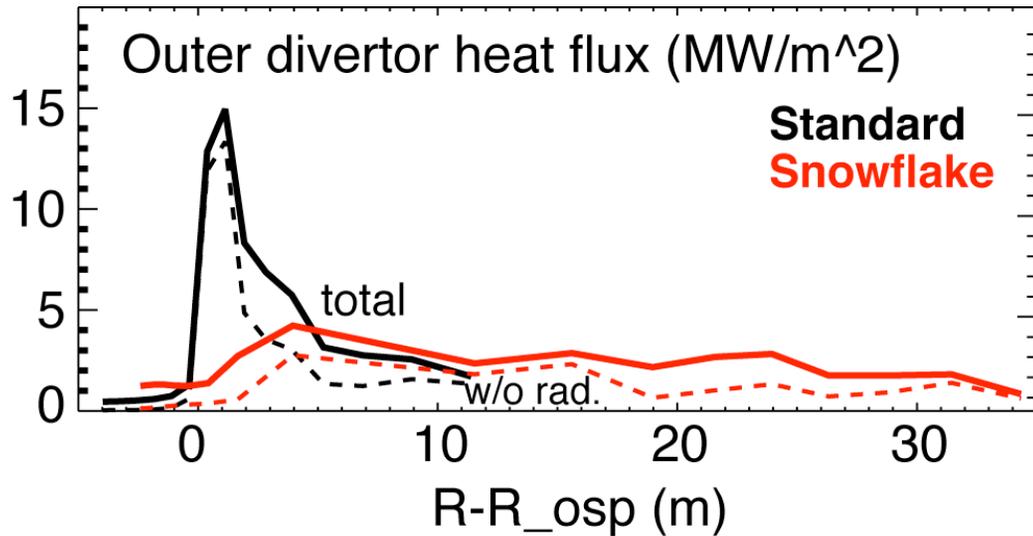
- Fluid (Braginskii) model for ions and electrons
- Fluid for neutrals
- Classical parallel transport, anomalous radial transport
- Core interface:
 - $P_{SOL90} = 5; 7; 9$ MW
- $D = 0.1-0.5$ m²/s
- $\chi_{e,i} = 1-2$ m²/s
- $R_{recy} = 0.99$
- Carbon 5 %

- Grids extend from $\psi=0.9$ to $\psi=1.2$
- STD grid covers 3.1 cm outside the separatrix at the outer MP
- SNF grid covers 3.4 cm outside the separatrix at the outer MP.

In modeled NSTX-U snowflake configuration magnetic geometry shows clear benefits (cf. standard divertor)



UEDGE predicts significant divertor heat flux reduction and attached conditions in NSTX-U at 12 MW NBI heating



- Predictions for 12 MW NBI case
 - $P_{SOL} = 9$ MW
 - Outer divertor attached
 - $T_e, T_i \leq 80$ eV
 - Inner divertor detached

